

ME453 - Homework 3

Herman Kolstad Jakobsen
20196493

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Problem 7a)

Know that JJ^T is symmetric since

$$B = JJ^T$$

$$B^T = (JJ^T)^T = (J^T)^T J^T = JJ^T = B$$

Further, let λ be an arbitrary eigenvalue of JJ^T and let v be an eigenvector corresponding to the eigenvalue λ .

Then

$$(JJ^T)v = \lambda v \quad (*)$$

The Jacobian J is obtained from physical quantities such as positions and coordinates. Hence, it is fair to assume that the Jacobian, and then also JJ^T , is real.

Taking the complex conjugate of $(*)$ therefore yields

$$(JJ^T)\bar{v} = \bar{\lambda}\bar{v}$$

Pre-multiplying $(*)$ with \bar{v}^T gives

$$\begin{aligned} \bar{v}^T (JJ^T)v &= \bar{v}^T \lambda v \\ \Rightarrow \lambda \bar{v}^T v &= ((JJ^T)^T \bar{v})^T v \\ &= (JJ^T \bar{v})^T v \\ &= (\bar{\lambda} \bar{v})^T v \\ &= \bar{\lambda} \bar{v}^T v \end{aligned}$$

So

$$\lambda \bar{v}^T v = \bar{\lambda} \bar{v}^T v \quad \Rightarrow \quad (\lambda - \bar{\lambda}) \bar{v}^T v = 0$$

Since v is an eigenvector and hence is non-zero, we have

$$\lambda = \bar{\lambda}$$

which means that λ is real. ■

Have that

$$x^T J J^T x = (J^T x)^T (J^T x) = \|J^T x\|^2 \geq 0$$

So the matrix $J J^T$ is positive semi-definite

$$J J^T \geq 0$$

This implies

$$\lambda \geq 0 \quad \blacksquare$$

7b)

Let $\lambda_i \neq \lambda_j$, and

$$(A^T)v_i = \lambda_i v_i \quad (*)$$

$$(A^T)v_j = \lambda_j v_j \quad (**)$$

Pre-multiplying $(*)$ with v_j^T yields

$$\lambda_i v_j^T v_i = v_j^T (A^T) v_i = ((A^T) v_j)^T v_i = (\lambda_j v_j)^T v_i = \lambda_j v_j^T v_i$$

Thus

$$\lambda_i v_j^T v_i - \lambda_j v_j^T v_i = 0$$

$$(\lambda_i - \lambda_j) v_j^T v_i = 0$$

Since $\lambda_i \neq \lambda_j$, we must have

$$v_j^T v_i = 0, \quad i \neq j$$

Hence, all eigenvectors are orthogonal to each eigenvector. ▀

Problem 2a)

We are given the rotation matrix

$$R = R_{z,\alpha} R_{y,\beta} R_{z,\gamma}$$

Using the relationship

$$S(\omega) = \dot{R} R^T$$

we obtain

$$\dot{R} = S(\omega) R$$

Using this, and the product rule, we get

$$\begin{aligned} \dot{R} &= \dot{R}_{z,\alpha} R_{y,\beta} R_{z,\gamma} + R_{z,\alpha} \dot{R}_{y,\beta} R_{z,\gamma} + R_{z,\alpha} R_{y,\beta} \dot{R}_{z,\gamma} \\ &= S(\dot{\alpha} k) R_{z,\alpha} R_{y,\beta} R_{z,\gamma} + R_{z,\alpha} S(\dot{\beta} j) R_{y,\beta} R_{z,\gamma} + R_{z,\alpha} R_{y,\beta} S(\dot{\gamma} k) R_{z,\gamma} \end{aligned}$$

Expressing the angular velocities in the correct frame (base frame) yields

$$\begin{aligned} \dot{R} &= S(\dot{\alpha} k) R_{z,\alpha} R_{y,\beta} R_{z,\gamma} + S(R_{z,\alpha} \dot{\beta} j) R_{z,\alpha} R_{y,\beta} R_{z,\gamma} + S(R_{z,\alpha} R_{y,\beta} \dot{\gamma} k) R_{z,\alpha} R_{y,\beta} R_{z,\gamma} \\ &= \left[S(\dot{\alpha} k) + S(R_{z,\alpha} \dot{\beta} j) + S(R_{z,\alpha} R_{y,\beta} \dot{\gamma} k) \right] R \end{aligned}$$

Angular velocities expressed in the same frame can be added together, so

$$\begin{aligned} \dot{R} &= S(\dot{\alpha} k + R_{z,\alpha} \dot{\beta} j + R_{z,\alpha} R_{y,\beta} \dot{\gamma} k) R \\ &= S(\omega) R \\ &= \hat{\omega} R \end{aligned}$$

Thus

$$\hat{\omega} = S(\dot{\alpha} k + R_{z,\alpha} \dot{\beta} j + R_{z,\alpha} R_{y,\beta} \dot{\gamma} k)$$

where

$$\dot{\alpha} k = \begin{bmatrix} 0 \\ 0 \\ \dot{\alpha} \end{bmatrix}$$

$$R_{z,\alpha} \dot{\beta} j = \dot{\beta} \begin{bmatrix} c\alpha & -s\alpha & 0 \\ s\alpha & c\alpha & 0 \\ 0 & 0 & 1 \end{bmatrix} \begin{bmatrix} 0 \\ 1 \\ 0 \end{bmatrix} = \begin{bmatrix} -s\alpha \\ c\alpha \\ 0 \end{bmatrix} \dot{\beta}$$

$$\begin{aligned}
 R_{z,\alpha} R_{y,\beta} j_k &= j^i \begin{bmatrix} c_\alpha & -s_\alpha & 0 \\ s_\alpha & c_\alpha & 0 \\ 0 & 0 & 1 \end{bmatrix} \begin{bmatrix} c_\beta & 0 & s_\beta \\ 0 & 1 & 0 \\ -s_\beta & 0 & c_\beta \end{bmatrix} \begin{bmatrix} 0 \\ 0 \\ 1 \end{bmatrix} \\
 &= j^i \begin{bmatrix} c_\alpha & -s_\alpha & 0 \\ s_\alpha & c_\alpha & 0 \\ 0 & 0 & 1 \end{bmatrix} \begin{bmatrix} s_\beta \\ 0 \\ c_\beta \end{bmatrix} \\
 &= j^i \begin{bmatrix} c_\alpha s_\beta \\ s_\alpha s_\beta \\ c_\beta \end{bmatrix}
 \end{aligned}$$

Then

$$w = \begin{bmatrix} 0 \\ 0 \\ \dot{\alpha} \end{bmatrix} + \begin{bmatrix} -\dot{\beta} s_\alpha \\ \dot{\beta} c_\alpha \\ 0 \end{bmatrix} + \begin{bmatrix} \dot{\gamma} c_\alpha s_\beta \\ \dot{\gamma} s_\alpha s_\beta \\ \dot{\gamma} c_\beta \end{bmatrix}$$

$$= \begin{bmatrix} \dot{\gamma} c_\alpha s_\beta - \dot{\beta} s_\alpha \\ \dot{\gamma} s_\alpha s_\beta + \dot{\beta} c_\alpha \\ \dot{\gamma} c_\beta + \dot{\alpha} \end{bmatrix}$$

$$= \begin{bmatrix} c_\alpha s_\beta & -s_\alpha & 0 \\ s_\alpha s_\beta & c_\alpha & 0 \\ c_\beta & 0 & 1 \end{bmatrix} \begin{bmatrix} \dot{\gamma} \\ \dot{\beta} \\ \dot{\alpha} \end{bmatrix}$$

where

$$J_w = \begin{bmatrix} c_\alpha s_\beta & -s_\alpha & 0 \\ s_\alpha s_\beta & c_\alpha & 0 \\ c_\beta & 0 & 1 \end{bmatrix}$$

2b)

The Jacobian loses its rank if its determinant is zero.

Thus

$$\det(J_w) = c_\beta \begin{vmatrix} -s_\alpha & 0 \\ c_\alpha & 0 \end{vmatrix} + \begin{vmatrix} c_\alpha s_\beta & -s_\alpha \\ s_\alpha s_\beta & c_\alpha \end{vmatrix}$$

$$= c_\alpha^2 s_\beta + s_\alpha^2 s_\beta$$

$$= s_\beta$$

So the Jacobian loses its rank if

$$\sin(\beta) = 0$$

which implies

$$\underline{\underline{\beta = \pm n\pi, \quad n=0, 1, 2, \dots}}$$

Problem 3

The MATLAB code for this assignment is listed in lst 1.

3a)

By using forward kinematics, the homogeneous transformation matrices H_2^0 and H_e^0 were found. Since all the joints are revolute, the translation velocity part of the Jacobian matrix of the end-effector is given by

$$J_v = [z_0^0 \times (P_e^0 - P_0^0) \quad | \quad z_1^0 \times (P_e^0 - P_1^0) \quad | \quad z_2^0 \times (P_e^0 - P_2^0)] \quad (1)$$

The position vectors and axis vectors can be easily obtained by looking at the third and fourth column of the corresponding homogeneous transformation matrix. Performing the cross-products then yields

$$J_v = \begin{bmatrix} -L_3 c_1 c_{23} - L_2 c_1 c_2 & L_3 s_1 s_{23} + L_2 s_1 s_2 & L_3 s_1 s_{23} \\ -L_3 s_1 c_{23} - L_2 s_1 c_2 & -L_3 c_1 s_{23} - L_2 c_1 s_2 & -L_3 c_1 s_{23} \\ 0 & L_3 c_{23} + L_2 c_2 & L_3 c_{23} \end{bmatrix} \quad (2)$$

3b)

Using MATLAB, the determinant was calculated to be

$$\det(J_v) = -L_2 L_3 (L_2 c_2 s_3 - L_3 s_3 + L_3 c_3^2 s_2 + L_3 c_2 c_3 s_3) \quad (3)$$

Applying algebra and trigonometric identities, the determinant can be rewritten as

$$\det(J_v) = -L_2 L_3 s_3 (L_2 c_2 + L_3 c_{23}) \quad (4)$$

We can see from eq. (4) that the manipulator has singular position whenever

$$s_3 = 0 \implies \theta_3 = 0 \vee \theta_3 = \pi \quad (5)$$

and whenever

$$L_2 c_2 + L_3 c_{23} = 0 \quad (6)$$

3c)

When J_v is rank deficient, we have that $N(J_v) \neq \phi$. As found in the previous task, the Jacobian is rank deficient in three different cases.

Case 1

This singular position is obtained when $\theta_3 = 0$. Using MATLAB, we obtain the following basis for the null space of the Jacobian

$$Null(J_v) = span \left\{ \begin{bmatrix} 0 \\ -2/5 \\ 1 \end{bmatrix} \right\} \quad (7)$$

In this configuration the manipulator has its third joint fully extended. It is therefore intuitive that no values of $\dot{\theta}_1$ lies in the null space of J_v . A rotation around the z_0 -axis will impose a movement in the end-effector. The last two elements of the vector spanning the null space represents a linear relationship between $\dot{\theta}_2$ and $\dot{\theta}_3$. In order to keep the end-effector still, a decrease in θ_2 imposes an increase in θ_3 . By looking at a drawing of the manipulator in this configuration, the linear relationship between the two angular velocities makes sense. The ratio between the two angular velocities is a consequence of non-equal link lengths.

Case 2

This singular position is obtained when $\theta_3 = \pi$. The basis for the null space of the Jacobian is in this case the following

$$Null(J_v) = span \left\{ \begin{bmatrix} 0 \\ 2 \\ 1 \end{bmatrix} \right\} \quad (8)$$

In this configuration the manipulator has its third joint fully contracted. Equal to the previous case, a rotation around the z_0 -axis will impose a movement in end-effector. Picturing the manipulator in this configuration, the linear relationship between θ_2 and θ_3 is sensible. If θ_2 increases, θ_3 must also increase in order to make end-effector still.

Case 3

This singular position is obtained when $L_2 c_2 + L_3 c_{23} = 0$. The expression can be rewritten into the following expression

$$\theta_3 = \cos^{-1} \left(-\frac{L_2}{L_3} \cos \theta_2 \right) - \theta_2 \quad (9)$$

The basis of the null space of Jacobian is in this case the following

$$Null(J_v) = span \left\{ \begin{bmatrix} 1 \\ 0 \\ 0 \end{bmatrix} \right\} \quad (10)$$

This singular configuration is shown in the textbook, where it is illustrated that the end-effector lies on the z_0 -axis. Looking at the figure, it becomes clear that the only rotation that will not impose a movement in the end-effector is a rotation around the z_0 -axis.

Code

Listing 1: Code for problem 3

```

1  clc; clear; close all;
2
3  %% Parameters
4
5  syms theta1 theta2 theta3 L1 L2 L3 real;
6
7
8  %% Problem 3a
9
10 % Forward kinematics
11 H01 = DH_matrix(L1,theta1+sym(pi)/2,0,sym(pi)/2);
12 H12 = DH_matrix(0,theta2,L2,0);
13 H2e = DH_matrix(0,theta3,L3,0);
14
15 H02 = H01*H12;
16 H0e = H02*H2e;
17
18 % Extract position
19 P01 = H01(1:3,4);
20 P02 = H02(1:3,4);
21 P0e = H0e(1:3,4);
22
23 % Extract z-axis
24 z0 = [0 0 1]';
25 z1 = H01(1:3,3);
26 z2 = H02(1:3,3);
27 ze = H0e(1:3,3);
28
29 % Every joint is revolute
30 % Calculate translation velocity part of Jacobian matrix
   of end-effector
31 Jv = [cross(z0,P0e) cross(z1,(P0e-P01)) cross(z2,(P0e-P02
   ))];
32
33
34 %% Problem 3b
35
36 % Calculate determinant
37 detJv = simplify(det(Jv));
38
39 % Applying further algebraic manipulation and
   trigonometric identities on the determinant gives

```

```

        condition for
40 % singular configuration
41
42
43 %% Problem 3c
44
45 Jv = simplify(subs(Jv, [L1 L2 L3], [0.5 1.5 1]));
46
47 % Case 1, theta3 = 0
48 Jv1 = subs(Jv, theta3, 0);
49 nullsp1 = null(Jv1);
50
51 % Case 2, theta3 = pi
52 Jv2 = subs(Jv, theta3, pi);
53 nullsp2 = null(Jv2);
54
55 % Case 3, L2c2 + L3c23 = 0
56 % The expression can be rewritten as
57 % theta3 = acos(-L2/L3*cos(theta2))-theta2
58 Jv3 = subs(Jv, theta3, acos(-L2/L3*cos(theta2))-theta2);
59 Jv3 = simplify(subs(Jv3, [L1 L2 L3], [0.5 1.5 1]));
60 nullsp3 = null(Jv3);
61
62
63 %% Functions
64
65 function M = DH_matrix(d,theta,a,alpha) % Calculate
    Denavit-Hartenberg Matrix
66     M = [cos(theta) -sin(theta)*cos(alpha) sin(theta)*sin
           (alpha) a*cos(theta); sin(theta) cos(theta)*cos(
           alpha) -cos(theta)*sin(alpha) a*sin(theta); 0 sin(
           alpha) cos(alpha) d; 0 0 0 1];
67 end

```