

**LA TROBE UNIVERSITY**

# **Delta Printer Project Report**

by

**Keith Brown**

Final Year Project Report

in the  
Faculty of Science, Technology and Engineering  
Department of Electronic Engineering

December 2013



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La Trobe University

Department of Electronic Engineering

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LA TROBE UNIVERSITY

## *Abstract*

Faculty of Science, Technology and Engineering  
Department of Electronic Engineering

Bachelor of Electronic Engineering

by Keith Brown

This document describes the design and development of an inexpensive 3D printer. The project is developed for the final year engineering project at La Trobe University by Keith Brown.

The printer will be in the form of a delta machine. The intention is to reduce the number of components and utilise cheaper hardware while still achieving a fast accurate print. The electronics will not be a direct derivative of current implementations. Experimentation with alternative architecture will be trialled with the goal of delivering a more computational capable system.

An introduction into 3D Printing and its concepts, advantages and issues is outlined. The commercial viability for both commercial and consumer markets is described. An analysis of both the structure and the systems inverse kinematic equations are included. Considerations regarding fluid motion is outlined. Hardware diagrams and descriptions follow. The electronic and software systems are discussed in detail. Testing procedures and associated results are also examined. Finally, project management tasks are reviewed.

## *Acknowledgements*

I would like to share my sincere gratitude to Dr Robert Ross, my primary supervisor whom has given me so much creative control. Robert has provided constant assistance. He also has bestowed me with his precious technical expertise. Adam Console my co-supervisor, has helped steer this project in the right direction on numerous occasions. It was Adam that suggested the delta machine design. His diverse knowledge is irreplaceable.

The RepRap community has paved the way for projects like this. There is a wealth of freely available information on their website and forums. I hope that I will be able to express my appreciation by giving something back to the open source community.

I would like to personally thank everyone who has supported me. I have discussed this project with many of my friends and family, who have contributed with valuable support and feedback.



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# Chapter 1

## Introduction

3D Printers have received a lot of media attention recently. Additive manufacturing has been around for at least 30 years [1, 2]. However, in the last five years popularity has increased dramatically due to the availability of much cheaper entry level machines. It is now possible for the general public to purchase pre-assembled printers at a similar cost as a personal computer.

There will always be innovation and dangers associated with a new technology. We already have prime examples of both aspects; At a 2011 TED talk, Dr Anthony Atala presented a human kidney prototype that his team had printed [3]. Late 2012 Cody Wilson uploaded a video to Youtube that showed himself firing a gun mostly composed of 3D printed parts [4].

The environment will benefit from this new way of producing products. Firstly, plastic items can be recycled and reused to create new, more useful items. This not only reduces costs but it also eliminates transportation of new items. They no longer need to be imported and transported all over the country, they can just be downloaded.

Whilst companies like Objet and Stratasys produce printers for the commercial sector, it is hobbyist style printers that have spread awareness of such technology. The RepRap foundation has produced numerous models under the GPL licence. Their main goal is to produce an affordable device that can self replicate. All of the designs are available to download and print. Makerbot Industries is a commercial operation that was born from an open source community.

Online services such as Shapeways provides 3D printing services. This allows their customers to receive a higher quality print without investing in expensive hardware. CAD design community sites have also been very popular such as 'thingiverse.com'.

There are over 30,000 free designs including a key-chain fob, mobile phone case, model radial engine and even 3D printer parts and upgrades.

## 1.1 3D printing methods

Additive manufacturing is the process of constructing a three-dimensional object by depositing material in discrete layers. Conversely, traditional machining methods are subtractive; material is removed to expose the desired object. This printer utilises an additive method as it produces fine plastic layers to build an object. There are many different approaches of additive manufacturing. The main four methods are outlined in the following paragraphs.

Fused deposition modelling or FDM is the method of extruding thermoplastics in layers. This project is considered to use an FDM method as it extrudes fine plastic layers to build an object. The printer deposits plastic material by melting it through a hot extruder. The extruder resembles a metal funnel that takes solid plastic and produces liquid plastic out of a small hole. The liquid plastic can be fused to previously deposited material. The machine must physically move the extruder around an area, while placing plastic where it is required. This process is repeated layer by layer to achieve a three-dimensional object. The technology was invented by S. Scott in 1980 [2].

Selective laser sintering or SLS is a technique that allows either metal, plastic, ceramic and glass powder to be fused together with a powerful laser. The laser targets cross-sections, selectively fusing a fine layer of powder to the object. Once a layer has been complete, a fresh layer of powder is dusted over the object and the process repeats. The left over material acts as a support for the object being manufactured. After the procedure has finished, the excess powder can be removed and used for the next print. The process is slow, producing porous but strong results.

Stereolithography or SLA is the method of using an ultraviolet light to cure a photopolymer. The printing platform sits in a vat of liquid resin. The light targets a cross-section of the desired object and the exposed resin will solidify. Once the layer has completed, the platform will move down allowing for another layer to be added to the model. SLA produces accurate results but is a very slow process. SLA has received a lot of attention recently as the method has been adopted by a handful of young start ups. It offers a much greater result compared to the current generation of FDM printers. However the hardware and resin is very expensive.

Laminated object manufacturing or LOM is another rapid prototyping method. It uses a laser or a knife to cut out layers from an adhesive-coated material. The layer is

then heated and pressed onto the previous layers. A new sheet of material is rolled in place and the process repeats. This method can be relatively cheap as readily available material such as paper can be used.

Each process is managed by a technique called '*computer numerical control*' or CNC. This method is essentially computer controlled automation. Three-dimensional models are developed using '*Computer aided design*' or CAD. These CAD models are processed to produce CNC commands known as G-code. The G-codes are instructions that tell the machine how to produce the CAD model.

## 1.2 FDM Articulation implementations

A Cartesian Gantry structure is the most common implementation. It consists of a linear actuator for each axis of freedom. The horizontal plane generally has a sturdy rail that a bridge is mounted on, this rail permits motion in the x direction. A carriage is mounted to a rail that connects the bridge together. The carriage can move along this rail and therefore permits motion in the y direction. Lastly the carriage has a tool that is capable of actuating in and out in the z direction.

The Gantry system is a well tested framework and is industry standard. It can be found in many applications from small desktop CNC machines to huge container cranes. While the frame is very strong, each linear actuator is dependent on another. The bridge actuator has to be the strongest as it must provide enough force to move the bridge, carriage and tool. This becomes an issue for fast moving applications as the momentum will be relatively large.

The Delta robot has three vertical rails placed in the formation of an equilateral triangle. Each linear actuator moves in the same direction and has kinetic linkages that connect each carriage to a central platform. This platform can be positioned by placing each carriage at a certain height. This is an improvement over the Gantry setup because each actuator shares the load equally. It is capable of faster speeds because there is less load on the tool end.

## 1.3 FDM accuracy and materials

Currently, leading consumer 3D printers can produce objects with layers heights of 0.1 millimetres. Such an accurate print will generally take around five hours for a medium sized print. Pricing for a mostly pre-assembled unit is around USD\$2,200.

Currently there are two main types of plastics readily available for FDM printing. Firstly Acrylonitrile Butadiene Styrene or ABS is a strong material. It is a oil based plastic that can be melted and extruded at a temperature of approximately 105 °C. It is fairly cheap at \$40 a Kg. It does contract slightly as it cools.

Polylactic Acid or PLA is another alternative that can be used for FDM printing. It is marginally less expensive then ABS. While being more brittle then ABS it does not contract as much. PLA is a biodegradable polymer and actually is produced by corn starch. Because of it's lower melting point it is not ideal for applications related to heat.

## 1.4 Proposed Solution

The delta machine design has been adopted for this project. Recently the Rostock project has spawned many derivatives, most achieving cheaper construction over the last generation of reprap printers. Delta machines have been used for many applications including; pick and placers, packaging and production line sorters.

Its simplicity helps reduce hardware costs. But the biggest advantage is the machines speed and accuracy. If the central platform is kept light, fast acceleration can be maintained. This permits the machine to perform in a sporadic manner while maintaining an accurate position.

The electronics system will not be a derivative of current implementations. I will experiment with different architectures with the goal of producing a much cheaper but fully capable system. The components will be made modular to allow for a high level of customisation. This helps to keep the main-board costs low but still permits additional more expensive upgrades such as a Ethernet add on.

## 1.5 Commercial Viability

This old technology is becoming established in a new market. While it becomes more accessible, new opportunities begin to emerge and intern, increases demand. Prices are decreasing, materials are becoming more accessible and there is an increasing amount of printable designs being uploaded to the Internet. The later attributes the most positive influence to the 3D printing market. This makes an old product more valuable.

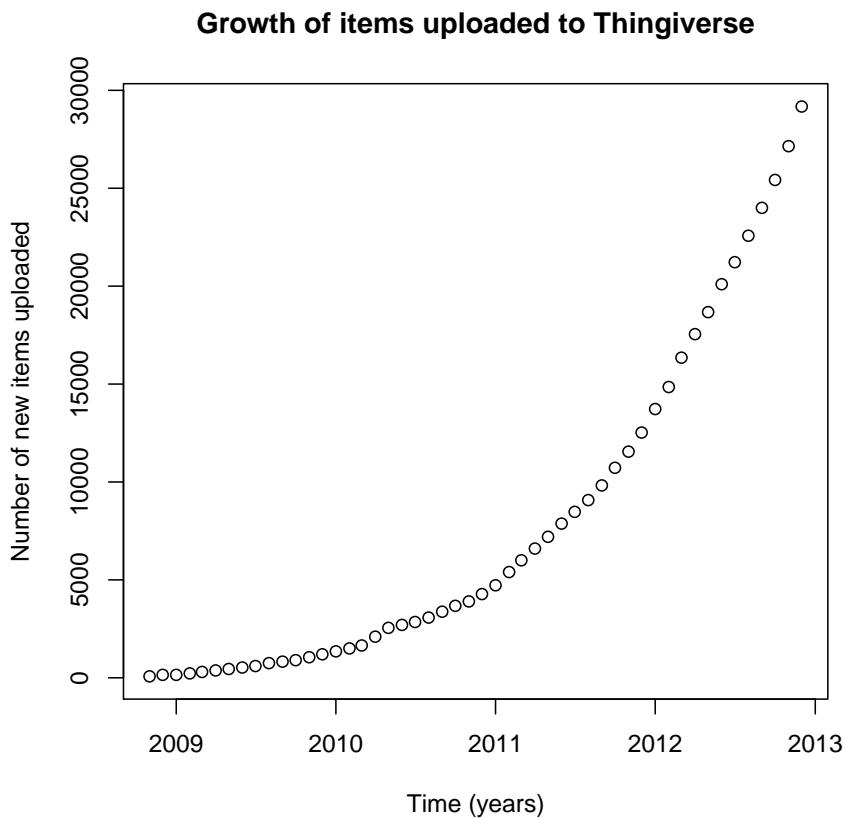


FIGURE 1.1: Growth of CAD designs on thingiverse.com [5]

It is clear that this market is expanding at a promising rate. Furthermore because there is such a diverse range of neighbouring markets that will benefit from this technology, it is likely that it will be supported by commercial demand alone. Applications for 3D printing have yet to be completely discovered, the boundaries are always being pushed by innovators. It is apparent that a very successful industry has been created.

### 1.5.1 Commercial Market

3D printing can help many different businesses. For example; Product designers can produce prototypes within a few hours, prosthetics can be made for a person more frequently and engineers can produce custom parts easily. It is important to note that even if a 3D printer existed in every home, there are still many skills that can't be replaced by automation. Downloading a generalised product will never replace a professionally crafted custom version. 3D printing just streamlines the development cycle and promotes rapid growth.

Rapid prototyping reduces development costs and creates new opportunities. It is possible that we will see a rise in hardware start-ups similar to the influx of software start-ups we have seen recently. It may be more feasible for a young company to attempt entering into established markets with little overhead.

### **1.5.2 Consumer Market**

There is a number of reasons why an individual might desire a 3D printer. It may help reduce our consumption rate by allowing us to easily repair broken household items. While it is unlikely for the average person to need a miniature factory, it is ideal for hackers, hobbyists, artists and craftsmen

Currently, the largest consumer market for 3D printing falls inside the open source community. Although intellectual property is freely shared, support and labour is very valuable. These customers are generally open to early adoption of new technology. The network of passionate, diversely skilled customers strive to improve the current designs and collaboratively innovate the CNC scene.

## Chapter 2

# Structure and Inverse Kinematics

The hardware design will be in the form of a delta machine. These devices can perform fast accurate tasks as the light-weight print head is capable of quick acceleration. This design has been adopted from a current reprap project [6]. The delta machine will use less parts then a traditional Cartesian machine.

For a detailed overview of this projects design please refer to the Design Document

### 2.1 Structure

A delta machine consists of a number of kinetic chains that meet at a central platform. This platform can be moved by actuating the pivots connected to the main structure. The platform is kept parallel to the floor during motion. Figure 2.1 represents a simple two armed delta machine. The two-dimensional diagram helps to illustrate the important lengths and vectors. After we have analysed a two dimensional machine we will apply these concepts to three-dimensions.

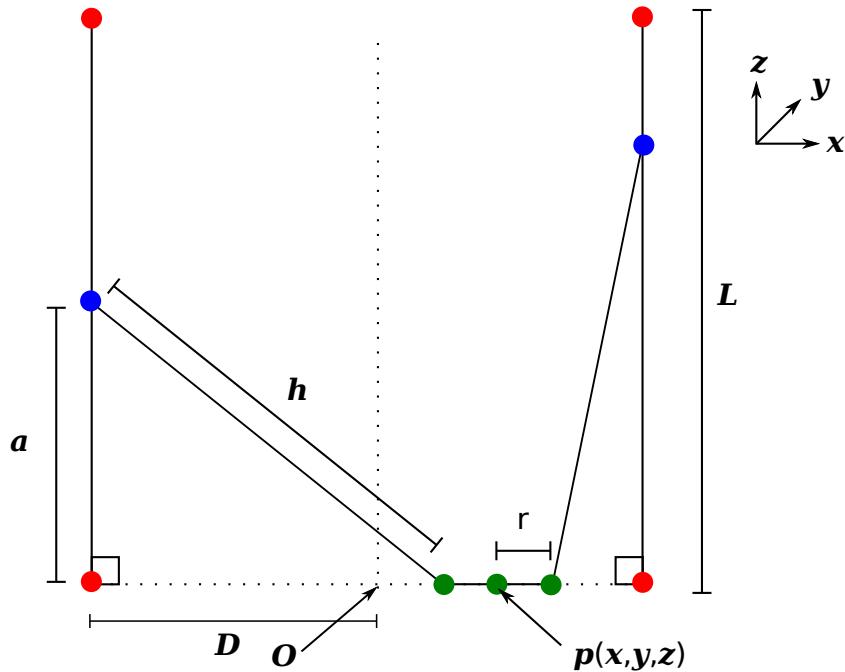


FIGURE 2.1: Structure Diagram

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$D$	Distance from actuator to origin
$L$	Vertical length of the frame
$a$	Height of the actuator pivot point from the origin
$h$	Length of the kinetic linkage
$r$	Radius of the platform
$p$	Position of the extruder tip or centre of the platform
$O$	Origin of the system
$x$	Horizontal vector
$y$	Vertical vector
$z$	Depth vector

---

TABLE 2.1: List of vectors

The following assumptions are made to help define the system:

- Platform and linkages must stay within the frame's outer rails.
- Linkages are not restricted in any way, they may swivel on their joins in any direction.
- The platform can not move down past the base.
- Linkages are restricted to the rail's length.
- Linkages can not stretch or contract.

## 2.2 Simple one dimension position

Lets consider one dimension to begin with, Figure 1 illustrates the movement of three key points; the platform and the left and right linear actuators. We can see that if the linkages are the same length as the vertical distance, the platform is capable of reaching any position along the  $x$  axis.

Also, it can be seen that a vertical actuator requires an equal amount of travel to permit full movement. It is important to note that the platform is considered a point source in this example. Practically this is not the case as we will require a place to mount tools.

For a desired position of  $p(x)$ , we need to derive where to place linear actuators. Take fig. 2.2 below, lets derive the equations that will translate a desired  $x$  into  $a_1$  and  $a_2$ .

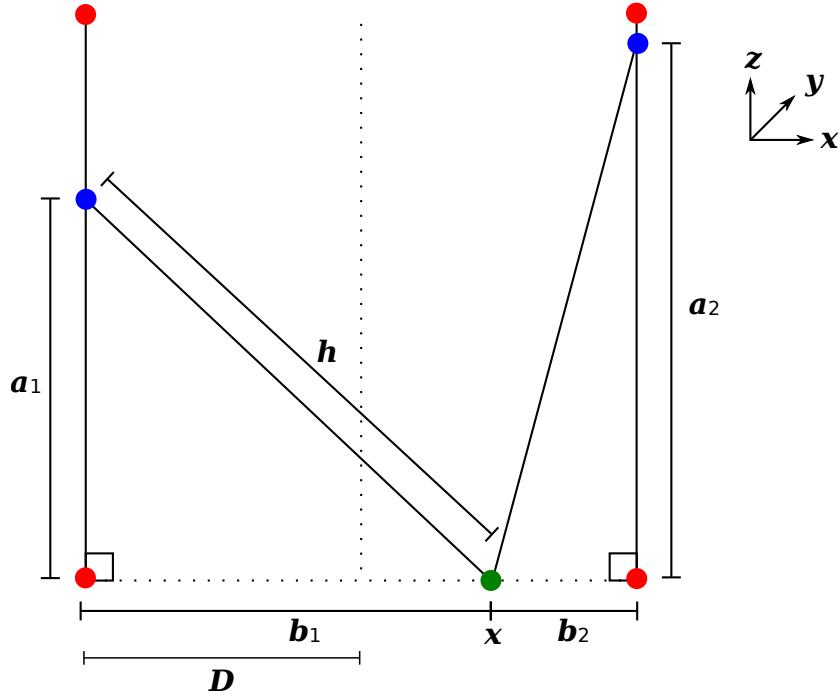


FIGURE 2.2: Simple one dimension parameters

Firstly, lets derive relationship between  $x$  and  $a_1$ :

$$(1) \quad h^2 = a_1^2 + b_1^2$$

$$\Leftrightarrow a_1 = \sqrt{h^2 - b_1^2}$$

$$(2) \quad b_1 = x - (-D)$$

$$\Leftrightarrow b_1 = x + D$$

substituting (1) into (2) gives

$$a_1(x) = \sqrt{h^2 - (x + D)^2}$$

Now, lets find the relationship between  $x$  and  $a_2$ :

$$(3) \quad h^2 = a_2^2 + b_2^2$$

$$\Leftrightarrow a_2 = \sqrt{h^2 - b_2^2}$$

$$(4) \quad b_2 = x - D$$

finally, substituting (4) into (3)

$$a_2(x) = \sqrt{h^2 - (x - D)^2}$$

## 2.3 Platform

We now need to consider what happens to the linkages when they are offset by the platforms width.

By adding extra length to the horizontal component, we have decreased the horizontal outer bounds of the system. The smaller the platform the more room we are able to travel. It should also be noted that the larger the platform, the less vertical travel is required for the actuators.

The Platform reduces the  $b_1$  and  $b_2$  term in our position equation by  $r$ . We now have:

$$a_1(x) = \sqrt{h^2 - (x + D - r)^2}$$

$$a_2(x) = \sqrt{h^2 - (x - D + r)^2}$$

## 2.4 Vertical travel constraints

We can also reduce the vertical travel required by reducing the linkages length. This intern reduces the available printing area. However, this can be used to our advantage. For example if we needed to restrict the horizontal bounds so that the platform can't physically interfere with the belt drive that runs alongside the vertical rails.

## 2.5 Two dimensional position in the vertical plane

Now we are able to examine how we may add a vertical component to the system. From the last sections we discovered that the length required for the vertical actuators is the equal the linkages length. In this example, we have created a square printable area of  $(2D)^2$ . This is possible as the rails are twice the length of the linkages length or  $L = 2(2D)$ .

Introducing the  $z$  component directly adds to the  $a_1$  and  $a_2$  terms. The position equations are amended as:

$$a_1(x) = \sqrt{h^2 - (x + D - r)^2} + z$$

$$a_2(x) = \sqrt{h^2 - (x - D + r)^2} + z$$

## 2.6 Two dimensional position in the horizontal plane

Now its time to examine how adding a third actuator allows for two dimensional movement in the horizontal plane. Figure 2.3 is a top-down view of our system. The actuators are placed in a equilateral triangle formation to distribute the load evenly. The position of the platform can be altered by changing the lengths of the linkages horizontal component, the  $b$  term. Remember, this is not stretching the linkages, it is merely displacing length between the horizontal and vertical component - the hypotenuse remains the same. By looking straight down into the system, only the  $b$  vectors are visible, the carriages on the rails or the  $a$  term is directed in/out of the page.

The coordinates system has been aligned with the actuators to help simplify the problem. The origin is placed at the centre of the print bed. Please note that the print bed is represented as a circle with its radius equal to the minimum distance from the origin to the frame.

To control the platforms position we must modify the carriages vertical position  $a$ . However, the horizontal plane position is completely dependent on  $b$ . We have already established the relationship between  $a$  and  $b$ , and that is  $a = \sqrt{h^2 - b^2}$ . We now need to develop the relationship between  $b$  and the position  $(x, y)$ .

Each actuator will have its own equation for calculating its  $b$  term. This is because they are not placed uniformly around the coordinates system even though they are equally apart. Firstly, the general rule for calculating  $b$  as a function of the platforms position:

$$b_n(x, y) = |\overrightarrow{R_n P(x, y)}|$$

Where  $R$  is the position vector of the target actuator and  $P$  is the position vector of the platform.

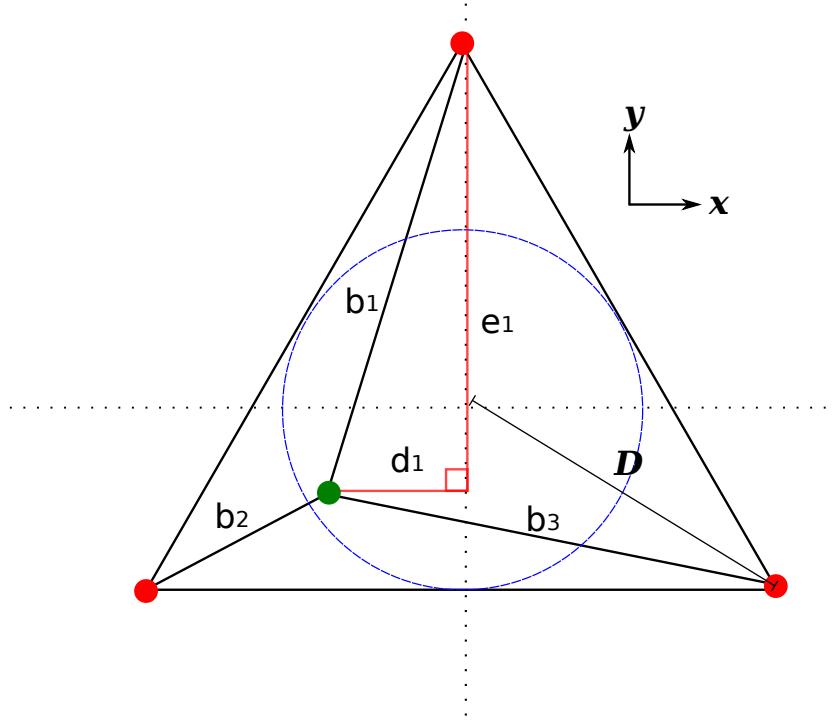


FIGURE 2.3: Top view components

Figure 2.3 illustrates that this problem can be solved by a simple application of Pythagoras' theorem again.

Top actuator:

$$d_1(x) = x$$

$$e_1(y) = y - D$$

$$b_1(x, y) = \sqrt{d_1^2 + e_1^2}$$

$$b_1(x, y) = \sqrt{x^2 + (y - D)^2}$$

Bottom left actuator:

$$d_2(x) = x - (-d\sqrt{3}/2)$$

$$e_2(y) = y - (-d/2)$$

$$b_2(x, y) = \sqrt{(x + \frac{d\sqrt{3}}{2})^2 + (y + \frac{d}{2})^2}$$

Bottom right actuator:

$$d_3(x) = x - D\sqrt{3}/2$$

$$e_3(y) = y - (-D/2)$$

$$b_3(x, y) = \sqrt{(x - \frac{D\sqrt{3}}{2})^2 + (y + \frac{D}{2})^2}$$

## 2.7 Platform in the horizontal plane

Adding a platform with a radius of  $r$  just offsets our  $x$  and  $y$  components. The amended equations are:

$$b_1(x, y) = \sqrt{x^2 + (y + r - D)^2}$$

$$b_2(x, y) = \sqrt{(x - \frac{r\sqrt{3}}{2} + \frac{d\sqrt{3}}{2})^2 + (y - \frac{r}{2} + \frac{d}{2})^2}$$

$$b_3(x, y) = \sqrt{(x + \frac{r\sqrt{3}}{2} - \frac{D\sqrt{3}}{2})^2 + (y - \frac{r}{2} + \frac{D}{2})^2}$$

## 2.8 Three dimensional positioning

Both horizontal and vertical components have been explained and now can be combined into one system. To implement a three dimensional system, we simply need to replace our  $b_n$  variable in the vertical plane equation with the horizontal plane equations. The result is:

$$a_1(x, y, z) = \sqrt{h^2 - |x^2 + (y + r - D)^2|}$$

$$a_2(x, y, z) = \sqrt{h^2 - |(x - \frac{r\sqrt{3}}{2} + \frac{d\sqrt{3}}{2})^2 + (y - \frac{r}{2} + \frac{d}{2})^2|}$$

$$a_3(x, y, z) = \sqrt{h^2 - |(x + \frac{r\sqrt{3}}{2} - \frac{D\sqrt{3}}{2})^2 + (y - \frac{r}{2} + \frac{D}{2})^2|}$$

## 2.9 Constraints

### 2.9.1 Printing Bed

A design assumption was made at the beginning of this section; The platform can not be positioned outside of the frame. To force this rule to apply, we must set the linkages length equal to the minimum distance from a rail to a side of the frame. The maximum length required is a line straight down the y axis from the rail to the frame which is equal to  $\frac{\sqrt{3}}{2}D$ . If we swing the platform around, pushing it to the maximum radius that this length permits, we see that the path is not actually a circle but a rounded triangle. The light blue path in fig. 2.4 is the maximum positions. Such an unusual path is typically not needed, so we will simplify our problem by using a circular print bed.

To allow for a platform, we must subtract its radius from each of the linkages length. So, our rule for  $h$  is:

$$h = \frac{\sqrt{3}}{2}D - r$$

### 2.9.2 Universal Joint Angle Range

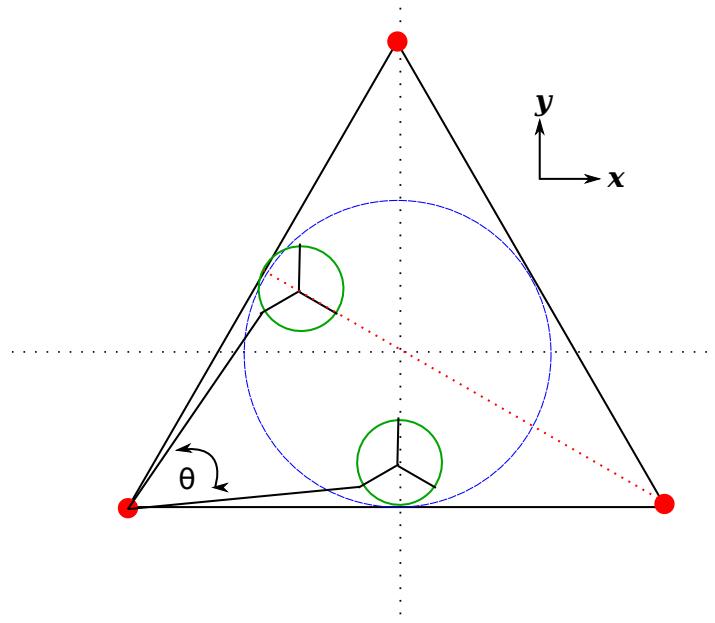


FIGURE 2.4: Universal joint angle horizontal range

The universal joints that will pivot to allow full movement will need to be capable of a certain range. This can be calculated exactly with:

$$\theta = 60 - 2 \arctan\left(\frac{\frac{2-\sqrt{3}}{2}r}{\frac{1}{2}D}\right)$$

Practically, we can simplify the problem by aiming for 60° in the horizontal direction and 90° in the vertical direction.



# Chapter 3

## Motion

### 3.1 Path Tracing

Once a three dimensional object has been split up into two dimensional layers, the extruder head must trace the outlines of each layer. Once a layer has been traced, the z component moves a step down and the extruder will trace the next layer. The process repeats until all layers have been extruded leaving a fully formed three dimensional object.

To move the extruder in a desired direction, we must calculate the distance and direction that each actuator must travel. This can be done by subtracting actuator heights from the last position with the heights of the next move. This gives us three vectors describing the distance and direction. The next step is to translate these distances into corresponding speeds. To move in a straight line, each actuator must complete their respective distances at the same time.

So to calculate how fast each actuator must move, we first start with:

$$speed = displacement / \Delta time$$

So we can see that keeping the time constant for all three actuators, only displacement affects speed. Actually speed is directly proportional to the distance that needs to be travelled.

But how long is an acceptable time to travel? This is quite simple once the maximum speed is determined. The actuator with the largest displacement should travel at maximum speed.

$$\Delta time = displacement / MAX(speed)$$

Now we simply substitute the same  $\Delta time$  for the other actuators. Now we have proportional motion!

## 3.2 Acceleration

Acceleration is required to ensure smooth motion is maintained. Smooth motion is essential for reaching high speeds and also to minimise a stepper motor skipping a step. The rate of acceleration can be written as a function of current and next frames momentum. We are only concerned with the momentum of the actuator carriages, not the momentum of the platform.

$$P = mv$$

where  $P$  is momentum,  $m$  is mass,  $v$  is velocity. So to decrease momentum around sharp bends, we must reduce the speed of the actuator.

Once the system has been constructed, we will need to run tests to work out the maximum speed that we should attempt to accelerate to. Jerk is the derivative of acceleration. It can be thought of as how fast can we accelerate? This also will need to be thoroughly tested. But we can write it as a variable so that we can later substitute different values.

The acceleration algorithm is as follows:

- calculate the closest change in direction for any actuator
- if change is less than 100 steps decrease speed by A
- if change is greater than 100 increase speed by A
- if maximum speed has been reached do nothing.
- repeat next step

This creates a smooth linear acceleration. We could also implement more detailed patterns that perhaps use a quadratic to reach the maximum speed sooner.

# Chapter 4

## Hardware

Now that we understand the physical constraints we can start to design the physical system. Firstly, lets reiterate over some of the main objectives that relate to this section:

- Kit like assembly
- Cheap hardware
- Solid and sturdy construction

### 4.1 Frame

The first iteration of design utilised aluminium to build the framework. It was selected due its strength and the modularity it offered during the prototyping stage.



FIGURE 4.1: System30 Beam

#### Positives

- Very strong in any direction
- Simple mounting and joining

- Reusable
- Easy to modify / tune

#### Negatives

- Relatively expensive at \$25 per meter
- Requires special cutting tools
- Hard to source

However during the initial design, it was decided that the carriage designs would be too complex which would violate one of our design goals. The very cheap and easily obtained 8mm threaded and smooth rods were used instead. This way we can use LM8UU linear bearings instead of investing a lot of time in hardware design.



FIGURE 4.2: 8mm round bar and LM8UU Linear bearings

#### Positives

- \$3.3 per meter for stainless steel round bar
- \$0.90 per meter for 8mm threaded rod.
- \$0.75 per unit for LM8UU linear bearings.
- Easy to obtain from metal fabricators or general hardware stores
- Can cut with a hacksaw or angle grinder

#### Negatives

- Flexes in the horizontal direction

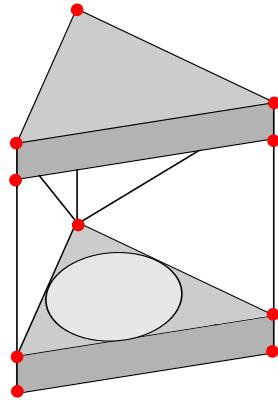


FIGURE 4.3: Early Sktech Of Frame Design

The frame will have a small enclosed area for the electronics and power supply. The printer bed is mounted on top of the case. There is a beam on the top level that intersects the face in half. This is primarily for a place to mount the plastic feeder but also serves as a structural support beam.

We will need to know how much material to order. There are 4 equilateral triangles with side lengths of  $D$  and there are 4 rails that need to be of  $D$ .

$$M_{threaded} = 3(4D) + 2(D\sqrt{3})$$

$$M_{smooth} = 3(2 * 2D)$$

To minimise waste,  $D$  needs to be a multiple of the purchased material's length. To further reduce waste, the purchased length should be close to a whole number.

## 4.2 Frame Brackets

### 4.2.1 Bottom Level

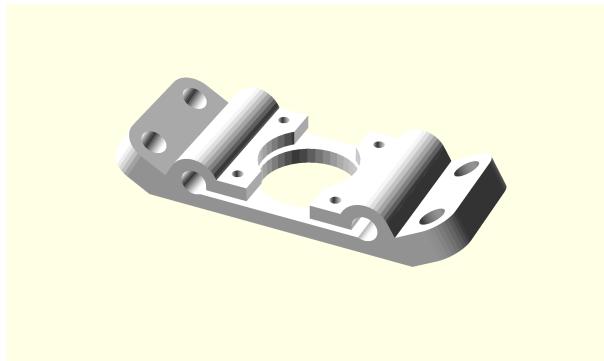


FIGURE 4.4: Frame Bottom Bracket

This design was an attempt to reduce the part count by incorporating as much functionality into a single piece. Firstly, the 4 holes on the outer perimeter are for threaded rods that will connect to other brackets that will form the base of the equilateral triangle. The clamps in the centre hold on to the parallel smooth rod that form the linear actuator and that attach to the top brackets. The screws that put pressure on the clamps also couple the stepper motor to the bracket.

#### 4.2.2 Top Level

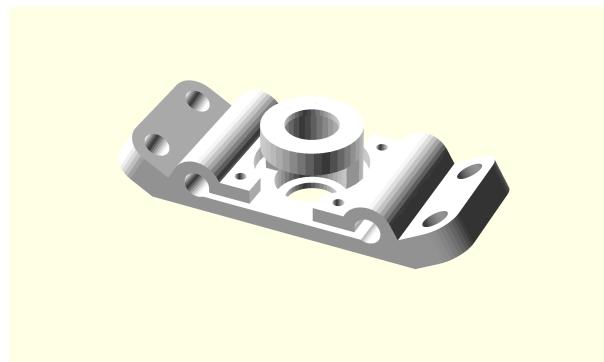


FIGURE 4.5: Frame Top Bracket

A symmetrical design allows us to recycle many similar parts. Comparing the bottom bracket to the top bracket we can see that the only difference is the recessed enclosure for a 608zz bearing. They are recessed so that the bearings do not fall out during operation.

### 4.3 Platform

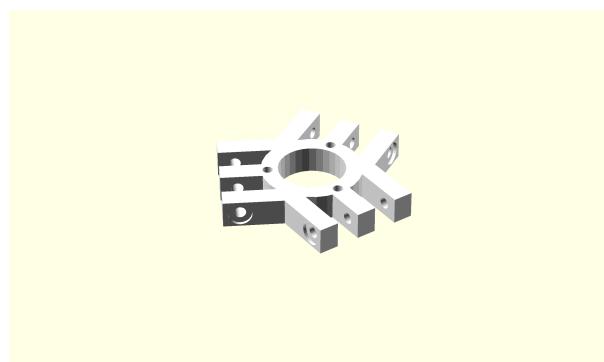


FIGURE 4.6: Platform

The platform is simply a base to mount a tool to while connecting each linkage to a linear actuator. In the Centre there are three holes that stand offs attach to. The outer holes are where the ball bearings are seated.

## 4.4 Linkages

The linkages are made up of 4mm threaded rod cut to a specific length. The rod is currently attached to 10mm Traxxas Rod Ends to allow movement between the carriages and the platform. These are originally for model RC car and are reasonably priced for their quality.



FIGURE 4.7: Traxxas Rod Ends w/Hollow Balls Large

## 4.5 Linear Actuators

### 4.5.1 Carriage



FIGURE 4.8: Carriage

The outer holes with the relief cut mount LM8UU linear bearings. They are placed in with M3 screws clamping them into place tightly. A belt runs up through the centre with a small plate pressing against the frame fixing the belt to the carriage. The horizontal bore are where the linkages mount to. A 30mm M3 bolt holds the rod ends in place.

#### 4.5.2 Belt Drive

I have opted to use GT-2 belt with 2mm pitch. The GT-2 grooves are far finer than the original T2.5 x 5mm Belt. Finer grooves will help produce smoother motion. The belts are made from neoprene rubber and have fibreglass reinforcing running through them.

#### 4.5.3 Pulley and idlers

The gears that match the belt were also printed. They were generated using the OpenScad [Parametric pulley library](#) by user '[droftart](#)' from Thingiverse. This is a great library, it offers great flexibility. The tooth profiles themselves are actually generated from the original manufacturers DXF images.

The Pulley attaches to the stepper motor in the reverse orientation so that the lock nut is easily accessible and so the belt lines up with the top bracket. The idler is sandwiched between two 608zz bearings in the top bracket.

The gears must be perfect. It took a few trial runs before a straight tooth profile was obtained. The best printing settings are obviously fine, 0.25mm layer heights and full infill. Care must be taken when leveling the printing bed, it is actually better to have the bed slightly further down from the extruder so the higher layers do not clump together and warp during printing.



FIGURE 4.9: Gear and idler

#### 4.5.4 Motors

Standard common Nema 17 stepper motors have been used in this design. They feature 1.8 deg/step and are capable at driving a single coil with up to 2.5A. They can be obtained for \$15 each.

They can provide plenty of torque and are typically powered with 12 to 24 volts. The Steppers that were purchased are a normal bipolar configuration with four leads.

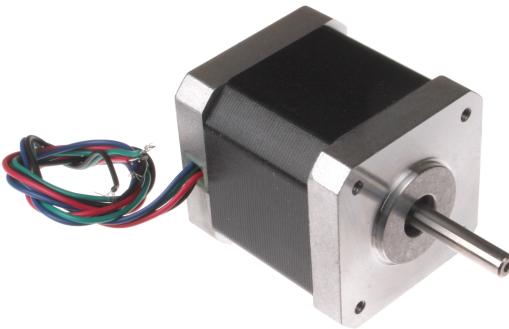


FIGURE 4.10: Nema 17 Stepper Motor

### 4.6 Tool End

#### 4.6.1 Plotter

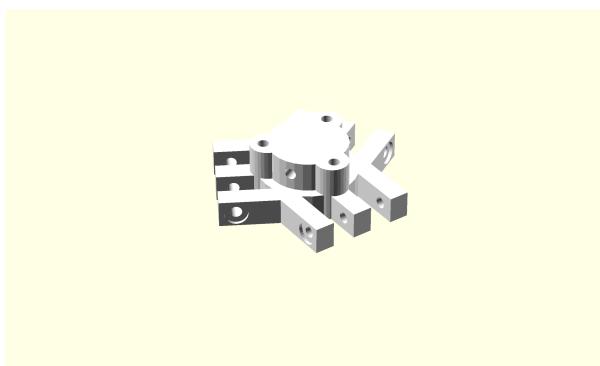


FIGURE 4.11: Plotter Attachment

Before 3D printing, I wanted to be able to test and perfect the performance of the machine. A plotter attachment was developed so that the paths generated could be analysed. A barrel was designed to hold a normal ball point pen. The pen is cut in half and the spring is reversed so that it is always pushing against the target surface.

Horizontal screws fix the pen in place and the vertical screws attach the plotter to the platform.

The metal tip of the pen has a wire soldered, this is to be used when automating the height calibration. The base is currently made from a copper plate which is kept at ground. The pen tip is pulled high with a 10K resistor, so if the tip meets the base the tip will be pulled low. We can detect the voltage change with our microcontroller.

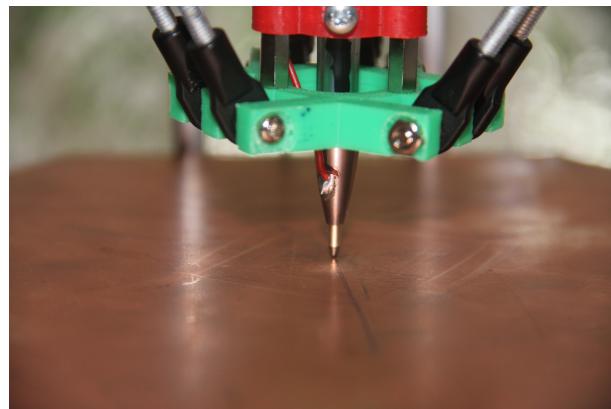


FIGURE 4.12: Plotter Homed

## 4.6.2 FDM Tool

### 4.6.2.1 Extruder

The extruder that will be used is the inexpensive common J-head extruder. It features a PEEK nylon tube with ventilation holes to help reduce heat transfer up into the platform. The hot end is a block of aluminium for a light weight tool. A 100K thermistor is embed in the block along side a 5.6 ohm, 1%, 5W resistor which is used as a heating element.



FIGURE 4.13: J-head Extruder

A clamp setup was developed to attach the extruder to the platform. Stand offs are used to space the extruder away from the platform so that the maximum printing depth is available. A tube clamp is fixed on top of the extruder for use with a Bowden feeder system (explained in the following section).

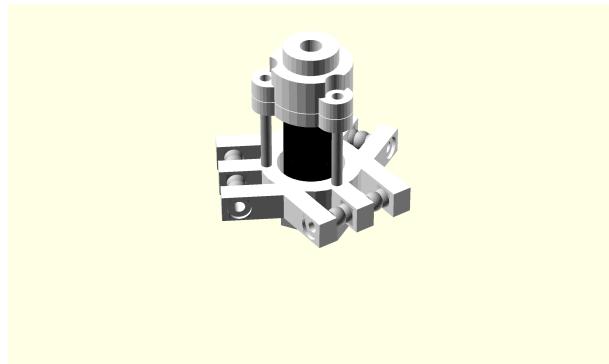


FIGURE 4.14: Extruder Attachment

#### 4.6.2.2 Bowden Filament Feeder

A Bowden Filament feeder is a design that aims to reduce the weight on the tool end. The principle is by reducing the mass, we can increase the acceleration. By shifting a heavy direct drive stepper motor off the platform and fixing it onto a stationary point, we have greatly reduced the moving mass.

Instead of feeding filament directly into the extruder, it is fed first through a strong PTFE tube. The tube itself does not flex much so the force eventually builds up enough that the filament must push through the least resistances and that becomes the hot end.

A fair amount of force is required to push the filament through a length of pipe and through the extruder. This is why I have selected to use a geared configuration to increase my motors torque. A Herringbone gear arrangement is used as transfers power more evenly because more than two teeth mesh together at one time. They are also easily manufactured with 3D printing. The gears were borrowed from [robo\\_kid22](#) on Thingiverse.

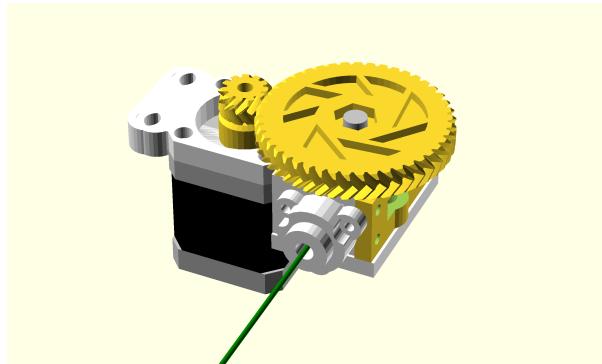


FIGURE 4.15: Bowden Filament Feeder

The design features a door like mechanism that is spring loaded to apply pressure on the filament. It pushes a bearing against a bolt that has had a rough surface machined into it. This provides good traction between the filament and does not slip. The filament is then fed directly into the tube which is coupled to the moving platform. The feeder is mounted on the top of the frame with a spool of plastic along side it.

## Chapter 5

# Electronic Systems

### 5.1 Methodology

The first iteration of electronics were designed around the goal of modularity. While it offered the needed flexibility during the prototyping stage, a few shortcomings forced a redesign. It featured small daughter boards that vertically plugged into a mainboard. Exposing a SPI bus as ports that could accept any type of add on provides a possible upgrade path in the event of a necessary addition.

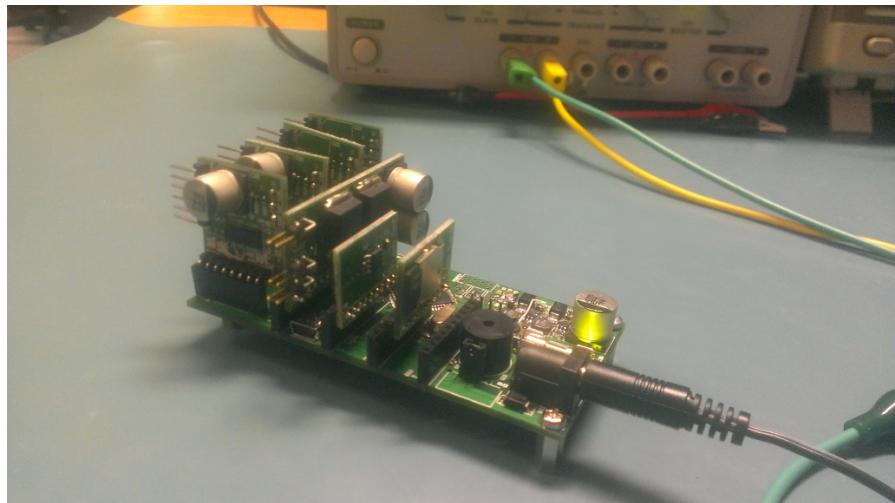


FIGURE 5.1: First iteration of electronics

Unfortunately this configuration was too flimsy. Stepper drivers were damaged during testing. There is a lot of manual work required to assemble such a design and would not be practical for a final product.

The second revision was designed to be a simple low-cost single board solution. Instead of being a complete standalone product, this version is designed to leverage of a host computer. No external memory is used so a computer must constantly feed G-Code commands during a print.

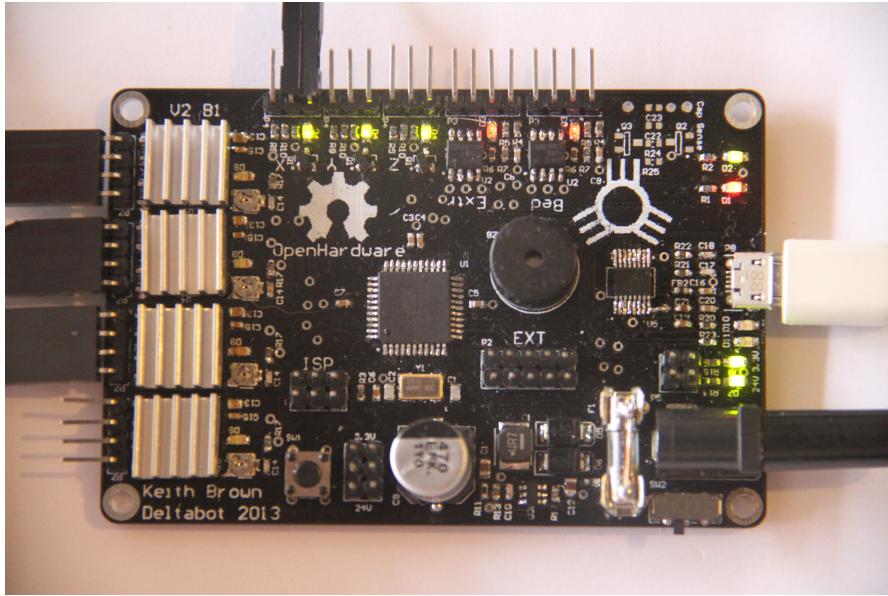


FIGURE 5.2: Second revision

One of the main goals of revision two was to be cross compatible with the exiting community firmware. The most compatible firmware is '[Teacup](#)' . Furthermore, any software that I develop should be cross compatible with existing hardware such as RAMPS.

## 5.2 High Level Diagram

Efficient circuit board design was achieved by using the hierarchy model. The numerous duplicated parts can be abstracted and then replicated the desired amount. This also makes managing a large project far easier. This also speeds up circuit board development since that we only need to lay tracks for a single component and then propagate them to similar 'rooms'.

Examining the top level diagram, we can see that the each of the three actuators utilise two components; the stepper driver and a end stop. The extruder component contains one stepper driver and also heater circuitry, while the heated bed only holds a heater.

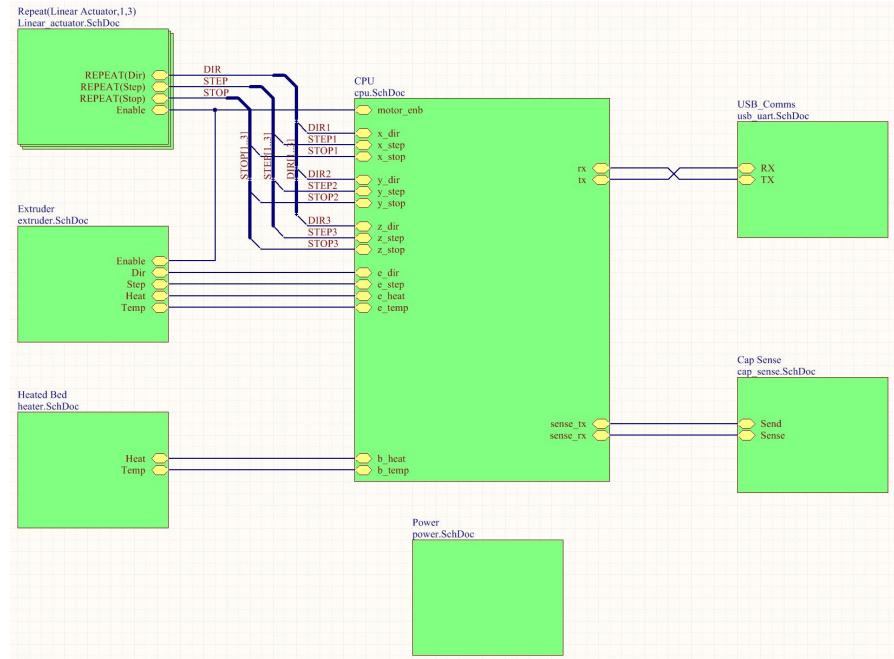


FIGURE 5.3: Top Level Diagram

### 5.3 Microcontroller

The Microcontroller that has been selected is an Atmel 8-bit ATmega644. It was selected due to its low cost, small footprint and compatibility with existing firmware. The large ATmega family also allows for an upgrade path if required. It can be clocked up to 20MHz however I am using 10AU model which has a maximum of 10Mhz. The 10AU is available in single quantities at \$4 compared to the 20Mhz at \$11.

The package includes 64 Kbytes of flash memory. It has 44 pins with a total of 32 GPIO available. No USB communication is integrated so a USB to UART chip is required. The physical package selected was a TQFP so that it can be easily soldered with a standard soldering iron.

### 5.4 Motor Drivers

TI DRV8825 integrated motor drivers were selected to drive the stepper motors. They can be configured to drive a single bipolar stepper motor at 2.5A with up to 1/32 microstepping. They do not require many external passive components. They feature a useful error signal pin that goes high in the event of over current or heating issues. A heat sink should provide adequate heat dissipation.

## 5.5 Communication

An FTDI FT220X USB to UART converter is used for communication between the host computer and the printer. It runs at a baud rate of 38400, however burst commands can be sent due the internal FILO buffer included in the integrated circuit. A micro USB header was selected so that common android phone cables can be used.

## 5.6 Heating elements

A powerful MOSFET is used to push large current through a small resistor. This produces heat. The heat can be monitored with a robust thermistor. A PID loop will smoothly and accurately maintain a specific temperature. Two heat ports are available; one for the extruder and one a heated bed.

## 5.7 Sensory input

To determine where the platform is in the work space, the printer must first 'home'. This is the act of synchronising the memory coordinates with the actual physical coordinates. It can be achieved by firstly, moving all actuators to the top of the rails. A sensor triggers when the carriage has reached the very top so that the motor can stop. Once all carriages have reached the very top, the platform is sent back down towards the base. This is done by moving all carriages at the same time. Another sensor detects when the tool end has just touched the platform signalling the end of travel. Once this occurs, all software variables ( $x, y, z$ ) can be set to 0 indicating a homed tool.

The top 'end stops' have been implemented with Photo-interrupter modules. These have a IR LED that shine a beam of light into a photo-transistor. If something gets in the way of this beam, the transistor will switch off. In this case, a small height adjustable square plate attached to the carriage breaks the IR beam. See figure x

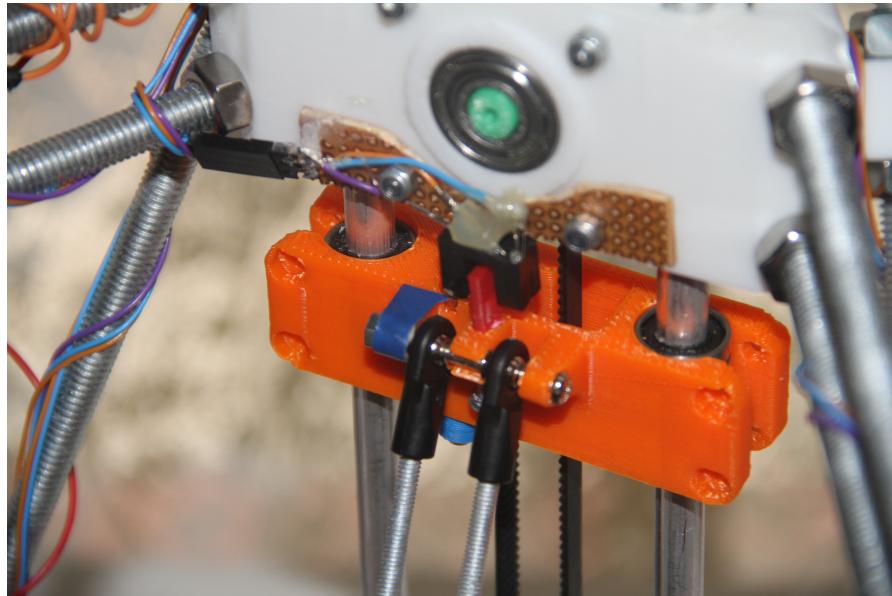


FIGURE 5.4: Photo-interrupter

The bottom plate contact is currently triggered when the tool end tip touches the grounded plate. The tip is pulled high through a 10K resistor and this level is monitored by a transistor. When a contact is made the transistor's base is forced low signalling the end of travel has occurred. While this produces great results, it is not practical in the long run once we move away from a copper plate. It would be nice to print on a fibreglass board so it can be removed. Fibreglass is not conductive so the current method will not work.

A possible alternative is to use a switch that can be retracted during print. This possible adds a servo to the tool end increasing weight. Another alternative would be to use a IR range finding system. While complex, it would mean that the platform could race towards the base but slow down as it approaches the base. It also would be extremely light weight as the only components required are a LED and a photo transistor.

## 5.8 Power

The AOZ1280 from Alpha & Omega Semiconductor is a 1.2A buck regulator. It is configured to +3.3V by using a resistor divider of 49.9K and 15.8K. 1.2A is more than enough to power all the logic and LEDs. Since the whole system is dependent on this switched, we can control the system's power by toggling the buck regulators enable pin. This means that we can use a very small chip and avoid large heavy duty power switches.

The Stepper drivers also require a 12V to 24V supply for the internal FETs. Status LEDs indicate both the 12V and 24V rail status. Currently 12 volts is brought in through a standard DC barrel jack.

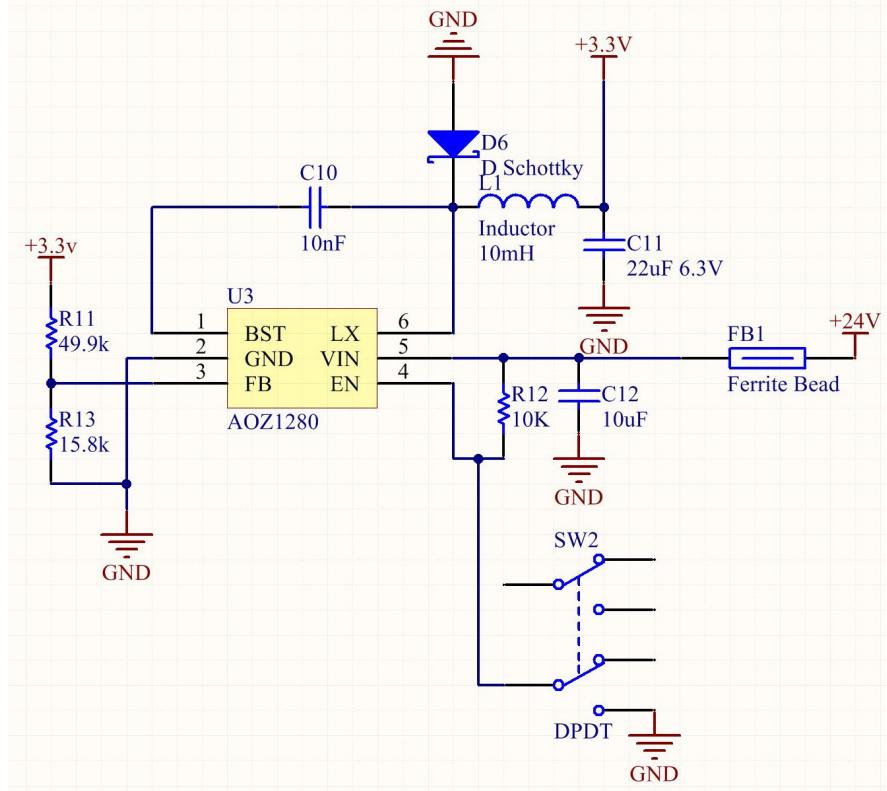


FIGURE 5.5: Power circuit

## 5.9 Safety

A fuse and schottky diode has been added to the power line. It prevents excessive current drawn. This usually occurs when a fault causes a short circuit. As mentioned above, the stepper drivers also have internal thermal fault sensors that cause the chip to shut down until the temperature reaches a reasonable level.

# **Chapter 6**

## **Software**

### **6.1 Major Functions**

The main purpose of the device is to offer basic computer numerical control functionality. This is accomplished by many sub modules successfully different smaller tasks. They can be broken down to:

- Accurately control the position of the tool end
- Smoothly manage speed and acceleration
- Provide a means of zeroing platform
- Manage communications to a computer
- Regulate temperature
- Implement error handling
- Process and cache data

### **6.2 Major Constraints**

The most obvious constraint is the processing power of the small microcontroller. A 10Mhz 8-bit CPU isn't the most impressive piece of hardware. Operations on ints and longs will take multiple clock cycles. Without a FPU any float operations will take a considerable amount of time. However, if we are careful with our design and execution, issues associated with these constraints can be mitigated.

The answer is to pre-process incoming data and cache it for future use. By implementing a queue like system we can evaluate and save upcoming tasks while the processor is not active. As long as we can queue up and process the commands faster than they are executed, the system will remain constantly active.

A work around is to simply offload a complex task to the host computer. For example, we will not transmit a raw STL file to the board. This would require the board to process a large 3D description and slice it into layers. This is actually relatively power hungry and while possible, it would be much more efficient to run an existing solution on a computer.

Furthermore running components on a computer opens up debugging options. We can simulate a part of the program in real time and visual display the results on a screen. Doing so will increase development time, but it also is a safer option considering the time constraints. Having greater debugging utilities should speed up the prototyping stage. Once working, individual components can be shifted to the board in iterations to slowly confirm correct operation.

### 6.3 High Level Diagram

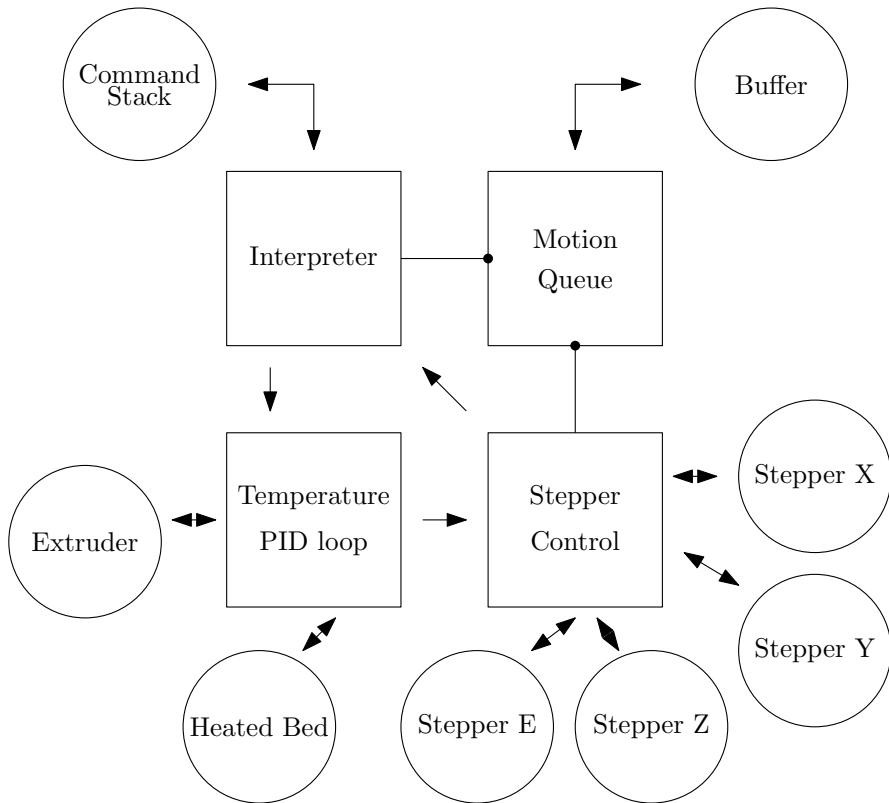


FIGURE 6.1: High level software diagram

## 6.4 Sequence Analysis

The following diagram represents the state machine that is implemented on the computer to handle model processing and communication.

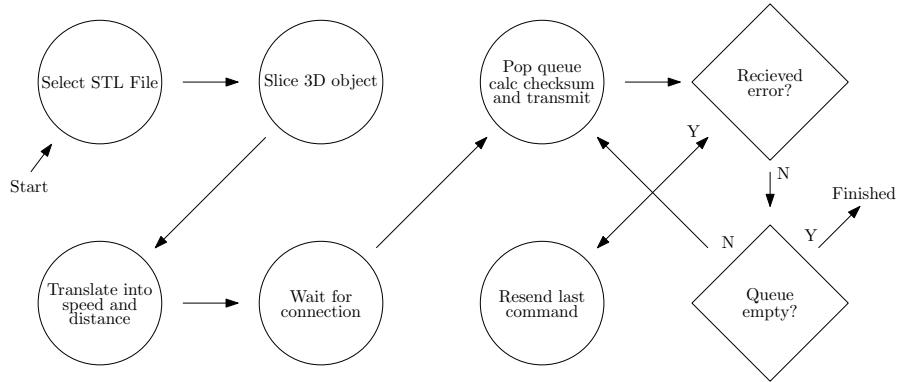


FIGURE 6.2: Transmission flow

## 6.5 Framework

The following sections describe key features of a framework that was developed. These aspects try to force a standard so that consistent readable code is produced. The main goal of this framework is to retain maintainability as the project grows and scales up.

### 6.5.1 Device Abstraction

Coming from a Computer Science background I felt it was necessary to try and force my devices into abstracted structures. The aim is to cleanly recycle as much code as possible while promoting clean and readable code.

```

typedef struct LCD{
    Spi *spi;
    int col;
    int row;
    int cursor;
    Pin *rst;
    Pin *mode;
    Pin *enb;
    CircularBuffer *buffer;
}LCD;
  
```

For example UART, SPI, position queue implement the same CircularBuffer structure. Each time a new 'device' is created a new instance of a CircularBuffer is instantiated and

its pointer is then associated to it. Furthermore, say we required 10 LCDs on a single SPI line. We can now simply create an array of LCD type and instantiate instances of a LCD. The flexibility is a clear advantage. Using this method of code recycle also reduces the amount of flash storage required to hold the program. Since the patterns are clearly described and reused, the compiler only needs to store the functions associated with an LCD once. If the code was written inline, the compiler would not be able to efficiently optimise the code.

However the drawbacks may force you into inline code depending on the application. The biggest issue is that for every execution of a abstracted LCD command adds an additional JMP command. This is one extra clock cycle opposed to inline code. However if speed is an issue, the inline function keyword can be used to tell the compiler to copy the following code instead of jumping to it. This obviously bloats your program size fast so it should be used sparingly.

### 6.5.2 Folder Structure

I have chosen to set the firmware directory in a way that attempt to separate non similar objects. For example system settings should not be located in the same directory as code for a LCD.

The following list illustrates the basic structure:

- **dev** contains sub folders that have code relating to physical components such as LCD and stepper motors
- **etc** contains configuration files such as clock speed, pin descriptions and macros
- **lib** contains reusable software objects such as buffers
- **main** holds different top level files (useful for different applications or tests)
- **sys** has anything to do with the microcontroller architecture

## 6.6 Implementation

### 6.6.1 Portability Header

With the addition of device abstraction, I have decided to even abstract pin hardware as well. By stripping the port pointer dereference in Atmel's avr/io.h file, we enable storage of useful memory locations such as ports and their corresponding modifiers.

```

Port PORT[] = {
    {(&vbyte *)_PIN_A, (&vbyte *)_PORT_A, (&vbyte *)_DDR_A},
    {(&vbyte *)_PIN_B, (&vbyte *)_PORT_B, (&vbyte *)_DDR_B},
    {(&vbyte *)_PIN_C, (&vbyte *)_PORT_C, (&vbyte *)_DDR_C},
    {(&vbyte *)_PIN_D, (&vbyte *)_PORT_D, (&vbyte *)_DDR_D},
}

#define PA &PORT[0]
#define PA0 &PA_PIN[0]
#define PA1 &PA_PIN[1]
...

```

Now that ports and pins are storables, we can associate our device structures with pins using pointers. An easy way to keep track of a boards implementation is to write a pin header file that maps symbolic names to actual pins. This allows us to easily maintain a software for a number of different hardware implementations.

```

#define y_step PA0
#define x_dir PA1
#define motor_enb PA2
#define x_step PA3
#define x_stop PA4
#define y_stop PA5
#define b_temp PA6
#define e_temp PA7

```

Furthermore, this method enables us to write portable C code. Multiple architectures can be handled by simply swapping out the pin.c file. It contains all the necessary architecture interaction. Machine code for MSP430, ATmega and ARM could be generated by the 'same' piece of code. The software can be written without being too concerned with the current architecture.

```

void pin_low(Pin *pin){
    *pin->port_ptr->out &= ~pin->mask;
}

```

For a fully cross compatible framework timers and interrupts need to be implemented in a similar method. This is definitely possible but out of this projects scope.

### 6.6.2 G code interpreter

A CAD design is saved to a STL file. The STL file is then parsed by a g-code converter such as [Slic3r](#). This process basically splits a 3D object into layers and then converts these into instructions that will trace the infill. The G-code is basically a set of Cartesian

points. Further processing needs to occur, translating the position points into actuator heights and then into speed descriptions.

Diagram here

Currently, all processing occurs on the host computer. The speed description is sent across USB and stored in a queue. Each command is validated with a string checksum. If an error occurred, then the board can request the computer to repeat.

The interpreter is implemented as a console like program. Firstly, a list of programs is stored in array. Each element contains a string to match on and the associated function pointer.

```
typedef struct Program{
    char name[20];
    void (*function)();
}Program;
```

A new line character signals the interpreter to parse the cached string. It runs through the string and assigns pointers to any character following a space. This is turned into an array of arguments that can easily be parse in the actual 'program'. The first token tell the interpreter which program to execute. For instance the command "home" will home the platform. A more complex "aprox 100 1 1 0.5" can signal the speed queue program to parse the arguments and check the checksum.

### 6.6.3 Positioning

The heights of the actuators are calculated with the following equations:

```
var a1 = z + Math.sqrt( r2 - Math.pow( dist( x, (y +pr) - D ),2) );
var a2 = z + Math.sqrt( r2 - Math.pow( dist( (x-.5*pr )+ root3*D/2, (y -
root32*pr ) + D/2 ),2) );
var a3 = z + Math.sqrt( r2 - Math.pow( dist( (x+.5*pr ) - root3*D/2, (y -
root32*pr ) + D/2 ),2) );
```

This is implemented on the host computer and written in JavaScript. Following those calculations, we need to determine the speeds and distance required. This is achieved by first determining which actuator needs to travel the furthest. Then we calculate the speed as a ratio that will make the carriage travel its distance in the same amount of time as the other carriages. This is simply the distance divided by the largest distance.

### 6.6.4 Motion

Before we can write software to control the hardware, we must mathematically define the system. Lets start with the pulley. The radius of our GT2 pulley is 11.5mm. I have selected to only microstep 8 times. This should give a reasonable balance between accuracy and speed.

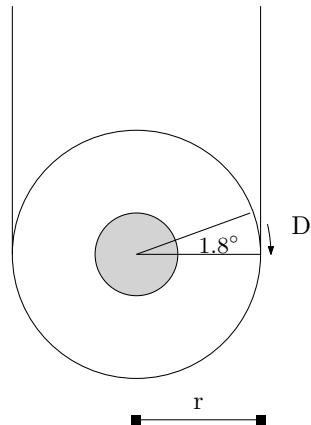


FIGURE 6.3: Pulley diagram

$$D = 2 * \pi * r * STEP\_DEG / 360$$

So pulse on the stepper drivers STEP line will make the stepper driver increment rotation by 0.225 degrees. This rotation is translated into linear motion via the belt drive. So for every step, the carriage vertically travels 45.1519 um. Direction is controlled by either a high or low on the DIR.

So a motion frame provided from the computer is described with a distance (how many steps) and three ratios of how often a specific motor should step (equivalent to the speed). For example "1337 1 0.5 0.2" translates to "Cycle 1337 times, every cycle step X, every second cycle step Y and every fifth cycle Z".

Lets say we had a vector circle. We need to break it up into straight lines so that we can use the method explained previously. Ideally we would break it up into many small lines, but for this example we will split it up into 8 paths. To help visualise the problem, we are going to assume that we are dealing with a gantry system.

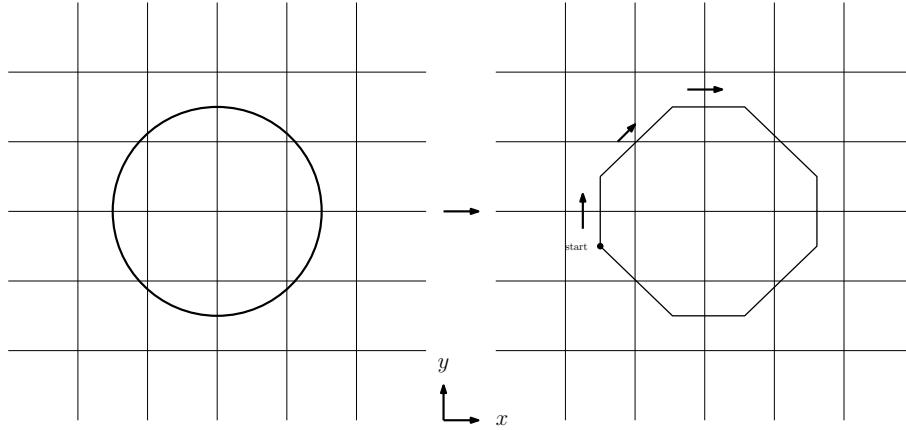


FIGURE 6.4: 'Physical Pixels'

Firstly, the circle is broken into straight paths. From the starting point we need to travel along the y axis 1 step. So this would be described with "1 0 1 0", following that we need to move in the x and y direction one step. That is "1 1 1 0". And so on. The only difference for a delta machine is that we are not directly plotting a image, we are controlling the actuator heights as a function of the image.

But what if we need a angle other then 0,45 or 90? That is why the speed is a fractional value. If we were to plot "10 1 0.2 0" would result in an angle of 17.84 degrees.

We could divide the clock up by 1000 to support a large decimal place with accuracy. However, if we were to divide the clock by 1000, it would need to be in the order of Ghz to support decent speed. A much more convenient method is to approximate absolute steps with a running total. Firstly, we need to increment a counter associated with an actuator with its ratio every clock cycle. We then check if the counter has incremented its unit value. If so, then we should send a signal to step. This method permits usage of a much smaller clock such as 10Mhz.

Furthermore, if we attach the procedure to a timer, global speed and accretion can be controlled easily by modifying the timer compare value. This is very important when trying to push the maximum speed of the steppers. It is important to smoothly accelerate to high speeds to minimise mis-steps. Conversely, all actuators must maintain a relative speed to each other, otherwise the path will be skewed.

Acceleration can be implemented as a function of the distance to the next direction change. Basically, we need to reduce speed as a turn approaches. Then we can take advantage of long straight runs by accelerating through them. A basic 'look ahead' function has been implemented that runs through the motion queue calculating the next direction change.

# Chapter 7

## Testing and Results

### 7.1 Accuracy

#### 7.1.1 Scale

Scale is a measure of the printed objects size compared to the desired size. It does not necessarily represent a large issue as the machine can be calibrated after a single test.

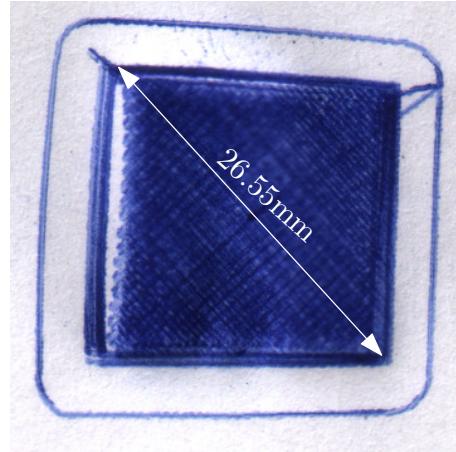


FIGURE 7.1: Scale measured

The desired print should have been  $70.71mm$ . Our design needs to be scaled 2.66 to achieve the same size.

### 7.1.2 Distortion

Distortion describes how 'warped' an object is. This could be in the form of a skew, perspective scale or a translation. The simplest way to inspect distortion is to print a perfect square and measure its sides.

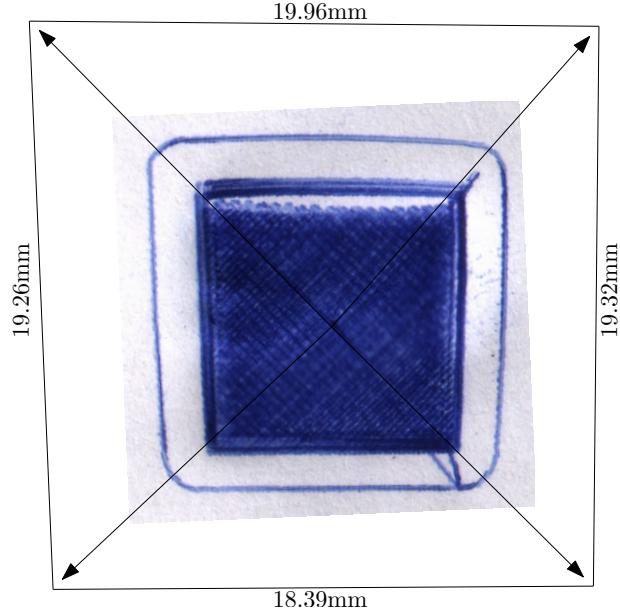


FIGURE 7.2: Distortion

Our results showed a slight warp that pushed outwards along the  $x$  axis. On closer inspection we can see the distortion is aligned with the face of frame that runs from the south-east actuator to the south-west. This error could be associated with a not perfectly trued frame. The frame was then measured:

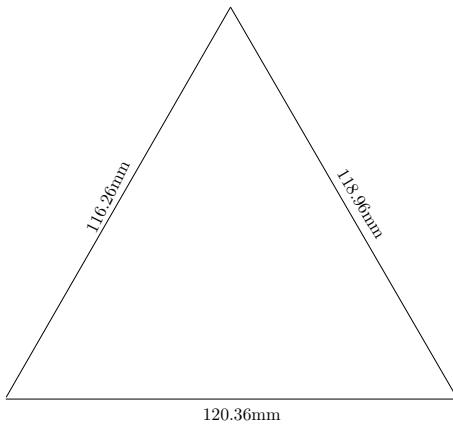


FIGURE 7.3: Frame lengths measured

It is clear that the frames current configuration is forcing the platform outwards as it approaches the north actuator due to the larger length in the south. We can also see a

slight push to the north-west due to the length differences on the east and west frame sides.

Further tests should be conducted once the frame is correctly trued. If the problem still occurs after the frame has been trued, the model can be translated in software to correct for the distortion. A simple calibration procedure would be required on set up.

## 7.2 Speed

A simple vertical speed test shows that the system is capable of relatively slow speeds.

Time taken to travel 10.3cm was 5.4 seconds.

$$\text{speed} = \text{distance}/\text{time}$$

$$\text{speed} = 0.0190740741 \text{m/s}$$

Currently, a combination of a high micro-stepping configuration and low system clock speed is limiting the speed of the stepper motors. By reducing the micro-stepping speed from 1/32 to 1/8, the step wave period can be decreased by four times. That is, the stepper drivers can be signalled four times faster. Increasing the clock speed from 10Mhz to 20Mhz will also double the possible speeds by twice and furthermore increase acceleration resolution by selecting a smaller clock divide for the stepper service routine.

So this is a possible speed increase of eight times. However, we must realise that we have not yet experimented with the physical limitations. This will need to be thoroughly tested. The acceleration and jerk variables will need to be calibrated.

## 7.3 Repeatability

Repeatability is how consistently can the machine produce the same result. This is extremely important as each layer is dependent on the previous layer. If there is a slight error, it is possible that the rest of the print will not align up resulting a mess.

The following figure is the output of 100 iterations printing a  $17\text{mm}^2$  square. It is very noticeable that there is a large amount of drift over the  $x$  axis while the  $y$  axis has minimal variance. It is very important that the distortion is so consistent. It should also be noted that the top actuator (the one at  $(0, D)$ ) has the majority of affect over the  $y$  direction. However, the  $x$  axis is affected by the two lower actuators equally.

This result may be caused by an algorithm error. But it also may be both actuators errors constantly adding up producing a uniform distortion. The ball point pen will also bleed through the paper increasing the thickness of the line.

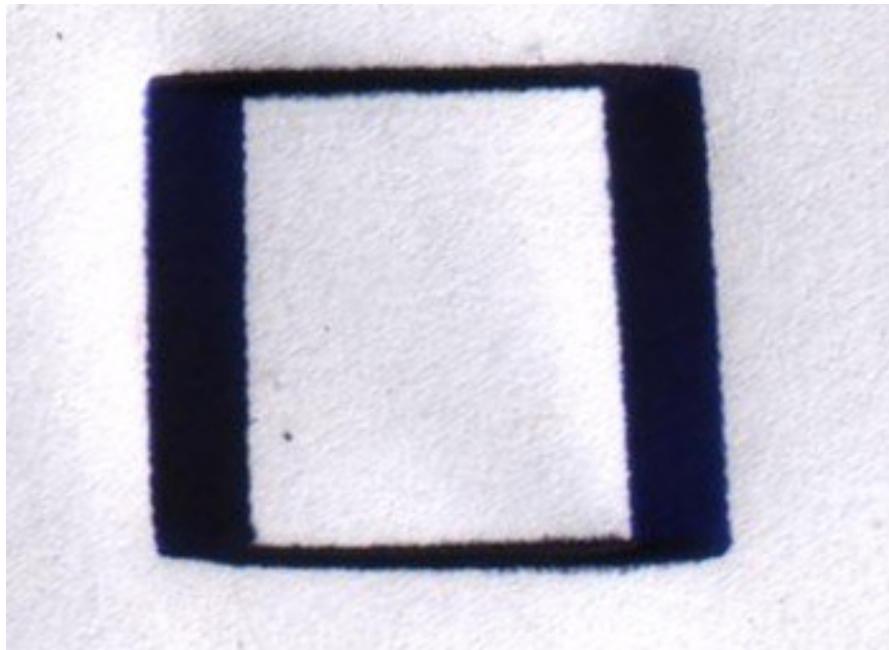


FIGURE 7.4: 100 iterations of a square

These results were measured using a digital caliper. This test is not conclusive as the drift could be also correct itself. This would then appear to have little to no difference as the net sum of error would be zero. However, practically this correction would only occur over simple straight line objects. More rigorous tests need to be conducted in the future. A combination of larger and more complex prints should be examined.

	Variance	Result over 100	Average
$x$		2.64mm	26um
$y$		0.63mm	6um

TABLE 7.1: Drift results

## Chapter 8

# Project Management

### 8.1 Schedule

The original schedule had to be modified in order to accommodate the extra unplanned revisions for both hardware and electronics. From May up until late October, three design iterations of hardware were developed. Each time improving on a major design flaw. Each iteration had a large impact on the schedule, however all were necessary hurdles that contributed to the final product. A second revision of electronics was required after the project goals were re-evaluated and to remove a few bugs.

The additional time added to the timeline pushed some of the key functionality past important dates such as the final presentation. Work has continued after the main delivery dates and a fully functioning 3D printer is estimated to be achieved at the end of January 2014.

An online project log was kept. Posts were made at regular intervals, discussing progress and small milestones. This served as a great resource and helped keep track of ongoing progress. It is available at <http://printer.epidev.com>.

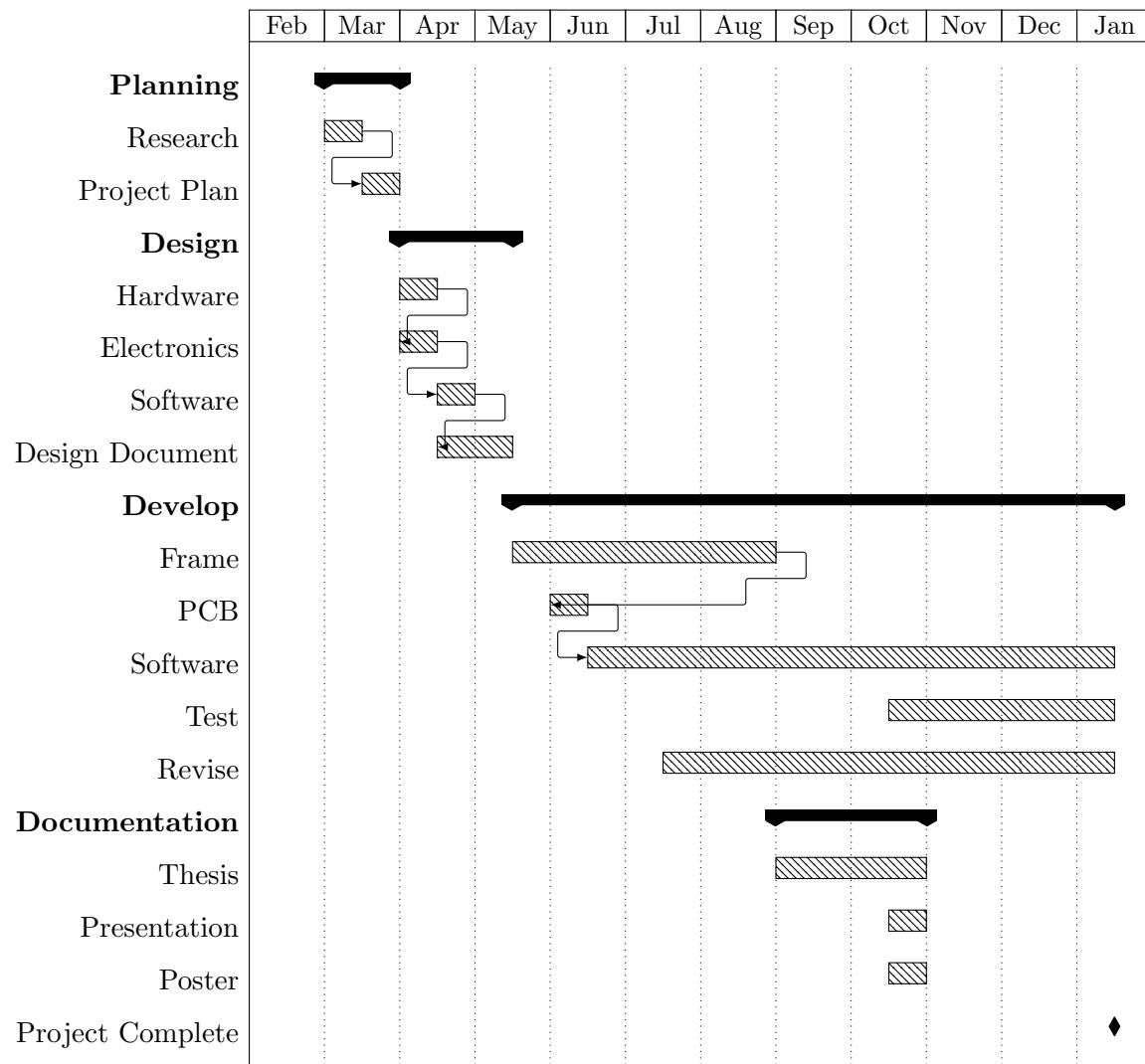


FIGURE 8.1: Gantt Chart

## 8.2 Progress

A two complete frame has been designed and assembled. The first desktop model has a print area of roughly  $10\text{cm}^3$ . The second was a larger version using all the same printed parts but increasing the rod lengths. It is twice as tall and wide, resulting eight times the volume. This design has had small revisions made along the way and seems quite stable. The larger version does require a double cross strut for stability.

A plotter attachment was developed first for testing purposes. This has been used extensively. The extruder feed has also been prototyped although it has not been properly tested.

The second revision of electronics has been assembled and tested. While far better than the first revision, a third would add extra features and improve stability. No hardware mods are required for basic functionality.

The firmware has been developed during the entire development stage. Slowly improving and adding additional features. Currently it supports:

- Queuing of motion instructions
- Acceleration
- Console interface over UART
- LCD interface
- Homing and auto height calibration
- Command checksum validation

The complementary computer software is currently stable for 2D plots. It takes g-code generated from slic3r and converts it to motion descriptions for the printer. The communication side is capable of sending the instructions and validating that they were successfully received.

### 8.2.1 Shortcomings

For a complete working 3D printer the following tasks need to be completed:

- Develop extruder calculations for software
- Implement extruder feeder control

- Implement temperature PID loop
- Extend auto calibration
- Increase system clock to 20Mhz

## 8.3 Budget

There are many consumer 3D printers on the market currently. They range from \$450 to over \$20,000. One of the primary goals of this project is to produce inexpensive electronics to help reduce the overall cost of 3D printing. \$450 is very competitive if the quality is reasonable. The final target cost for this project is a base model for \$350 AUD. I have considered many aspects that will help minimise costs:

- low end 8bit AVR ATmega value line microcontrollers
- Single board solution
- Optional components: Flash memory, LCD and Ethernet.
- Minimal hardware
- Printed gears for belt drive
- Balance of cost vs quality for stepper motors
- Use common hardware store smooth and threaded rods

### 8.3.1 Revenue

La Trobe University kindly provides a \$200 spending budget for final year projects. I will personally fund the remaining fees.

### 8.3.2 Expenses

Most parts were able to be recycled through each design iteration.

Item	Cost
6 meters of smooth rod	\$20
6 meters of threaded rod	\$6
PCB Fabrication	\$40
Electronic components	\$70
4 Stepper motors	\$60
1kg ABS Plastic	\$30
Assembled Extruder	\$50
Power supply	\$30
Heated Bed	\$50
4 metes of Belts	\$16
6 608zz Bearings	\$6
6 LM8UU Bearings	\$8
Assorted hardware	\$50
Total	\$436

TABLE 8.1: Budget allocation

### 8.3.3 Non-budgeted resources

Item	Provided By
Atmel AVR Dragon JTAG programmer	Robert Ross
Host computer and development software	Keith Brown
Soldering equipment	Department of Electronics Engineering
CRO and testing equipment	Department of Electronics Engineering
Breadboard, Pliers, cutters, Multimeter and other general electronic items	Keith Brown

TABLE 8.2: Non-budgeted resources

## 8.4 Risk Analysis

Risk mitigation is one of the most important aspects of managing a project. Possible predicted risks should be actively avoided. However not all are foreseen or are avoidable, in such case we should attempt to minimise the impact.

### 8.4.1 List of risks

Risk (event)	Likelihood (H/M/L)	Impact (H/M/L)	Ac- tion
Development starts late	M	L	2
Schematics Incorrect	M	L	1
PCB Incorrect	M	L	1
Unobtainable parts	H	L	3
Components break	H	M	3
Underestimate Project time frame	M	H	2
Underestimate Complexity	H	H	4
Implementation does not function	M	M	1
Incomplete project threat	L	H	4
Code is lost / corrupted	L	L	5
Hardware issues	L	M	1

TABLE 8.3: List of possible risks

#### 8.4.2 List of actions

Ac- tion	Comment
1	Diagnose and debug, attempt to develop work around depending on project stage. Redesign if problem is critical.
2	Adjust Gantt chart, design new tactics and re-prioritise if required.
3	Obtain new components. If unavailable or time frame does not permit, attempt to use alternative.
4	Discontinue development on selected components. Adopt complete and tested consumer alternatives.
5	Pull latest commit from off site Git repository server. Backups should be made nightly.

TABLE 8.4: List of actions

#### 8.4.3 Mitigated Risks

During the project a few events were mitigated with their associated actions. The following paragraphs discuss what occurred and how it was handled.

**Schematics Incorrect** The first revision had many issues. All were able to be averted during the prototyping stage by making modifications to the PCB. All current issues were amended on the revision 2 board.

**Components break** 4 Stepper drivers were damaged due to a poor PCB design. The new revision fixed these issues.

**Underestimate Project time frame** Deadlines were met by shifting priorities around. An extension was later required for the project report.

**Incomplete Project threat** Continued project development after final university deliverables have been met.

**Hardware issues** Design kept improving and complete reworks were undertaken.

**Code is corrupted** The current fork of code was in a non functioning state for the final presentation. Using Git as version control, I was able to checkout a previous working state ready for the presentation.



# Chapter 9

## Conclusion

The macro and micro effects of an introduction to a personal manufacturing device is fascinating. It has the possibility to facilitate innovation in many areas. Whether it is a domestic or commercial application, 3D printing can help produce specialised parts, reduce prototyping time and cost, promote first hand recycling and entice the next generation into a technical field.

Low cost additive manufacturing is still in early development. A young underdeveloped device or idea presents an opportunity for improvement. This technology will continue to advance as demand increases. The delta style of 3D printers already is faster and more accurate than the traditional Cartesian machines.

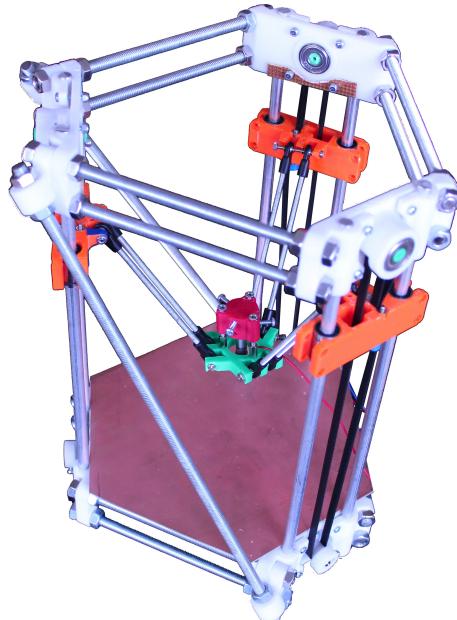


FIGURE 9.1: Final Deltabot Revision



## **Appendix A**

# **Reference Documents**

### **A.1 Existing Documentation**

- Keith Brown. Delta printer Project Plan: April 2013
- La Trobe University. ELE4EPA/EPB Subject learning guide: March 2013

### **A.2 Vendor Documentation**

- TI. MSP430x2xx Family Guide. <http://www.ti.com/lit/ug/slau144i/slau144i.pdf>: January 2012
- Atmel. ATmega644 Series Guide. <http://www.atmel.com/Images/doc2593.pdf>: January 2012

### **A.3 Other Documentation**

- Reprap Foundation website/forum <http://reprap.org/>: March 2013
- Brian W. Kernighan and Dennis M. Ritchie. The C Programming Language, Second Edition. Prentice Hall, Inc., 1988.



## Appendix B

### Abbreviations

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<b>ABS</b>	Acrylonitrile butadiene styrene (plastic)
<b>AVR</b>	Atmel's Alf (Egil Bogen) and Vegard (Wollan)'s RISC processor
<b>CAD</b>	Computer-aided design
<b>CPU</b>	Central Processing Unit
<b>CRC</b>	Cyclic Redundancy Check
<b>FPU</b>	Floating Point Unit
<b>MSP</b>	Mixed Signal Processor
<b>LCD</b>	Liquid Crystal Display
<b>PLA</b>	Polylactic acid (plasic)
<b>SPI</b>	Serial Peripheral Interface
<b>SVG</b>	Scalable Vector Graphics
<b>UART</b>	Universal Asynchronous Reciever/Transmitter
<b>USB</b>	Universal Serial Bus

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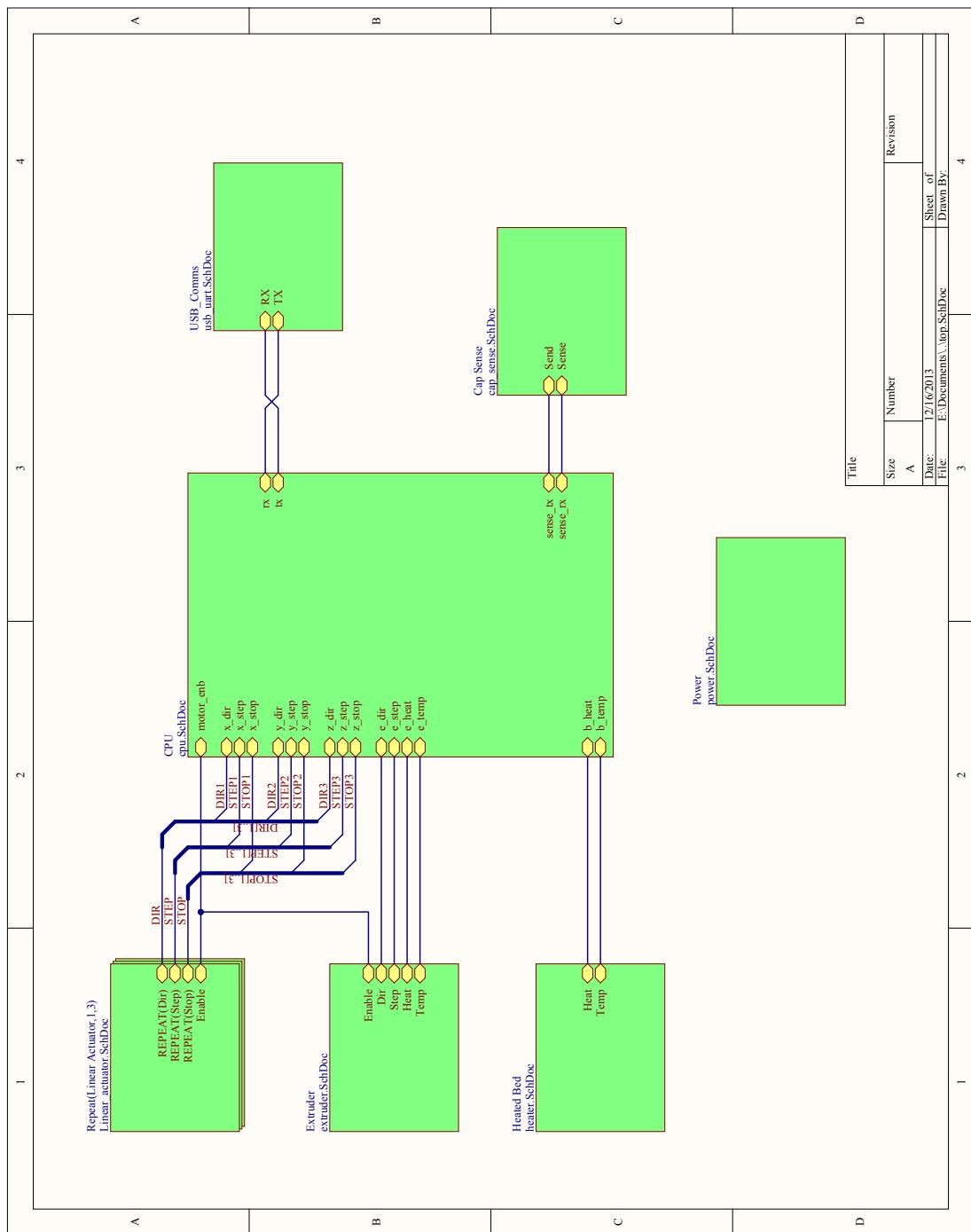
TABLE B.1: List of abbreviations



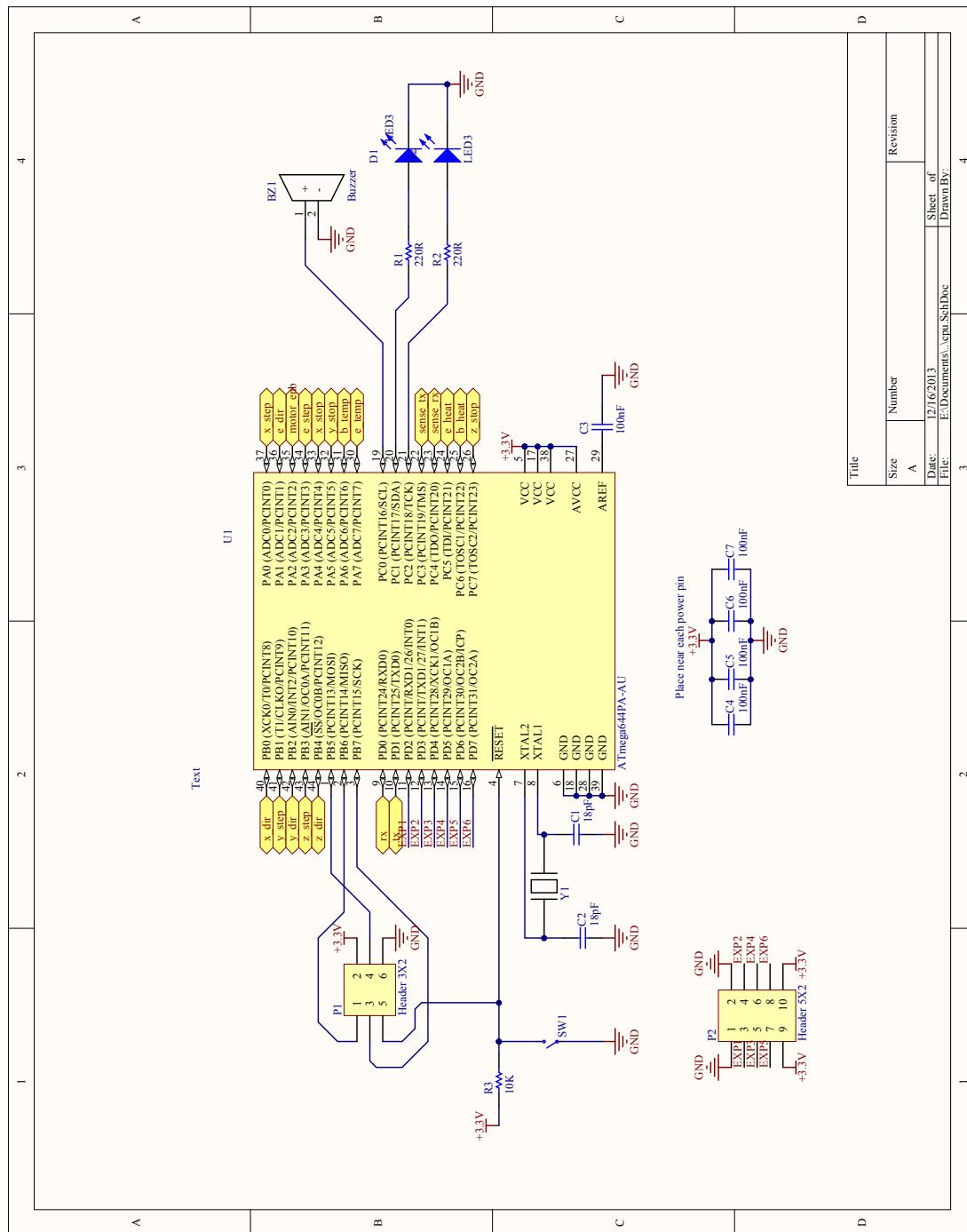
## **Appendix C**

### **Schematics**

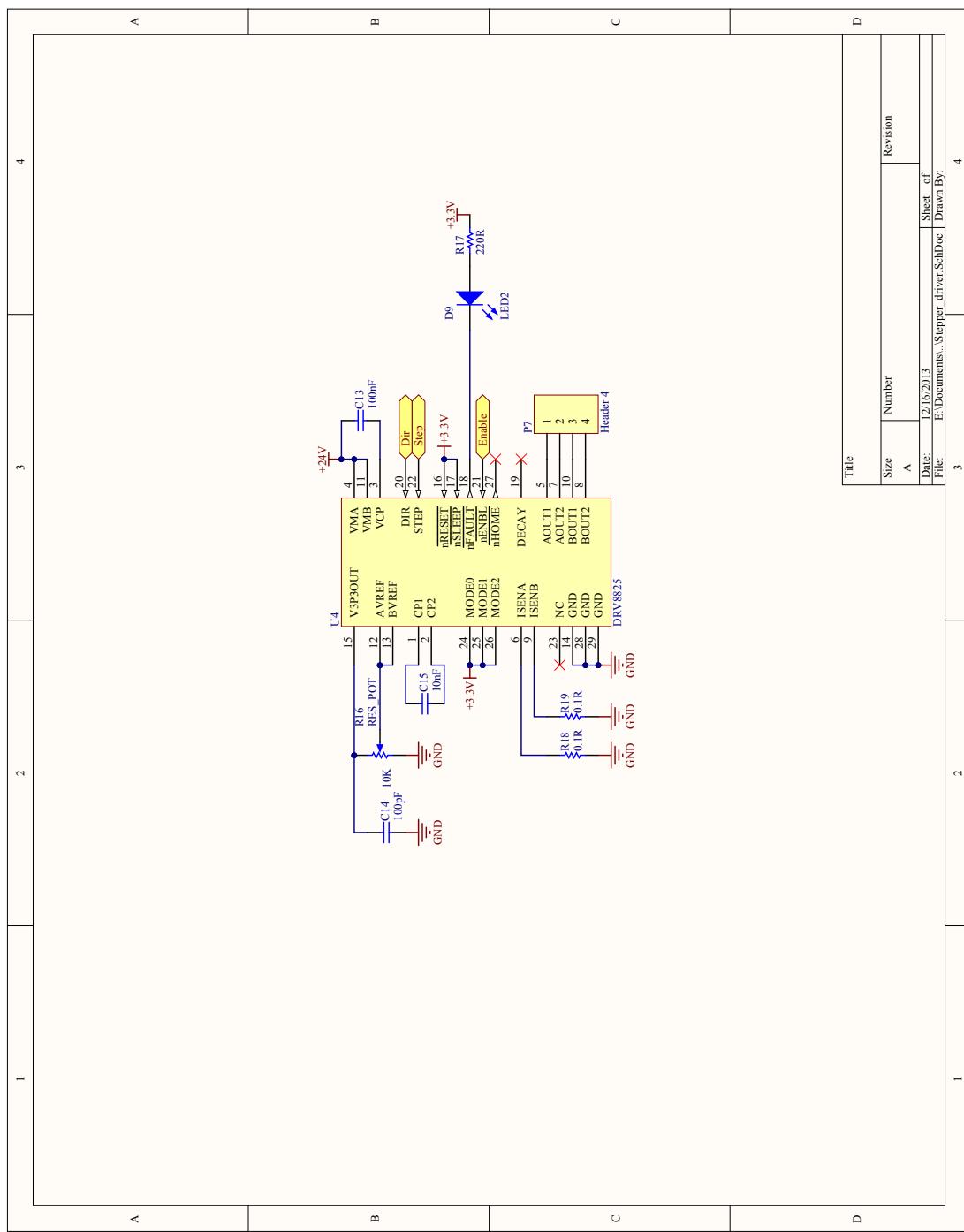
#### **C.1 Top Level**



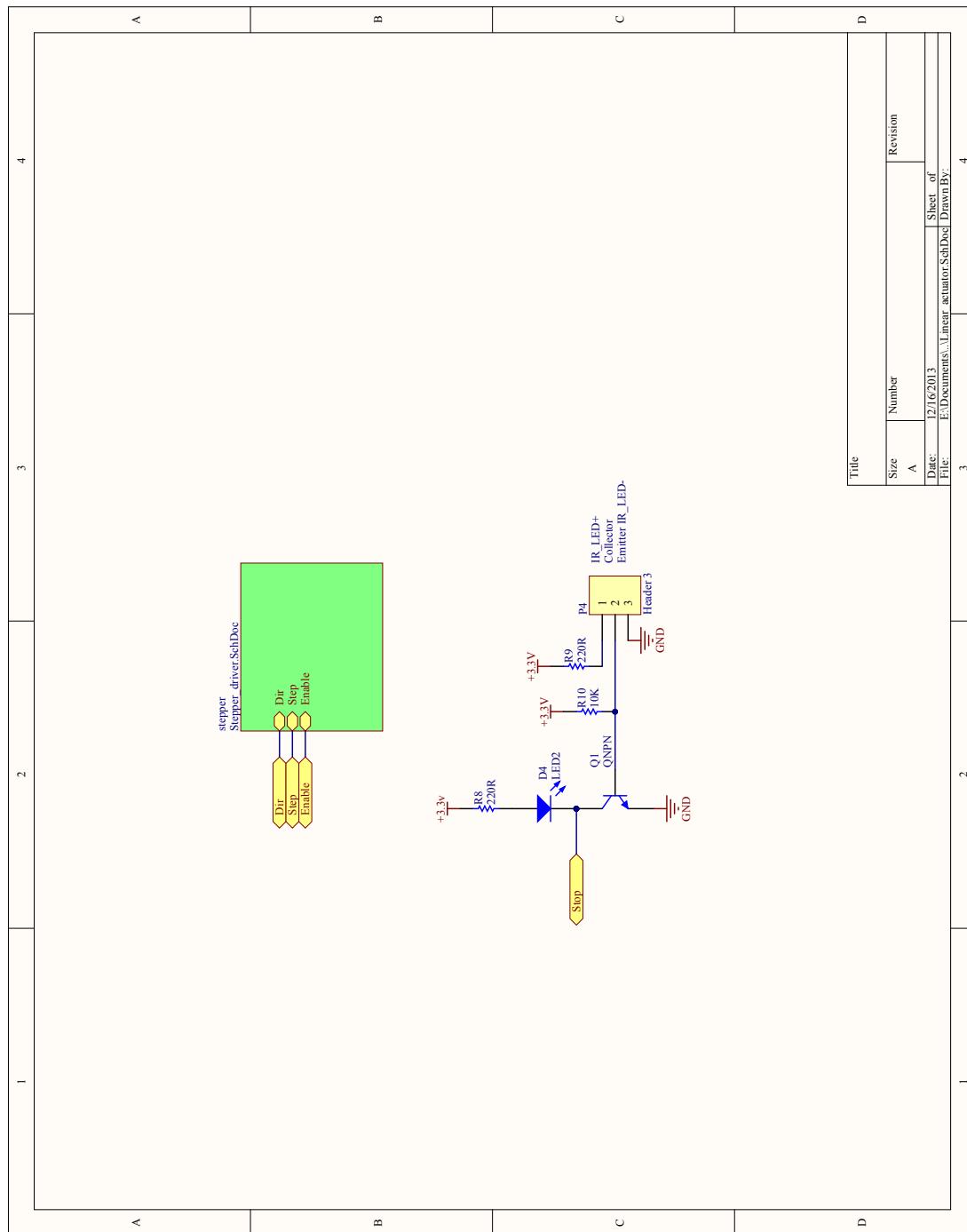
## C.2 CPU



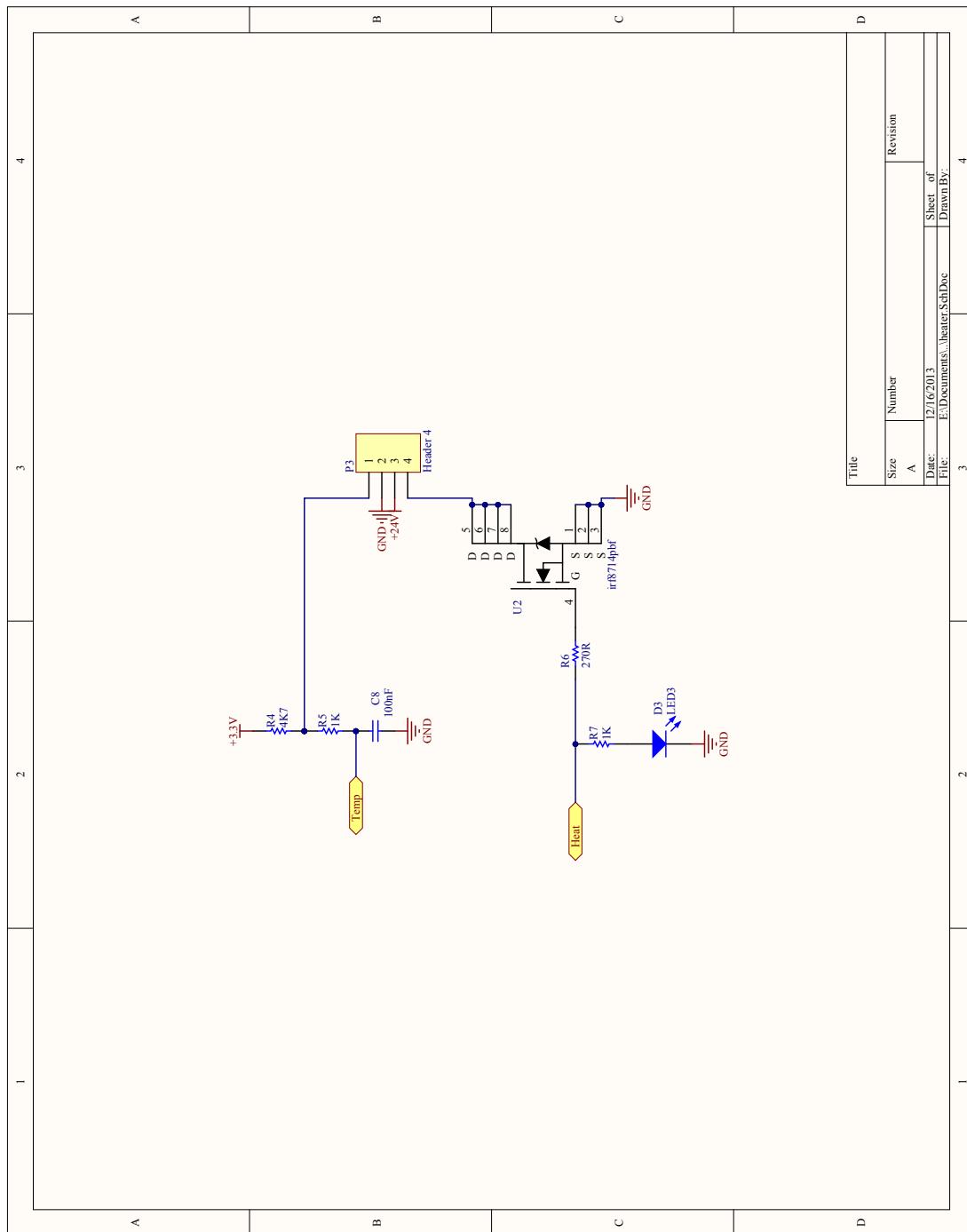
### C.3 Stepper Driver



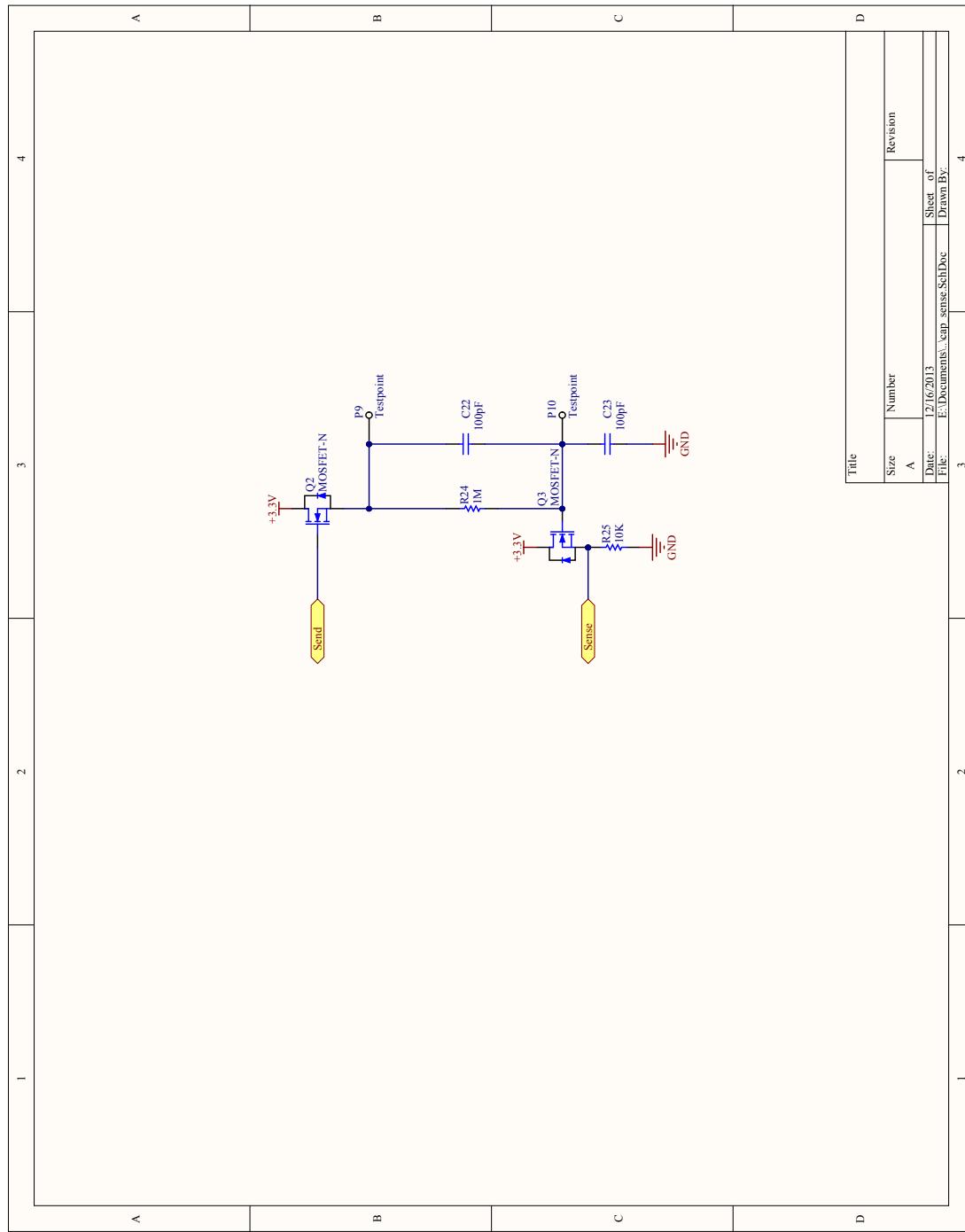
## C.4 Linear Actuator



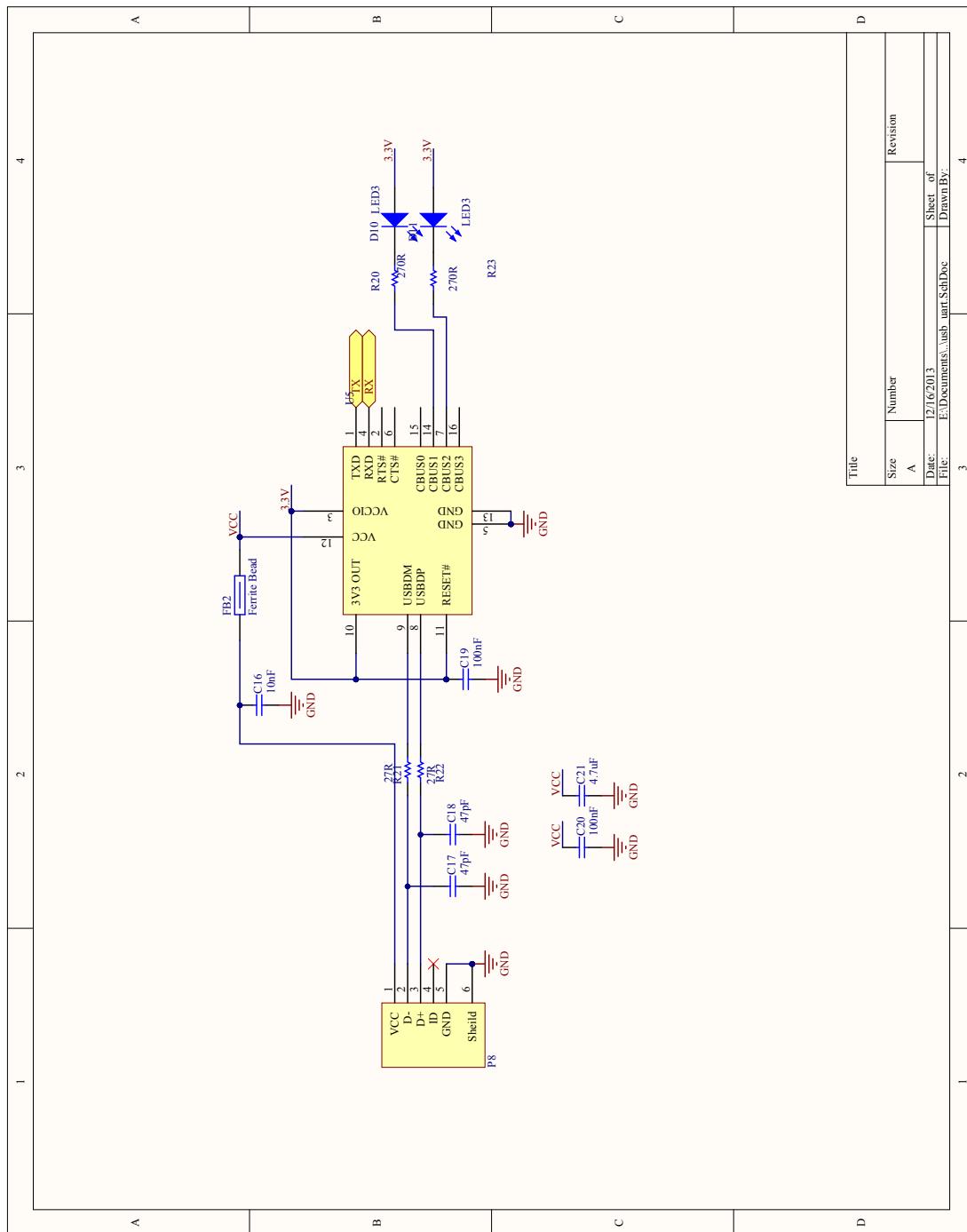
## C.5 Heater



## C.6 Capacitance Sense



## C.7 USB UART

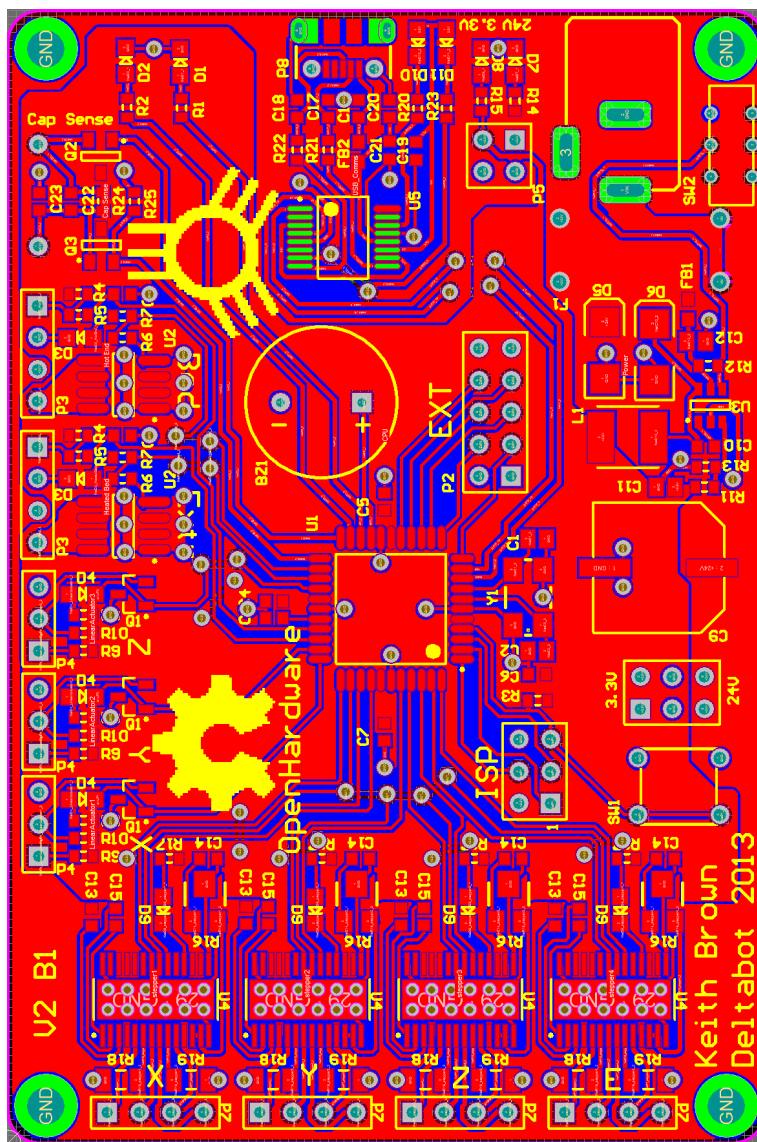




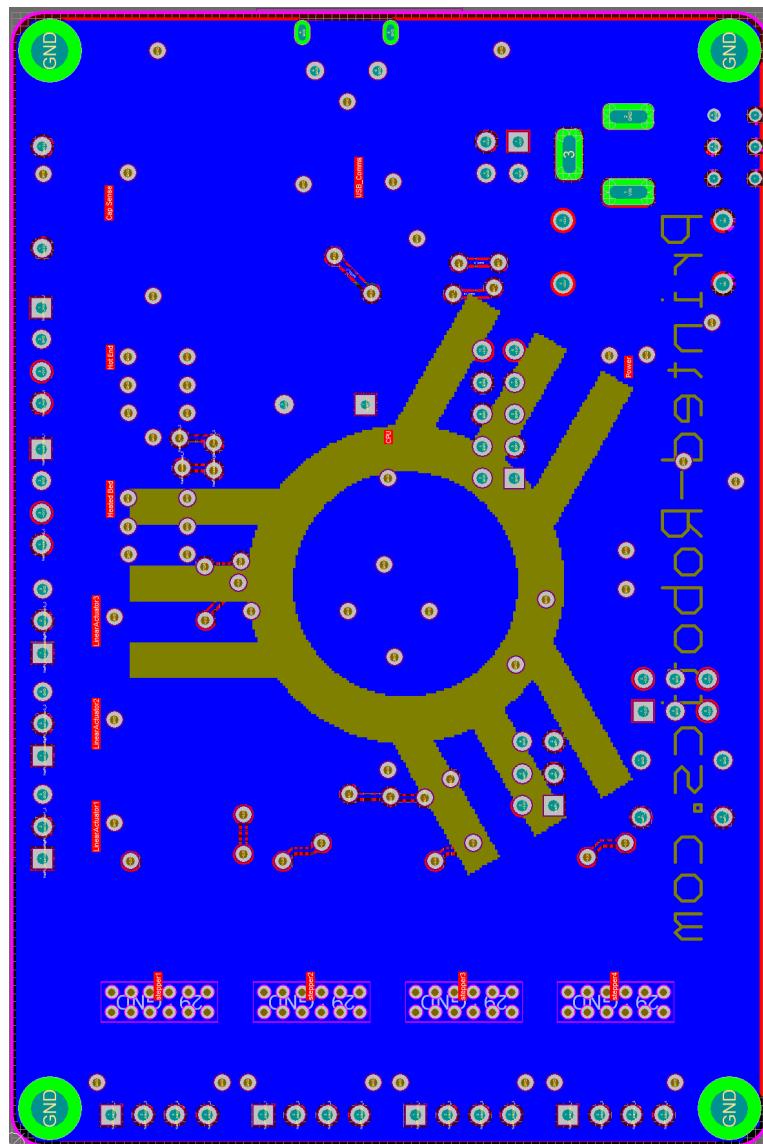
## Appendix D

# PCB Layout

## D.1 Top Level



## D.2 Bottom Side





## **Appendix E**

## **Source Code**

Please refer to the accompanying CD or the online github project at:

<https://github.com/keith-epidev/deltabot>.



## **Appendix F**

# **Hardware Designs**

Please refer to the accompanying CD or the online github project at:

<https://github.com/keith-epidev/deltabot>.



# Bibliography

- [5] Paul Brody, IBM, and Econolyst. Research preview: 3d printing goes exponential, March 2013. URL [https://www-304.ibm.com/connections/blogs/electronics/entry/research\\_preview\\_3d\\_printing\\_goes\\_exponential2?lang=en\\_us](https://www-304.ibm.com/connections/blogs/electronics/entry/research_preview_3d_printing_goes_exponential2?lang=en_us).
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- [2] S. Scott Crump. Apparatus and method for creating three-dimensional objects, October 1989. URL <http://www.google.com/patents?vid=5121329>.
- [3] Anthony Atala. Printing a human kidney, March 2011. URL [http://www.ted.com/talks/anthony\\_atala\\_printing\\_a\\_human\\_kidney.html](http://www.ted.com/talks/anthony_atala_printing_a_human_kidney.html).
- [4] Erin Lee Carr. 3d printed guns (documentary), March 2013. URL <http://www.youtube.com/watch?v=DconsfGsXyA>.
- [6] Johann C. Rocholl. Rostock - delta robot, 2012. URL <http://reprap.org/wiki/Rostock>.