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**IPVS**



**SimTech**  
Cluster of Excellence

## Parallelizing a Multiscale Model Of a Skeletal Muscle

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Simulation of Large Systems  
Institute for Parallel and Distributed Systems  
University of Stuttgart



# Overview

## ① Motivation

## ② Physiological Introduction

## ③ The Mathematical Model

## ④ The Computational Framework OpenCMISS

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## The musculoskeletal system

- Fitness for different tasks: endurance, fine control, strength



- Enabled by same muscle tissue
- Complex system: skeletal muscles, bones, tendons, motor neurons

## Understanding the system

- Experimentally difficult

- Need for simulation

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  - Hard measurements of inner quantities  $\sim$  EMG
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Source: <http://www.ncbi.nlm.nih.gov/pmc/articles/PMC2735073/>  
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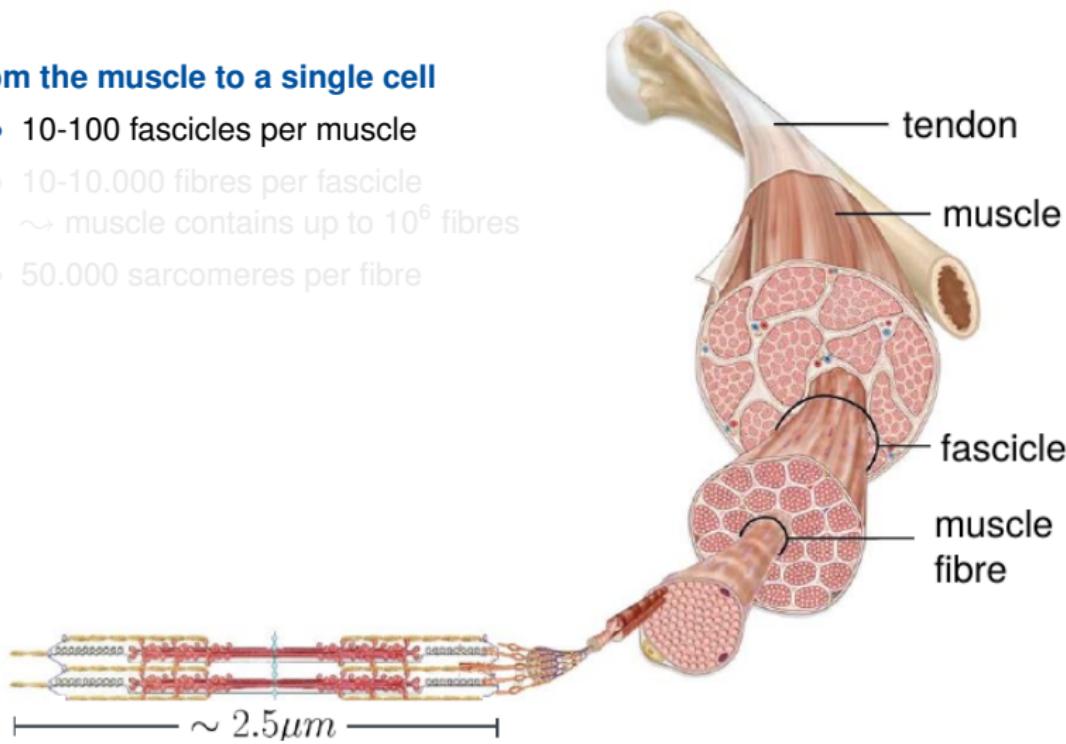
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# Physiological Introduction

## From the muscle to a single cell

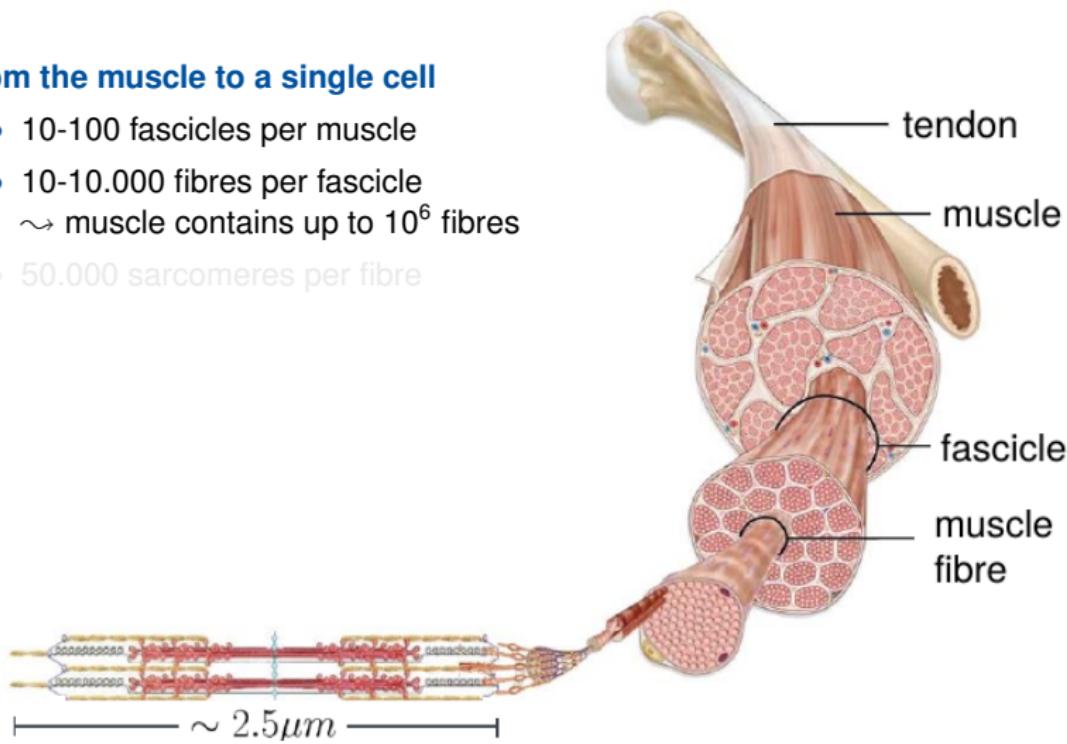
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- 50.000 sarcomeres per fibre



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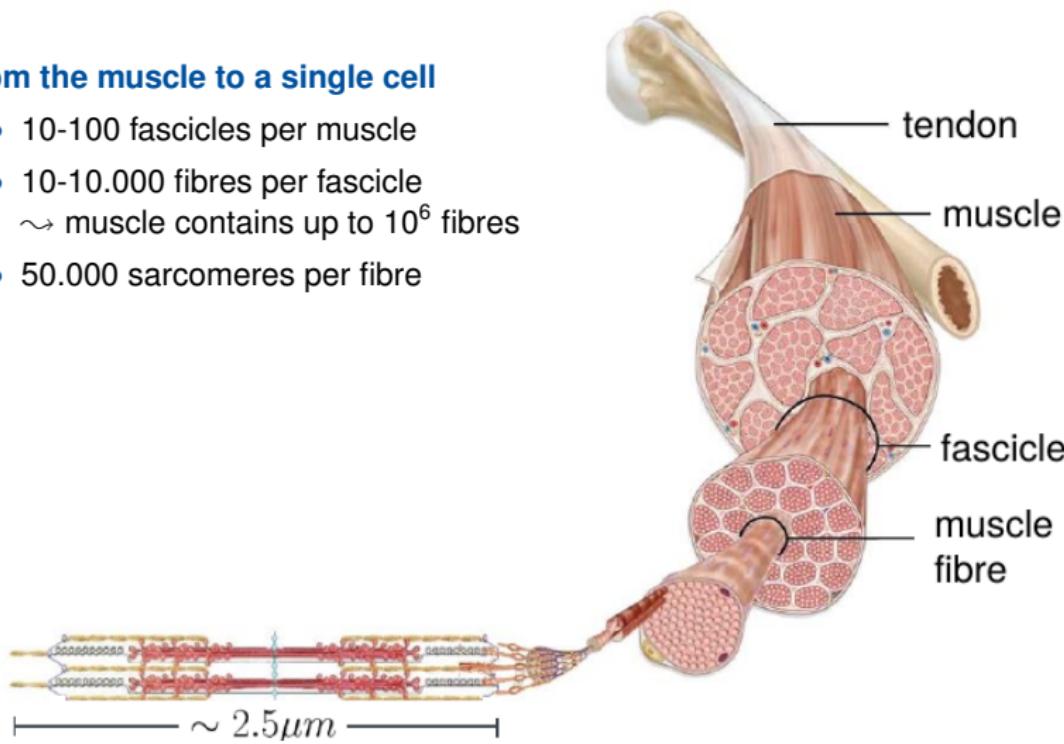
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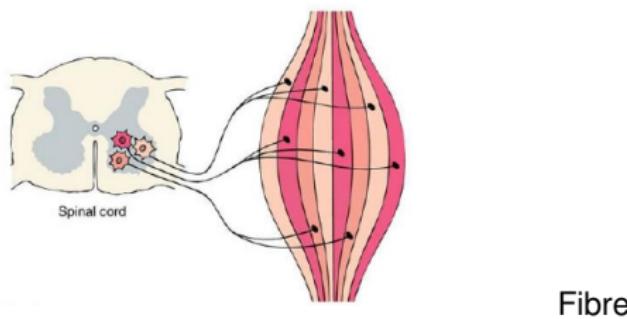
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## Activation of muscle fibres

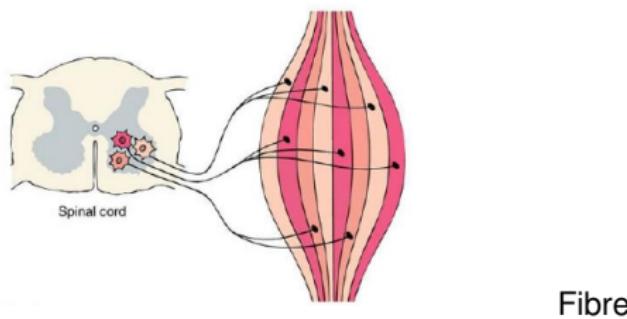
- Origin of stimulation is motor neuron pool in spinal cord
- Transport of electrical signals via nerves
- Activation level proportional to frequency of "spike trains"
- Fibres are addressed as motor units (MU), all fibres of a MU are excited simultaneously
- Exponential MU distribution
- Action potential travels along muscle fibre
- Neighbouring fibres are not electrophysiologically coupled



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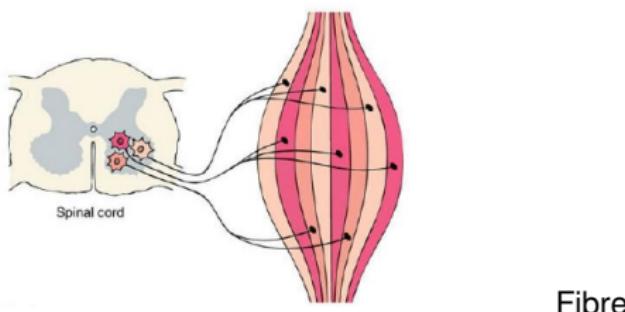
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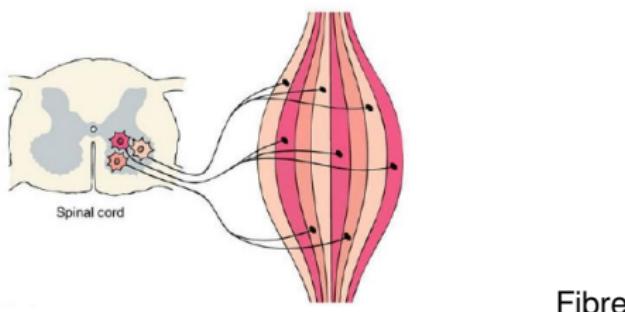
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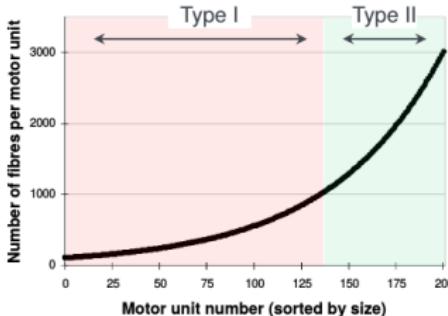
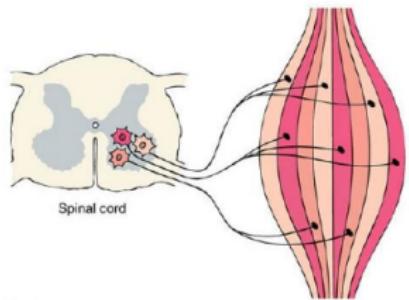
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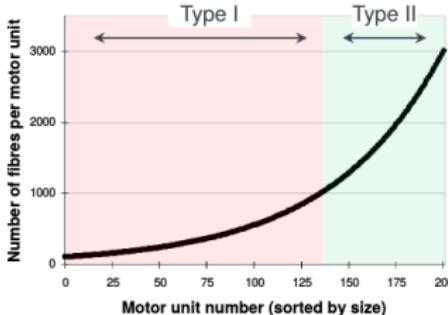
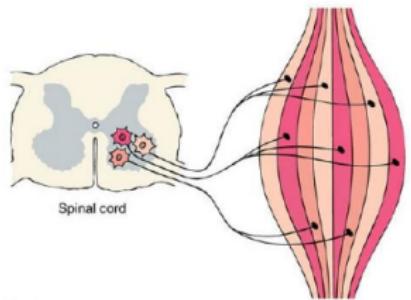
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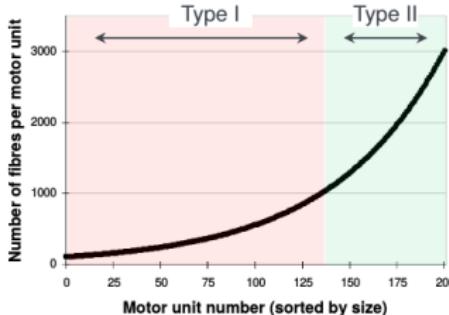
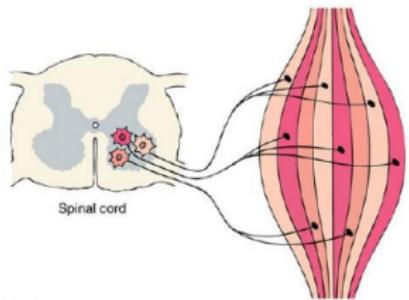
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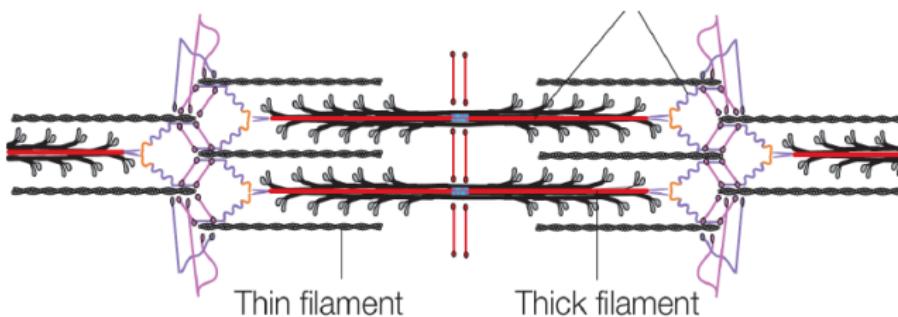


Fibre

# Physiological Introduction

## Force generation

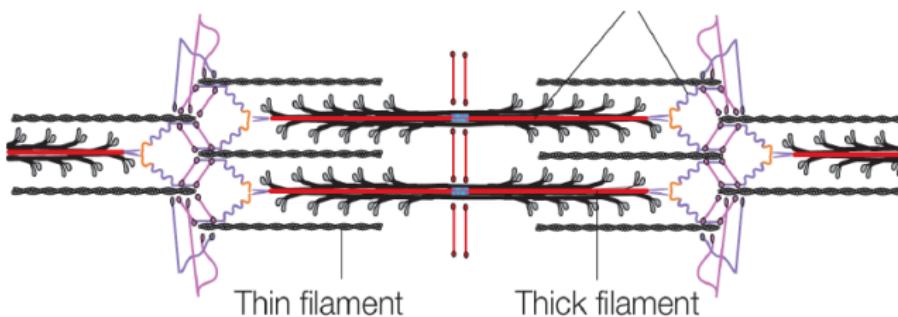
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- Crossbridges attach and detach to thin filament
- Passive behaviour: hyperelastic



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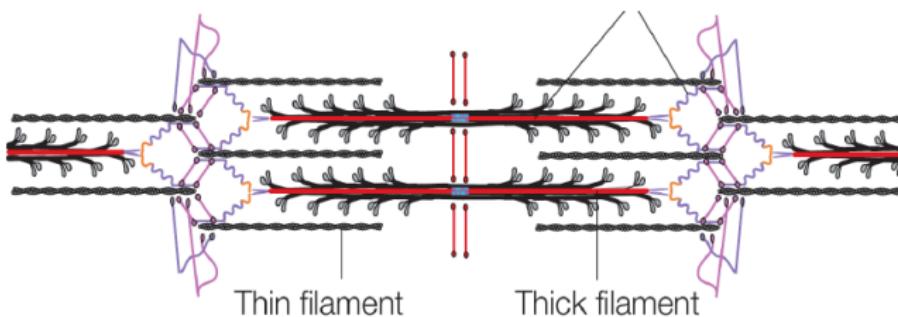
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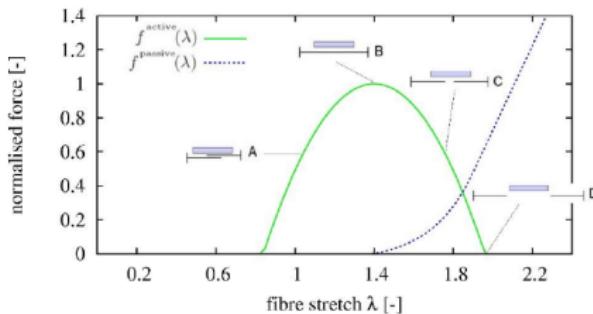
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# Physiological Introduction

## Force generation characteristics

- Force-length relationship

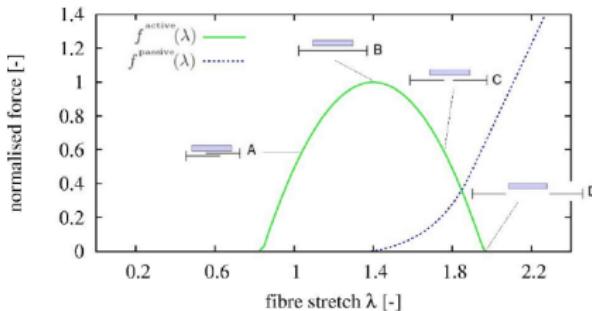


- Force-velocity relationship

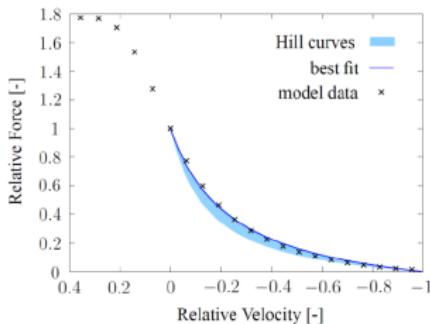
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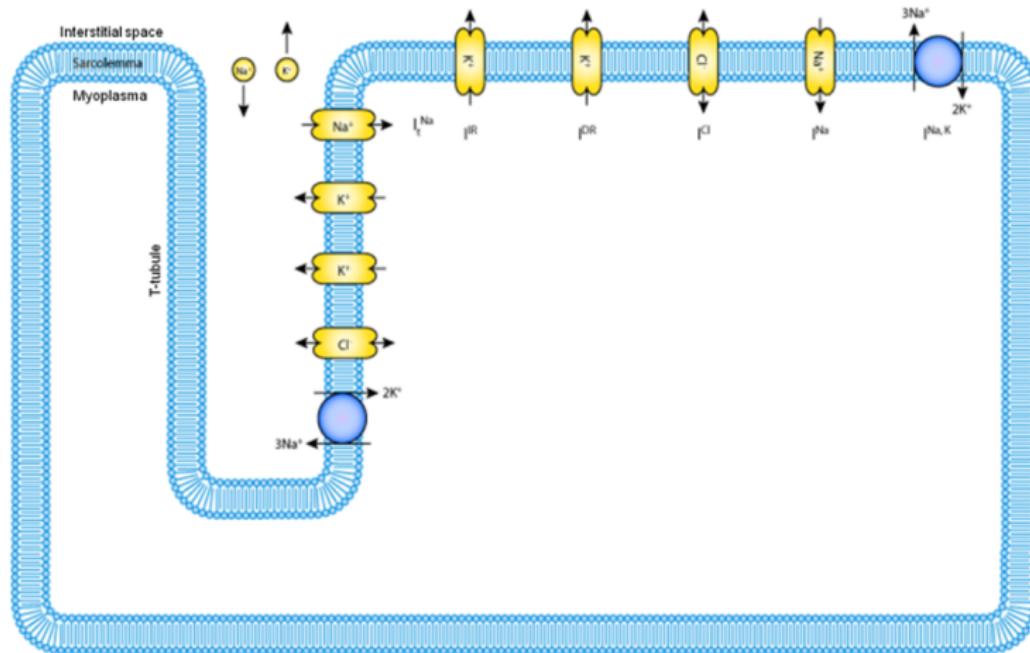
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# Model on cellular level

## Ion currents

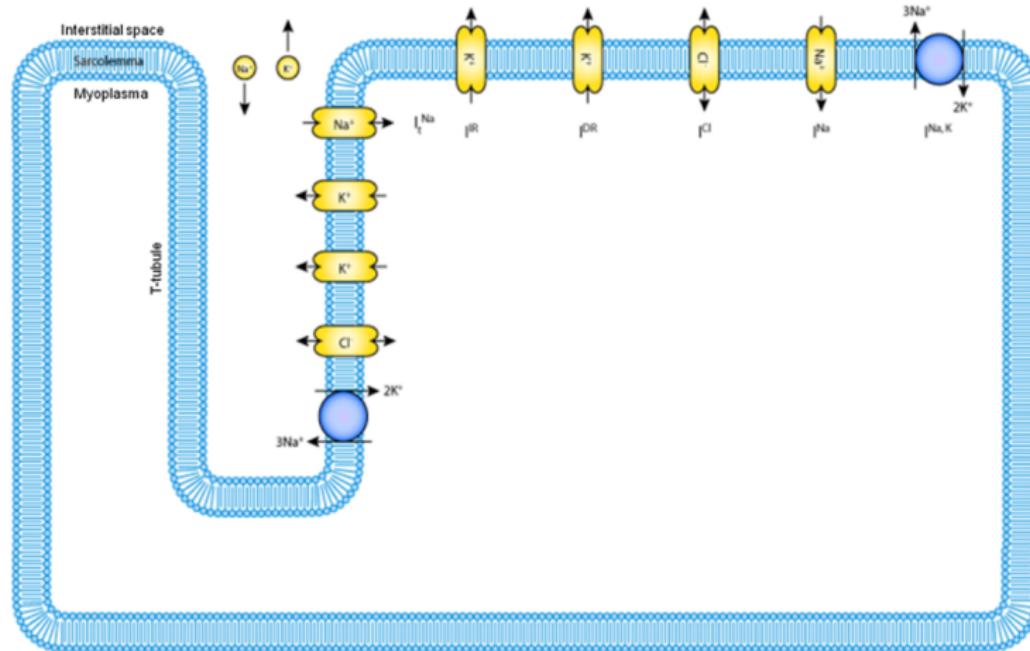
- Ionic currents between intracellular and extracellular space
- Different ions pass through dedicated channels and carry charge



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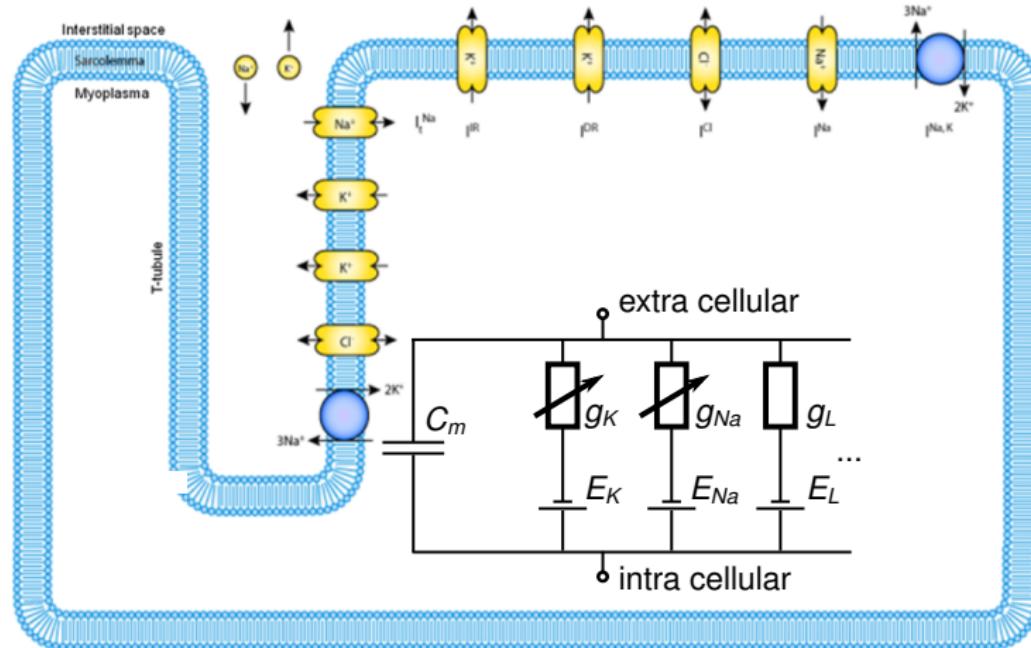
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$$\begin{aligned} \frac{dV_m}{dt} &= -\frac{1}{C_m} \cdot (I_{ionic}(V_m) - I_{stim}/A) \\ I_{ionic} &= I_{Cl} + I_{IR} + I_{DR} + I_{Na} + I_{NaK} \\ I_{Cl} &= g_{Cl}(V_m) \cdot J_{Cl}(Cl_i, Cl_o, V_m), \end{aligned} \quad (1)$$

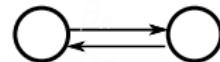
where  $g_i(V_m)$  ... conductance of ion channel  $i \in \{Cl, Na, \dots\}$

## Conductances

Conductance of individual channels

$$g_{Cl} = g_{Cl}^0 \cdot \exp\left(\frac{-E_{Cl} - E_{Cl}^0}{RT}\right)$$

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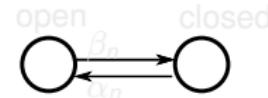
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## Conductances

- Channels open on molecular level

$$g_{Na} = \bar{g}_{Na} m^3 h$$

$$\frac{dm}{dt} = \alpha_m(1-m) + \beta_m m, \quad \frac{dh}{dt} = \alpha_h(1-h) + \beta_h h \quad (2)$$



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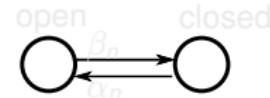
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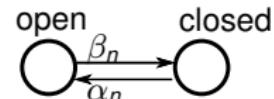
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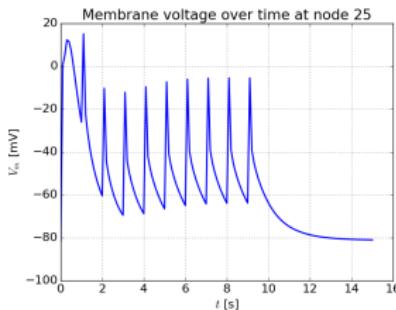
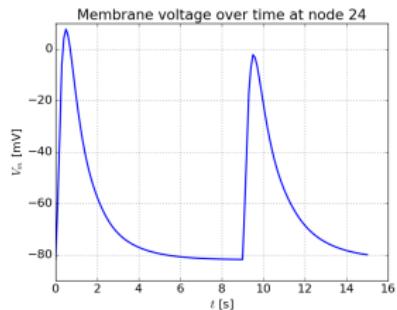


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# Model on cellular level

## Behaviour of electrodynamics model

- Fatigue is included in the model



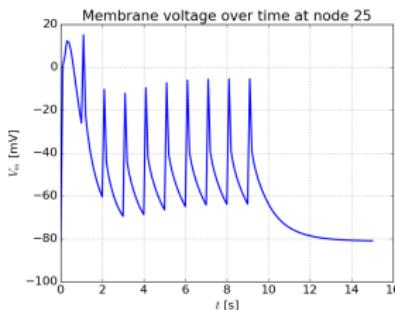
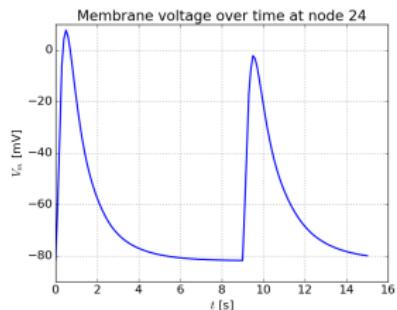
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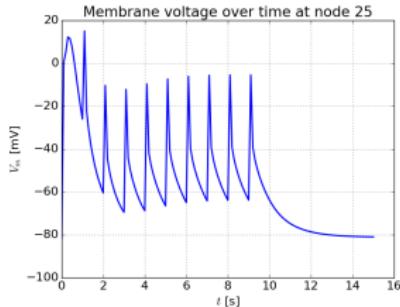
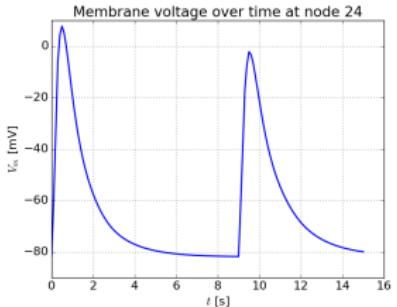
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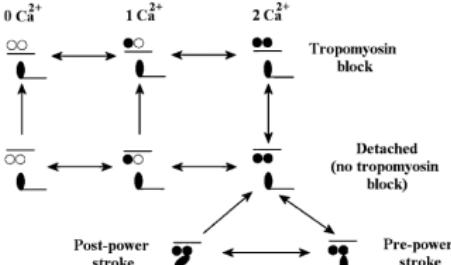
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## Force generation

- State model with transition parameters



# Model on cellular level

## Model overview

- System of ordinary differential equations with 56 variables
- Input:  $I_{stim}$ , Output:  $F$

Two compartment model

$$I_T = (v_t - v_c)/R_t 10^9 \mu A/cm^2 (\text{access current})$$

$$\frac{dv_t}{dt} = -[(I_{stim} + I_T)/C_m] mV/ms (\text{sarcoplasm membrane voltage})$$

$$\frac{dI_t}{dt} = -[I_{stim} - I_T]/C_m mV/ms (\text{i - tube membrane voltage})$$

$$\frac{dI_h}{dt} = \frac{dI_n}{dt} = \frac{dI_K}{dt} = \frac{dS}{dt} = Z_t(v_t, h_t, m_t, n_t, h_t^K, S_t, K_t, Na_t, Na_t)$$

$$I_{stim} = I^K + I^Na + I^K_{inh} + I^{Na}_{inh} + I^{Na,K} mV/cm^2 (\text{sarcoplasm current})$$

$$\frac{dI_K}{dt} = I^K + I^Na + I^K_{inh} + I^{Na}_{inh} + I^{Na,K} mV/cm^2 (\text{i - tube current})$$

$$\frac{dK_t}{dt} = -(I^K + I^Na + I^K_{inh} + I^{Na}_{inh})/(1000C_t) mM/ms (\text{intracellular } [K^+])$$

$$\frac{dNa_t}{dt} = (I^K + I^Na + I^K_{inh} + I^{Na}_{inh})/(1000C_t) - (K_t - K_{Na})/r_Na mM/ms (\text{i - tube } [K^+])$$

$$\frac{dK_t}{dt} = (I^K + I^Na + I^K_{inh} + I^{Na}_{inh})/(1000C_t) + (K_t - K_{Na})/r_Na mM/ms (\text{interstitial } [K^+])$$

$$\frac{dNa_t}{dt} = -I_2 (I^K + I^Na + I^K_{inh} + I^{Na}_{inh})/(1000C_t) - (I^K + I^Na + I^K_{inh} + I^{Na}_{inh})/(1000C_t) mM/ms (\text{intracellular } [Na^+])$$

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where the function  $Z_t$  is defined by

$$\left[ \frac{dI_h}{dt}, \frac{dI_n}{dt}, \frac{dI_K}{dt}, \frac{dS}{dt} \right] = [I^K, I^Na, I^K_{inh}, I^{Na}_{inh}]$$

$$= Z_t(v_t, h_t, m_t, n_t, h_t^K, S_t, K_t, Na_t, Na_t)$$

$$h_t = \beta_h((1 + \exp(-(V - V_{Na})/K_{Na}))^{-1}$$

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$$h_t^{inh} = 1/(1 + \exp(-(V - V_{Na})/K_{Na}))$$

$$S^H = 1/(1 + \exp(-(V - V_{Na})/K_{Na}))$$

$$S^W = 1/(1 + \exp(-(V - 40)/25.75))$$

$$t_{Na} = 1000 \times \exp(-(V - 40)/25.75) \text{ ms}$$

$$t_K = 8571(0.2 + 5.65(V - V_{Na})/1000)^{-1} \text{ ms}$$

$$t_H = 8571(0.75) \mu A/cm^2 (\text{Na current})$$

$$E_g = RT/(F \log(K_e/K_i)) \text{ mV } (K^+ \text{ Nernst potential})$$

$$E_K = Rg/(C^*) \text{ mV } (Na^+ \text{ Nernst potential})$$

$$E_{Na} = RT/(F \log(Na_e/Na_i)) \text{ mV } (Na^+ \text{ Nernst potential})$$

$$C_h = (128 + 5 \times 5.7) \text{ pF } (\text{intracellular } [Cl^-])$$

$$C_{inh} = (128 + 5 \times 5.7) \text{ pF } (\text{extracellular } [Cl^-])$$

$$I_{stim} = V(C_t - C_l \exp(-F(V)/(RT)))/(1 - \exp(-F(V)/(RT)))$$

$$I_T = V(K_t - K_{Na} \exp(-F(V)/(RT)))/(1 - \exp(-F(V)/(RT)))$$

$$J_{Na} = V(Na_t/(50 \text{ Hz})/50) \mu A/cm^2 (\text{K+ IR current})$$

$$I_{Na} = J_{Na}(Na_t/(50 \text{ Hz})/50) \mu A/cm^2 (\text{K+ DR current})$$

$$I_{Na,K} = J_{Na,K}(Na_t/(50 \text{ Hz})/50) \mu A/cm^2 (\text{K+ CR current})$$

$$I_{inh} = J_{inh}(Na_t/(50 \text{ Hz})/50) \mu A/cm^2 (\text{Na+ current})$$

$$I_{inh} = G_{inh} I_{inh}^2 \text{ mV/cm}^2 (\text{Na+ current})$$

$$I_{inh}^2 = I_{inh}^K + I_{inh}^{Na} + I_{inh}^{Na,K} \text{ mV/cm}^2 (\text{Na+ current})$$

$$I_{inh}^K = I_{inh}^K((1 + \exp(-(V - V_{inh})/K_{inh}))^{-1})$$

$$I_{inh}^K = 1/(1 + \exp(-(V - V_{inh})/K_{inh}))$$

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# Propagation of electrical signals

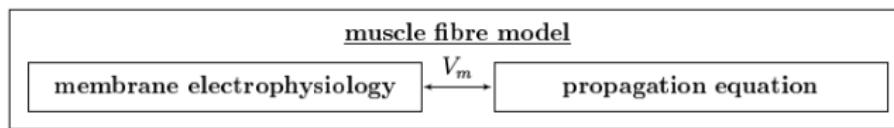
## Overview

- Model the propagation of electric stimuli along the muscle fibres
  - Extend the existing local model
- 
- Current can not only pass through membrane but also flow along the fibre

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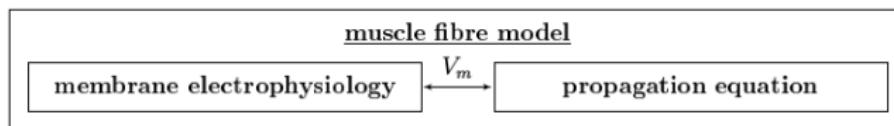


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- Extend the existing local model

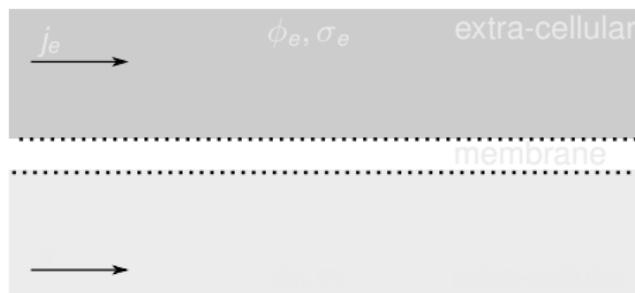


- Current can not only pass through membrane but also flow along the fibre

# Propagation of electrical signals

## Model setting

- 2 domains: intra-, extracellular
- Homogenised: domains occupy the same space
- Electric potentials  $\phi_i, \phi_e$ , conductivities  $\sigma_i, \sigma_e$ , membrane voltage  $V_m = \phi_i - \phi_e$



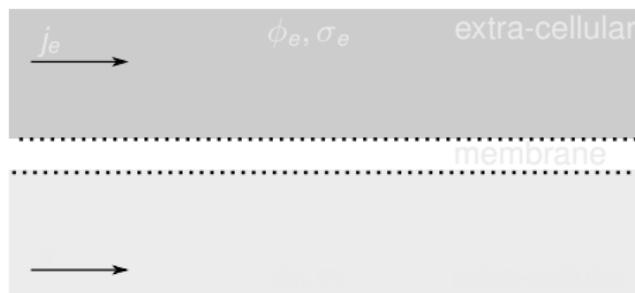
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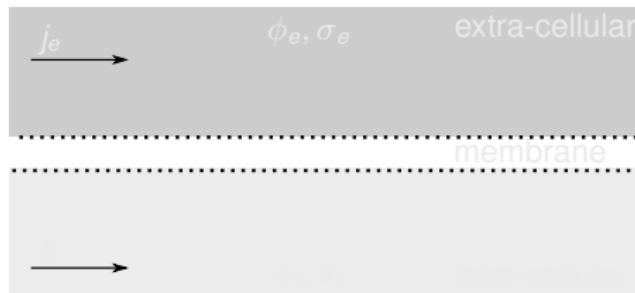
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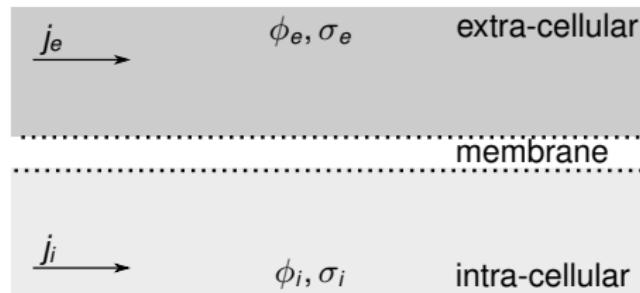
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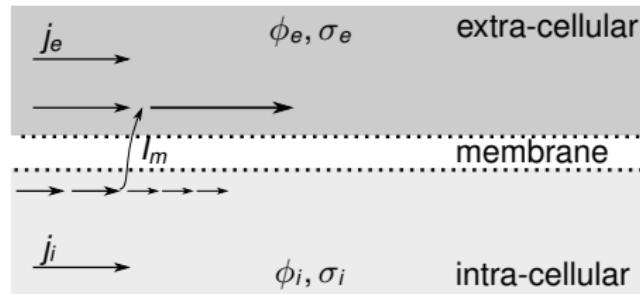


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# Propagation of electrical signals

## Model setting



- Conservation of charges: local changes in current density affect other domain

$$\begin{aligned} \frac{\partial}{\partial x} j_i &= - \frac{\partial}{\partial x} j_e \\ \Leftrightarrow \quad \frac{\partial}{\partial x} \left( \sigma_i \frac{\partial \phi_i}{\partial x} \right) &= - \frac{\partial}{\partial x} \left( \sigma_e \frac{\partial \phi_e}{\partial x} \right) = I_m \\ &= A_m \left( C_m \frac{\partial V_m}{\partial t} + I_{ionic}(V_m) \right) \end{aligned}$$

# Propagation of electrical signals

- Substitute  $V_m = \phi_i - \phi_e$  to eliminate  $\phi$ s:

$$\frac{\partial}{\partial x} \left( \sigma_{eff} \frac{\partial V_m}{\partial x} \right) = A_m \left( C_m \frac{\partial V_m}{\partial t} + I_{ionic}(V_m) \right), \quad \text{with } \sigma_{eff} := \sigma_i || \sigma_e$$

## Numerical treatment

- Equation solved for  $V_m$  using:
  - Explicit Euler scheme
  - Implicit Euler scheme
  - Forward difference approximation
  - Central difference approximation
- Employ finite differencing and splitting operator splitting

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## Numerical treatment

- Equation solved for  $V_m$  using finite difference methods
  - Explicit Euler scheme
  - Implicit Euler scheme
  - Central difference scheme
- Employ finite difference method and explicit operator splitting



# Propagation of electrical signals

- Substitute  $V_m = \phi_i - \phi_e$  to eliminate  $\phi$ s:

$$\frac{\partial}{\partial x} \left( \sigma_{eff} \frac{\partial V_m}{\partial x} \right) = A_m \left( C_m \frac{\partial V_m}{\partial t} + I_{ionic}(V_m) \right), \quad \text{with } \sigma_{eff} := \sigma_i || \sigma_e$$

## Numerical treatment

- Equation solved for  $\frac{\partial V_m}{\partial t}$ :

$$\frac{\partial V_m}{\partial t} = -\frac{1}{C_m} I_{ionic}(V_m) + \frac{1}{A_m C_m} \frac{\partial}{\partial x} \left( \sigma_{eff} \frac{\partial V_m}{\partial x} \right)$$

- Employ finite differences in  $t$  and Godunov operator splitting:

$$\frac{V_m^* - V_m^{(k)}}{\Delta t} = -\frac{1}{C_m} I_{ionic}(V_m^{(k)}),$$

$$\frac{V_m^{(k+1)} - V_m^*}{\Delta t} = \frac{1}{A_m C_m} \frac{\partial}{\partial x} \left( \sigma_{eff} \frac{\partial V_m^{(k+1)}}{\partial x} \right),$$

# Propagation of electrical signals

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$$\frac{\partial}{\partial x} \left( \sigma_{\text{eff}} \frac{\partial V_m}{\partial x} \right) = A_m \left( C_m \frac{\partial V_m}{\partial t} + I_{\text{ionic}}(V_m) \right), \quad \text{with } \sigma_{\text{eff}} := \sigma_i || \sigma_e$$

## Numerical treatment

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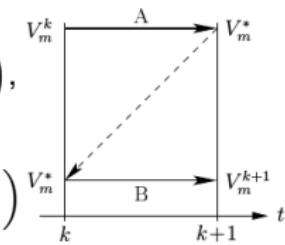
$$\frac{\partial V_m}{\partial t} = -\frac{1}{C_m} I_{\text{ionic}}(V_m) + \frac{1}{A_m C_m} \frac{\partial}{\partial x} \left( \sigma_{\text{eff}} \frac{\partial V_m}{\partial x} \right)$$

- Employ finite differences in  $t$  and Godunov operator splitting:

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$$V_m^{(k+1)} = V_m^* + \Delta t \cdot \frac{1}{A_m C_m} \frac{\partial}{\partial x} \left( \sigma_{\text{eff}} \frac{\partial V_m^{(k+1)}}{\partial x} \right)$$



# Continuum mechanics model

## Basics in continuum mechanics

- Consider muscle in reference configuration,  $\mathbf{X} \in \mathcal{B}_0$  and in deformed state at time  $t$ ,  $\mathbf{x} \in \mathcal{B}_t$
- Mapping is called placement function  $\mathbf{x} = \chi(\mathbf{X}, t)$
- Deformation gradient:  $\mathbf{F} = \frac{\partial \chi(\mathbf{X}, t)}{\partial \mathbf{X}}$ , right Cauchy-Green tensor:  $\mathbf{C} = \mathbf{F}^T \mathbf{F}$
- Strain: Green-Lagrangian strain tensor:  $\mathbf{E} = 1/2(\mathbf{C} - \mathbf{I})$
- Stress: 2nd Piola-Kirchhoff stress tensor:  $\mathbf{S} = (\det \mathbf{F}) \mathbf{F}^{-1} \mathbf{T} \mathbf{F}^{-T}$ ,  $\mathbf{t} = \mathbf{T} \mathbf{n}$
- Constitutive assumptions + balance laws to get relation between stresses ( $\mathbf{S}$ ) and strains ( $\mathbf{E}$ )

# Continuum mechanics model

## Basics in continuum mechanics

- Consider muscle in reference configuration,  $\mathbf{X} \in \mathcal{B}_0$  and in deformed state at time  $t$ ,  $\mathbf{x} \in \mathcal{B}_t$
- Mapping is called placement function  $\mathbf{x} = \chi(\mathbf{X}, t)$
- Deformation gradient:  $\mathbf{F} = \frac{\partial \chi(\mathbf{X}, t)}{\partial \mathbf{X}}$ , right Cauchy-Green tensor:  $\mathbf{C} = \mathbf{F}^T \mathbf{F}$
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# Continuum mechanics model

## Model assumptions of muscle

- Incompressibility, i.e.  $\det(\mathbf{F}) = 1$
- Quasi-static conditions: no inertial terms
- No external body forces: no gravity, no contact e.g. to bones
- Isothermal conditions: no balance of energy
- Stress tensor can be additively composed into active and passive part:

$$\mathbf{S} = \mathbf{S}_{pass} + \mathbf{S}_{act} - p \mathbf{C}^{-1}$$

## Passive stresses

- Modelled as fibre reinforced material with isotropic and anisotropic part

$$\mathbf{S}_{pass} = \mathbf{S}_{iso} + \mathbf{S}_{aniso}$$

- Isotropic part, "ground matrix" modelled by Mooney-Rivlin material:

$$\mathbf{S}_{iso} = 2\alpha_1 I + 2\alpha_2 (\ln(\mathbf{C})) \mathbf{I} - \mathbf{C}$$

- Anisotropic part act in fibre direction as with fibre stretch  $\lambda_f$ :

$$\mathbf{S}_{aniso} = \lambda_f (\mathbf{C}_f - \mathbf{I}) + \frac{1}{\lambda_f} (\mathbf{C}_f - \mathbf{I})^T$$

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- Anisotropic part act in fibre direction as well like elastic fibres

$$\mathbf{S}_{aniso} = \mathbf{S}_{fibre} + \mathbf{S}_{transverse}$$

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$$\mathbf{S}_{\text{pass}} = \mathbf{S}_{\text{iso}} + \mathbf{S}_{\text{aniso}}$$

- Isotropic part, "ground material" modelled by Mooney-Rivlin material:

$$\mathbf{S}_{\text{iso}} = 2 \lambda \mu I + 2 \mu \ln(\det(\mathbf{F})) \mathbf{I} - \mathbf{C}$$

- Anisotropic part adds in fibre direction  $\lambda$  with fibre stretch  $\lambda_f$ :

$$\mathbf{S}_{\text{aniso}} = \lambda_f \mu I + \mu \ln(\lambda_f) \mathbf{I} - \mathbf{C}$$

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## Passive stresses

- Modeling of the material with isotropic and anisotropic part

Isotropic part

- Isotropic part, "round muscle" modeled by Mooney-Rivlin material

$$\sigma_{ij} = 2\alpha_1(1-\alpha_1)\delta_{ij} + 2\alpha_2(1-\alpha_2)\delta_{ij}$$

- Anisotropic part added to the direction of the fiber elasticity

$$\sigma_{ij} = 2\alpha_1(1-\alpha_1)\delta_{ij} + 2\alpha_2(1-\alpha_2)\delta_{ij} + \alpha_3\delta_{ij}\delta_{kl}\delta_{kl}$$

# Continuum mechanics model

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## Passive stresses

- Modeling of the material with isotropic and anisotropic part

Isotropic part

• Neo-Hookean, "around muscle modeled by Mooney-Rivlin material"

$$\sigma_{ij} = 2\mu \epsilon_{ij} + \lambda \epsilon_{kk} \delta_{ij} - \lambda$$

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- Modelled as fibre reinforced material with isotropic and anisotropic part:

$$\mathbf{S}_{pass} = \mathbf{S}_{iso} + \mathbf{S}_{ani}$$

- Isotropic part, "ground matrix" modelled by *Mooney-Rivlin* material:

$$\mathbf{S}_{iso} = 2 c_{10} \mathbf{I} + 2 c_{01} (tr(\mathbf{C}) \mathbf{I} - \mathbf{C})$$

- Anisotropic part acts in fibre direction  $\mathbf{a}_0$  with fibre stretch  $\lambda_f$ :

$$\mathbf{S}_{ani} = b_1 (\lambda_f^{d_1-2} - \lambda_f^{-2}) \mathbf{a}_0 \otimes \mathbf{a}_0$$

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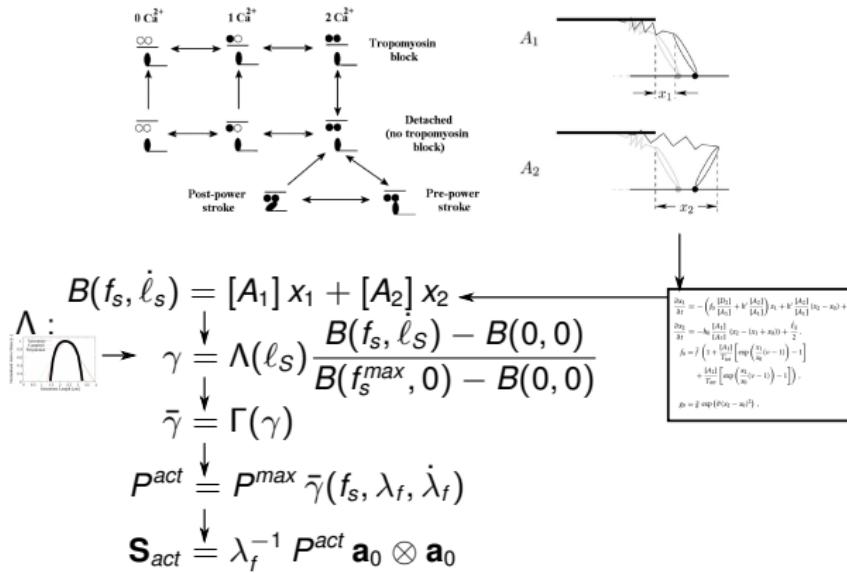
# Continuum mechanics model

## Active stresses

- From crossbridge dynamics to a stress tensor field

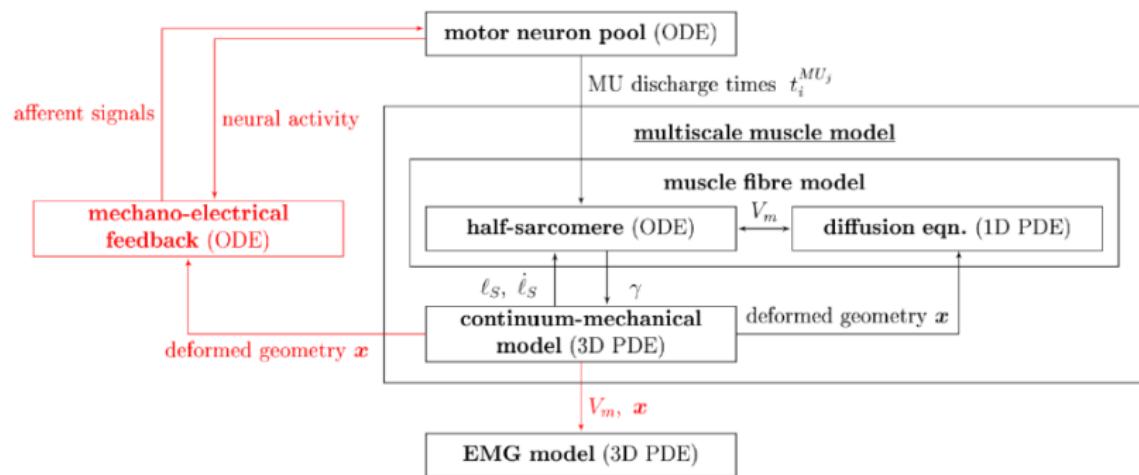
$\ell_s$ : sarcomere length,  $f_s$ : stimulation frequency

$$\lambda_f = \ell_s / \ell_s^0$$



# The Mathematical Model

## The full multiscale model



# Timestepping scheme

## Discretization and solver types

- ODE: finite differences, forward Euler
- 1D PDE: 1D finite elements, Crank-Nicholson ( $\theta = \frac{1}{2}$ )  $\sim$  nonlinear system, solved using newton search, linear system in each step: GMRES (PETSc)
- 3D PDE: 3D finite elements, backtracking line search (PETSc)
- The solvers have different time steps according to characteristic sizes of the scales
- Typical values:  $h^{ODE} = 10^{-4} \text{ ms}$ ,  $h^{DEQ} = 50 \cdot 10^{-4} \text{ ms}$ ,  $h^{CMM} = 10^{-1} \text{ ms}$

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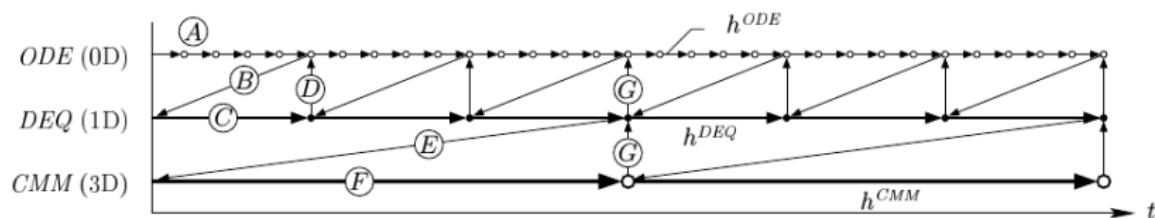
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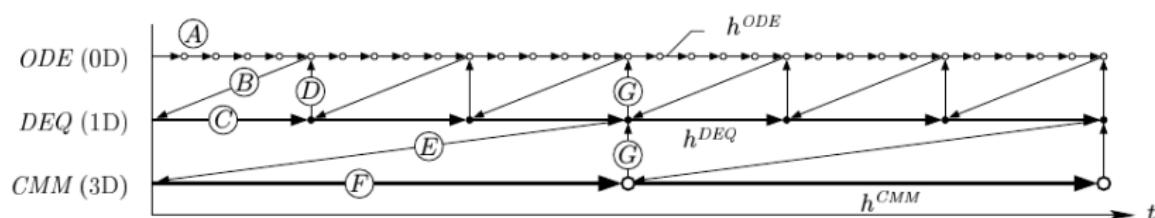


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# The Computational Framework OpenCMISS

## ① Motivation

## ② Physiological Introduction

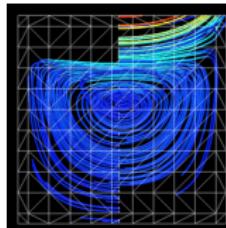
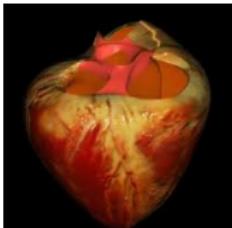
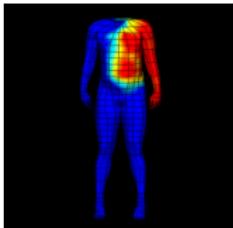
## ③ The Mathematical Model

## ④ The Computational Framework OpenCMISS

# The computational framework OpenCMISS

## History

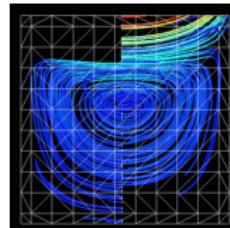
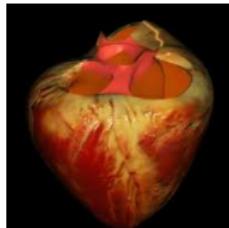
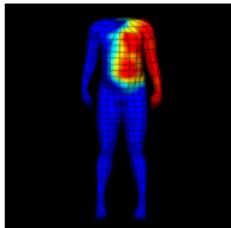
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# The computational framework OpenCMISS

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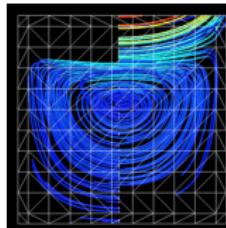
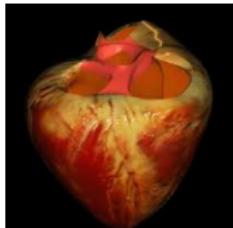
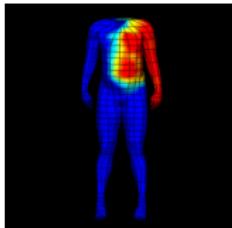
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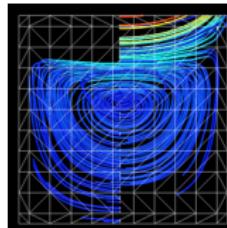
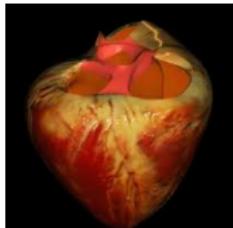
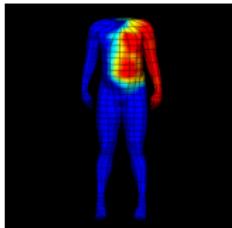
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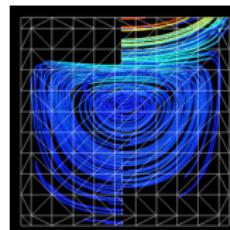
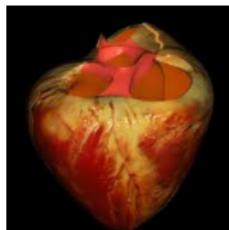
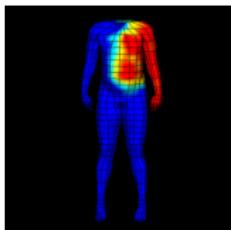
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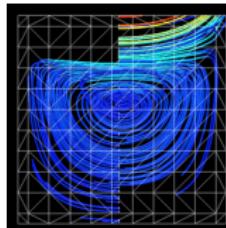
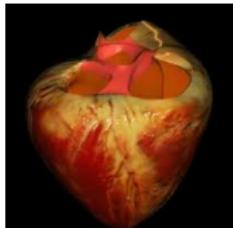
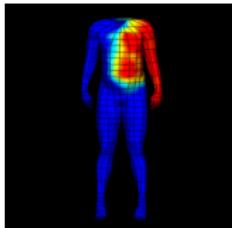
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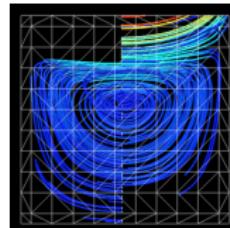
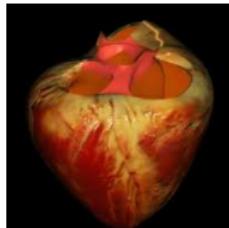
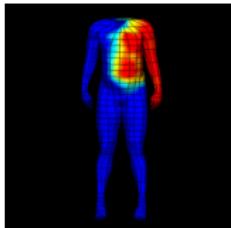
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- Predecessor CMISS: Continuum Mechanics, Image analysis, System identification and Signal processing
- Development began in 1980 in Auckland, NZ
- First application: heart and lungs
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- Number of lines of code today (only core): 300k fortran, 2k C++



# The computational framework OpenCMISS

## History

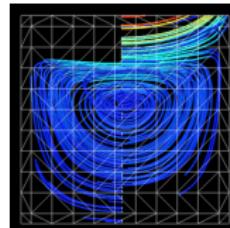
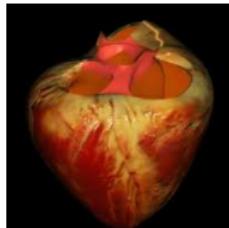
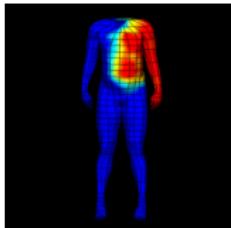
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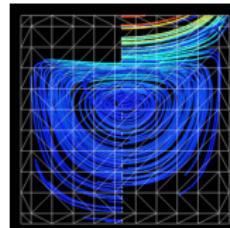
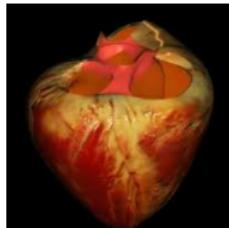
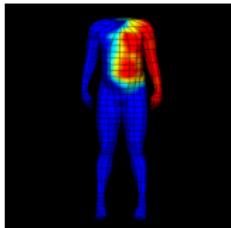
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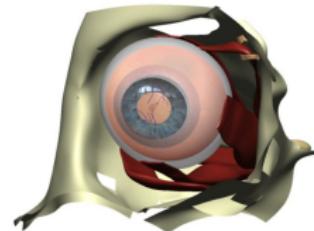
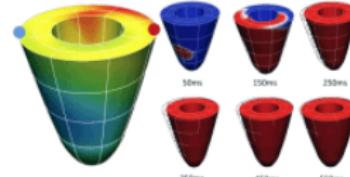
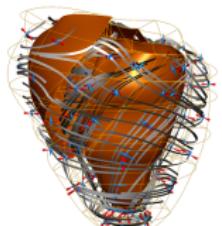
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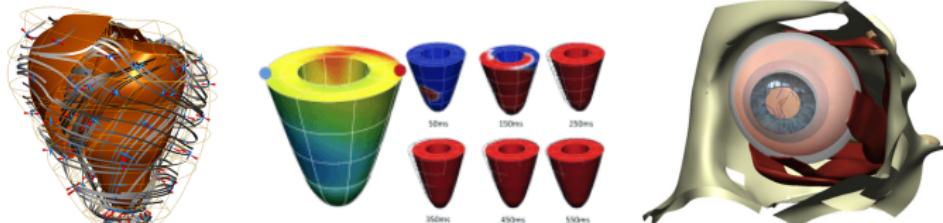
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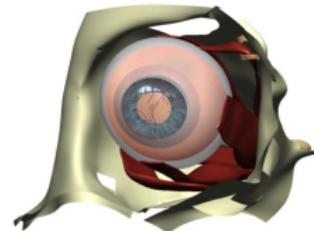
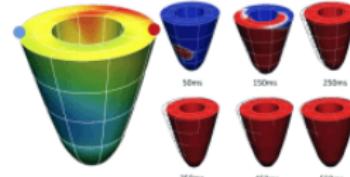
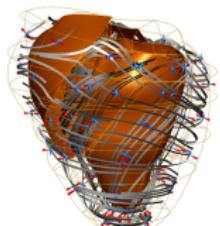
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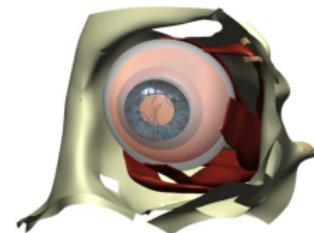
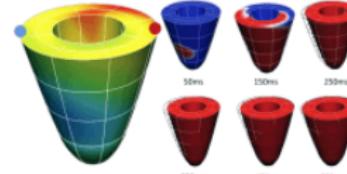
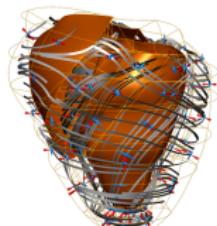
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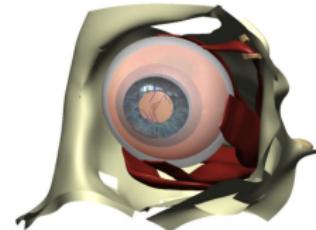
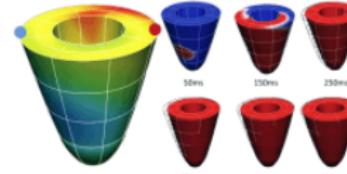
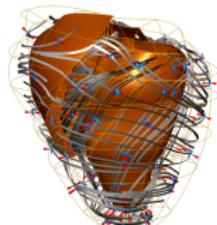
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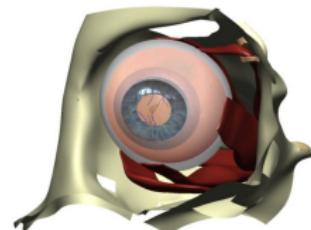
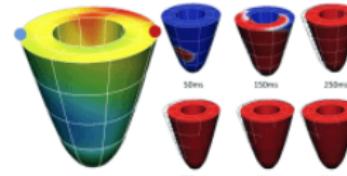
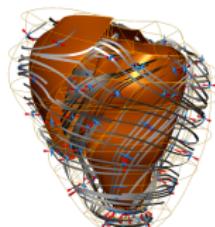
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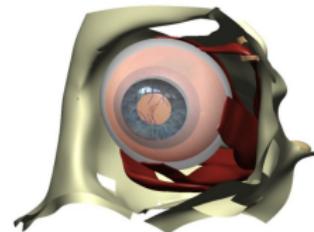
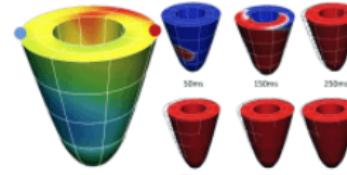
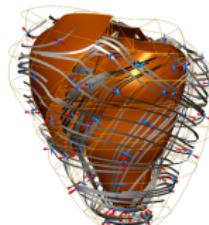
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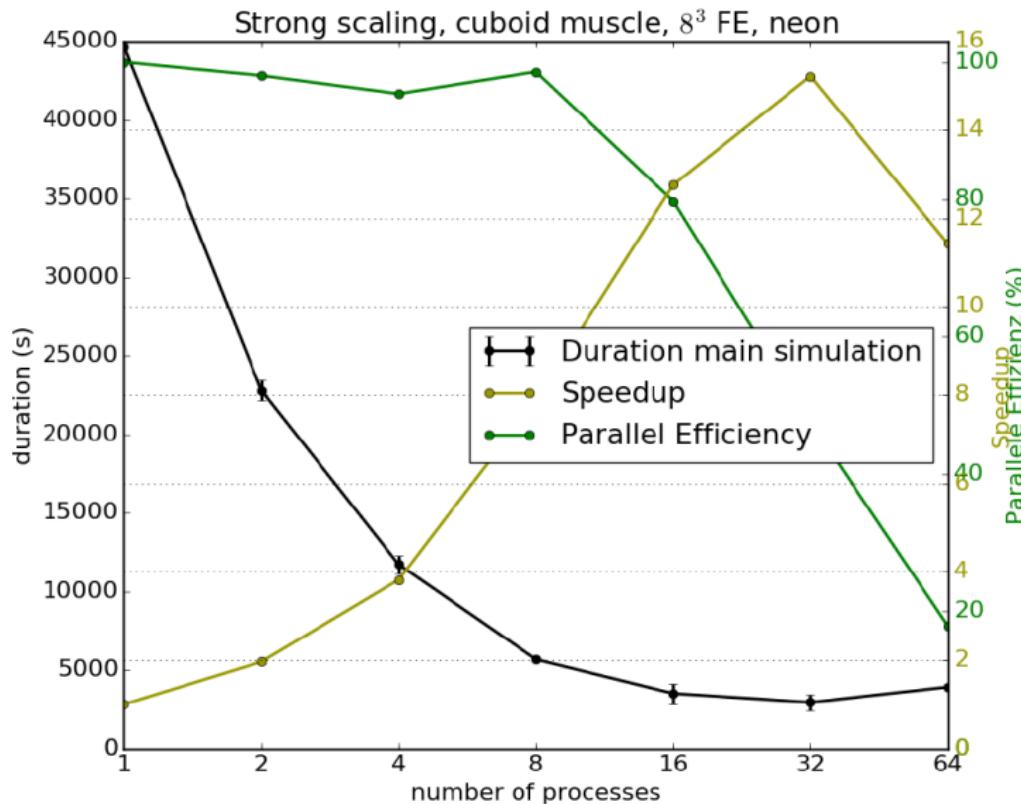
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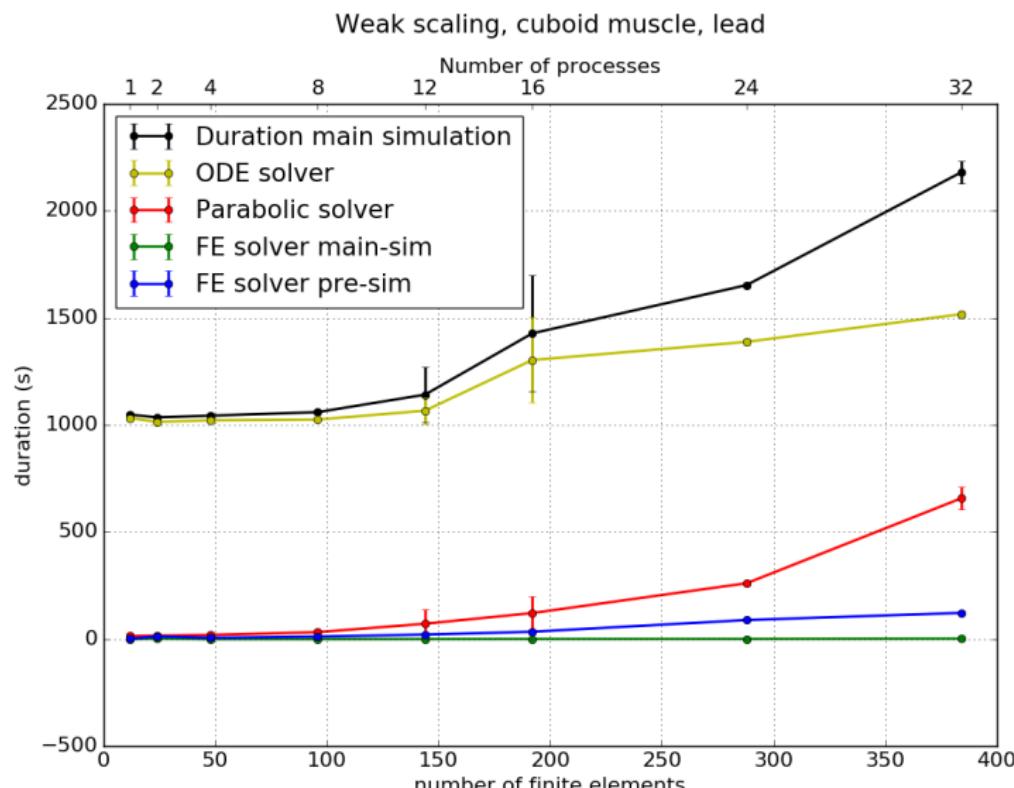
# The computational framework OpenCMISS

## Simulation

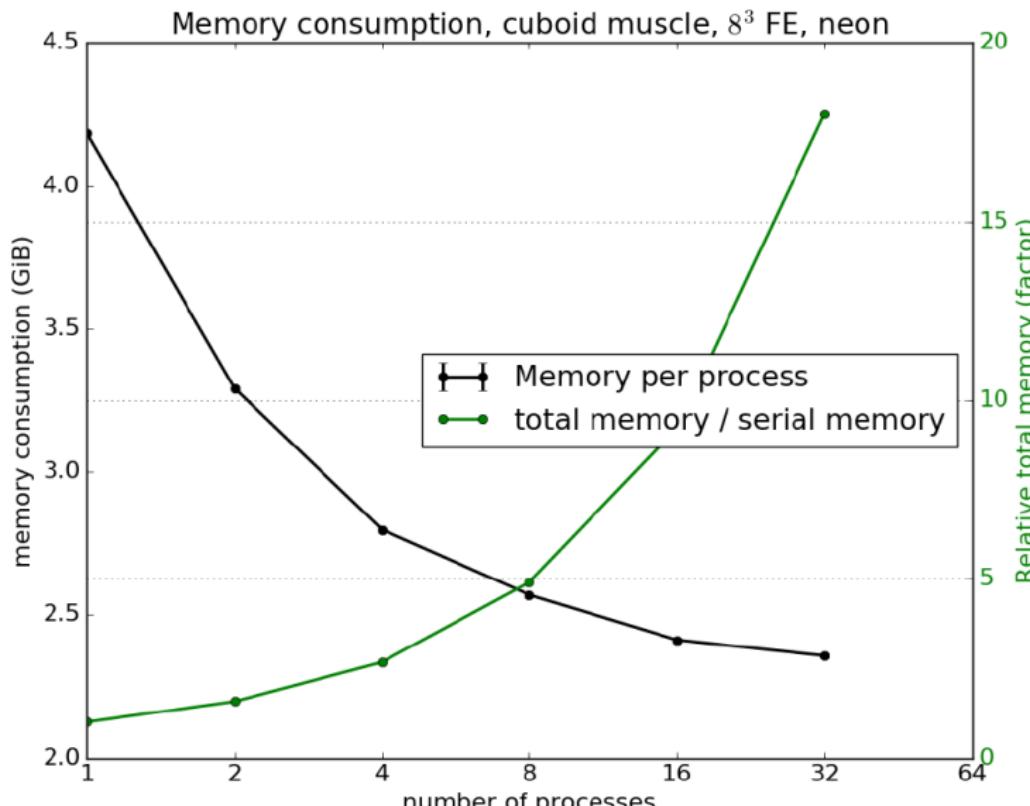
# Scaling Properties



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Thank you for your attention!

