

# GRAVITATIONAL LENSING

## 16 - AXIALLY SYMMETRIC LENSES

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*Massimo Meneghetti*  
AA 2019-2020

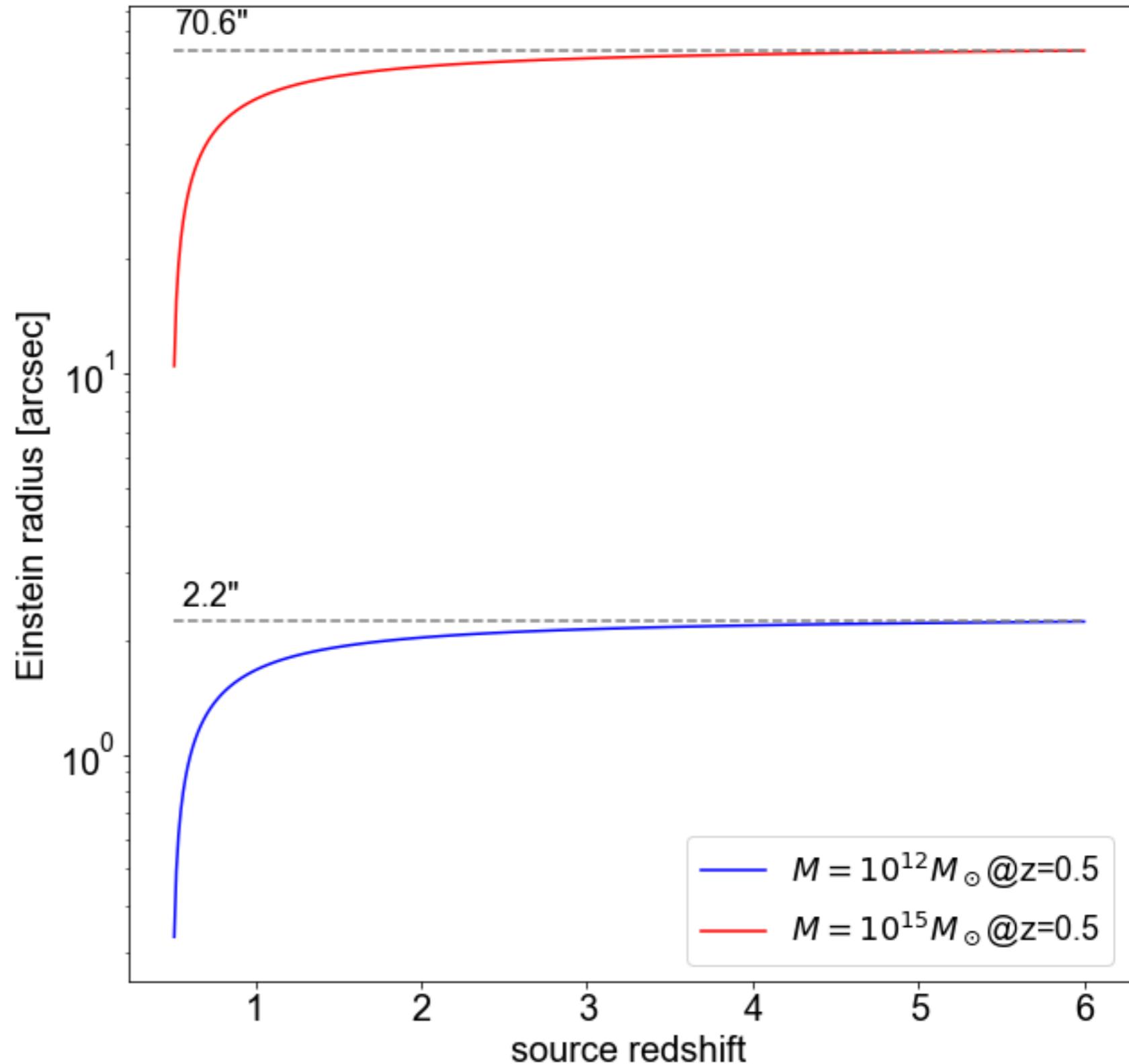
# LENSING BY GALAXIES AND GALAXY CLUSTERS

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- Much more massive than stars!
- At cosmological distances
- Extended!
- Complex (more parameters)

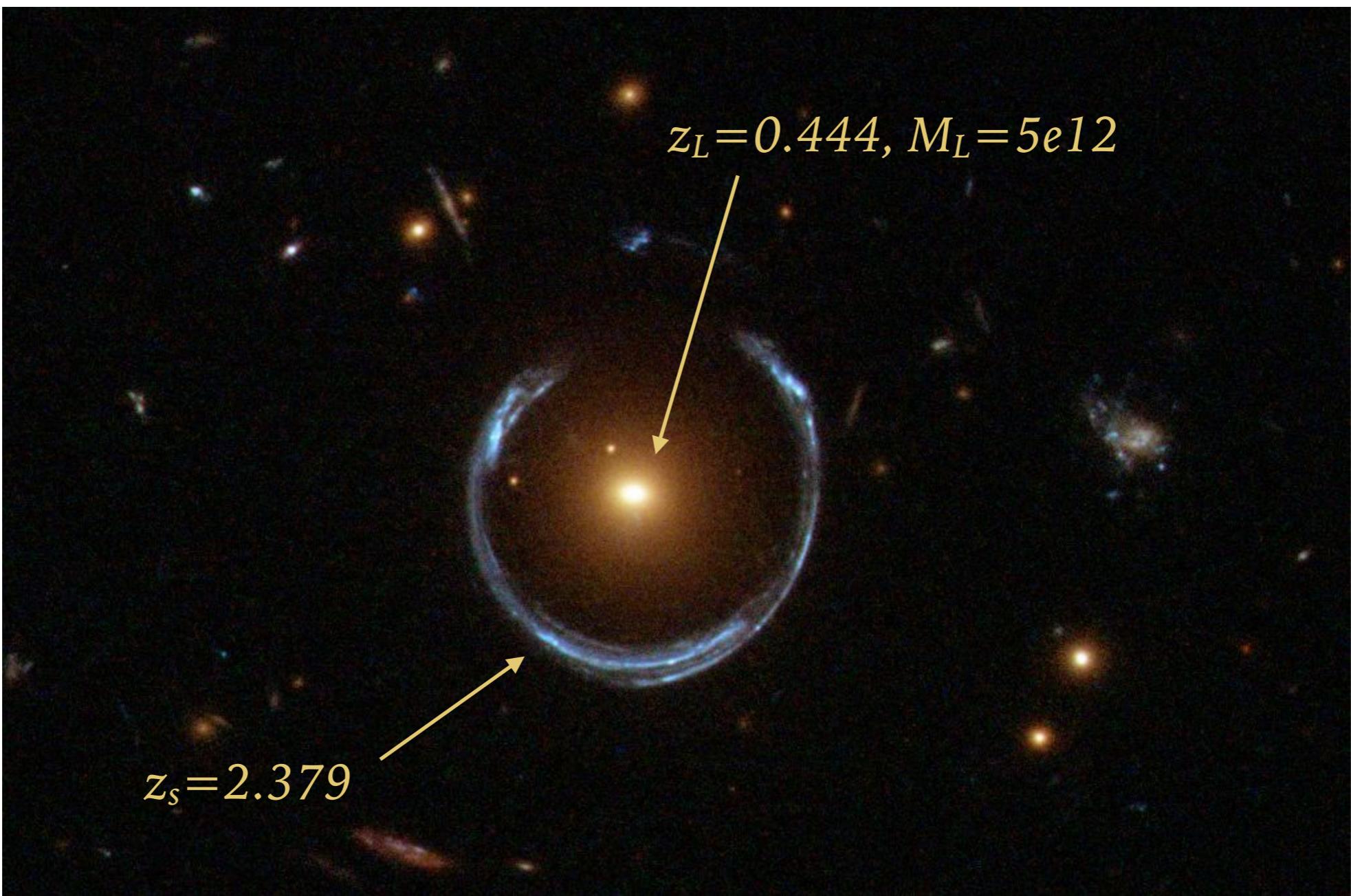
Note: computed using

$$\theta_E = \sqrt{\frac{4GM}{c^2} \frac{D_{LS}}{D_L D_S}}$$



# EXTENDED LENSES

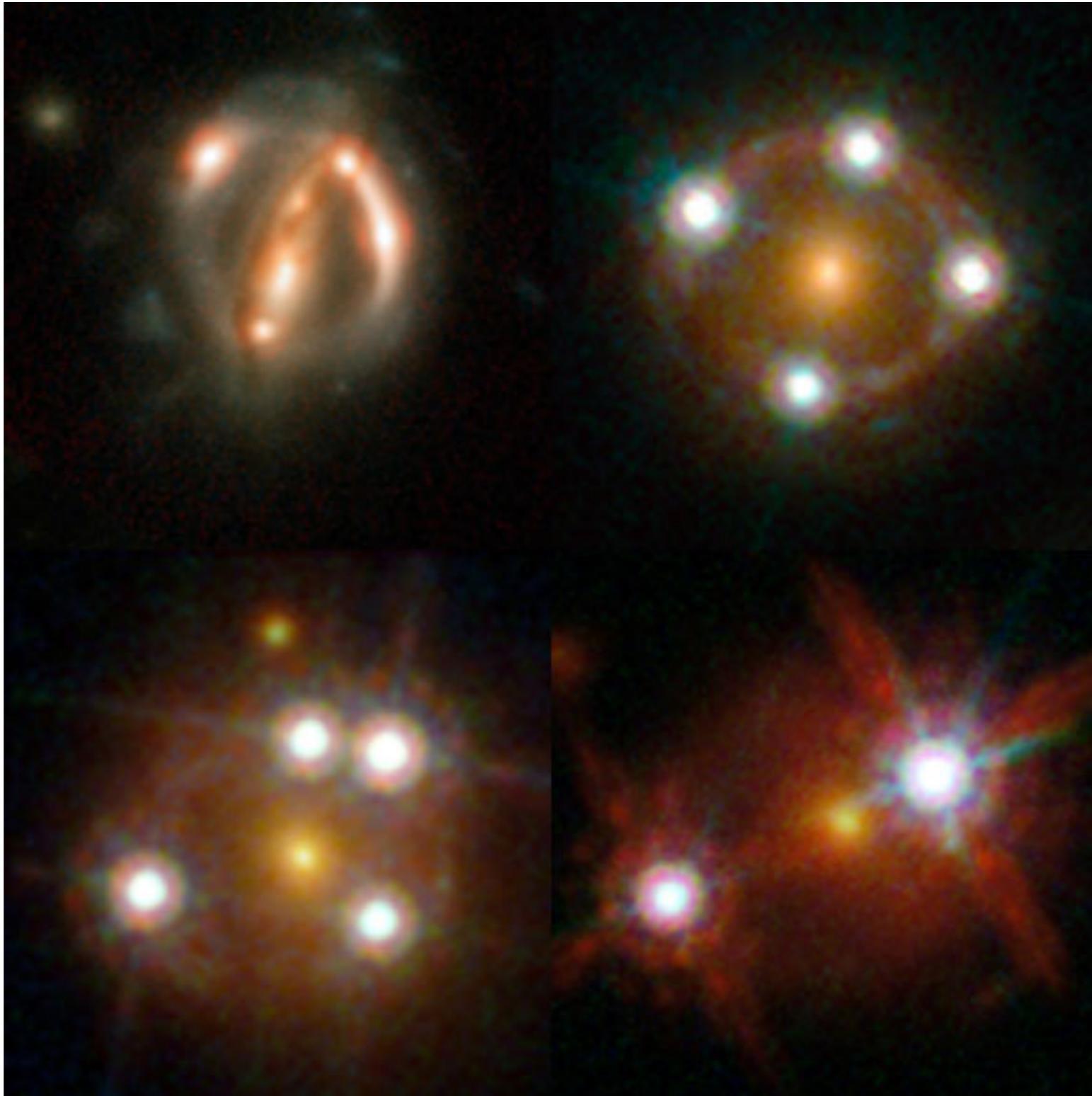
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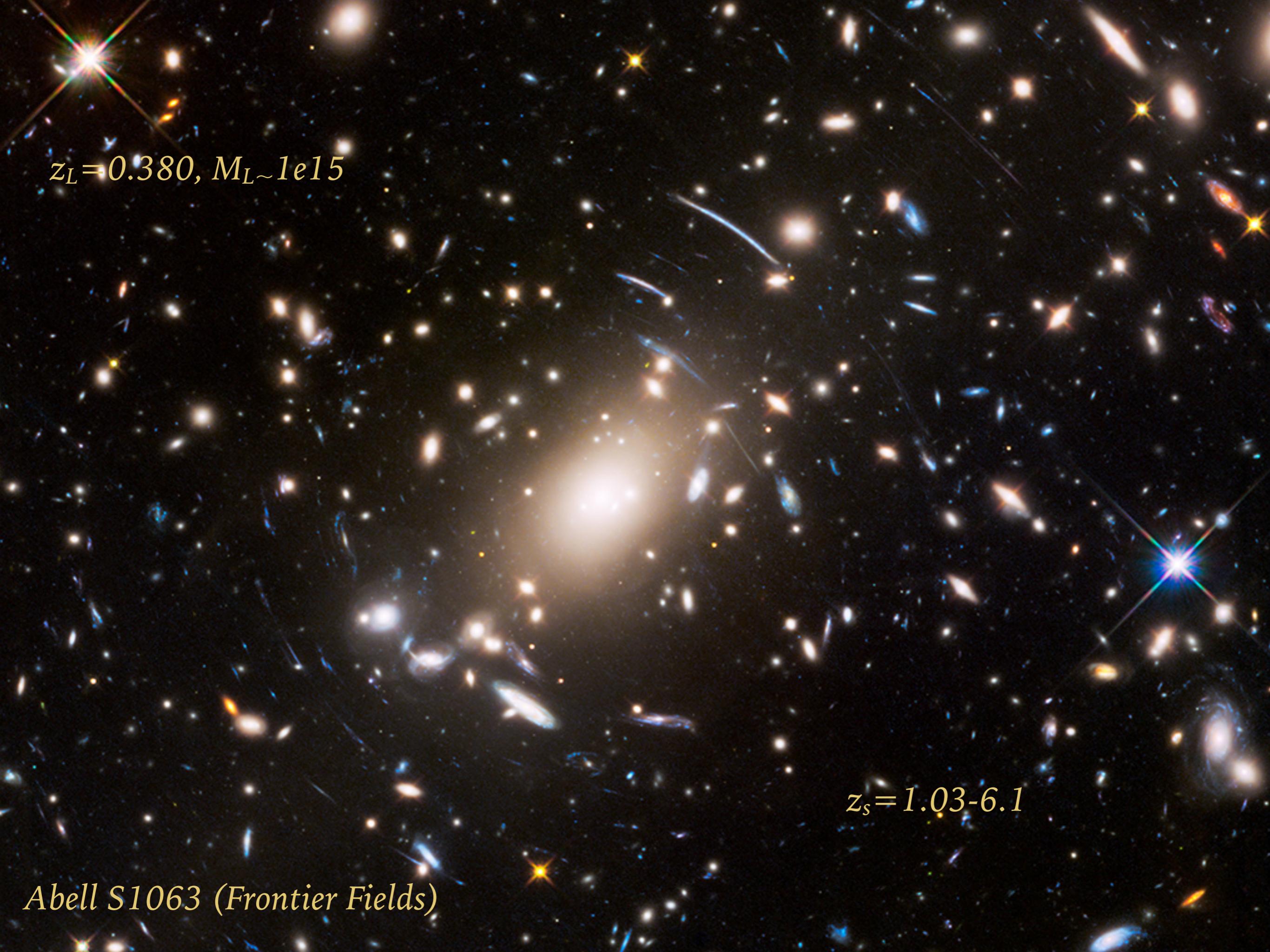
*Cosmic horseshoe (Belokurov et al. 2007)*

# EXTENDED LENSES

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*Suyu et al. (HOLiCOW team)*



$z_L = 0.380$ ,  $M_L \sim 1e15$

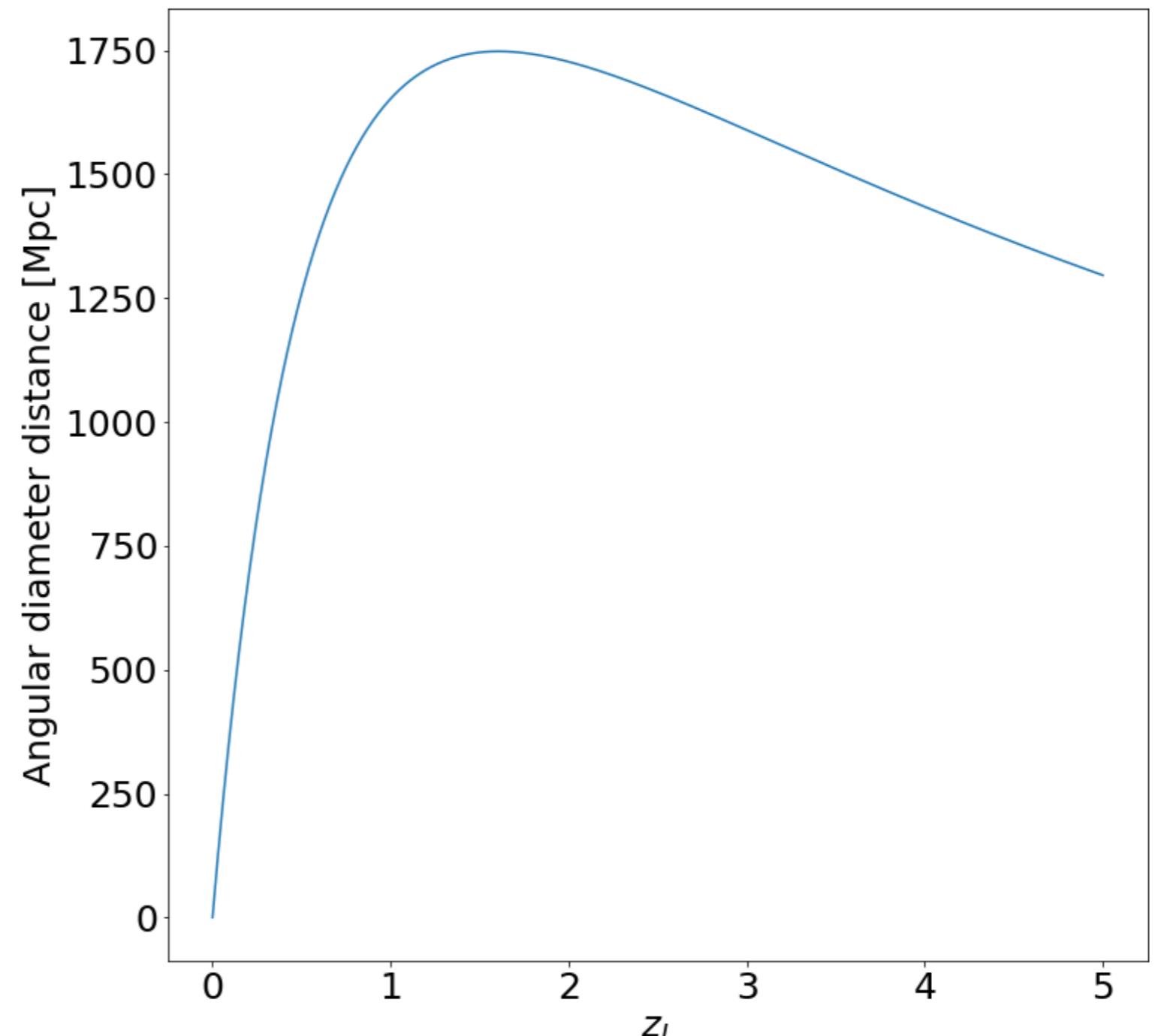
$z_s = 1.03-6.1$

*Abell S1063 (Frontier Fields)*

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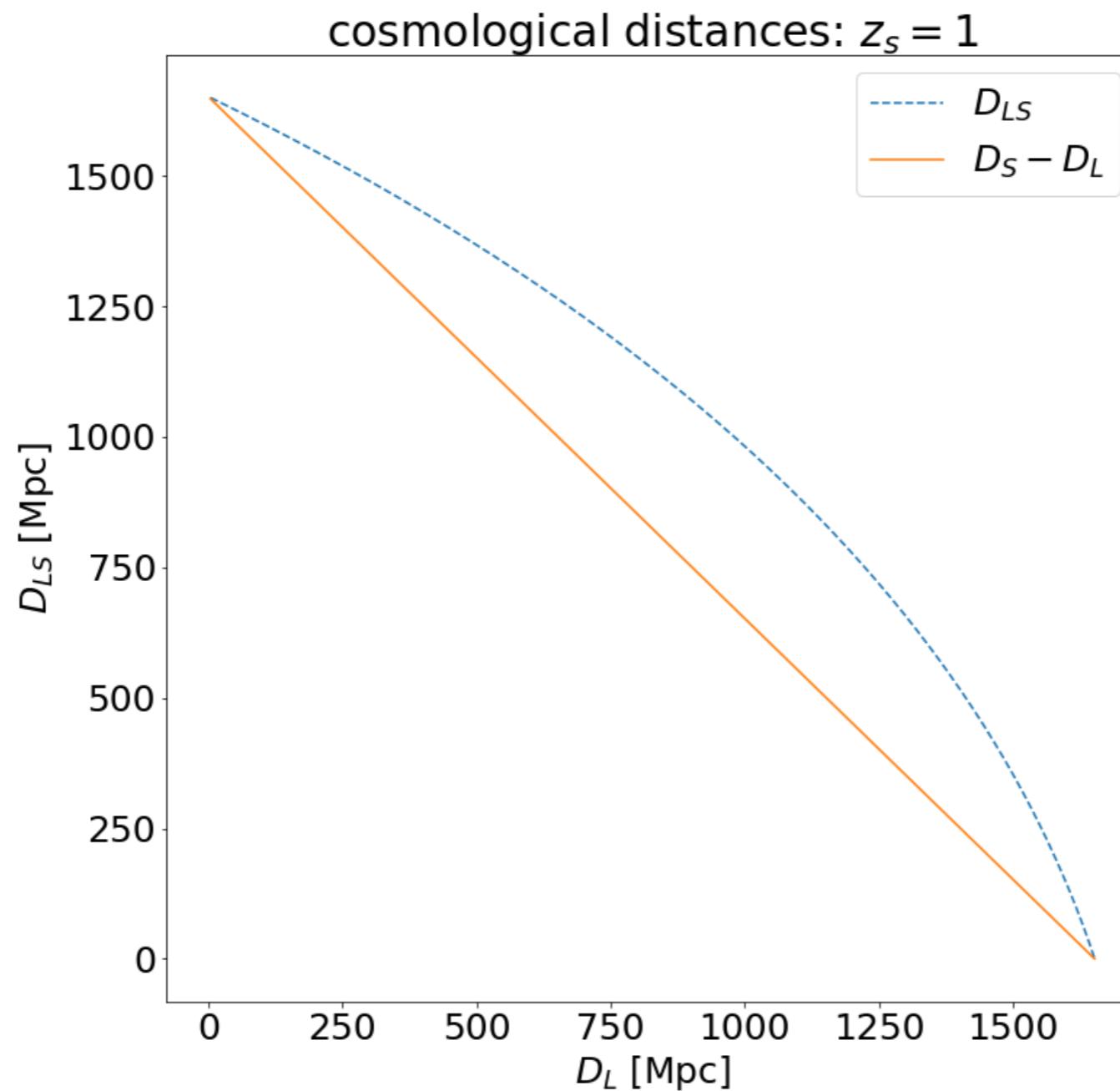
$$D_A(z) = \frac{c}{1+z} \int_0^z \frac{dz}{H(z)}$$

$$H^2(z) = H_0^2 [\Omega_m(z)(1+z)^3 + \Omega_{DE}(1+z)^{3(1+w)}]$$

# AGAIN ON ANGULAR DIAMETER DISTANCES...

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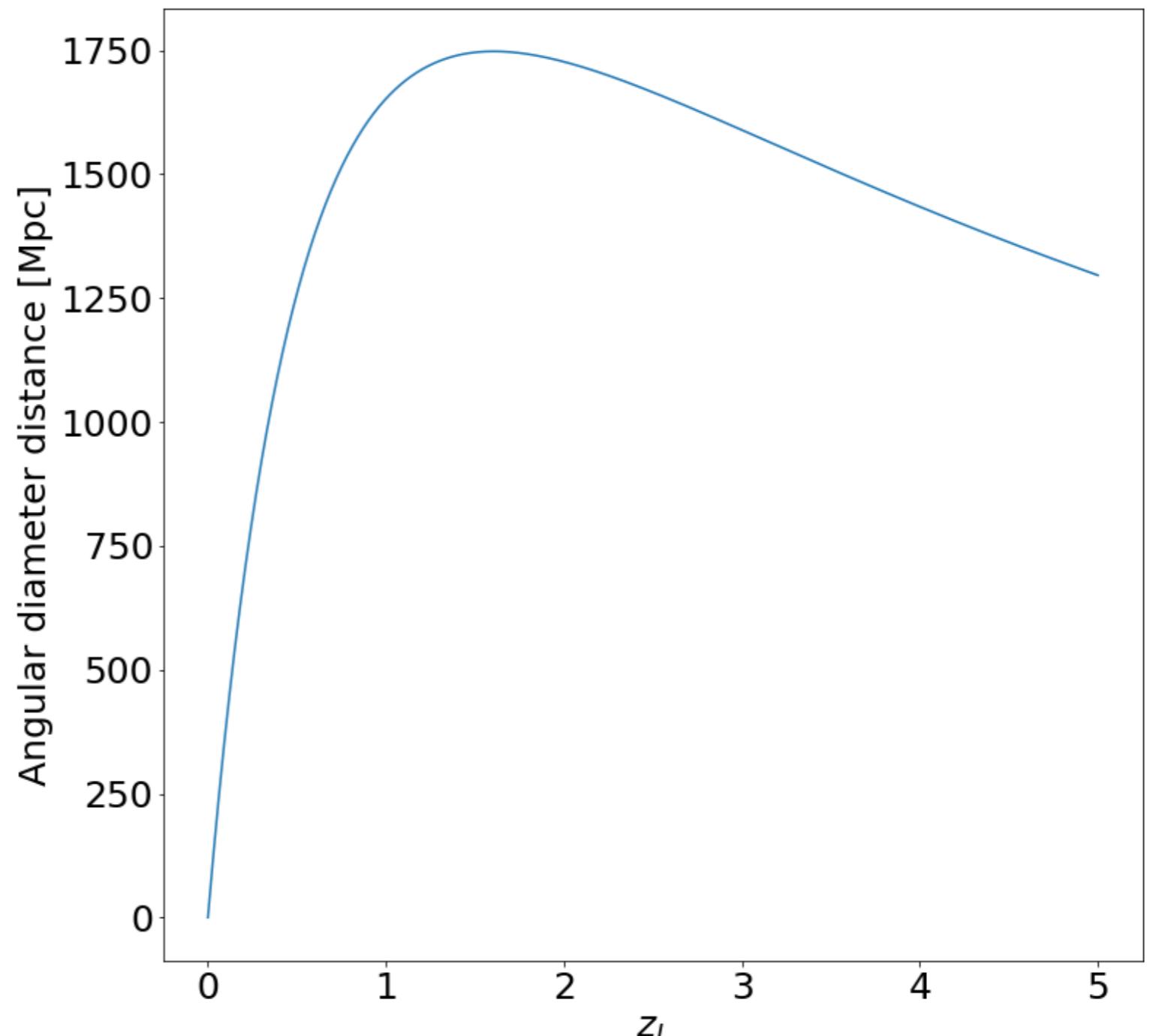
*On cosmological scales  $D_{LS} \neq D_S - D_L$*



# LENSING BY GALAXIES AND GALAXY CLUSTERS

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$$D_A(z) = \frac{c}{1+z} \int_0^z \frac{dz}{H(z)}$$

$$H^2(z) = H_0^2 [\Omega_m(z)(1+z)^3 + \Omega_{DE}(1+z)^{3(1+w)}]$$

# EXTENDED LENSES

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- Cosmic structures like galaxies and galaxy clusters are characterized by bound mass distributions, which cannot be approximated by point lenses
- Indeed these are *extended lenses*, and their lensing properties are determined by e.g. their surface mass density:

$$\Sigma(\vec{\xi}) = \int \rho(\vec{\xi}, z) \, dz$$

$$\vec{\alpha}(\vec{\xi}) = \frac{4G}{c^2} \int \frac{(\vec{\xi} - \vec{\xi}') \Sigma(\vec{\xi}')}{|\vec{\xi} - \vec{\xi}'|^2} \, d^2 \xi'$$

# EXTENDED LENSES

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- Recall that the surface density is related to the lensing potential by

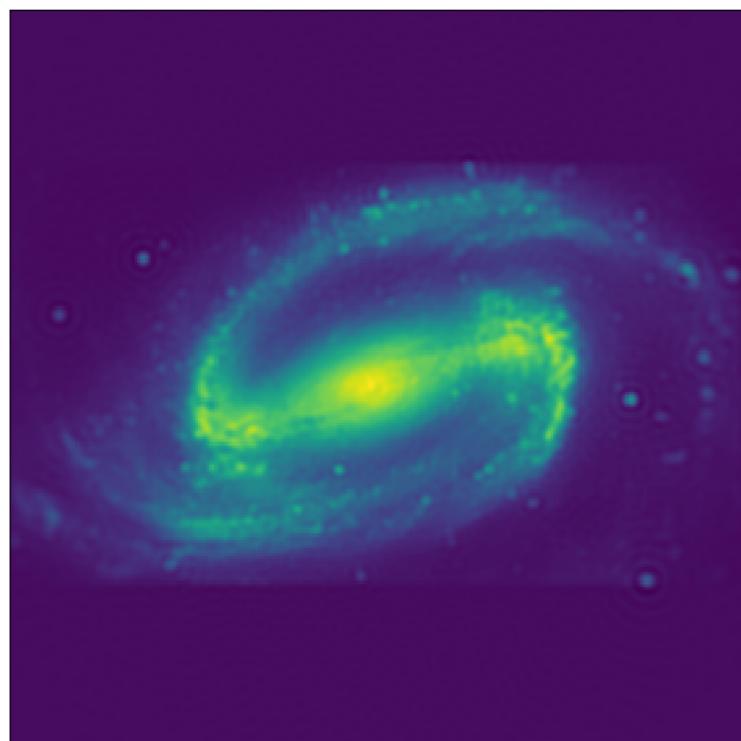
$$\Delta_{\theta} \Psi(\vec{\theta}) = 2\kappa(\vec{\theta})$$

$$\kappa(\vec{\theta}) \equiv \frac{\Sigma(\vec{\theta})}{\Sigma_{\text{cr}}} \quad \text{with} \quad \Sigma_{\text{cr}} = \frac{c^2}{4\pi G} \frac{D_S}{D_L D_{LS}}$$

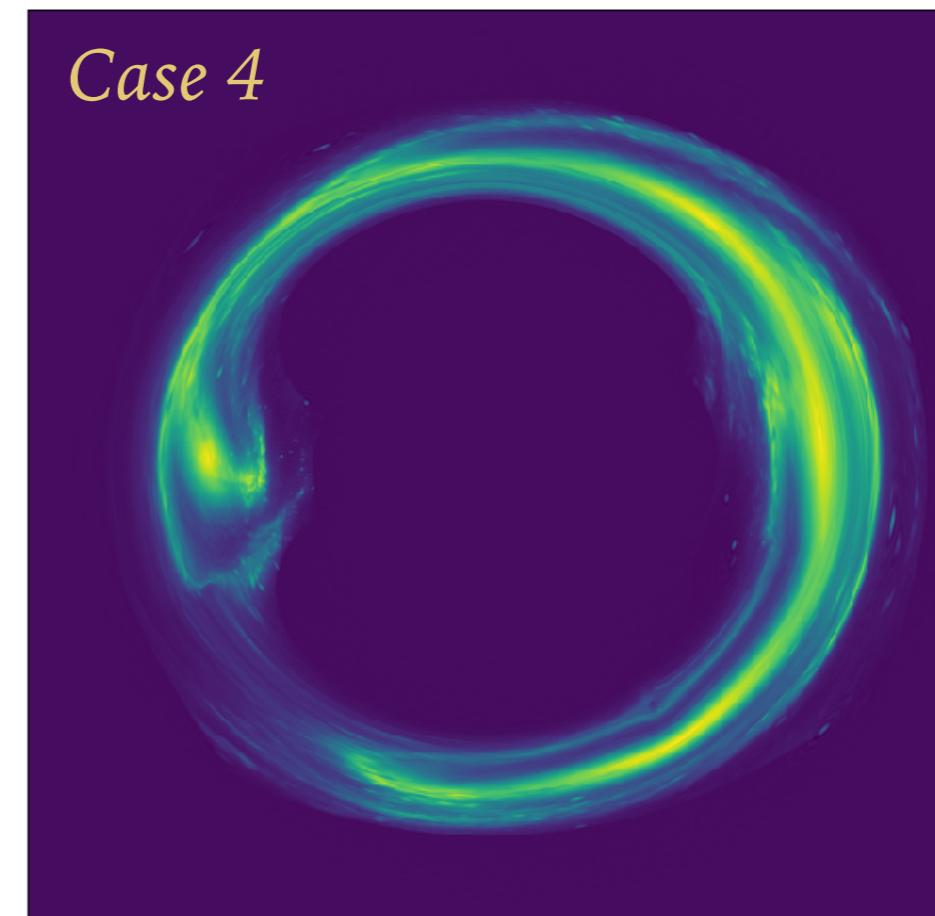
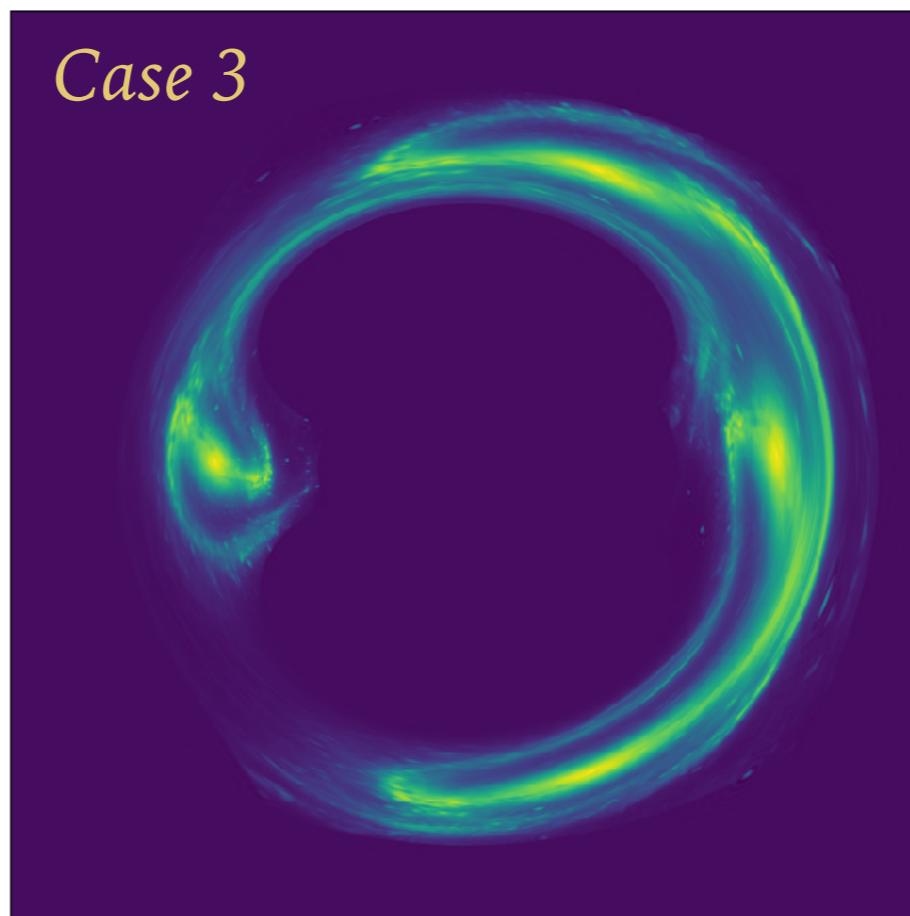
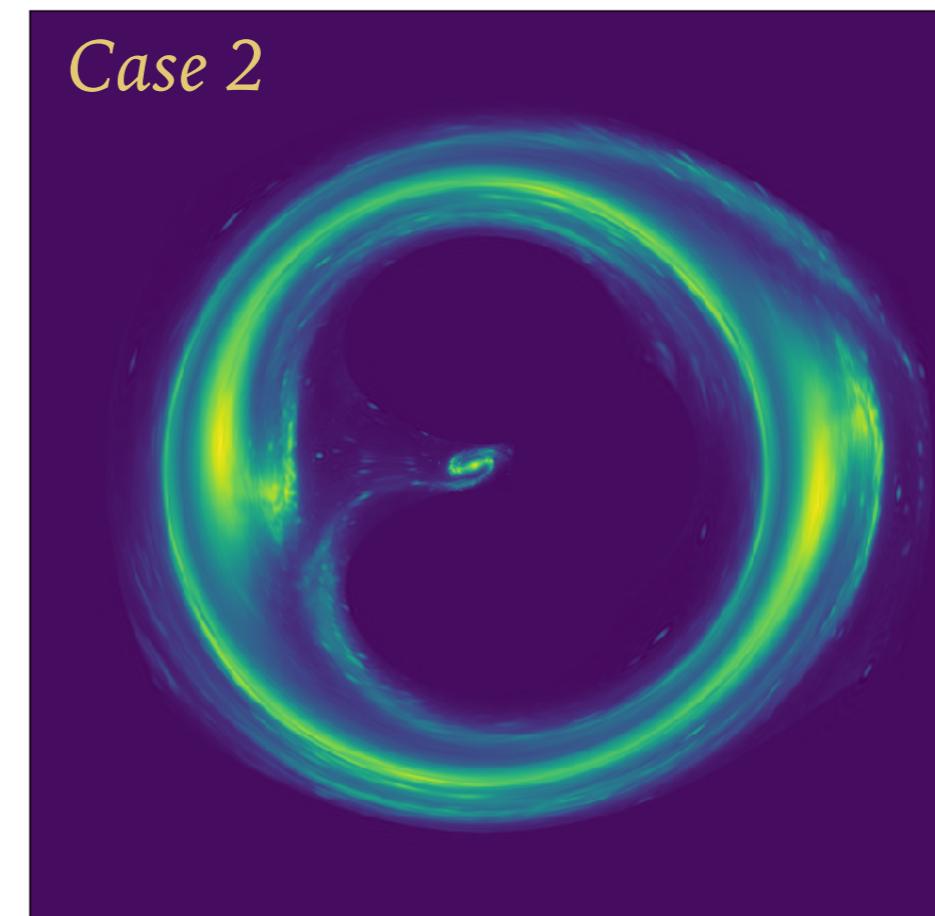
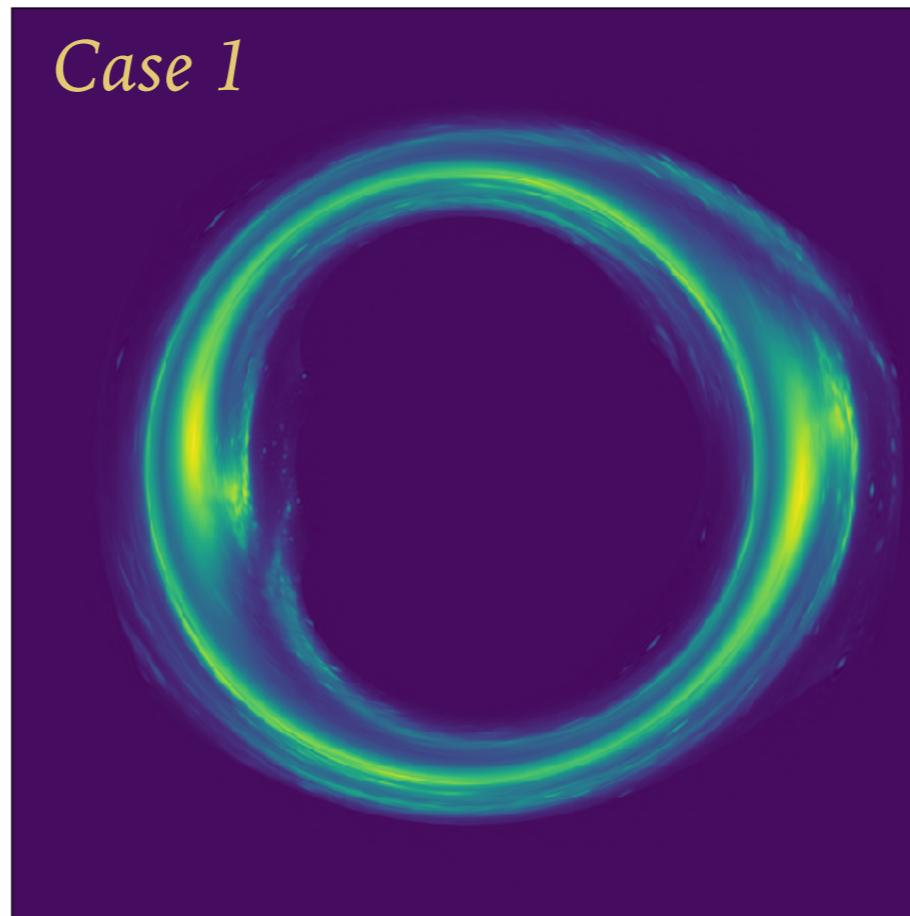
# LENSING BY GALAXIES AND GALAXY CLUSTERS

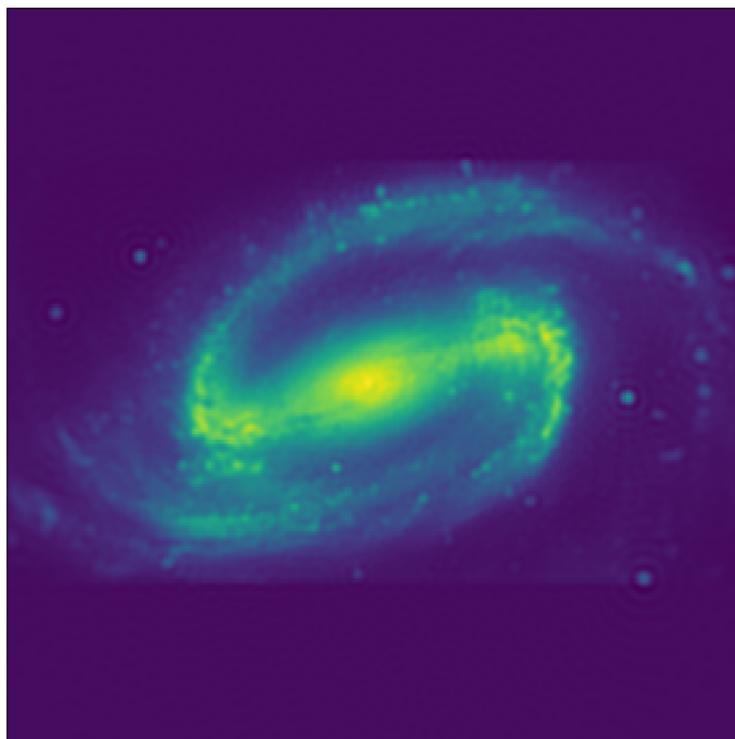
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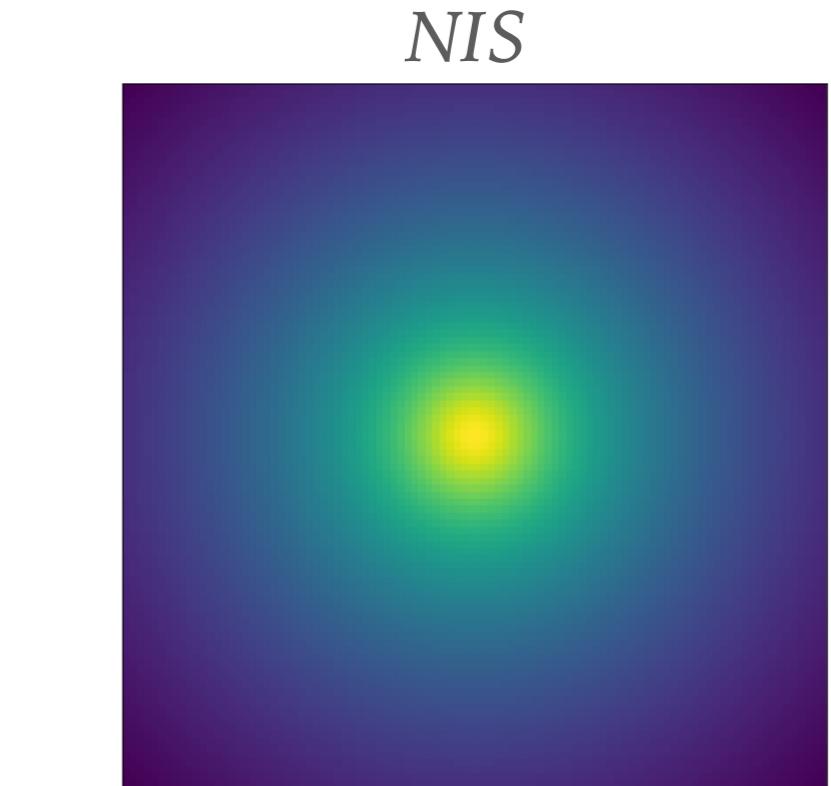
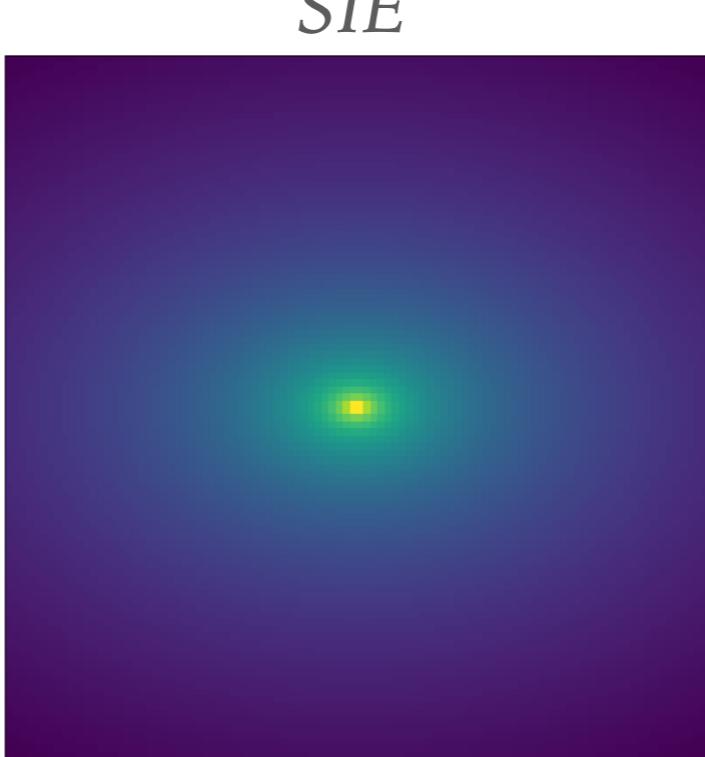
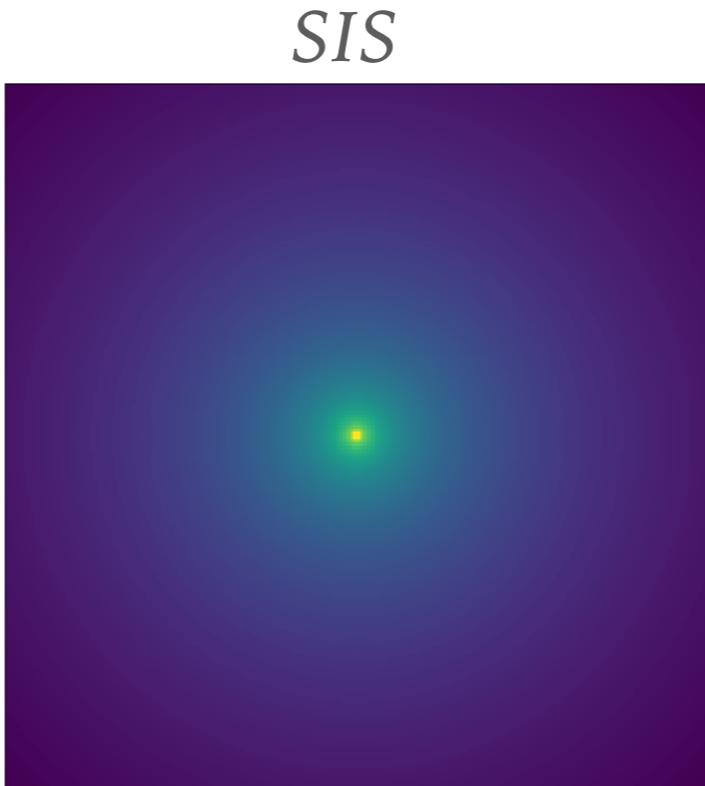


*Unlensed source*

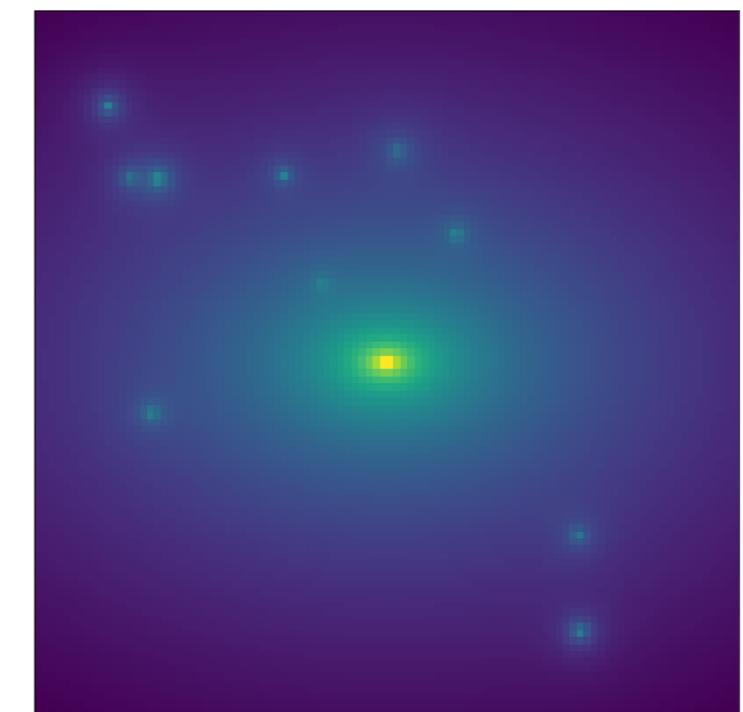




*Unlensed source*



*SIE+tNFW subs+ext. shear*



# WHAT ARE THE RELEVANT PROPERTIES OF THE LENSES?

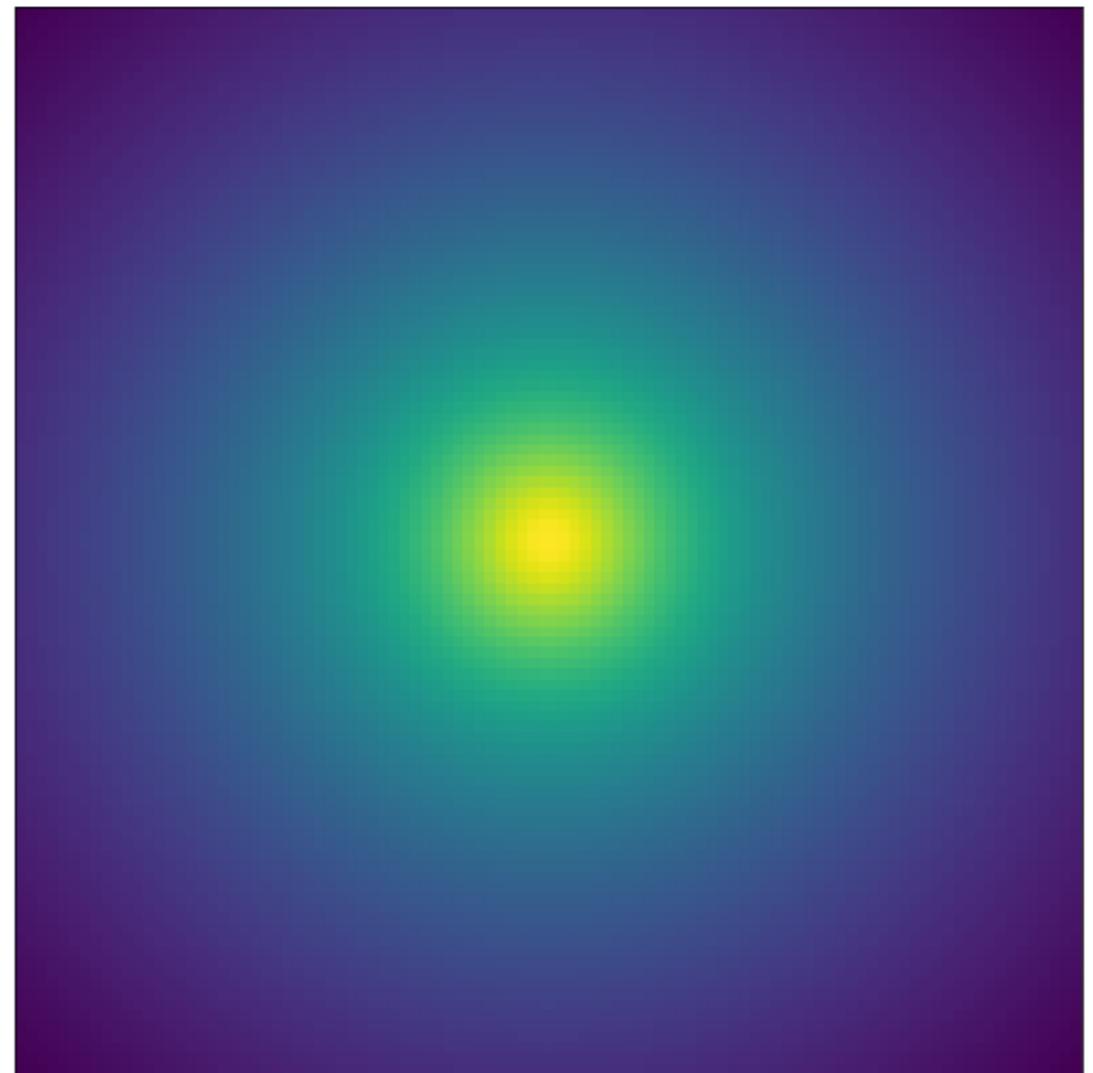
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- The surface density distribution of a lens (and its potential) can be characterized by means of
  - the profile
  - the shape of the iso-density (iso-potential) contours
  - the smoothness
  - the environment where the lens resides
- In this and in the following lessons, we will study how these features determine the ability of a mass distribution to produce lensing effects.
- We will do that by building analytical models with increasing level of complexity.

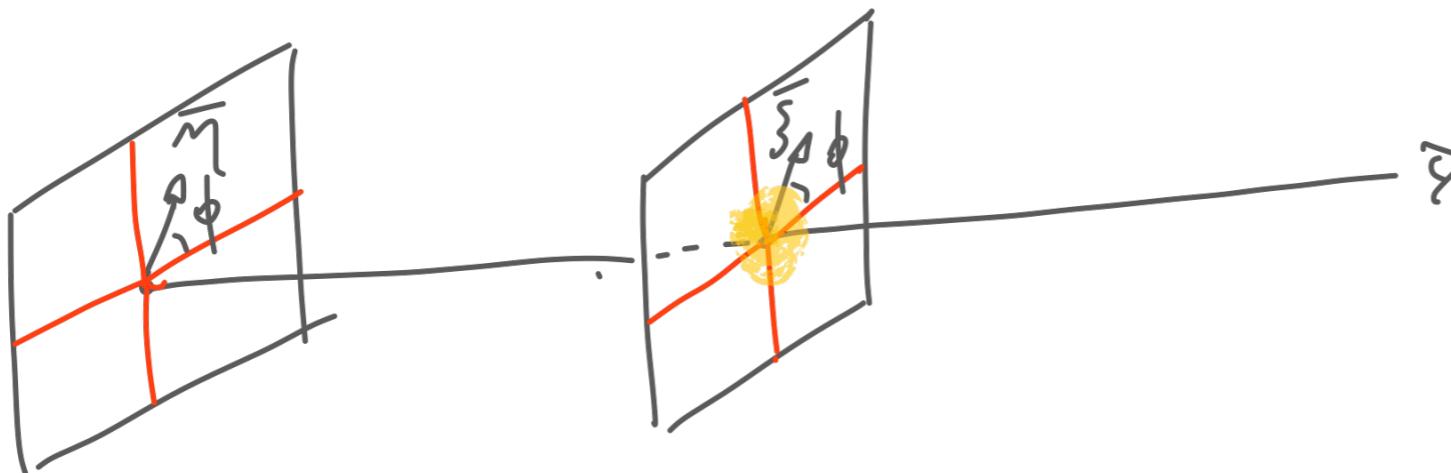
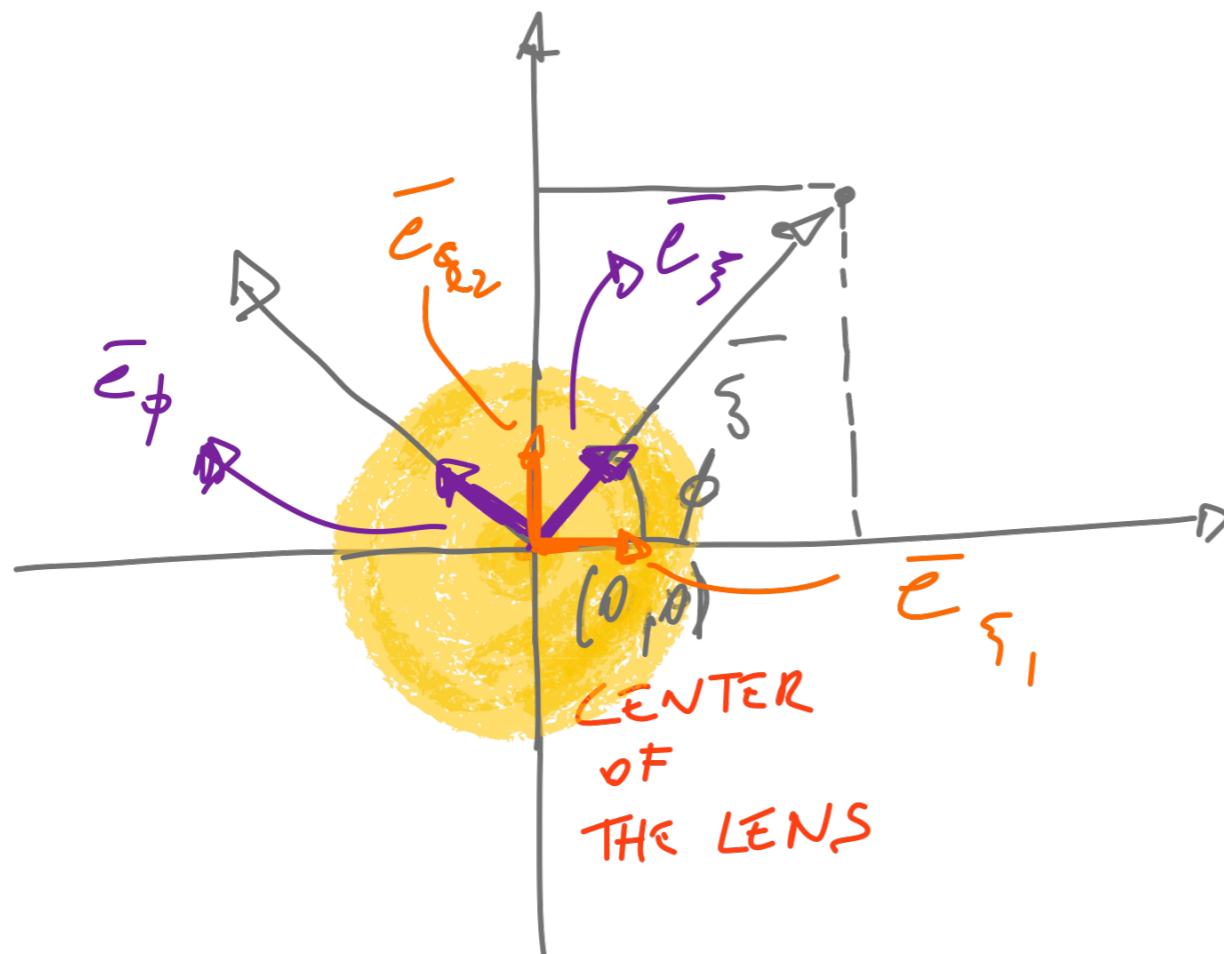
# AXIALLY SYMMETRIC, CIRCULAR LENSES

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- Axially symmetric, circular models are the simplest lens models for describing extended mass distributions
- For these lenses  $\hat{\Psi}(\vec{\theta}) = \hat{\Psi}(\theta)$
- Several quantities relevant for lensing can be derived in a simple manner by using the symmetry properties of the lens.
- One example is the deflection angle...



# POLAR COORDINATES IN THE LENS OR IN THE SOURCE PLANES



$$\bar{\xi} = \xi_1 \bar{e}_{\xi_1} + \xi_2 \bar{e}_{\xi_2}$$

$$\xi_1 = \xi \cdot \cos \phi \quad \xi_2 = \xi \cdot \sin \phi$$

$$\bar{e}_{\xi_1} = \cos \phi \cdot \bar{e}_\xi - \sin \phi \cdot \bar{e}_\phi$$

$$\bar{e}_{\xi_2} = \sin \phi \cdot \bar{e}_\xi + \cos \phi \cdot \bar{e}_\phi$$

Analogously:

$$\gamma_1 = \gamma \cdot \cos \phi$$

$$\gamma_2 = \gamma \cdot \sin \phi$$

...

# DEFLECTION ANGLE OF AN AXIALLY SYMMETRIC LENS

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$$\vec{\nabla}_\xi = \frac{\partial}{\partial \xi_1} \vec{e}_{\xi_1} + \frac{\partial}{\partial \xi_2} \vec{e}_{\xi_2} = \frac{\partial}{\partial \xi} \vec{e}_\xi + \frac{1}{\xi} \frac{\partial}{\partial \phi} \vec{e}_\phi$$

$$\vec{\nabla}_\theta = D_L \left( \frac{\partial}{\partial \xi} \vec{e}_\xi + \frac{1}{\xi} \frac{\partial}{\partial \phi} \vec{e}_\phi \right) = \left( \frac{\partial}{\partial \theta} \vec{e}_\theta + \frac{1}{\theta} \frac{\partial}{\partial \phi} \vec{e}_\phi \right)$$

$$\vec{\nabla}_\theta \hat{\Psi}(\theta) = \frac{\partial \hat{\Psi}(\theta)}{\partial \theta} \vec{e}_\theta = \Psi'(\theta) \vec{e}_\theta = \alpha(\theta) \vec{e}_\theta = \vec{\alpha}(\vec{\theta})$$

*For an axially symmetric lens, the deflection is “radial”: it depends only on the distance from the lens center.*

# DEFLECTION ANGLE OF AN AXIALLY SYMMETRIC LENS

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$$\nabla_\theta^2 = \frac{1}{\theta} \frac{\partial}{\partial \theta} \left( \theta \frac{\partial}{\partial \theta} \right) + \frac{1}{\theta^2} \frac{\partial^2}{\partial \phi^2}$$

$$\frac{1}{\theta} \frac{\partial}{\partial \theta} \left( \theta \frac{\partial}{\partial \theta} \right) \hat{\Psi}(\theta) = 2\kappa(\theta)$$

*From this equation, we obtain*

$$\begin{aligned}\alpha(\theta) &= \frac{2 \int_0^\theta \kappa(\theta') \theta' d\theta'}{\theta} \\ &= \frac{2 \int_0^\theta \Sigma(\theta') \theta' d\theta'}{\theta \Sigma_{cr}} \\ &= \frac{D_{LS}}{D_S} \frac{4GM(\theta)}{c^2 D_L \theta} \\ &= \frac{D_{LS}}{D_S} \hat{\alpha}(\theta).\end{aligned}$$

$$\kappa(\theta) = \frac{\Sigma(\theta)}{\Sigma_{cr}}$$

$$\Sigma_{cr} = \frac{c^2}{4\pi G} \frac{D_S}{D_L D_{LS}}$$

# DEFLECTION ANGLE OF AN AXIALLY SYMMETRIC LENS

---

$$\nabla_\theta^2 = \frac{1}{\theta} \frac{\partial}{\partial \theta} \left( \theta \frac{\partial}{\partial \theta} \right) + \frac{1}{\theta^2} \frac{\partial^2}{\partial \phi^2}$$

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$$\kappa(\theta) = \frac{\Sigma(\theta)}{\Sigma_{\text{cr}}}$$

$$\Sigma_{\text{cr}} = \frac{c^2}{4\pi G} \frac{D_S}{D_L D_{\text{LS}}}$$

*Identical to point-mass lens!*

# DEFLECTION ANGLE OF AN AXIALLY SYMMETRIC LENS

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*Dimensionless form:*

$$\begin{aligned}\alpha(x) &= \frac{D_L D_{LS}}{\xi_0 D_S} \hat{\alpha}(\xi_0 x) \\ &= \frac{D_L D_{LS}}{\xi_0 D_S} \frac{4GM(\xi_0 x)}{c^2 \xi} \frac{\pi \xi_0}{\pi \xi_0} \\ &= \frac{M(\xi_0 x)}{\pi \xi_0^2 \Sigma_{cr}} \frac{1}{x} \equiv \frac{m(x)}{x}, \quad \text{Dimensionless mass}\end{aligned}$$

$$\alpha(x) = \frac{2}{x} \int_0^x x' \kappa(x') dx' \Rightarrow m(x) = 2 \int_0^x x' \kappa(x') dx'$$

# LENS EQUATION

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$$\vec{y} = \vec{x} - \vec{\alpha}(\vec{x}) \quad \vec{\alpha}(\vec{x}) = \frac{m(\vec{x})}{x} \vec{e}_x$$

*Given that the deflection angle and  $x$  are parallel, so will be  $y$ !*

$$y = x - \alpha(x) = x - \frac{m(x)}{x}$$

# CONVERGENCE

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$$\frac{1}{\theta} \frac{\partial}{\partial \theta} \left( \theta \frac{\partial}{\partial \theta} \right) \hat{\Psi}(\theta) = 2\kappa(\theta) \rightarrow \frac{1}{x} \frac{\partial}{\partial x} \left( x \frac{\partial}{\partial x} \right) \Psi(x) = 2\kappa(x)$$



$$\kappa(\theta) = \frac{1}{2} \left( \hat{\Psi}''(\theta) + \frac{\hat{\Psi}'(\theta)}{\theta} \right) \rightarrow \kappa(x) = \frac{1}{2} \left( \Psi''(x) + \frac{\Psi'(x)}{x} \right)$$



$$\hat{\Psi}'(\theta) = \alpha(\theta)$$

$$\kappa(\theta) = \frac{1}{2} \left( \alpha'(\theta) + \frac{\alpha(\theta)}{\theta} \right) \rightarrow \kappa(x) = \frac{1}{2} \left( \alpha'(x) + \frac{\alpha(x)}{x} \right)$$



$$\alpha'(x) = \frac{m'(x)}{x} - \frac{m(x)}{x^2}$$

$$\kappa(x) = \frac{1}{2} \frac{m'(x)}{x}$$

# SHEAR

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*The shear components are derived from the second derivatives of the potential or from the first derivatives of the deflection angle components:*

$$\frac{\partial}{\partial \theta_1} = \cos \phi \frac{\partial}{\partial \theta} - \frac{\sin \phi}{\theta} \frac{\partial}{\partial \phi}$$

$$\frac{\partial}{\partial \theta_2} = \sin \phi \frac{\partial}{\partial \theta} + \frac{\cos \phi}{\theta} \frac{\partial}{\partial \phi}$$

$$\alpha_1 = \alpha \cos \phi$$

$$\alpha_2 = \alpha \sin \phi$$

# SHEAR

---

$$\frac{\partial}{\partial \theta_1} = \cos \phi \frac{\partial}{\partial \theta} - \frac{\sin \phi}{\theta} \frac{\partial}{\partial \phi} \quad \alpha_1 = \alpha \cos \phi$$

$$\frac{\partial}{\partial \theta_2} = \sin \phi \frac{\partial}{\partial \theta} + \frac{\cos \phi}{\theta} \frac{\partial}{\partial \phi} \quad \alpha_2 = \alpha \sin \phi$$

$$\begin{aligned}\gamma_1(\theta) &= \frac{1}{2} \left[ \frac{\partial}{\partial \theta_1} \alpha_1(\theta) - \frac{\partial}{\partial \theta_2} \alpha_2(\theta) \right] \\ &= \frac{1}{2} \left[ (\cos^2 \phi - \sin^2 \phi) \alpha'(\theta) - (\cos^2 \phi - \sin^2 \phi) \frac{\alpha(\theta)}{\theta} \right] \\ &= \frac{\cos 2\phi}{2} \left[ \alpha'(\theta) - \frac{\alpha(\theta)}{\theta} \right],\end{aligned}$$

# SHEAR

---

$$\frac{\partial}{\partial \theta_1} = \cos \phi \frac{\partial}{\partial \theta} - \frac{\sin \phi}{\theta} \frac{\partial}{\partial \phi} \quad \alpha_1 = \alpha \cos \phi$$

$$\frac{\partial}{\partial \theta_2} = \sin \phi \frac{\partial}{\partial \theta} + \frac{\cos \phi}{\theta} \frac{\partial}{\partial \phi} \quad \alpha_2 = \alpha \sin \phi$$

$$\begin{aligned}\gamma_2(\theta) &= \frac{\partial}{\partial \theta_2} \alpha_1(\theta) \\ &= \left[ \sin \phi \cos \phi \alpha'(\theta) - \sin \phi \cos \phi \frac{\alpha(\theta)}{\theta} \right] \\ &= \frac{\sin 2\phi}{2} \left[ \alpha'(\theta) - \frac{\alpha(\theta)}{\theta} \right].\end{aligned}$$

# SHEAR

---

$$\begin{aligned}
 \gamma_1(\theta) &= \frac{1}{2} \left[ \frac{\partial}{\partial \theta_1} \alpha_1(\theta) - \frac{\partial}{\partial \theta_2} \alpha_2(\theta) \right] \\
 &= \frac{1}{2} \left[ (\cos^2 \phi - \sin^2 \phi) \alpha'(\theta) - (\cos^2 \phi - \sin^2 \phi) \frac{\alpha(\theta)}{\theta} \right] \\
 &= \frac{\cos 2\phi}{2} \left[ \alpha'(\theta) - \frac{\alpha(\theta)}{\theta} \right],
 \end{aligned}$$

$$\begin{aligned}
 \gamma_2(\theta) &= \frac{\partial}{\partial \theta_2} \alpha_1(\theta) \\
 &= \left[ \sin \phi \cos \phi \alpha'(\theta) - \sin \phi \cos \phi \frac{\alpha(\theta)}{\theta} \right] \\
 &= \frac{\sin 2\phi}{2} \left[ \alpha'(\theta) - \frac{\alpha(\theta)}{\theta} \right].
 \end{aligned}$$

$$\alpha(x) = \frac{m(x)}{x} \quad \alpha'(x) = \frac{m'(x)}{x} - \frac{m(x)}{x^2}$$

$$\begin{aligned}
 \gamma(x) &= \frac{1}{2} \left| \frac{m'(x)}{x} - \frac{2m(x)}{x^2} \right| \\
 &= |\kappa(x) - \bar{\kappa}(x)|,
 \end{aligned}
 \quad \kappa(x) = \frac{1}{2} \frac{m'(x)}{x}$$

$$\bar{\kappa}(x) = \frac{m(x)}{x^2} = 2\pi \frac{\int_0^x x' \kappa(x') dx'}{\pi x^2}$$

# LENSING JACOBIAN

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$$A = \left[ 1 - \frac{m'(x)}{2x} \right] I - \frac{1}{2} \left[ \frac{m'(x)}{x} - \frac{2m(x)}{x^2} \right] \begin{pmatrix} \cos 2\phi & \sin 2\phi \\ \sin 2\phi & -\cos 2\phi \end{pmatrix}$$



$$A = I + \frac{m}{x^2} C(\phi) - \frac{m'(x)}{2x} [I + C(\phi)]$$

$$\begin{aligned} C(\phi) &= \begin{pmatrix} \cos 2\phi & \sin 2\phi \\ \sin 2\phi & -\cos 2\phi \end{pmatrix} \\ &= \begin{pmatrix} \cos^2 \phi - \sin^2 \phi & 2\sin \phi \cos \phi \\ 2\sin \phi \cos \phi & \sin^2 \phi - \cos^2 \phi \end{pmatrix} \end{aligned}$$

$$\begin{aligned} I + C(\phi) &= \begin{pmatrix} 1 + \cos 2\phi & \sin 2\phi \\ \sin 2\phi & 1 - \cos 2\phi \end{pmatrix} \\ &= 2 \begin{pmatrix} \cos^2 \phi & \sin \phi \cos \phi \\ \sin \phi \cos \phi & \sin^2 \phi \end{pmatrix} \end{aligned}$$

# DETERMINANT OF THE LENSING JACOBIN

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$$y = x - \alpha(x) = 1 - \frac{m(x)}{x}$$

$$\begin{aligned}\det A &= \frac{y \, dy}{x \, dx} = \left[ 1 - \frac{\alpha(x)}{x} \right] [1 - \alpha'(x)] \\ &= \left[ 1 - \frac{m(x)}{x^2} \right] \left[ 1 + \frac{m(x)}{x^2} - \frac{m'(x)}{x} \right] \\ &= [1 - \bar{\kappa}(x)] [1 + \bar{\kappa}(x) - 2\kappa(x)] .\end{aligned}$$

# CRITICAL LINES

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$$\begin{aligned}\det A &= \frac{y \, dy}{x \, dx} = \left[ 1 - \frac{\alpha(x)}{x} \right] [1 - \alpha'(x)] \\ &= \left[ 1 - \frac{m(x)}{x^2} \right] \left[ 1 + \frac{m(x)}{x^2} - \frac{m'(x)}{x} \right] \\ &= [1 - \bar{\kappa}(x)] [1 + \bar{\kappa}(x) - 2\kappa(x)].\end{aligned}$$

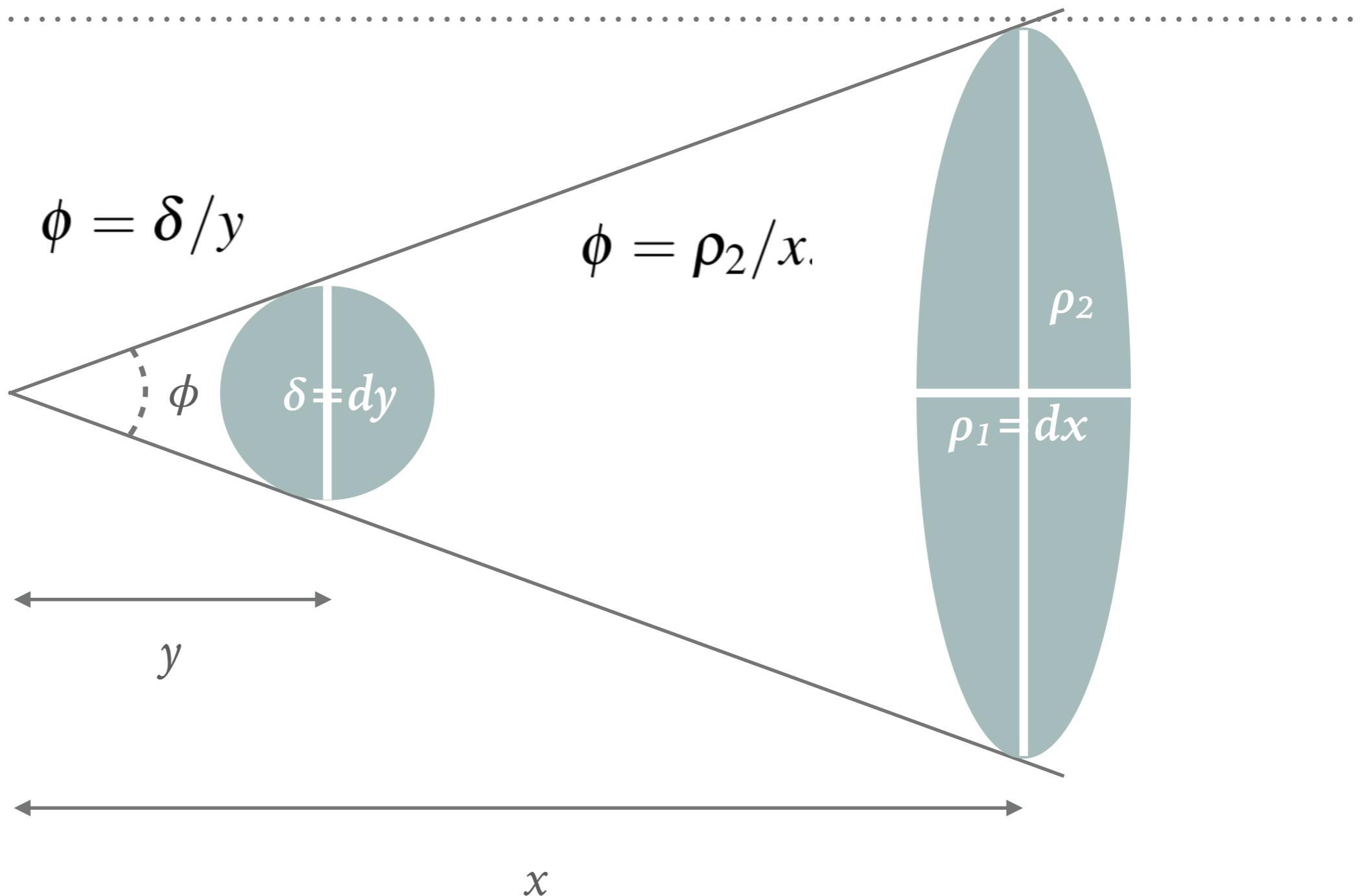
*First critical line:*

$$\alpha(x)/x = m(x)/x^2 = \bar{\kappa}(x) = 1$$

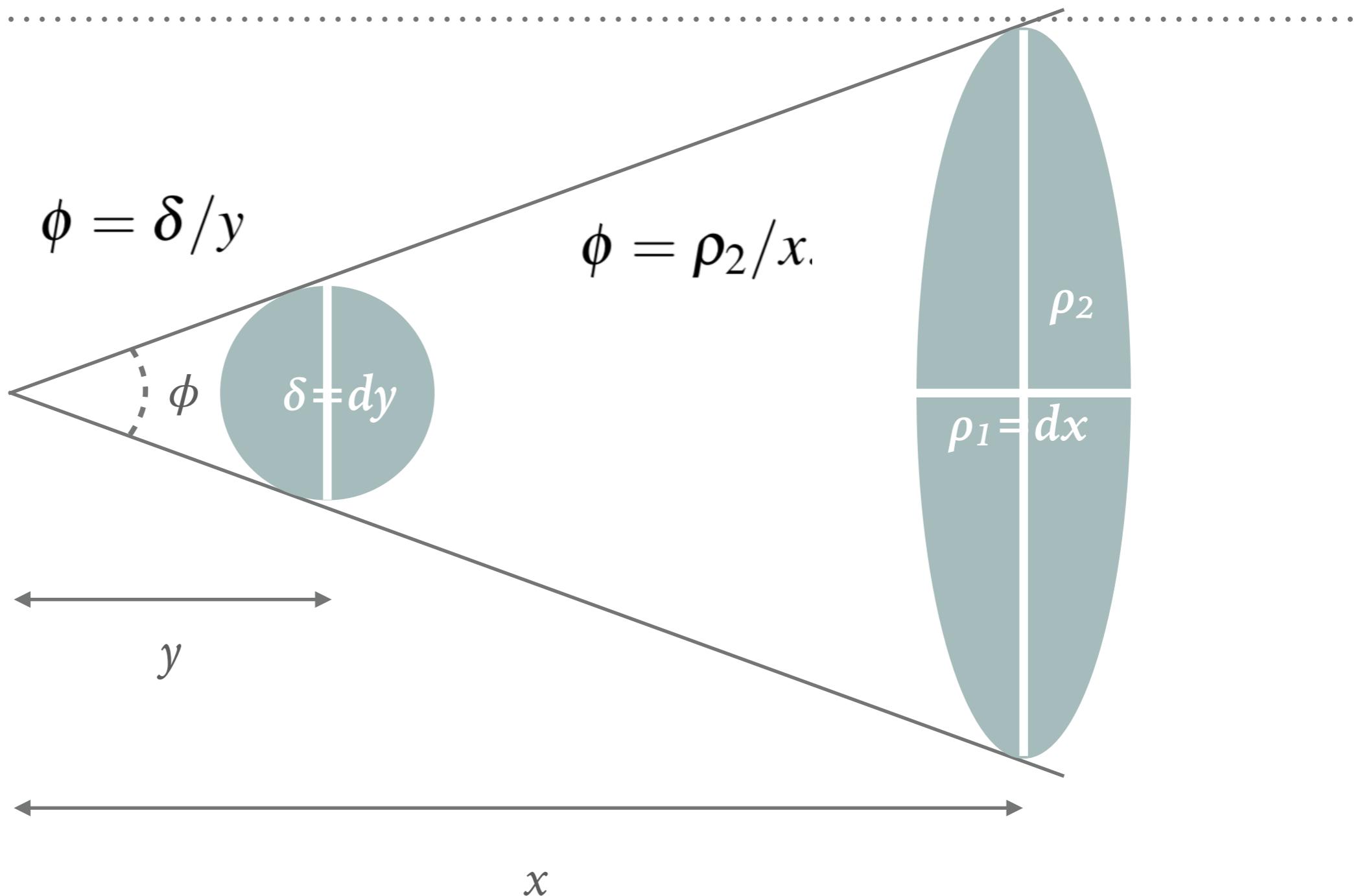
*Second critical line:*

$$\alpha'(x) = m'(x)/x - m/x^2 = 2\kappa(x) - \bar{\kappa}(x) = 1$$

# RADIAL AND TANGENTIAL MAGNIFICATION



# RADIAL AND TANGENTIAL MAGNIFICATION



$$\frac{\delta}{\rho_2} = 1 - \frac{m(x)}{x^2}$$

$$\frac{\delta}{\rho_1} = 1 + \frac{m(x)}{x^2} - 2\kappa(x)$$

# CRITICAL LINES

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The tangential critical line occurs where  $\alpha(x)/x = m(x)/x^2 = \bar{\kappa}(x) = 1$

$$\kappa(\vec{\theta}) \equiv \frac{\Sigma(\vec{\theta})}{\Sigma_{\text{cr}}} \quad \text{with} \quad \Sigma_{\text{cr}} = \frac{c^2}{4\pi G} \frac{D_S}{D_L D_{LS}}$$

$$M(\theta_E) = \pi \Sigma_{\text{cr}} \theta_E^2 D_L^2$$

$$\theta_E = \sqrt{\frac{4GM(\theta_E)}{c^2} \frac{D_{LS}}{D_L D_S}}$$