

Department of Electrical and Computer Engineering

University of Colorado at Boulder

ECEN5730 - Practical PCB design



Lab:18, SBB version of Board 4

Report



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1 Objective / Purpose of Lab

1. One of the key parameters used to characterize VRMs is the Thevenin equivalent circuit model. The Thevenin model represents a voltage source as a combination of an ideal voltage source (Thevenin voltage, V_{TH}) and a series resistance (Thevenin resistance, R_{TH}). This model is particularly useful for analyzing the behavior of VRMs under varying load conditions, as the output voltage and current will depend on the values of V_{TH} and R_{TH} , as well as the load resistance.
- 2.
3. The objective of this lab is to design, build, and test a custom instrument, the "Instrument Droid," capable of measuring the Thevenin parameters (V_{TH} and R_{TH}) of various voltage sources and regulators as a function of the output current load. By sweeping the load current and measuring the corresponding output voltages, the Instrument Droid can determine the Thevenin voltage (the open-circuit voltage) and the Thevenin resistance (the slope of the voltage-current curve).
4. To precisely control the voltage across the sense resistor, and consequently the current through the MOSFET, an external digital-to-analog converter (DAC) is utilized. The DAC, in this case, the MCP4725, receives digital inputs from an Arduino microcontroller and generates an analog voltage output proportional to the desired current level.
5. the Instrument Droid incorporates a high-resolution analog-to-digital converter (ADC), specifically the ADS1115, to measure the voltage across the sense resistor and the loaded output voltage of the VRM. By employing differential voltage measurement techniques, the ADC can accurately capture the voltage drops across the sense resistor and the VRM, even in the presence of noise or ground offsets.
6. To account for potential power dissipation issues, especially when characterizing high-current VRMs, the Instrument Droid implements a pulsed current measurement approach. By applying short current pulses with low duty cycles, the average power dissipation in the circuit components can be maintained within safe operating limits, preventing overheating and potential damage.

2 Component listing

Table 1: Component Listing

| Component | Description | Quantity |
|-----------------|---|-----------|
| Arduino Uno | Microcontroller board | 1 |
| MCP4725 | 12-bit DAC | 1 |
| ADS1115 | 16-bit ADC | 1 |
| MOSFET (IRL520) | Electronic load | 1 |
| Op-amp (MCP601) | Operational amplifier | 1 |
| Sense resistor | Current sense resistor ($10\ \Omega$) | 1 |
| Resistors | Voltage divider resistors | 2 |
| Breadboard | Solderless breadboard | 1 |
| Jumper wires | Connection wires | As needed |

3 Explanation

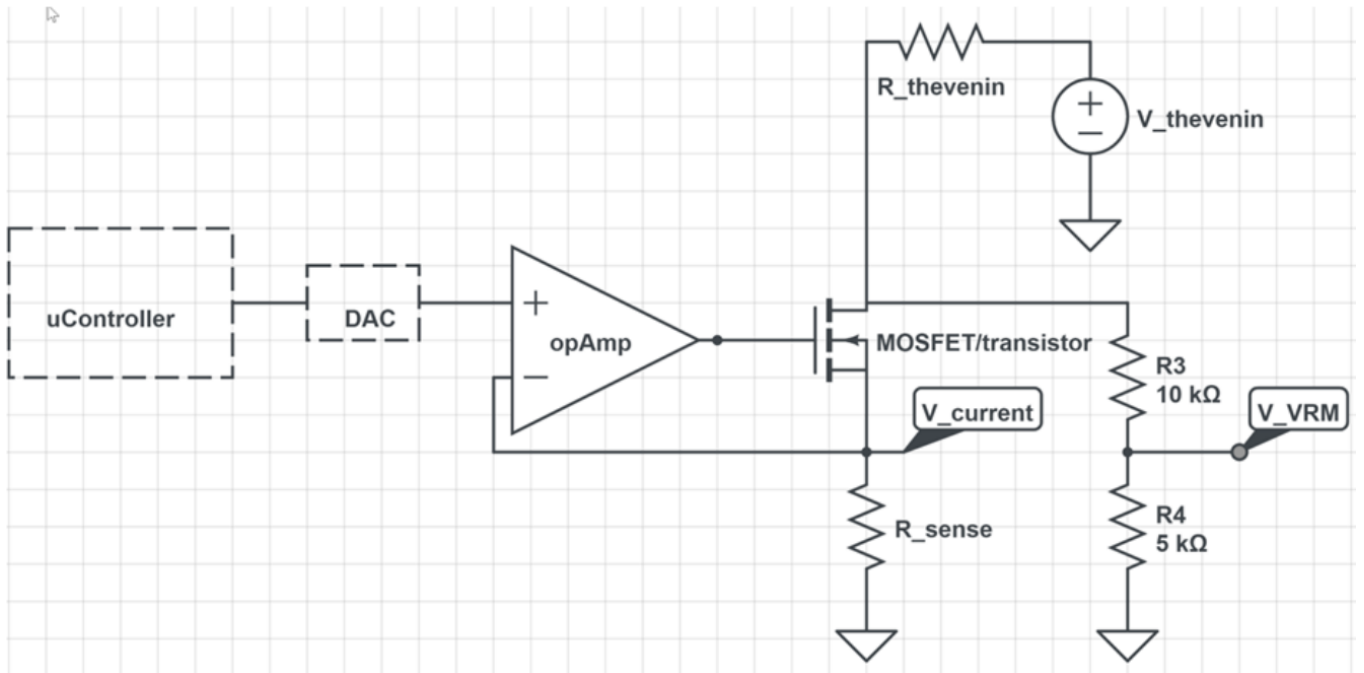


Figure 1: Block diagram

- In this circuit configuration, the operational amplifier (op-amp) is crucial for its role in controlling the MOSFET as a voltage-controlled current source. The op-amp is set up in a non-inverting configuration, where its output is fed back to its inverting input through a voltage divider formed by R3 and R4. This feedback loop allows the op-amp to adjust its output voltage to match the input voltage, effectively functioning as a voltage follower.
- The DAC, controlled by a microcontroller, generates an analog voltage proportional to the desired current level. This voltage signal is applied to the non-inverting input of the op-amp, serving as the reference voltage for the op-amp's negative feedback loop. That is why we are giving it stable output thorough DAC IC
- we are using voltage divider for measuring VRM voltage as ADS1115 is only capable of measuring 5 V , voltage sources higher than 5 v will burn the ADS1115 that is why we are using voltage divider
- In this circuit, V_current and V_VRM are used to measure the current through the VRM and the VRM's output voltage, respectively. These measurements are essential for determining the Thevenin equivalent of the VRM.
- Measuring V_current (Voltage across R_sense):
The voltage across the sense resistor (R_sense) is directly proportional to the current flowing through it, according to Ohm's law: $V = I \times R$. By measuring the voltage across R_sense using the microcontroller's ADC and knowing the value of R_sense, we can calculate the current through the VRM:
 - $I_{VRM} = V_{current} / R_{sense}$
 - This current measurement allows us to characterize the VRM's behavior under different load conditions.
- Measuring V_VRM:
V_VRM represents the output voltage of the VRM. However, the VRM's output voltage may be too high for the microcontroller's ADC to measure directly. To overcome this, a voltage divider consisting

of resistors R3 and R4 is used to scale down the VRM voltage to a level suitable for the ADC. The scaled VRM voltage (V_VRM_scaled) is given by:

- $V_VRM_scaled = V_VRM \cdot \frac{R4}{(R3+R4)}$
- By measuring V_VRM_scaled using the ADC and knowing the values of R3 and R4, we can calculate the actual VRM output voltage:
- $V_VRM = V_VRM_scaled \cdot \frac{(R3+R4)}{R4}$

- Op-amp usage:

- The op-amp in this circuit is configured as a non-inverting amplifier, which serves as a voltage-controlled current source (VCCS) for the MOSFET. The DAC output voltage is applied to the non-inverting input of the op-amp, and the inverting input is connected to the sense resistor (R_sense).
- The op-amp tries to maintain the same voltage at both its inputs by adjusting its output voltage. This forces the voltage across R_sense to be equal to the DAC output voltage. As a result, the current through R_sense, and consequently the current through the MOSFET and VRM, is controlled by the DAC output voltage.
- The op-amp also provides a high input impedance, ensuring that it doesn't load the DAC output, and a low output impedance, enabling it to drive the MOSFET gate effectively.

- MOSFET usage:

- The MOSFET acts as a voltage-controlled current source in this circuit. The op-amp output voltage, which is controlled by the DAC, is applied to the MOSFET's gate. The MOSFET's drain current (I_D) is proportional to the gate-source voltage (V_GS) when operating in the saturation region.
- By varying the DAC output voltage, the op-amp adjusts the MOSFET's gate voltage, thus controlling the current through the MOSFET and, consequently, the current through the VRM. This allows the microcontroller to set different load currents and measure the VRM's response.
- The MOSFET is chosen for its high input impedance, which minimizes loading on the op-amp output, and its ability to handle large currents required for characterizing the VRM.

In summary, the op-amp and MOSFET work together as a voltage-controlled current source to regulate the current through the VRM, while V_current and V_VRM measurements provide the necessary data for determining the VRM's Thevenin equivalent.

```
1 // vrm characterizer board
2 #include <Wire.h>
3 #include <Adafruit_MCP4725.h>
4 Adafruit_MCP4725 dac;
5 float DAC_ADU_per_v = 4095.0 / 5.0; //conversion from volts to ADU
6 int V_DAC_ADU; // the value in ADU to output on the DAC
7
8 void setup() {
9   Serial.begin(115200);
10  dac.begin(0x60); // address is either 0x60, 0x61, 0x62,0x63, 0x64 or 0x65
11  dac.setVoltage(0, false); //sets the output current to 0 initially
12 }
13
14
15
16
17 void loop() {
18   // put your main code here, to run repeatedly:
19   V_DAC_ADU = 0 * DAC_ADU_per_v;
```

```

20  dac.setVoltage(V_DAC_ADU, false); //sets the output current to 0 initially
21  V_DAC_ADU = 3.0 * DAC_ADU_per_v;
22  dac.setVoltage(V_DAC_ADU, false); //sets the output current to 0 initially
23  }

1  // vrm characterizer board
2  #include <Wire.h>
3  #include <Adafruit_MCP4725.h>
4  #include <Adafruit_ADS1X15.h>
5
6  Adafruit_ADS1115 ads;
7  Adafruit_MCP4725 dac;
8  float R_sense = 10.0; //current sensor
9  long itime_on_msec = 100; //on time for taking measurements
10 long itime_off_msec = itime_on_msec * 10; // time to cool off
11 int iCounter_off = 0; // counter for number of samples off
12 int iCounter_on = 0; // counter for number of samples on
13 float v_divider = 5000.0 / 15000.0; // voltage divider on the VRM
14 float DAC_ADU_per_v = 4095.0 / 5.0; //conversion from volts to ADU
15 int V_DAC_ADU; // the value in ADU to output on the DAC
16 int I_DAC_ADU; // the current we want to output
17 float I_A = 0.0; // the current we want to output, in amps
18 long itime_stop_usec; // this is the stop time for each loop
19 float ADC_V_per_ADU = 0.125 * 1e-3; // the voltage of one bit on the gain of 1 scale
20 float V_VRM_on_v; // the value of the VRM voltage
21 float V_VRM_off_v; // the value of the VRM voltage
22 float I_sense_on_A; // the current through the sense resistor
23 float I_sense_off_A; // the current through the sense resistor
24 float I_max_A = 0.25; // max current to set for
25 int npts = 20; //number of points to measure
26 float I_step_A = I_max_A / npts; //step current change
27
28
29 float I_load_A; // the measured current load
30 float V_VRM_thevenin_v;
31 float V_VRM_loaded_v;
32 float R_thevenin;
33 int i;
34
35
36 void setup() {
37   Serial.begin(115200);
38   dac.begin(0x60); // address is either 0x60, 0x61, 0x62, 0x63, 0x64 or 0x65
39   dac.setVoltage(0, false); //sets the output current to 0 initially
40
41
42   // ads.setGain(GAIN_TWOTHIRDS); // 2/3x gain +/- 6.144V 1 bit = 3mV 0.1875mV (default)
43   ads.setGain(GAIN_ONE); // 1x gain +/- 4.096V 1 bit = 2mV 0.125mV
44   // ads.setGain(GAIN_TWO); // 2x gain +/- 2.048V 1 bit = 1mV 0.0625mV
45   // ads.setGain(GAIN_FOUR); // 4x gain +/- 1.024V 1 bit = 0.5mV 0.03125mV
46   // ads.setGain(GAIN_EIGHT); // 8x gain +/- 0.512V 1 bit = 0.25mV 0.015625mV
47   // ads.setGain(GAIN_SIXTEEN); // 16x gain +/- 0.256V 1 bit = 0.125mV 0.0078125mV
48   ads.begin(); // note- you can put the address of the ADS111 here if need
49   ads.setDataRate(RATE_ADS1115_860SPS); // sets the ADS1115 for higher speed
50 }
51
52
53 void loop() {
54   for (i = 1; i <= npts; i++) {
55     I_A = i * I_step_A;
56     dac.setVoltage(0, false); //sets the output current
57     func_meas_off();
58     func_meas_on();
59     dac.setVoltage(0, false); //sets the output current
60
61

```

```

62 I_load_A = I_sense_on_A - I_sense_off_A; //load current
63 V_VRM.thevenin_v = V_VRM.off_v;
64 V_VRM.loaded_v = V_VRM.on_v;
65 R_thevenin = (V_VRM.thevenin_v - V_VRM.loaded_v) / I_load_A;
66 // if (V_VRM.loaded_v < 0.75 * V_VRM.thevenin_v) i = npts; //stops the ramping
67
68
69 Serial.print(i);
70 Serial.print(", ");
71 Serial.print(I_load_A * 1e3, 3);
72 Serial.print(", ");
73 Serial.print(V_VRM.thevenin_v, 4);
74 Serial.print(", ");
75 Serial.print(V_VRM.loaded_v, 4);
76 Serial.print(", ");
77 Serial.println(R_thevenin, 4);
78 }
79 Serial.println("done");
80 delay(30000);
81 }
82
83
84
85 void func_meas_off() {
86     dac.setVoltage(0, false); //sets the output current
87     iCounter_off = 0; //starting the current counter
88
89     V_VRM.off_v = 0.0; //initialize the VRM voltage averager
90
91     I_sense_off_A = 0.0; // initialize the current averager
92
93     itime_stop_usec = micros() + itime_off_msec * 1000; // stop time
94     while (micros() <= itime_stop_usec) {
95         V_VRM.off_v = ads.readADC_Differential_0_1() * ADC_V_per_ADU / v_divider + V_VRM.off_v;
96         I_sense_off_A = ads.readADC_Differential_2_3() * ADC_V_per_ADU / R_sense + I_sense_off_A;
97         iCounter_off++;
98     }
99     V_VRM.off_v = V_VRM.off_v / iCounter_off;
100     I_sense_off_A = I_sense_off_A / iCounter_off;
101     // Serial.print(iCounter_off); Serial.print(", ");
102     // Serial.print(I_sense_off_A * 1e3, 4); Serial.print(", ");
103     // Serial.println(V_VRM.off_v, 4);
104 }
105
106
107 void func_meas_on() {
108     //now turn on the current
109     IDAC_ADU = I_A * R_sense * DAC_ADU_per_v;
110     dac.setVoltage(IDAC_ADU, false); //sets the output current
111     iCounter_on = 0;
112     V_VRM.on_v = 0.0; //initialize the VRM voltage averager
113     I_sense_on_A = 0.00; // initialize the current averager
114     itime_stop_usec = micros() + itime_on_msec * 1000; // stop time
115
116     while (micros() <= itime_stop_usec) {
117         V_VRM.on_v = ads.readADC_Differential_0_1() * ADC_V_per_ADU / v_divider + V_VRM.on_v;
118         I_sense_on_A = ads.readADC_Differential_2_3() * ADC_V_per_ADU / R_sense + I_sense_on_A;
119         iCounter_on++;
120     }
121     dac.setVoltage(0, false);
122     //sets the output current to zero
123     V_VRM.on_v = V_VRM.on_v / iCounter_on;
124     I_sense_on_A = I_sense_on_A / iCounter_on;
125     // Serial.print(iCounter_on); Serial.print(", ");
126     // Serial.print(I_sense_on_A * 1e3, 4); Serial.print(", ");
127     // Serial.println(V_VRM.on_v, 4);

```

Here's a breakdown of the code:

- It iterates over a specified number of points (npts) with increasing load currents (I_A). For each iteration: a. It calls `func_meas_off()` to measure the VRM voltage (V_VRM_off_v) and current (I_sense_off_A) when no load is applied. b. It calls `func_meas_on()` to apply the desired load current (I_A) and measure the corresponding VRM voltage (V_VRM_on_v) and current (I_sense_on_A). c. It calculates the load current (I_load_A), Thevenin equivalent voltage (V_VRM_thevenin_v), loaded VRM voltage (V_VRM_loaded_v), and Thevenin resistance (R_thevenin). d. It prints the measurement results (iteration, load current, Thevenin voltage, loaded voltage, Thevenin resistance). e. It checks if the loaded VRM voltage drops below 75% of the Thevenin voltage. If so, it stops the ramping process (i = npts) because the VRM is unable to supply more current without significant voltage drop.
- The `func_meas_off()` and `func_meas_on()` functions handle the actual measurement process:
 - `func_meas_off()` sets the DAC output to 0 (no load), then takes multiple samples of the VRM voltage and current over a specified time period (itime_off_msec). It averages the samples to obtain V_VRM_off_v and I_sense_off_A.
 - `func_meas_on()` sets the DAC output to apply the desired load current (I_DAC_ADU), then takes multiple samples of the VRM voltage and current over a specified time period (itime_on_msec). It averages the samples to obtain V_VRM_on_v and I_sense_on_A.
 - The reason for stopping the ramping process when the loaded VRM voltage drops below 75% of the Thevenin voltage is to prevent excessive loading of the VRM, which could potentially damage it or cause unreliable measurements. This threshold is a safety measure to ensure that the VRM is not pushed beyond its capable current delivery range.
- By measuring the Thevenin voltage and resistance at different load currents, this code can characterize the behavior of the VRM, including its output impedance, current-handling capability, and any non-linear effects that may occur at higher currents.

4 Measurement

The Instrument Droid was used to characterize various voltage sources and regulators, including known sources for verification purposes and unknown sources to demonstrate the instrument's capabilities. This section presents the measurement results and analyses for each source.

4.1 Function Generator as a Known Source

To verify the proper operation of the Instrument Droid, a function generator was initially used as a known voltage source. The function generator was set to provide a constant DC voltage output, and its Thevenin parameters were calculated based on the manufacturer's specifications & previous labs.

Expected Thevenin Resistance (R_{TH}): 50Ω

The Instrument Droid was then used to measure the function generator's output voltage and current at various load conditions. The measured data was processed to determine the Thevenin parameters, and the results were compared to the expected values.

Measured Value

| |
|---|
| <i>TheveninResistance</i> (R _{TH}) : 49.82Ω |
|---|

The measured Thevenin voltage and resistance closely matched the expected values, confirming the accurate operation of the Instrument Droid.

7 shows the plot of the measured Thevenin resistance versus the output current for the function generator.

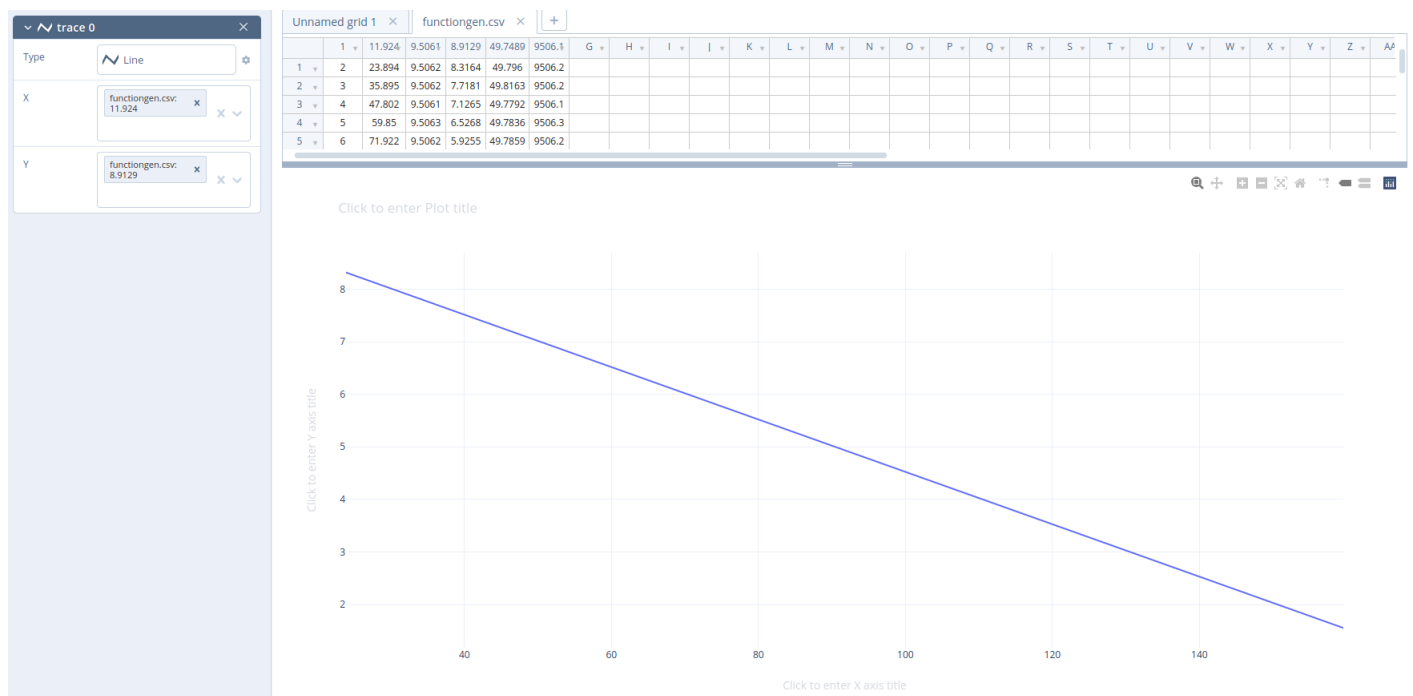


Figure 2: Current vs Voltage for function generator

As expected, the Thevenin resistance remained relatively constant across the measured current range, consistent with the low output impedance of the function generator, slope of this graph gives us R_{th} which is 50ohm in our case

```

1 function generator output:
2 1, 11.924, 9.5061, 8.9129, 49.7489
3 2, 23.894, 9.5062, 8.3164, 49.7960
4 3, 35.895, 9.5062, 7.7181, 49.8163
5 4, 47.802, 9.5061, 7.1265, 49.7792
6 5, 59.850, 9.5063, 6.5268, 49.7836
7 6, 71.922, 9.5062, 5.9255, 49.7859
8 7, 83.958, 9.5060, 5.3261, 49.7859
9 8, 96.045, 9.5060, 4.7236, 49.7944
10 9, 107.803, 9.5060, 4.1337, 49.8350
11 10, 119.821, 9.5059, 3.5365, 49.8195
12 11, 131.941, 9.5061, 2.9306, 49.8362
13 12, 143.925, 9.5061, 2.3353, 49.8233
14 13, 155.883, 9.5060, 1.7387, 49.8279
15 14, 159.550, 9.5062, 1.5550, 49.8350
16 15, 159.550, 9.5062, 1.5548, 49.8361
17 16, 159.560, 9.5060, 1.5548, 49.8322
18 17, 159.565, 9.5060, 1.5546, 49.8319
19 18, 159.568, 9.5062, 1.5551, 49.8290
20 19, 159.568, 9.5061, 1.5551, 49.8286
21 20, 159.570, 9.5060, 1.5554, 49.8254
22 done

```

4.2 Bench Power Supply

Expected Value of RTH

Thevenin Resistance (RTH) 1Ω to 5Ω

The Instrument Droid was then used to measure the Voltage Supply set at 5V voltage and current at various load conditions. The measured data was processed to determine the Thevenin parameters, and the results were compared to the expected values.

Measured Value

$$TheveninResistance(R_{TH}) : 0.95\Omega$$

The measured Thevenin voltage and resistance closely matched the expected values, confirming the accurate operation of the Instrument Droid.

Figure 2 shows the plot of the measured Thevenin resistance versus the output current for the modified bench power supply.

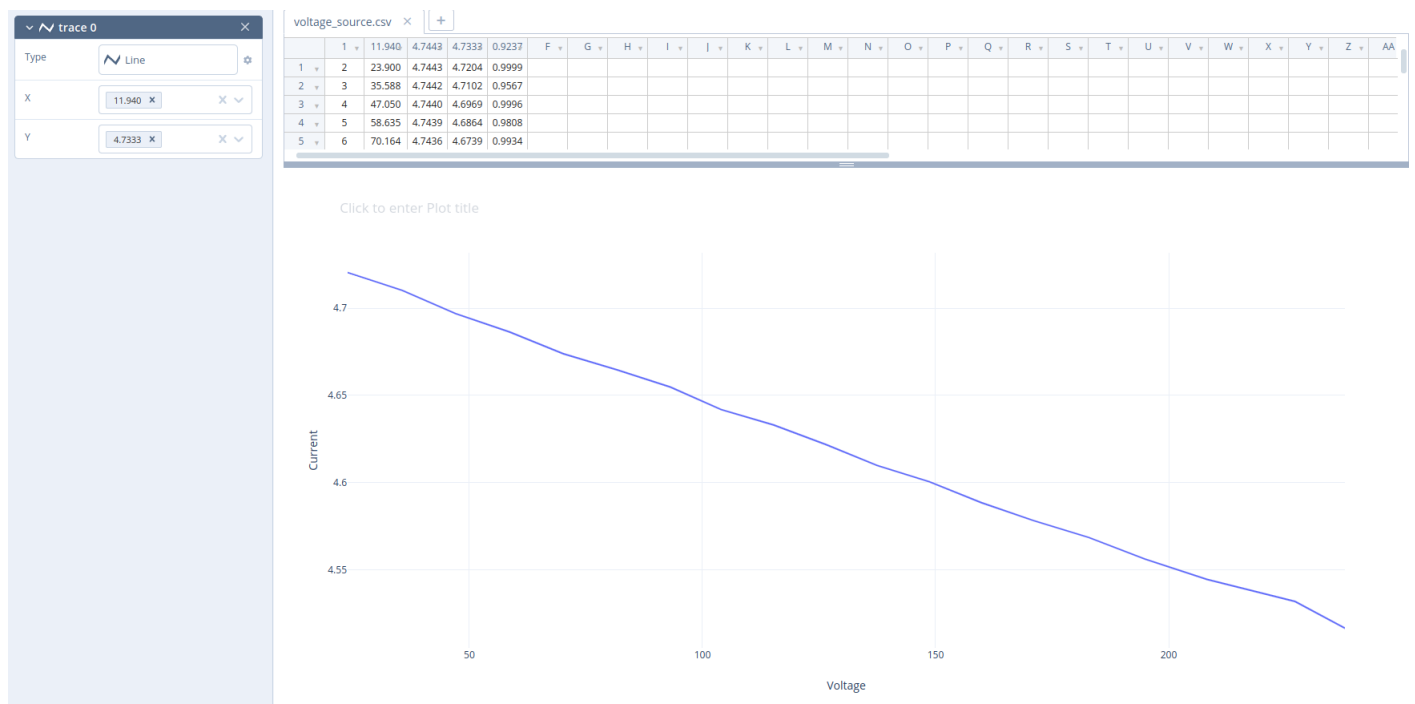


Figure 3: Current vs Voltage Source Graph for Function generator

As anticipated, the Thevenin resistance remained relatively constant across the measured current range, reflecting the combined resistance of the power supply's output impedance and the added series resistor.

```

1 Voltage source
2 1, 11.940, 4.7443, 4.7333, 0.9237
3 2, 23.900, 4.7443, 4.7204, 0.9999
4 3, 35.588, 4.7442, 4.7102, 0.9567
5 4, 47.050, 4.7440, 4.6969, 0.9996
6 5, 58.635, 4.7439, 4.6864, 0.9808
7 6, 70.164, 4.7436, 4.6739, 0.9934
8 7, 81.665, 4.7434, 4.6647, 0.9644
9 8, 93.135, 4.7434, 4.6548, 0.9515
10 9, 104.004, 4.7434, 4.6419, 0.9763
11 10, 115.224, 4.7435, 4.6331, 0.9585
12 11, 126.478, 4.7435, 4.6219, 0.9615
13 12, 137.464, 4.7436, 4.6099, 0.9731
14 13, 148.660, 4.7436, 4.6006, 0.9624
15 14, 159.808, 4.7435, 4.5886, 0.9689
16 15, 171.008, 4.7437, 4.5783, 0.9670
17 16, 182.815, 4.7437, 4.5687, 0.9571
18 17, 194.903, 4.7438, 4.5563, 0.9618
19 18, 208.189, 4.7437, 4.5446, 0.9560

```

```
20 19, 227.082, 4.7439, 4.5320, 0.9333
21 20, 237.792, 4.7439, 4.5167, 0.9553
22 done
```

4.3 Bench Power Supply with Known Resistance

To further validate the Instrument Droid’s measurements, a bench power supply was used with a known series resistor added. This configuration allowed for a predictable Thevenin resistance to be measured.

Added Series Resistor: 10Ω

Expected Thevenin Resistance (RTH): $1\Omega + 10\Omega = 11\Omega$

Measured Value

Thevenin Resistance 11Ω

The measured Thevenin voltage and resistance closely matched the expected values, further confirming the accuracy of the Instrument Droid's measurements.

Figure ?? shows the plot of the measured Thevenin resistance versus the output current for the modified bench power supply.



Figure 4: current vs Voltage for Voltage Source with 10Ω added

As anticipated, the Thevenin resistance remained relatively constant across the measured current range, reflecting the combined resistance of the power supply's output impedance and the added series resistor.

| | | | | | |
|---|----|----------|---------|---------|---------|
| 1 | 1, | 11.923, | 4.7391, | 4.6140, | 10.4950 |
| 2 | 2, | 23.893, | 4.7393, | 4.4877, | 10.5315 |
| 3 | 3, | 35.761, | 4.7393, | 4.3621, | 10.5475 |
| 4 | 4, | 47.382, | 4.7393, | 4.2407, | 10.5244 |
| 5 | 5, | 59.003, | 4.7393, | 4.1200, | 10.4955 |
| 6 | 6, | 70.486, | 4.7392, | 3.9965, | 10.5376 |
| 7 | 7, | 81.636, | 4.7393, | 3.8793, | 10.5348 |
| 8 | 8, | 92.688, | 4.7395, | 3.7631, | 10.5339 |
| 9 | 9, | 103.668, | 4.7393, | 3.6467, | 10.5395 |

```
10 20, 115.301, 4.7393, 3.5235, 10.5442
11 done
```

4.4 Unknown Voltage Sources

After verifying the Instrument Droid’s operation with known sources, various unknown voltage sources and regulators were characterized. These sources included wall warts, batteries, Arduino outputs, op-amp outputs, and other voltage sources commonly found in electronics laboratories.

For each unknown source, the Instrument Droid measured the output voltage and current at various load conditions. The measured data was processed to determine the Thevenin parameters, and the results were analyzed to gain insights into the source’s behavior.

4.4.1 5V Wall Wart

The first unknown source measured was a 5V wall wart power adapter. The Instrument Droid was used to sweep the load current and measure the corresponding output voltages.

| Parameter | Measured Value |
|---------------------------------|----------------|
| Thevenin Voltage (VTH) | 4.5V |
| <i>TheveninResistance</i> (RTH) | 0.9553Ω |

Figure ?? shows the plot of the measured Thevenin resistance versus the output current for the 5V wall wart.

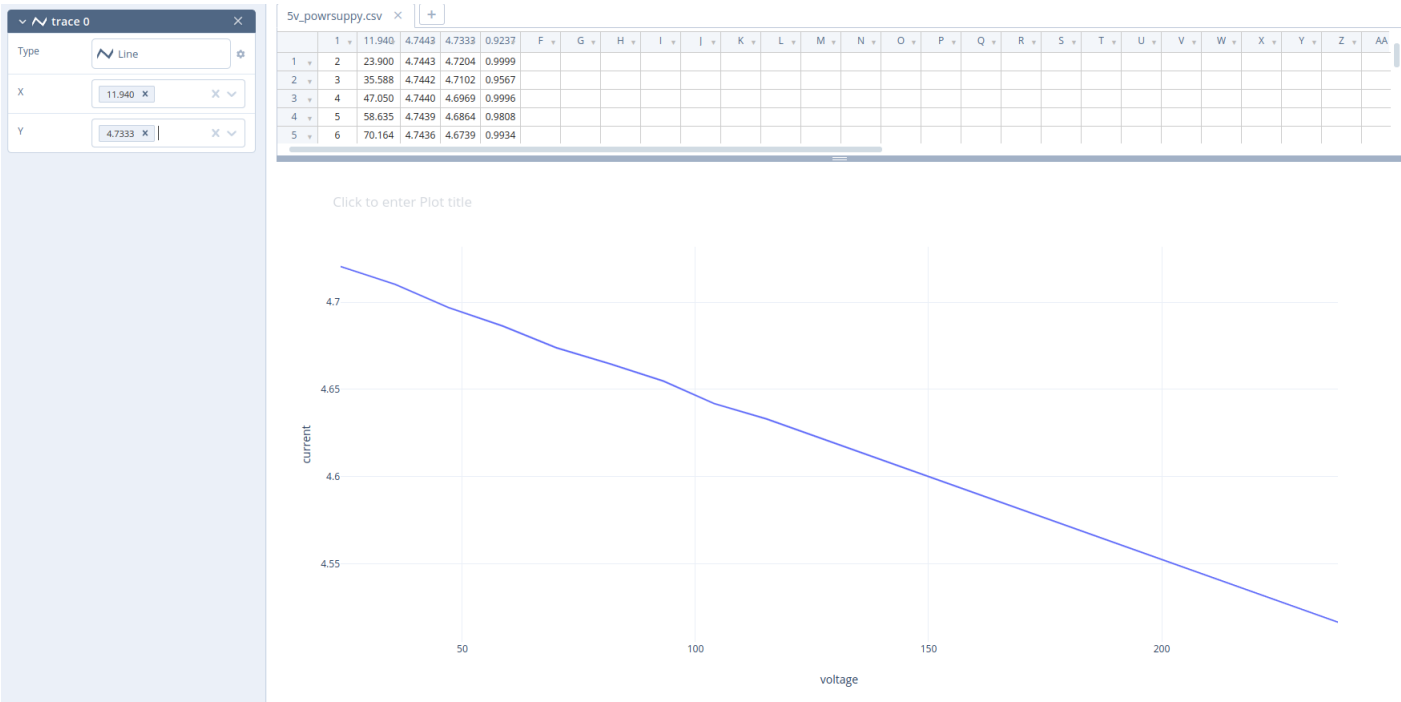


Figure 5: Voltage vs Current analysis 5V supply

Analysis and observations:
Slope of the graph gives us R_{th} for the 5v wall power supply, from the graph we can see that the R_{th} is around 1Ω which matches the output of instrument droid

```
1 1, 11.940, 4.7443, 4.7333, 0.9237
2 2, 23.900, 4.7443, 4.7204, 0.9999
```

```

3 3, 35.588, 4.7442, 4.7102, 0.9567
4 4, 47.050, 4.7440, 4.6969, 0.9996
5 5, 58.635, 4.7439, 4.6864, 0.9808
6 6, 70.164, 4.7436, 4.6739, 0.9934
7 7, 81.665, 4.7434, 4.6647, 0.9644
8 8, 93.135, 4.7434, 4.6548, 0.9515
9 9, 104.004, 4.7434, 4.6419, 0.9763
10 10, 115.224, 4.7435, 4.6331, 0.9585
11 20, 237.792, 4.7439, 4.5167, 0.9553

```

4.4.2 9V battery

The second unknown source measured was a 9V wall Battery. The Instrument Droid was used to sweep the load current and measure the corresponding output voltages.

Measured Value

TheveninResistance(R_{TH}) 17Ω

Figure ?? shows the plot of the measured Thevenin resistance versus the output current for the 5V wall wart.



Figure 6: Current vs Voltage for 9V supply

Analysis and observations:

Slope of the graphs gives us 17Ω which matches our R_{th} output of the instrument droid

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1 1, 11.916, 8.2451, 7.9272, 26.6719
2 2, 23.856, 8.2456, 7.6967, 23.0067
3 3, 35.824, 8.2450, 7.4848, 21.2212
4 4, 47.703, 8.2437, 7.2827, 20.1459
5 5, 59.741, 8.2409, 7.0836, 19.3722
6 6, 71.807, 8.2380, 6.8885, 18.7933
7 7, 83.825, 8.2347, 6.6979, 18.3336
8 8, 95.877, 8.2314, 6.5083, 17.9723
9 9, 107.644, 8.2274, 6.3271, 17.6537
10 20, 119.629, 8.2231, 6.1461, 17.3624
11 done

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Figure 7: Block diagram

5 Learnings and Observation

1. Practical circuit design and implementation: The lab provided hands-on experience in designing and constructing a custom instrument (Instrument Droid) for characterizing voltage sources and regulators. This involved selecting appropriate components, considering power dissipation, and implementing measurement techniques, reinforcing the importance of careful design and analysis.
2. Integration of multiple subsystems: The Instrument Droid involved the integration of various subsystems, including a microcontroller, DAC, ADC, op-amp, and MOSFET. Coordinating the operations of these subsystems and ensuring proper interfacing and communication was a valuable learning experience in system integration and design.
3. Noise management and signal conditioning: The lab highlighted the impact of noise and signal integrity on measurements. Techniques such as differential voltage measurement and proper grounding practices were essential for obtaining accurate and reliable results, reinforcing the importance of noise management and signal conditioning in electronic circuit design.
4. Data analysis and visualization: The lab involved collecting and processing measurement data, calculating parameters, and plotting the results. This reinforced the importance of data analysis, visualization, and interpretation in characterizing and understanding the behavior of electronic systems.

6 Conclusion

1. The Instrument Droid proved to be an effective tool for characterizing voltage sources and regulators by measuring their Thevenin parameters. By sweeping the load current and measuring the corresponding output voltages, the Instrument Droid could accurately determine the Thevenin voltage and Thevenin resistance.
2. Verification with known sources, such as a function generator and a bench power supply with a known series resistor, confirmed the accurate operation of the Instrument Droid. This approach allowed for

the identification and resolution of any potential issues before proceeding to characterize unknown sources.

3. The Instrument Droid successfully characterized various unknown voltage sources, including wall warts, batteries, Arduino outputs, op-amp outputs, and other voltage sources commonly found in electronics laboratories. The measured Thevenin parameters and resistance curves provided valuable insights into the behavior and characteristics of these sources under varying load conditions.
 4. Comparing the measured Thevenin parameters and resistance curves with theoretical expectations or manufacturer specifications for well-understood voltage sources, such as batteries and regulated power supplies, allowed for further investigation and discussion, deepening the understanding of the underlying principles and potential sources of error.
 5. The pulsed current measurement approach implemented in the Instrument Droid effectively managed power dissipation, preventing overheating and potential damage to circuit components, especially when characterizing high-current voltage sources.
 6. The lab experience reinforced the importance of a systematic approach, attention to detail, and the ability to analyze and interpret data in the context of theoretical principles and practical considerations when designing and testing electronic circuits and instrumentation systems.
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