

Gravity Gradient Stabilization

Sam Schreiner

$$B\ddot{\theta} + 3n^2(A-C)\theta = 0$$

$$A\ddot{\psi} + (B-A-C)n\dot{\phi} + 4n^2(B-C)\psi = 0$$

$$C\ddot{\phi} + (A+C-B)n\dot{\psi} + n^2(B-A)\phi = 0$$

Frame:

$$\bar{I}Z = \begin{bmatrix} n\gamma_{yaw} \\ n \\ n\gamma_{roll} \end{bmatrix}$$

$$K_y = \frac{I_p - I_R}{I_y} \quad || \quad K_R = \frac{I_p - I_y}{I_R}$$

Stability: $I_R > I_y$ $(1 + 3K_R + K_R K_y) > 4\sqrt{K_R K_y}$
 $(K_R > K_y)$ $K_R K_y > 0$

* For nadir-pointing satellite, region II is good.

$$w_{pitch} = n \sqrt{3 \frac{(I_R - I_y)}{I_p}}$$

$$b = (1 + 3K_R + K_R K_y) \text{ and } c = (4K_R K_y)$$

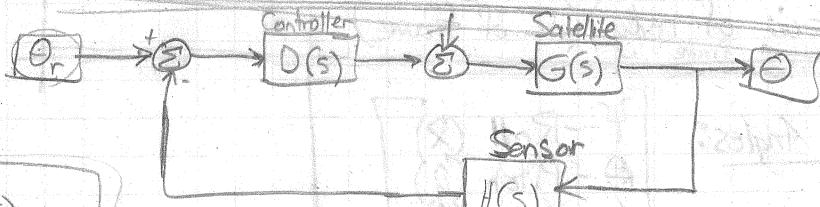
$$w_{yaw/roll} = n \sqrt{\frac{1}{2}(b \pm \sqrt{b^2 - 4c})}$$

Debra-Depp ($I_R > I_y > I_p$)

w off?

$$w = \frac{2\pi}{T}$$

Control Systems:



$$\frac{\theta}{\theta_r} = \frac{D(s)G(s)}{1 + H(s)D(s)G(s)}$$

Root Locus Plots the zeros of $[1 + H(s)D(s)G(s)] = 0$ as K changes

PID Controllers:

$$D(s) = \left\{ K_I \frac{1}{s} + K_P + K_D s \right\} = K_S \left\{ \frac{(s-z_1)(s-z_2)}{s} \right\}$$

$$K_D = K_S; K_I/K_D = z_1 z_2; K_P/K_D = -(z_1 + z_2)$$

$$L(s) = K_S \frac{(s-z_1)(s-z_2)}{s^3}$$

(w/ $H(s)=1$) $\Rightarrow G(s) = \frac{1}{s^3}$

Laplace Transforms

$f(t)$	$F(s)$
1	$1/s$
$\sin(at)$	$a/(s^2 + a^2)$
$\cos(at)$	$s/(s^2 + a^2)$
Unit Step @ $t=0$	$1/s$
$t^n e^{-at}$	$\frac{n!}{(s+a)^{n+1}}$
e^{-at}	$\frac{1}{s+a}$

Basics

$$\ddot{\vec{r}}_g = \ddot{\vec{r}}_o + \ddot{\vec{r}}_{rel} + 2\vec{\omega}_o \times \vec{v}_{rel} + \vec{\omega}_o \times \vec{r}_{rel} + \vec{\omega}_o \times (\vec{\omega}_o \times \vec{r}_{rel})$$

rel: in the ~~non~~ non-inertial coordinate system

$\ddot{\vec{r}}_o$: acceleration of origin of non-I coord in inertial coord
rotation

$$I = \begin{bmatrix} y^2+z^2 & -xy & -xz \\ -xy & x^2+z^2 & -yz \\ -xz & -yz & x^2+y^2 \end{bmatrix} dm$$

M

$$\vec{M} = \vec{H}_G = \frac{d\vec{H}_G}{dt}_{rel} + \vec{\omega}_{frame} \times \vec{H}_{G, rel} \quad \vec{H}_G = [I]\vec{\omega}$$

$$T_{rot} = \frac{1}{2} \vec{\omega} \cdot \vec{H}_G$$

$$\begin{cases} mK_x^2 = A \\ mK_y^2 = B \\ mK_z^2 = C \end{cases} \quad \left. \begin{array}{l} \\ \\ \end{array} \right\} \text{Radius of Gyration}$$

$$\vec{M} = \begin{bmatrix} Ax_x + C\Omega_y w_z - B\Omega_z w_y \\ Bw_y + A\Omega_z w_x - C\Omega_x w_z \\ Cw_z + B\Omega_x w_y - A\Omega_y w_x \end{bmatrix} = \begin{bmatrix} Aw_{ox} + (C-B)w_y w_z \\ Bw_{oy} + (A-C)w_x w_z \\ Cw_{oz} + (B-A)w_x w_y \end{bmatrix}$$

($\alpha = \dot{\omega}$ of body)
in frame (Ω of frame)

Euler Angles:

ψ - Roll (x)
θ - Pitch (y)
ϕ - Yaw (z)

$$R_1 = \begin{bmatrix} 1 & 0 & 0 \\ 0 & \cos\psi & \sin\psi \\ 0 & -\sin\psi & \cos\psi \end{bmatrix} \quad R_2 = \begin{bmatrix} \cos\theta & 0 & -\sin\theta \\ 0 & 1 & 0 \\ \sin\theta & 0 & \cos\theta \end{bmatrix} \quad R_3 = \begin{bmatrix} \cos\phi & \sin\phi & 0 \\ -\sin\phi & \cos\phi & 0 \\ 0 & 0 & 1 \end{bmatrix}$$

Direction-Cosine Matrix: $[b] = [Q_{lb}] [L]$

For 2-1-2-1

$$[Q_{lb}] = [R_1(\psi)] [R_2(\theta)] [R_3(\phi)] = \begin{bmatrix} \cos\phi \cos\theta & \sin\phi \cos\theta & -\sin\theta \\ \cos\phi \sin\theta & \sin\phi \sin\theta & \cos\theta \\ -\sin\phi & \cos\phi & 0 \end{bmatrix}$$

For 3-2-1

$$\begin{bmatrix} \dot{\phi} \\ \dot{\theta} \\ \dot{\psi} \end{bmatrix} = \begin{bmatrix} 0 & \frac{\sin\theta}{\cos\theta} & \frac{\cos\theta}{\cos\theta} \\ 0 & \cos\theta & -\sin\theta \\ 1 & \sin\theta/\cos\theta & \cos\theta/\cos\theta \end{bmatrix} \begin{bmatrix} \dot{w}_x \\ \dot{w}_y \\ \dot{w}_z \end{bmatrix}$$

3-2-1

$$3+3: \begin{bmatrix} -\sin\phi \cos\theta \sin\psi + \cos\phi \cos\psi & \cos\phi \cos\theta \sin\psi + \sin\phi \cos\psi & \sin\theta \sin\psi \\ \cos\phi \cos\theta \sin\psi - \sin\phi \cos\psi & -\sin\phi \cos\theta \cos\psi - \cos\phi \sin\psi & \cos\theta \sin\psi \\ \sin\phi \sin\theta & -\cos\phi \sin\theta & \cos\theta \end{bmatrix}$$

$$\vec{q} = \begin{bmatrix} \sin\theta/2 \cdot u_1 \\ \sin\theta/2 \cdot u_2 \\ \sin\theta/2 \cdot u_3 \\ \cos\theta/2 \end{bmatrix}$$

$$[Q_{lb}] = \begin{bmatrix} q_1^2 q_2^2 q_3^2 q_4^2 & 2(q_1 q_2 + q_3 q_4) & 2(q_1 q_3 - q_2 q_4) \\ 2(q_1 q_2 - q_3 q_4) & q_1^2 q_2^2 q_3^2 q_4^2 & 2(q_1 q_2 + q_3 q_4) \\ 2(q_1 q_3 + q_2 q_4) & 2(q_1 q_2 - q_3 q_4) & q_1^2 q_2^2 q_3^2 q_4^2 \end{bmatrix}$$

$$\frac{\partial \vec{q}}{\partial t} = \frac{1}{2} \begin{bmatrix} 0 & w_z & -w_y & w_x \\ w_x & 0 & w_y & -w_z \\ -w_y & -w_z & 0 & w_x \\ w_z & w_y & -w_x & 0 \end{bmatrix} \cdot \vec{q}_{rel}$$

$$q_1 = \frac{Q_{23} - Q_{33}}{4q_4} \quad q_2 = \frac{Q_{31} - Q_{13}}{4q_4} \quad q_3 = \frac{Q_{12} - Q_{21}}{4q_{11}} \quad q_4 = \frac{1}{2} [1 + Q_{11} + Q_{22} + Q_{33}]$$

LLH Coord: $x: \text{along velocity}$
 $y: \perp \text{to orbital plane}$
 $z: \text{nadir}$

Spacecraft Attitude Dynamics & Control

$$\bar{\alpha}_p = \bar{\alpha}_p + \bar{\alpha}_{p,\text{rel}} + 2\bar{\omega} \times \bar{r}_{p,\text{rel}} + \bar{\omega} \times \bar{r}_{p,\text{rel}} + \bar{\omega} \times (\bar{\omega} \times \bar{r}_{p,\text{rel}})$$

Transport Theorem:

$$\bar{M} = \dot{\bar{H}}_G = \frac{d\bar{H}_G}{dt}_{\text{rel}} + \sum_{\text{force}} \times \bar{H}_{G,\text{rel}}$$

$$\bar{M}_G = \dot{\bar{H}}_G$$

$$\bar{H}_G = [I] \bar{\omega}$$

$$\bar{M} = \begin{bmatrix} Ax_x + (C-B)w_z w_y \\ Bw_y + (A-C)w_x w_z \\ Cw_z + (B-A)w_x w_y \end{bmatrix}$$

$$I = \begin{bmatrix} y^2 + z^2 & -xy & -xz \\ -xy & x^2 + z^2 & -yz \\ -xz & -yz & x^2 + y^2 \end{bmatrix} dm$$

LLH Coordinate Frame:

x : along velocity
 y : \perp to orbital plane
 z : Nadir

$$\bar{M} = \begin{bmatrix} A\Omega_x + C\Omega_y w_z - B\Omega_z w_y \\ B\Omega_y + A\Omega_z w_x - C\Omega_x w_z \\ C\Omega_z + B\Omega_y w_x - A\Omega_x w_y \end{bmatrix}$$

$$T_{\text{tot}} = \frac{1}{2} \bar{\omega} \cdot \bar{H}_G$$

$$mk_x^2 = A$$

$$mk_y^2 = B$$

$$mk_z^2 = C$$

"Radius of gyration"

Euler Angles:

ψ : Roll (\hat{x})

vectors in b

vectors in L

θ : Pitch (\hat{y})

$$[b] = [Q_{Lb}] [L]$$

$$[Q_{Lb}] = \begin{bmatrix} 0 & w_3 - w_2 \\ w_3 & 0 & w_1 \\ w_2 & -w_1 & 0 \end{bmatrix} [Q_{lb}]$$

ϕ : Yaw (\hat{z})

$$R_3(\phi) = \begin{bmatrix} \cos \phi & \sin \phi & 0 \\ -\sin \phi & \cos \phi & 0 \\ 0 & 0 & 1 \end{bmatrix}$$

$$\phi = \tan^{-1} \left(\frac{Q_{12}}{Q_{11}} \right)$$

$$\theta = -\sin^{-1} (Q_{13}) \quad 3-2-1$$

$$\psi = \tan^{-1} \left(\frac{Q_{23}}{Q_{33}} \right)$$

For
3-2-1

$$[Q_{Lb}] = [R_1(\psi)] [R(\theta)] [R_3(\phi)] = \begin{bmatrix} \cos \theta \cos \psi & \sin \theta \cos \psi & -\sin \psi \\ \cos \theta \sin \psi & \sin \theta \sin \psi & \cos \psi \\ -\sin \theta & \cos \theta & 0 \end{bmatrix} \quad 3-2-1$$

For
3-2-1

$$\begin{bmatrix} \dot{\phi} \\ \dot{\theta} \\ \dot{\psi} \end{bmatrix} = \begin{bmatrix} 0 & \frac{\sin \psi}{\cos \theta} & \frac{\cos \psi}{\cos \theta} \\ 0 & \cos^2 \psi & -\sin \psi \\ 1 & \sin \theta \tan \psi & \cos \theta \tan \psi \end{bmatrix} \begin{bmatrix} w_x \\ w_y \\ w_z \end{bmatrix} \quad 3-1-3$$

$$\bar{q} = \begin{bmatrix} \sin \theta_1 \cdot u_1 \\ \sin \theta_2 \cdot u_2 \\ \sin \theta_3 \cdot u_3 \\ \cos \theta_2 \end{bmatrix} = \begin{bmatrix} q_1 \\ q_2 \\ q_3 \\ q_4 \end{bmatrix} \quad [\Omega_b] = \begin{bmatrix} q_1^2 - q_2^2 - q_3^2 + q_4^2 & 2(q_1 q_2 + q_3 q_4) & 2(q_1 q_2 - q_3 q_4) \\ 2(q_1 q_2 - q_3 q_4) & q_1^2 + q_2^2 - q_3^2 + q_4^2 & 2(q_2 q_3 + q_1 q_4) \\ 2(q_1 q_3 + q_2 q_4) & 2(q_2 q_3 - q_1 q_4) & q_1^2 - q_2^2 + q_3^2 + q_4^2 \end{bmatrix}$$

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$$q_1 = \frac{\Omega_{23} - \Omega_{32}}{4q_4} \quad q_2 = \frac{\Omega_{31} - \Omega_{13}}{4q_4} \quad q_3 = \frac{\Omega_{12} - \Omega_{21}}{4q_4} \quad q_4 = \frac{1}{2} \sqrt{1 + \Omega_{11} + \Omega_{22} + \Omega_{33}}$$

$$\frac{\partial \bar{q}}{\partial t} = \frac{1}{2} [S \bar{q}] \Rightarrow [\Omega] = \begin{bmatrix} 0 & w_z & -w_y & w_x \\ -w_z & 0 & w_x & w_y \\ w_y & -w_x & 0 & w_z \\ -w_x & -w_y & -w_z & 0 \end{bmatrix}_{\text{rel}} \quad w: \text{in body frame}$$

Star Trackers: We have $\bar{r}_1^L, \bar{r}_2^L, \bar{r}_1^B, \bar{r}_2^B$

$$[Q_{bL}] = [L][b]^{-1}$$

$$[L] = \begin{bmatrix} \bar{r}_1^L & \bar{r}_2^L & \bar{r}_1^B & \bar{r}_2^B \end{bmatrix}; \quad [b] = \begin{bmatrix} \text{some} \end{bmatrix}; \quad [L] = [Q_{bL}] [b]$$

Dual Spinners: $\frac{\partial}{\partial t}(\omega_\perp^2) = \frac{2I}{A_\perp} \left[\bar{T}_P + \frac{Cr}{Cr - A_\perp} \bar{T}_r \right] \Rightarrow Cr > A_\perp : \underline{\text{unconditionally stable}}$

Momentum Wheels: $M_1 = Aw_1 + (C-B)w_2w_3 + [(I+2J)w_1] + I[w_{\text{rel}}^{(1)} - w_{\text{rel}}^{(2)}w_3 + w_{\text{rel}}^{(3)}w_2]$
 $w_{\text{rel}}^{(i)} = \text{relative spin of } i\text{th wheel in its own local frame}$
 $M_2 = Bw_2 + (A-C)w_1w_3 + [(I+2J)w_2] + I[w_{\text{rel}}^{(2)} - w_{\text{rel}}^{(3)}w_1 + w_{\text{rel}}^{(1)}w_3]$
 $M_3 = Cw_3 + (B-A)w_1w_2 + [(I+2J)w_3] + I[w_{\text{rel}}^{(3)} - w_{\text{rel}}^{(1)}w_2 + w_{\text{rel}}^{(2)}w_1]$

Yo-Yo Despin: tangential release: $\ell_f = R \sqrt{K \frac{(w_0 - w_f)}{(w_0 w_f)}}$ $\Delta t = \frac{\Delta \ell}{R w_f}$
 $K = 1 + \frac{C}{2mR^2}$
radial release: $\ell_f = R \sqrt{K - 1} \quad (w_f = 0)$