

APPENDIX A
CONTROLLABILITY OF THE LINEARIZED VSG MODEL
Consider the linearized VSG model

$$\Delta \dot{\mathbf{x}} = \mathbf{A}\Delta \mathbf{x} + \mathbf{B}\Delta \mathbf{u}, \quad \Delta \mathbf{x} \in \mathbb{R}^5, \Delta \mathbf{u} \in \mathbb{R}^2, \quad (1)$$

with the shorthand parameters $a := D_p K_p$, $b := K_p k_{pv}$, $c := K_p k_{p\delta}$, $d := D_q K_q$, $e := D_q K_q + K_q k_{qv}$, $f := K_q k_{q\delta}$, and system matrices

$$\mathbf{A} = \begin{bmatrix} 0 & 0 & a & b & c \\ 0 & 0 & d & e & f \\ 0 & 0 & 0 & 0 & 0 \\ 0 & 0 & 0 & 0 & 0 \\ 0 & 0 & 1 & 0 & 0 \end{bmatrix}, \quad \mathbf{B} = \begin{bmatrix} 1 & 0 \\ 0 & 1 \\ 1 & 0 \\ 0 & 1 \\ 0 & 0 \end{bmatrix}, \quad (2)$$

It is clear that $\mathbf{A}^3 = 0$, hence the controllability matrix

$$\mathbf{C} = [\mathbf{B} \quad \mathbf{AB} \quad \mathbf{A}^2\mathbf{B}]$$

is sufficient to decide controllability. Direct multiplication gives

$$\mathbf{AB} = \begin{bmatrix} a & b \\ d & e \\ 0 & 0 \\ 0 & 0 \\ 1 & 0 \end{bmatrix}, \quad \mathbf{A}^2\mathbf{B} = \begin{bmatrix} c & 0 \\ f & 0 \\ 0 & 0 \\ 0 & 0 \\ 0 & 0 \end{bmatrix},$$

Therefore

$$\mathbf{C} = \begin{bmatrix} 1 & 0 & a & b & c & 0 \\ 0 & 1 & d & e & f & 0 \\ 1 & 0 & 0 & 0 & 0 & 0 \\ 0 & 1 & 0 & 0 & 0 & 0 \\ 0 & 0 & 1 & 0 & 0 & 0 \end{bmatrix}, \quad (3)$$

Among all 5×5 minors of \mathbf{C} , the only nonzero one is the minor constructed from the first five columns:

$$\det(\mathbf{C}) = \det \begin{bmatrix} 1 & 0 & a & b & c \\ 0 & 1 & d & e & f \\ 1 & 0 & 0 & 0 & 0 \\ 0 & 1 & 0 & 0 & 0 \\ 0 & 0 & 1 & 0 & 0 \end{bmatrix} = bf - ce, \quad (4)$$

Hence $\text{rank } \mathbf{C} = 5$ if and only if $bf - ce \neq 0$, which is the necessary and sufficient condition for controllability. Writing this condition back in the original parameters yields

$$bf - ce = K_p K_q (k_{pv} k_{q\delta} - k_{p\delta} (D_q + k_{qv})) \neq 0, \quad (5)$$

In particular, when $K_p, K_q \neq 0$, the model is controllable iff

$$k_{pv} k_{q\delta} \neq k_{p\delta} (D_q + k_{qv}), \quad (6)$$

Using the small-signal coefficients from (??), (??), (??), and (??) with $D > 0$, all factors $1/D$ cancel in (6). For $k_{p\delta} \neq 0$, (6) is equivalent to

$$D_q \neq D_q^* \triangleq \frac{k_{pv} k_{q\delta}}{k_{p\delta}} - k_{qv}, \quad (7)$$

After substitution and simplification,

$$D_q^* = \frac{(R_g^2 + X_g^2) (V_g - 2V_0 \cos \delta_0)}{R_g \sin \delta_0 + X_g \cos \delta_0}, \quad (8)$$

Writing $Z_g \triangleq \sqrt{R_g^2 + X_g^2}$ and $\theta_g \triangleq \text{atan2}(X_g, R_g)$, note that $R_g \sin \delta_0 + X_g \cos \delta_0 = Z_g \sin(\delta_0 + \theta_g)$, hence

$$D_q^* = Z_g \frac{V_g - 2V_0 \cos \delta_0}{\sin(\delta_0 + \theta_g)}, \quad (9)$$

If $k_{p\delta} = 0$: (6) reduces to $k_{pv} k_{q\delta} \neq 0$ with $k_{q\delta}$ is always nonzero as long as the network impedance is not zero. Therefore the remaining condition is simply $k_{pv} \neq 0$ and is equivalent to $2R_g V_0 \neq \pm Z_g V_g$ [Cite documents](#). This condition is unlikely to occur in usual operating conditions.

If $k_{p\delta} \neq 0$:

- If δ_0 approaches $-\theta_g$, $\sin(\delta_0 + \theta_g) \rightarrow 0$ and $|D_q^*|$ blows up: controllability then holds for any practical finite D_q .
- In typical operation $V_g \approx V_0$ and δ_0 small, so $V_g - 2V_0 \cos \delta_0 < 0$. With standard $D_q > 0$, the inequality $D_q \neq D_q^*$ is automatically satisfied.

Therefore, (??) is always controllable if $2R_g V_0 \neq \pm Z_g V_g$.