

## Appendix

### An $O(1)$ Orientation Comparison Metric: The RMSD Between Two Orientations of a Rigid Body.

This section describes a method to calculate the sum-squared-distance between the positions of a rigid set of  $N$  points after being rotated and translated in two different ways (the rotations and translations are denoted  $R, \vec{T}$  and  $R', \vec{T}'$ ).

Definition: metric,  $\Phi$

$$\Phi(R, \vec{T}, R', \vec{T}') = \sum_{\alpha=1}^N |(Rx_{\alpha}^{\vec{}} + \vec{T}) - (R'x_{\alpha}^{\vec{}} + \vec{T}')|^2 \quad (1)$$

where  $x_{\alpha}^{\vec{}}$  = the position of the  $\alpha$ th point in question.

Method:

This metric can be calculated with 17 floating-point multiplies, and 15 additions per comparison, independent of the number of points being rotated.

Proof:

Let  $\{r_{\alpha}^{\vec{}}\}$ , be the original set of points  $\{x_{\alpha}^{\vec{}}\}$ , only translated and rotated so that the principle axis are now aligned with the  $\hat{x}$ ,  $\hat{y}$ , and  $\hat{z}$  axis, and the centroid is located at the origin. Let  $\mathcal{R}, \vec{\mathcal{T}}, \mathcal{R}', \vec{\mathcal{T}'}$ , be the same rotations and translations expressed in this new coordinate system. It turns out to be much easier to calculate  $\Phi$  using this new data-set,  $\{r_{\alpha}^{\vec{}}\}$ . Below is a short detour to review principle axis. It can be skipped without loss of continuity.

#### Principle-Axis

The principle axis of a set of points,  $\{\hat{\mathbf{p}}_i\}$  are defined to be the eigenvectors of the matrix  $\chi$ , where:

$$\chi_{ij} = \sum_{\alpha=1}^N (x_{\alpha i} - x_{cm\ i})(x_{\alpha j} - x_{cm\ j}) \quad (2)$$

where  $x_{cm}^{\vec{}}$  is the location of the centroid ( $x_{cm}^{\vec{}} \equiv \sum_{\alpha=1}^N x_{\alpha}^{\vec{}}/N$ ) and  $x_{cm\ j}$  is its  $j$ th component.

Note  $\chi$  is a symmetric matrix, so its eigenvectors (the principle axis) form an orthogonal basis. This means it is always possible to rotate and translate our initial coordinate data  $\{x_{\alpha}^{\vec{}}\}$ , to a new orientation so that the principle-axis are aligned with the  $\hat{x}$ ,  $\hat{y}$ , and  $\hat{z}$  axis, and the centroid at the origin. We rename the rotated, translated data  $\{r_{\alpha}^{\vec{}}\}$ .

The transformation between these two sets of data is:

$$x_{\alpha}^{\vec{}} = Pr_{\alpha}^{\vec{}} + x_{cm}^{\vec{}} \quad (3)$$

where  $P$  is a 3x3 pure rotation matrix (determinant 1) storing the 3 normalized principle-axis as column vectors  $P \equiv [\hat{\mathbf{p}}_1, \hat{\mathbf{p}}_2, \hat{\mathbf{p}}_3]$ . We go to all this trouble because this new set of points  $\{\vec{r}_\alpha\}$  has the following desirable properties: (which you can verify by substituting Eq.(3) into Eq.(2))

$$\sum_{\alpha=1}^N \vec{r}_\alpha = \vec{0} \quad (4)$$

$$\sum_{\alpha=1}^N r_{\alpha i} r_{\alpha j} = \lambda_i \delta_{ij} \quad (5)$$

where  $r_{\alpha j}$  = the  $j$ th component of  $\vec{r}_\alpha$ , where  $\delta_{ij}$  is the Kronecker-Delta function, ( $\delta_{ij} \equiv 1$  if  $i = j$ , and 0 otherwise) and  $\lambda_1, \lambda_2$ , and  $\lambda_3$  are the eigenvalues corresponding to  $\hat{\mathbf{p}}_1, \hat{\mathbf{p}}_2, \hat{\mathbf{p}}_3$ .

In order to express  $\Phi$ , in terms of  $\{\vec{r}_\alpha\}$ , instead of  $\{\vec{x}_\alpha\}$  we need to modify  $R, \vec{T}, R'$ , and  $\vec{T}'$ . in order to compensate for the rotation and translation we just applied. Substituting Eq.(3) into Eq.(1) yields:

$$\Phi = \sum_{\alpha=1}^N |(\mathcal{R} \vec{r}_\alpha + \vec{T}) - (\mathcal{R}' \vec{r}_\alpha + \vec{T}')|^2 \quad (6)$$

where:

$$\begin{aligned} \mathcal{R} &\equiv RP \\ \mathcal{R}' &\equiv R'P \\ \mathcal{T} &\equiv P \vec{x}_{cm} + \vec{T} \\ \mathcal{T}' &\equiv P \vec{x}_{cm} + \vec{T}' \end{aligned}$$

Calculating  $\Phi$

Suppose

$\Delta \vec{r}_\alpha$  = the displacement vector of the  $\alpha$ th point between the two orientations and  $\Delta r_{\alpha\nu}$  is its  $\nu$ th component.

Re-expressing Eq.(6) in terms of components, we get:

$$\Phi = \sum_{\alpha=1}^N \sum_{\nu=1}^3 (\Delta r_{\alpha\nu})^2$$

where

$$(\Delta r_{\alpha\nu})^2 = \left( \sum_{i=1}^3 (\mathcal{R}_{\nu i} r_{\alpha i} + \mathcal{T}_\nu) - (\mathcal{R}'_{\nu i} r_{\alpha i} + \mathcal{T}'_\nu) \right) \left( \sum_{j=1}^3 (\mathcal{R}_{\nu j} r_{\alpha j} + \mathcal{T}_\nu) - (\mathcal{R}'_{\nu j} r_{\alpha j} + \mathcal{T}'_\nu) \right) \quad (7)$$

When we expand the square, we can exploit the property that the centroid is at the origin, Eq.(4). This enables us to throw away the terms with odd powers of  $r_{\alpha i}$ , (for example:  $\mathcal{R}_{\nu i} r_{\alpha i} \mathcal{T}_\nu$ ) since they will be annihilated when we eventually sum over  $\alpha$ . Making these changes and collecting equivalent terms, Eq.(7) reduces to:

$$(\Delta r_{\alpha\nu})^2 = \sum_{i,j=1}^3 (\mathcal{R}_{\nu i} \mathcal{R}_{\nu j} r_{\alpha i} r_{\alpha j} - 2 \mathcal{R}_{\nu i} \mathcal{R}'_{\nu j} r_{\alpha i} r_{\alpha j} + \mathcal{R}'_{\nu i} \mathcal{R}'_{\nu j} r_{\alpha i} r_{\alpha j}) + (\mathcal{T}_\nu - \mathcal{T}'_\nu)^2$$

Summing over  $\nu$ :

$$\sum_{\nu=1}^3 (\Delta r_{\alpha\nu})^2 = \sum_{i,j=1}^3 (\delta_{ij} r_{\alpha i} r_{\alpha j} - 2 \sum_{\nu=1}^3 \mathcal{R}_{\nu i} \mathcal{R}'_{\nu j} r_{\alpha i} r_{\alpha j} + \delta_{ij} r_{\alpha i} r_{\alpha j}) + \sum_{\nu=1}^3 (\mathcal{T}_\nu - \mathcal{T}'_\nu)^2 \quad (8)$$

In this last step, we exploited the orthonormality of the rotation matrices  $\mathcal{R}$  and  $\mathcal{R}'$

Now, by summing Eq.(8) over  $\alpha$ , and exploiting Eq.(5), we can simplify Eq.(6) to get:

$$\begin{aligned} \Phi &= \sum_{i,j=1}^3 (2\delta_{ij} \lambda_i \delta_{ij} - 2 \sum_{\nu=1}^3 \mathcal{R}_{\nu i} \mathcal{R}'_{\nu j} \lambda_i \delta_{ij}) + N \sum_{\nu=1}^3 (\mathcal{T}_\nu - \mathcal{T}'_\nu)^2 \\ &= 2 \sum_{i=1}^3 \lambda_i (1 - \sum_{\nu=1}^3 \mathcal{R}_{\nu i} \mathcal{R}'_{\nu i}) + N \sum_{\nu=1}^3 (\mathcal{T}_\nu - \mathcal{T}'_\nu)^2 \end{aligned} \quad (9)$$

□

Property:

$\text{RMSD}(\sqrt{\Phi/N})$  obeys the

**Triangle Inequality:**

$$\sqrt{\Phi(R, \mathbf{T}, R'', \mathbf{T}'')/N} \leq \sqrt{\Phi(R, \mathbf{T}, R', \mathbf{T}')/N} + \sqrt{\Phi(R', \mathbf{T}', R'', \mathbf{T}'')/N} \quad (10)$$

Proof: Let

$$\mathbf{X}_\alpha \equiv R \mathbf{x}_\alpha + \mathbf{T}$$

$$\mathbf{X}'_\alpha \equiv R' \mathbf{x}_\alpha + \mathbf{T}'$$

Notice that the set of values  $\{X_{\alpha\nu}\}$  (ie. the set of all components of  $\mathbf{X}_\alpha$ ) itself forms a “vector” in a  $3N$  dimensional space, and:

$$\Phi = \sum_{\alpha,\nu} (X_{\alpha\nu} - X'_{\alpha\nu})^2$$

So  $\sqrt{\Phi(R, \mathbf{T}, R', \mathbf{T})}$  is simply a straight evenly weighted Euclidian-length of the differences between the primed and unprimed versions of  $X_{\alpha\nu}$ , all the components of all the vectors. For any finite-dimensional space of real numbers, Euclidian length, obeys the triangle inequality.