

FEM formulation for Schrödinger equation

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1 Weak form deduction

Consider the time-dependent Schrödinger equation

$$i\hbar \frac{\partial}{\partial t} \Psi = \hat{H} \Psi,$$

being \hat{H} the Hamiltonian Operator $(-\frac{\hbar^2}{2m} \nabla^2 + V(\vec{x}))$. $-\frac{\hbar^2}{2m} \nabla^2$ is the kinetic energy operator and $V(\vec{x})$ is the potential energy.

If we assume

$$\Psi = \Psi e^{-i\omega t}$$

we get

$$i\hbar(-i\omega e^{-i\omega t} \Psi) = \hat{H} e^{-i\omega t} \Psi$$

which yields

$$\hbar\omega \Psi = \hat{H} \Psi$$

and is the time-independent Schrödinger equation, usually written as

$$E \Psi = \hat{H} \Psi \quad (E = \hbar\omega = h\nu) . \quad (1)$$

For the FEM solution, let's multiply by a test function v and integrate over the domain Ω

$$\int_{\Omega} E \Psi v d\Omega = \int_{\Omega} \hat{H} \Psi v d\Omega$$

or

$$E \int_{\Omega} \Psi(x) v(x) d\Omega = -\frac{\hbar^2}{2m} \int_{\Omega} \nabla^2 \Psi(x) v(x) d\Omega + \int_{\Omega} V(x) \Psi(x) v(x) d\Omega . \quad (2)$$

(2) could be rewritten, via Green's theorem, as

$$E \int_{\Omega} \Psi(x) v(x) d\Omega = \frac{\hbar^2}{2m} \int_{\Omega} \nabla \Psi(x) \nabla v(x) d\Omega + \int_{\Omega} V(x) \Psi(x) v(x) d\Omega - \int_{\Gamma} v(x) \frac{\partial \Psi(x)}{\partial \vec{n}} d\Gamma \quad \text{with } \Gamma = \partial\Omega$$

The term $\int_{\Omega} v(x) \frac{\partial \Psi(x)}{\partial \vec{n}} \partial \Omega$ won't make any contribution to the discrete operators (matrices) of the system, so let us consider just

$$E \int_{\Omega} \Psi(x) v(x) d\Omega = \frac{\hbar^2}{2m} \int_{\Omega} \nabla \Psi(x) \nabla v(x) d\Omega + \int_{\Omega} V(x) \Psi(x) v(x) d\Omega \quad (3)$$

2 Approximated functions: interpolation

Functions $\Psi(x)$ and $v(x)$ need to be approximated as

$$\begin{aligned} \Psi(x) &= \sum_{i=1}^n \Psi_i N_i(x), \quad \text{with } \Psi_i = \Psi(x_i); \\ v(x) &= \sum_{i=1}^n v_i N_i(x), \quad \text{with } v_i = v(x_i); \end{aligned}$$

being these interpolation calculated over the (disjoint) elements.

Since $V(x)$ is the potential, it is known, and two approximations could be applied:

- Assume $V(x)$ constant over each element, or
- Interpolate it with the form functions $N_i(x)$.

Equation (3) could be stated as

$$\frac{\hbar^2}{2m} \sum_{el=1}^{N_{el}} \int_{\Omega} \nabla \Psi(x) \nabla v(x) d\Omega + \sum_{el=1}^{N_{el}} \int_{\Omega} V(x) \Psi(x) v(x) d\Omega = E \sum_{el=1}^{N_{el}} \int_{\Omega} \Psi(x) v(x) d\Omega ,$$

where el is a label for the elements.

Therefore, we need to compute it for a single element and then assemble.

$$\frac{\hbar^2}{2m} \sum_{el=1}^{N_{el}} \int_{\Omega} \nabla \Psi(x) \nabla v(x) d\Omega + \sum_{el=1}^{N_{el}} \int_{\Omega} V(x) \Psi(x) v(x) d\Omega = E \sum_{el=1}^{N_{el}} \int_{\Omega} \Psi(x) v(x) d\Omega ,$$

So, for each element we have

$$\frac{\hbar}{2m} \int_{\Omega_{el}} \nabla \Psi(x) \nabla v(x) d\Omega_{el} + \int_{\Omega_{el}} V(x) \Psi(x) v(x) d\Omega_{el} = E \int_{\Omega_{el}} \Psi(x) v(x) d\Omega_{el} . \quad (4)$$

Then, the approximate functions are replaced in (4). Two approximated versions of equation (4) are given

- assuming the potential $V(x)$ constant over the element, or
- using the same interpolation functions for $V(x)$.

2.1 Potential constant over the element

The resulting equation is

$$\frac{\hbar}{2m} \int_{\Omega_{el}} \Psi_i v_j \nabla N_i(x) \nabla N_j(x) d\Omega_{el} + V(x_m) \int_{\Omega_{el}} \Psi_i v_j N_i(x) N_j(x) d\Omega_{el} = E \int_{\Omega_{el}} \Psi_i v_j N_i(x) N_j(x) d\Omega_{el} , \quad (5)$$

where x_m is the centroid of the element.

2.2 Potential interpolated over the element

The resulting equation is

$$\frac{\hbar}{2m} \int_{\Omega_{el}} \Psi_i v_j \nabla N_i(x) \nabla N_j(x) d\Omega_{el} + \int_{\Omega_{el}} V_i \Psi_i v_j N_i^2(x) N_j(x) d\Omega_{el} = E \int_{\Omega_{el}} \Psi_i v_j N_i(x) N_j(x) d\Omega_{el} . \quad (6)$$

3 Discrete form

Equation (4) could be written in an abstract (inner-product) fashion like

$$\langle \mathbb{K}\Psi, \mathbf{v} \rangle + \langle \mathbb{V}\Psi, \mathbf{v} \rangle = E \langle \mathbb{M}\Psi, \mathbf{v} \rangle ,$$

this is the same that

$$\langle \mathbb{K}\Psi + \mathbb{V}\Psi - E\mathbb{M}\Psi, \mathbf{v} \rangle = 0 ,$$

and since $v(x)$ is an *arbitrary* function the vector \mathbf{v} it's too. As a consequence we have

$$\mathbb{K}\Psi + \mathbb{V}\Psi = E\mathbb{M}\Psi ,$$

The final discrete system, with boundary conditions, will take the form

$$\mathbb{K}\Psi + \mathbb{V}\Psi = E\mathbb{M}\Psi + \mathbf{d} + \mathbf{q}$$

where \mathbb{K} is the equivalent *kinetic energy operator* (stiffness matrix), \mathbb{V} is the *potential energy operator*, \mathbb{M} is the *momentum operator* (mass matrix), \mathbf{d} is the vector with Dirichlet's conditions and \mathbf{q} is the vector with Neumann's conditions.

In quantum mechanics Neumann's boundary conditions don't have a great physical meaning and the most common Dirichlet's conditions are the homogeneous ones, furthermore one is interested in the values of E and the functions Ψ that satisfy the original equation. So the discrete system to solve is

$$\mathbb{K}\Psi_n + \mathbb{V}\Psi_n = E_n \mathbb{M}\Psi_n , \quad (7)$$

or

$$\hat{\mathbb{K}}\Psi_n = E_n \mathbb{M}\Psi_n ,$$

where E_n is the n th eigenvalue of the system and Ψ_n the n th eigenvector, and $\hat{\mathbb{K}}$ is an equivalent *stiffness* matrix.

4 Matrix computation

The stiffness and mass matrices, for a single element, could be computed as

$$\mathbb{K}_{ij}^{(el)} = \frac{\hbar}{2m} \int_{\Omega_{el}} \nabla N_i \nabla N_j d\Omega_{el}$$

$$\mathbb{M}_{ij}^{(el)} = \int_{\Omega_{el}} N_i N_j d\Omega_{el}$$

4.1 Potential constant over the element

With constant $V(x)$ over each element, the potential matrix is

$$\mathbb{V}_{ij}^{(el)} = V(x_m) \mathbb{M}_{ij}^{(el)}, \quad \text{with } x_m \text{ the centroid of each element .}$$

4.2 Potential interpolated over the element

In this case the potential energy operator is

$$\mathbb{V}_{ij}^{(el)} = \int_{\Omega_{el}} V(x_i) N_i^2 N_j d\Omega_{el}$$

4.3 1D - Linear elements

The functions $N(r)$ are

$$N = \begin{pmatrix} 1 - r \\ r \end{pmatrix}$$

so

$$\mathbb{K}_{ij}^{(el)} = \frac{\hbar}{2m} \begin{pmatrix} 1 & -1 \\ -1 & 1 \end{pmatrix}, \quad \mathbb{M}_{ij}^{(el)} = \frac{1}{6} \begin{pmatrix} 2 & 1 \\ 1 & 2 \end{pmatrix},$$

and

$$\mathbb{V}_{\text{constant}}^{(el)} = V(x_m) \mathbb{M}^{(el)}.$$

Making $V^{(el)} = (V_1, V_2)$, the value for the potential in each node, we get

$$\mathbb{V}_{\text{interpolated}}^{(el)} = \frac{1}{12} \begin{pmatrix} 3V_1 & V_1 \\ V_2 & 3V_2 \end{pmatrix}.$$

4.3.1 Global Matrices

(This is not clear in my mind)

The global *equivalent stiffness* matrix is computed as

$$\begin{aligned}\mathbb{K}_{ii} &= \left(\frac{1}{L_{i-1}} + \frac{1}{L_i} \right) \frac{\hbar}{2m} + \frac{1}{3} [V_{i-1}L_{i-1} + V_iL_i] \quad \forall i \neq 1, i \neq n, \\ \mathbb{K}_{ii+1} &= \left[-\frac{1}{L_{i-1}} \frac{\hbar}{2m} + L_{i-1} \frac{V_{i-1}}{6} \right] = \mathbb{K}_{i+1i} \quad \forall i \neq n, \text{ and} \\ \mathbb{K}_{11} &= \left[\frac{1}{L_1} \frac{\hbar}{2m} + L_1 \frac{V_1}{3} \right], \\ \mathbb{K}_{nn} &= \left[\frac{1}{L_{n-1}} \frac{\hbar}{2m} + L_{n-1} \frac{V_{n-1}}{3} \right],\end{aligned}$$

being L_i the length of the i th element, if the mesh has a constant size so the previous expressions are simpler.

The global mass matrix is computed as

$$\begin{aligned}\mathbb{M}_{ii} &= \frac{L_i + L_{i+1}}{3} \quad \forall i \neq 1, i \neq n, \\ \mathbb{M}_{ii+1} &= \frac{L_i}{6} = \mathbb{M}_{i+1i} \quad \forall i \neq n, \text{ and} \\ \mathbb{M}_{11} &= \frac{L_1}{3}, \\ \mathbb{K}_{nn} &= \frac{L_{n-1}}{3},\end{aligned}$$

4.4 2D - Linear elements

The functions $N(r, s)$ are

$$N = \begin{pmatrix} 1 - r - s \\ r \\ s \end{pmatrix}$$

so

$$\mathbb{K}_{ij}^{(el)} = \frac{\hbar}{4m} \begin{pmatrix} 2 & -1 & -1 \\ -1 & 1 & 0 \\ -1 & 0 & 1 \end{pmatrix}, \quad \mathbb{M}_{ij}^{(el)} = \frac{1}{24} \begin{pmatrix} 2 & 1 & 1 \\ 1 & 2 & 1 \\ 1 & 1 & 2 \end{pmatrix},$$

and

$$\mathbb{V}_{\text{constant}}^{(el)} = V(x_m) \mathbb{M}^{(el)}.$$

Making $V^{(el)} = (V_1, V_2, V_3)$, the value for the potential in each node, we get

$$\mathbb{V}_{\text{interpolated}}^{(el)} = \frac{1}{60} \begin{pmatrix} 3V_1 & V_1 & V_1 \\ V_2 & 3V_2 & V_2 \\ V_3 & V_3 & 3V_3 \end{pmatrix}.$$

4.5 3D - Linear elements

The functions $N(r, s, t)$ are

$$N = \begin{pmatrix} 1 - r - s - t \\ r \\ s \\ t \end{pmatrix}$$

so

$$\mathbb{K}_{ij}^{(el)} = \frac{\hbar}{6m} \begin{pmatrix} 3 & -1 & -1 & -1 \\ -1 & 1 & 0 & 0 \\ -1 & 0 & 1 & 0 \\ -1 & 0 & 0 & 1 \end{pmatrix}, \quad \mathbb{M}_{ij}^{(el)} = \frac{1}{60} \begin{pmatrix} 2 & -1 & 0 & -1 \\ -1 & 4 & 3/2 & 3 \\ 0 & 3/2 & 2 & 3/2 \\ -1 & 3 & 3/2 & 4 \end{pmatrix},$$

and

$$\mathbb{V}_{\text{constant}}^{(el)} = V(x_m) \mathbb{M}^{(el)}.$$

Making $V^{(el)} = (V_1, V_2, V_3, V_4)$, the value for the potential in each node, we get

$$\mathbb{V}_{\text{interpolated}}^{(el)} = \frac{1}{360} \begin{pmatrix} 0 & 5V_1 & 2V_1 & 5V_1 \\ -5V_2 & 15V_2 & 4V_2 & 10V_2 \\ 0 & 3V_3 & 6V_3 & 3V_3 \\ -5V_4 & 10V_4 & 4V_4 & 15V_4 \end{pmatrix}.$$