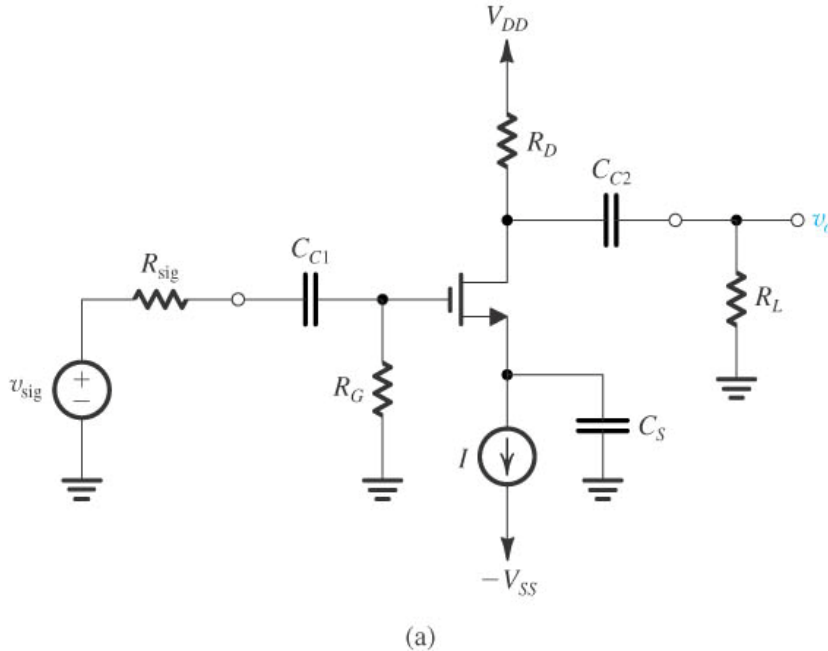


## 4.7 Single stage MOSFET Amplifiers

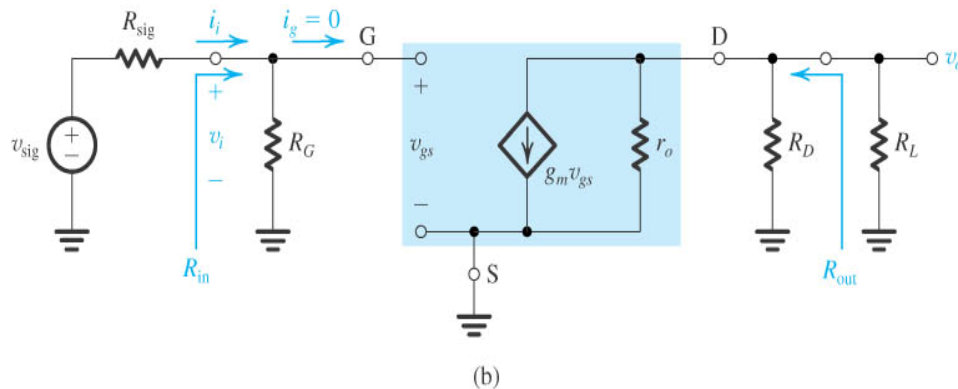
### 1. Common Source (CS) Amplifier :

A Common Source amplifier has the source terminal connected between the input and output. Input is applied between Gate –Source terminals and output is measured between the Drain-Source terminals. Any proper biasing method is used. Consider a CS amplifier with Constant current source biasing as shown below:



**Figure 4.43 (a)** Common-source amplifier

The ac equivalent circuit can be obtained by replacing the MOSFET with its small signal hybrid- $\pi$  model and writing the remaining components between the respective terminals of the MOSFET in the model as shown below:



**Figure 4.43 (b)** Equivalent circuit of the amplifier for small-signal analysis. Now, the electro-mathematical analysis of the CS amplifier for the voltage gain ( $A_v$ ), Input impedance ( $Z_{in}$ ) and Output impedance ( $Z_{out}$ ) is as shown below:

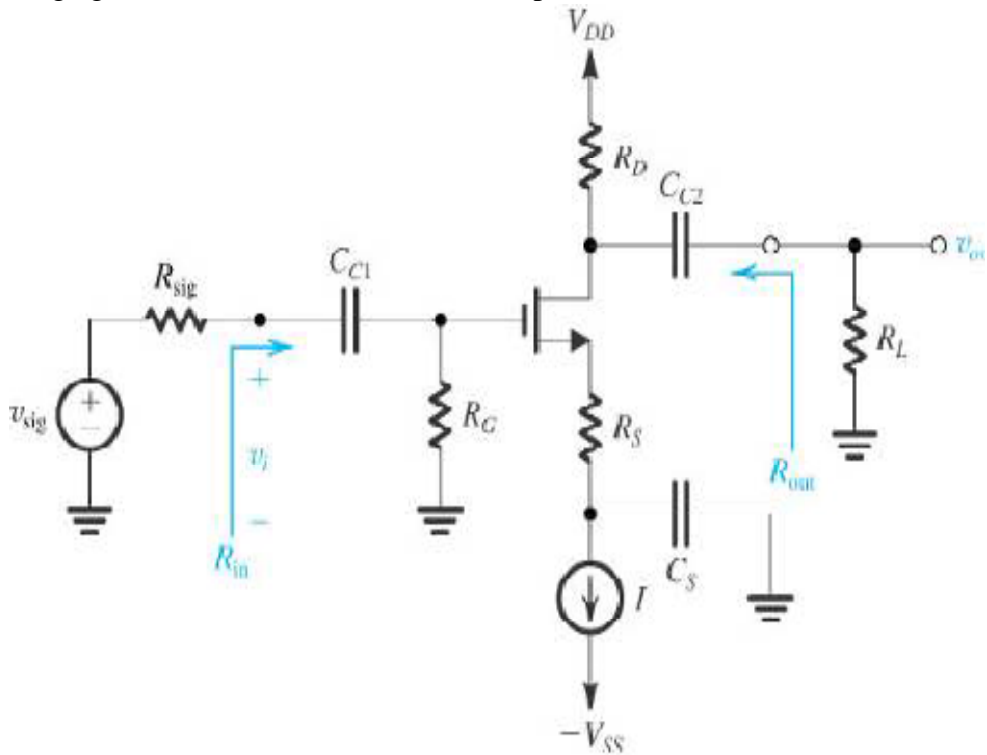
$$R_{in} = R_G$$

$$A_v = -g_m(r_o \parallel R_D \parallel R_L)$$

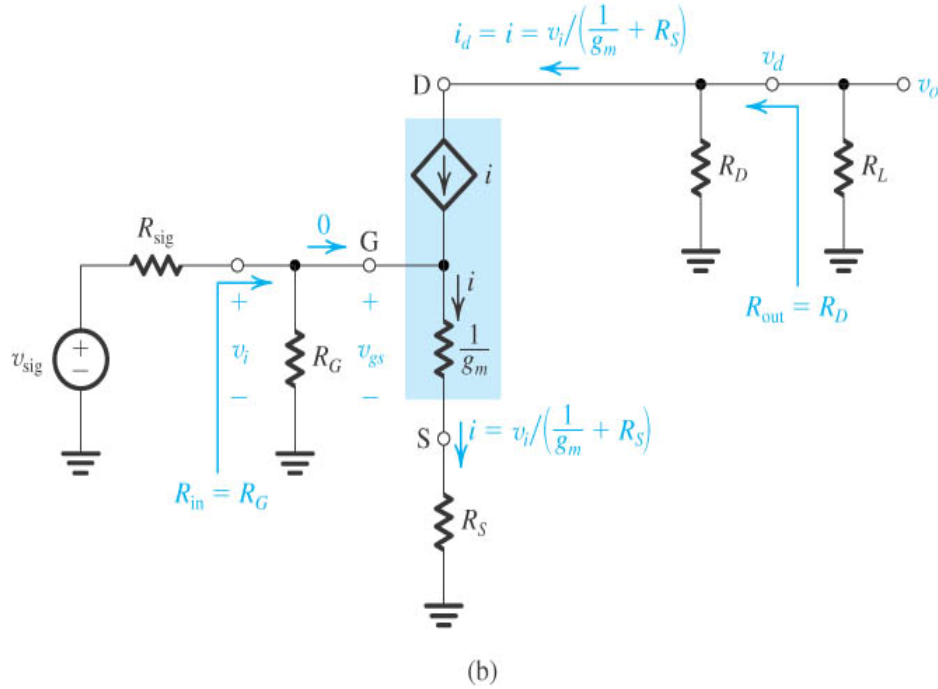
$$R_{out} = r_o \parallel R_D$$

$$G_v = -\frac{R_G}{R_G + R_{sig}} g_m(r_o \parallel R_D \parallel R_L)$$

Generally a Common Source amplifier will have a source resistance to improve the stability of the bias point. But this resistance also causes negative feedback and hence the voltage gain will be lesser than in a CS amplifier without source resistance.



**Figure 4.44 (a)** Common-source amplifier with a resistance  $R_S$  in the source lead. The small signal equivalent circuit with  $r_o$  neglected is as shown below:



**Figure 4.44** Small signal equivalent model of Common Source amplifier with  $R_s$

From the figure we can see that as in the case of the CS amplifier,

$$R_{in} = R_i = R_G \quad \text{and thus}$$

$$V_i = V_{sig} \frac{R_G}{R_G + R_{sig}}$$

But, here unlike the previous CS circuit,  $v_{gs}$  is only a fraction of  $v_i$ . It can be determined from the voltage divider composed of  $1/g_m$  and  $R_s$  that appears across the amplifier input as follows:

$$v_{gs} = v_i \frac{\frac{1}{g_m}}{\frac{1}{g_m} + R_s} = \frac{v_i}{1 + g_m R_s}$$

Hence  $v_{gs}$  can be controlled by  $R_s$ .

The current  $i_d$  is equal to the current  $I$  flowing in the source lead, thus

$$i_d = i = \frac{v_i}{\frac{1}{g_m} + R_s} = (g_m v_i) / (1 + g_m R_s)$$

Thus including  $R_s$  reduces  $i_d$  by the factor  $(1 + g_m R_s)$ .  
The output is now found from

$$v_o = -i_d(R_D || R_L)$$

$$= - \frac{g_m(R_D || R_L)}{\frac{1}{g_m} + R_S} v_i$$

$$A_v = - \frac{g_m(R_D || R_L)}{\frac{1}{g_m} + R_S} \text{ and setting } R_L \text{ as } \infty \text{ gives}$$

$$A_{vo} = - \frac{g_m R_D}{\frac{1}{g_m} + R_S}$$

The overall voltage gain  $G_v$  is,

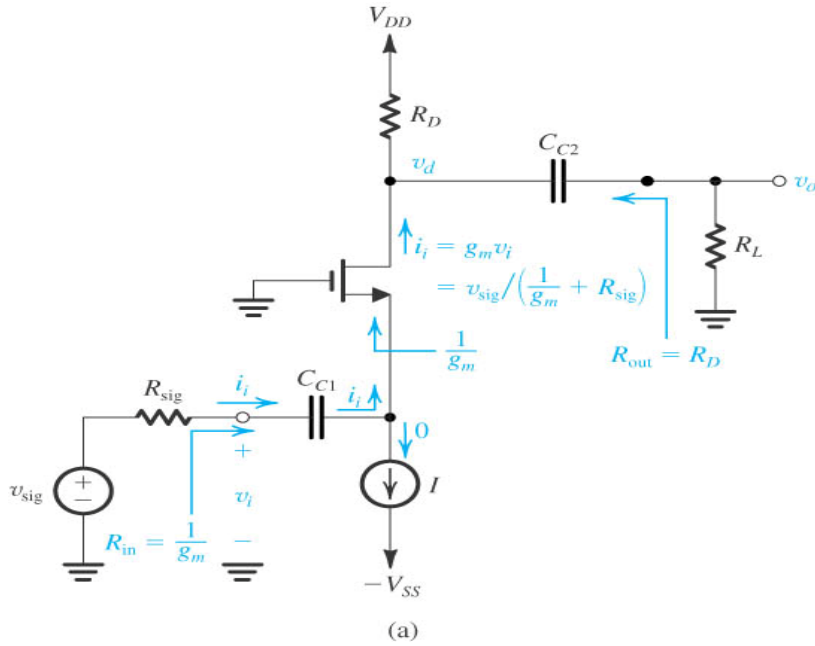
$$G_v = - \frac{R_G}{R_G + R_{sig}} \frac{g_m(R_D || R_L)}{\frac{1}{g_m} + R_S}$$

This shows that gain is reduced by a factor  $(1 + g_m R_S)$  than in the previous CS amplifier without  $R_S$ . This factor is called the “amount of feedback” and that it determines both the magnitude of performance improvement and as a tradeoff, the reduction in gain. Since this  $R_S$  was used to improve the stability under dc conditions, by reducing the variability of  $I_D$ , for ac operation it has a similar action (reducing  $i_d$ ), it is called “**Source degeneration resistance**”.

Another useful interpretation of the gain expression is that the gain from gate to drain is simply the ratio of the total resistance in the drain,  $(R_D || R_L)$  to the total resistance in the source,  $[\frac{1}{g_m} + R_S]$

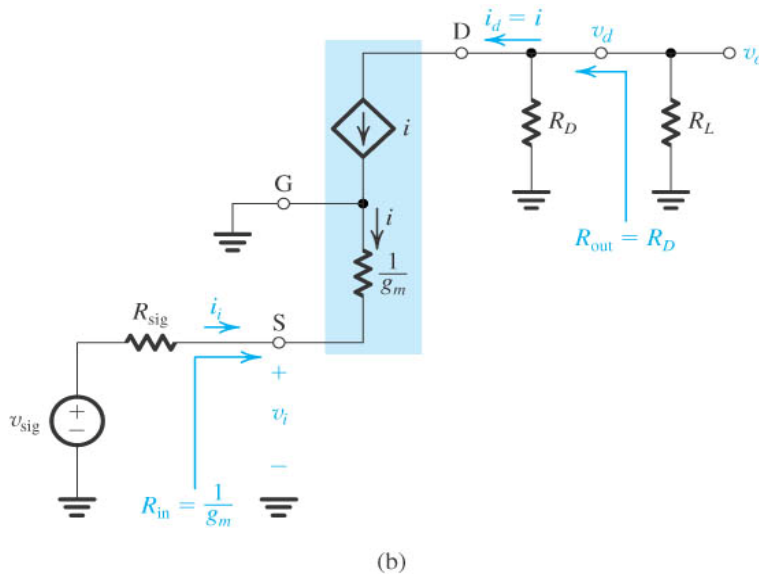
## Common Gate Amplifier [CG amplifier]

By applying a signal ground on the MOSFET gate terminal, a circuit configuration aptly named Common Gate or grounded gate amplifier is obtained. The input is applied between source and Gate and the Output is measured between the Drain and Gate. Since both the dc and ac voltages at the gate are zero, the gate terminal can be directly grounded as shown.



**Figure 4.45 (a)** A common-gate amplifier based on the circuit of Fig. 4.42.

The small signal equivalent circuit of the Common Gate Amplifier is as shown below. For simpler analysis we have used the T-model without considering the effect of  $r_o$ .



**Figure 4.45 (b)** A small-signal equivalent circuit of the amplifier in (a).

### Analysis:

The input resistance is given as

$$R_{in} = \frac{1}{g_m}$$

Since  $g_m$  is of the order of 1mA/V, the input resistance of the CG amplifier is relatively low (of the order of 1k $\Omega$ ) than in the CS amplifier.

$$V_i = V_{sig} \frac{R_{in}}{R_{in} + R_{sig}}$$

$$v_i = v_{sig} \frac{\frac{1}{g_m}}{\frac{1}{g_m} + R_{sig}} = \frac{v_{sig}}{1 + g_m R_{sig}}$$

The loss of signal strength in coupling the signal to input of the CG amplifier is due to the low value of  $R_{in}$ .

$$R_{sig} \ll \frac{1}{g_m}$$

The current  $i_i$  is given by,

$$i_i = \frac{v_i}{R_{in}} = \frac{v_i}{\frac{1}{g_m}} = (g_m v_i)$$

And the drain current  $i_d$  is

$$i_d = i = -i_i = -(g_m v_i)$$

Thus the output voltage can be found as

$$v_o = v_d - i_d(R_D || R_L) = g_m(R_D || R_L)$$

Resulting in voltage gained

$$A_v = g_m(R_D || R_L)$$

From which the open circuit voltage gain can be found as

$$A_{vo} = g_m R_D$$

The overall voltage gain can be obtained as follows:

$$G_v = \frac{R_{in}}{R_{in} + R_{sig}} A_v = A_v \frac{\frac{1}{g_m}}{\frac{1}{g_m} + R_{sig}} = \frac{A_v}{1 + g_m R_{sig}}$$

Resulting in

$$G_v = \frac{g_m(R_D || R_L)}{1 + g_m R_{sig}}$$

Finally the output resistance is found by inspection to be,

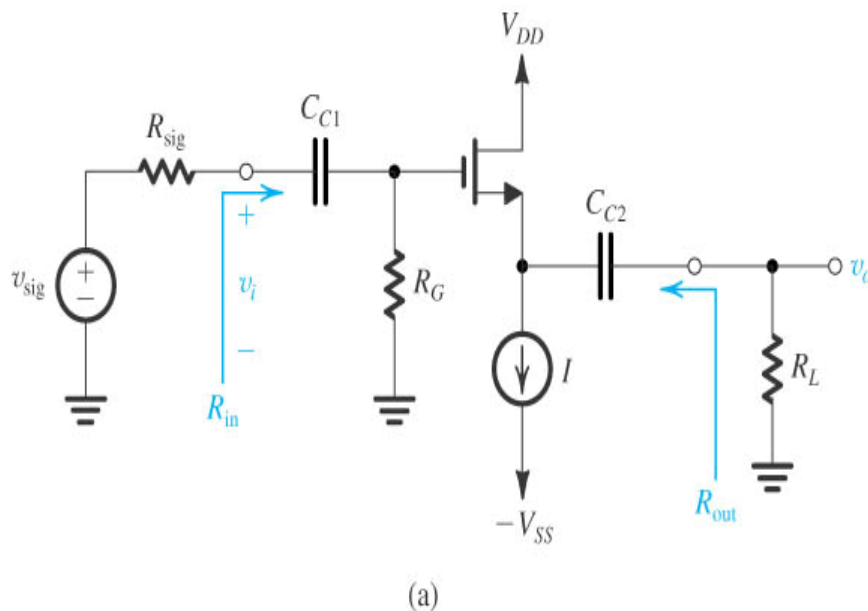
$$R_{out} = R_o = R_D$$

Note:

- The CG amplifier is non inverting
- The input resistance of CG amplifier is very low.
- Voltage gain is smaller than that of a CS amplifier by factor  $(1+g_m R_{sig})$  which is due to low  $R_{in}$ .
- This circuit also acts like a Unity gain current amplifier or a Current follower
- This is most commonly used in the Cascode amplifier.

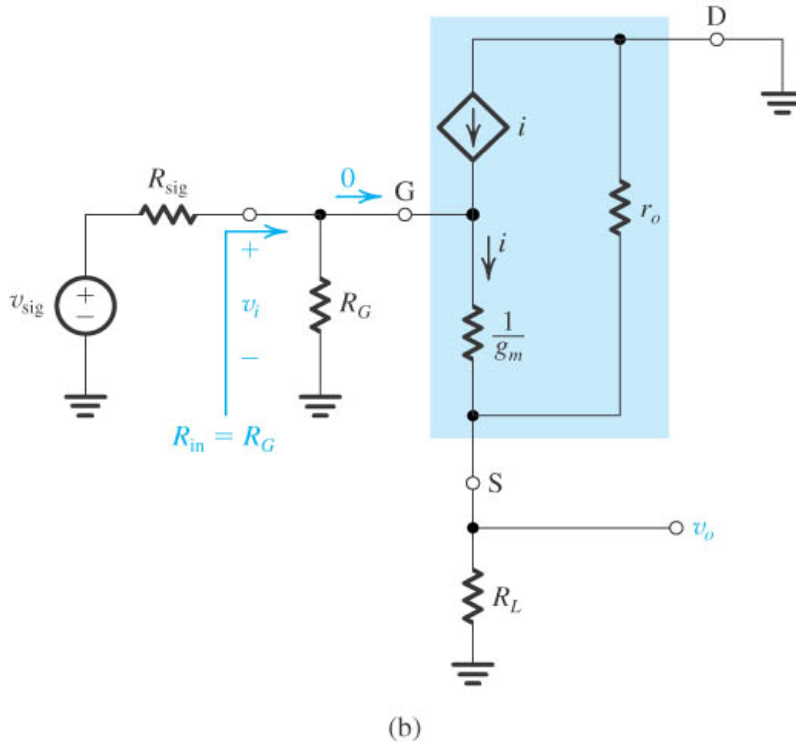
### Common Drain Amplifier (CD amplifier)

The signal ground is established at the drain terminal, input is given between the Gate and Drain terminals and Output is measured between the Source and Drain terminals as shown below:



**Figure 4.46 (a)** A common-drain or source-follower amplifier.

Here also, it is more convenient to use the small signal T-model for analysis, but including the resistance  $r_o$  as shown below:



**Figure 4.46 (b)** Small-signal equivalent-circuit model.

**Analysis:**

The input resistance is given as

$$R_{in} = R_G$$

$$V_i = V_{sig} \frac{R_{in}}{R_{in} + R_{sig}} = V_{sig} \frac{R_G}{R_G + R_{sig}}$$

Usually  $R_G$  is selected to be much larger than  $R_{sig}$  with the result that

$$v_i \cong v_{sig}$$

$$v_o = v_i \frac{R_L || r_o}{(R_L || r_o) + \frac{1}{g_m}}$$

From which the voltage gain  $A_v$  is obtained as



$$A_v = \frac{R_L || r_o}{(R_L || r_o) + \frac{1}{g_m}}$$

And the open circuit voltage gain  $A_{vo}$  as

$$A_{vo} = \frac{r_o}{r_o + \frac{1}{g_m}}$$

Normally  $r_o \gg \frac{1}{g_m}$ , causing voltage gain to become nearly unity. Thus the voltage at the source follows the voltage at the gate, giving the circuit its popular name of **source follower**. In many discrete circuits  $r_o \gg R_L$  which enables the equation to be approximated by,

$$A_v \cong \frac{R_L}{R_L + \frac{1}{g_m}}$$

The overall voltage gain  $G_v$  can be found as,

$$G_v = \frac{R_G}{R_G + R_{sig}} \frac{R_L || r_o}{(R_L || r_o) + \frac{1}{g_m}}$$

Which approaches unity for  $R_G \gg R_{sig}$ ,  $r_o \gg R_L$  and  $r_o \gg \frac{1}{g_m}$

The circuit for determining the output resistance  $R_{out}$  is as shown in figure. Because the gate voltage is now zero, looking back into the source, we see between the source and ground a resistance  $\frac{1}{g_m}$  in parallel with  $r_o$ , thus

$$R_{out} = \frac{1}{g_m} || r_o$$

Normally  $r_o \gg \frac{1}{g_m}$ , reducing  $R_{out}$  to

$$R_{out} \cong \frac{1}{g_m}$$

Which indicates  $R_{out}$  will be moderately low.

**Note:**

- In source follower,  $R_{in}$  is independent of  $R_L$  and  $R_{out}$  is independent of  $R_{sig}$ , due to zero gate current.
- Hence, it has a very high input resistance, very low output resistance and a voltage gain that is less than or close to unity.
- It is normally used as a buffer amplifier.

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**Summary:**

- The CS amplifier is best suited for obtaining the bulk of the gain required in an amplifier. Depending on the gain required, either a single stage or a cascade of two or three stages is used.
- Including a resistor  $R_S$  in the source terminal of the CS amplifier provides a number of improvements in its performance, as it behaves like an amplifier with negative Voltage series feedback amplifier, but at the expense of reduced gain.
- The low input resistance of the CG amplifier is used as unity gain current amplifier or current follower and also in Cascode amplifier.
- The source follower finds application as a voltage buffer for connecting a high resistance source to a low resistance load and as the output stage in a multistage amplifier.