

Institute of Systems Science and Intelligent Control Technology 系统科学与智能控制研究所

# 鲁棒控制： 建模、跟踪、抗扰、容错



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## Chapter 2: Linear Algebra

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- eigenvalues and eigenvectors
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- vector norms and matrix norms
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## Linear Subspaces

- **linear combination:**  $\alpha_1 x_1 + \alpha_2 x_2 + \dots + \alpha_k x_k$ ,  $x_i \in F^n$ ,  $\alpha_i \in F$   
 $\text{span}\{x_1, \dots, x_k\} := \{x = \alpha_1 x_1 + \dots + \alpha_k x_k : \alpha_i \in F\}$
- $x_1, \dots, x_k \in F^n$  **linearly dependent** if there exists  $\alpha_1, \dots, \alpha_k \in F$  not all zero such that  $\alpha_1 x_1 + \dots + \alpha_k x_k = 0$ ; otherwise they are **linearly independent**.
- $\{x_1, \dots, x_k\} \in S$  is a **basis** for  $S$  if  $x_1, \dots, x_k$  are linearly independent and  $S = \text{span}\{x_1, \dots, x_k\}$ .
- $\{x_1, \dots, x_k\}$  in  $F^n$  are **mutually orthogonal** if  $x_i^* x_j = 0$  for all  $i \neq j$  and **orthonormal** if  $x_i^* x_j = \delta_{ij}$
- **orthogonal complement** of a subspace  $S \subset F^n$   
 $S^\perp := \{y \in F^n : y^* x = 0 \text{ for all } x \in S\}$

- **linear transformation**  $A: F^n \rightarrow F^m$ .  
**kernel or null space:**  $\text{Ker} A = N(A) := \{x \in F^n : Ax = 0\}$   
**image or range of A:**  $\text{Im} A = R(A) := \{y \in F^m : y = Ax, x \in F^n\}$
- Let  $a_i, i=1, 2, \dots, n$  denote the columns of a matrix  $A \in F^{m \times n}$ . Then  
 $\text{Im } A = \text{span}\{a_1, a_2, \dots, a_n\}$ .
- The **rank** of a matrix  $A$  is defined by  $\text{rank}(A) = \dim(\text{Im } A)$ .  
 $\text{rank}(A) = \text{rank}(A^*)$ .  
 $A \in F^{m \times n}$  is **full row rank** if  $m \leq n$  and  $\text{rank}(A) = m$ .  
 $A$  is **full column rank** if  $n \leq m$  and  $\text{rank}(A) = n$ .
- **unitary matrix**  $U^* U = I = U U^*$ .
- Let  $D \in F^{m \times k}$  ( $n < k$ ) be such that  $D^* D = I$ . Then there exists a matrix  $D_1 \in F^{m \times (n-k)}$  such that  $[D \ D_1]$  is a unitary matrix

- **Sylvester equation**  
 $AX + XB = C$   
 with  $A \in F^{n \times n}$ ,  $B \in F^{m \times m}$ , and  $C \in F^{n \times m}$  has a unique solution  $X \in F^{n \times m}$ , if and only if  $\lambda_i(A) + \lambda_j(B) \neq 0, \forall i=1, 2, \dots, n$  and  $j=1, 2, \dots, m$ .
- “**Lyapunov Equation**”:  $B = A^*$ .
- Let  $A \in F^{n \times n}$  and  $B \in F^{n \times k}$ . Then  
 $\text{rank}(A) + \text{rank}(B) - n \leq \text{rank}(AB) \leq \min\{\text{rank}(A), \text{rank}(B)\}$ .
- the **trace** of  $A = [a_{ij}] \in C^{n \times n}$ :  $\text{Trace}(A) := \sum a_{ii}$   
**trace** has the following properties:  
 $\text{Trace}(\alpha A) = \alpha \text{Trace}(A), \forall \alpha \in C, A \in C^{n \times n}$   
 $\text{Trace}(A+B) = \text{Trace}(A) + \text{Trace}(B), \forall A, B \in C^{n \times n}$   
 $\text{Trace}(AB) = \text{Trace}(BA), \forall A \in C^{n \times m}, B \in C^{m \times n}$ .

## Eigenvalues and Eigenvectors

- The eigenvalues and eigenvectors of  $A \in \mathbb{C}^{n \times n}$ :  $\lambda \in \mathbb{C}, x \in \mathbb{C}^n$

$$Ax = \lambda x \quad x \text{ is a right eigenvector}$$

$y$  is a left eigenvector:  $y^* A = \lambda y^*$

- eigenvalues: the roots of  $\det(\lambda I - A)$ .  
 □ spectral radius:  $\rho(A) := \max |\lambda_i|$   
 □ Jordan canonical form:  $A \in \mathbb{C}^{n \times n}, \exists T$  such that  $A = T J T^{-1}$ .

$$J = \text{diag}\{J_1, J_2, \dots, J_l\} \quad J_{ij} = \begin{bmatrix} \lambda_i & 1 & & \\ & \lambda_i & 1 & \\ & & \ddots & \ddots \\ & & & \lambda_i & 1 \\ & & & & \lambda_i \end{bmatrix} \in \mathbb{C}^{n_i \times n_i}$$

$$J_l = \text{diag}\{J_{l_1}, J_{l_2}, \dots, J_{l_m}\}$$

The transformation  $T$  has the following form:

$$T = [T_1 \ T_2 \ \dots \ T_l], T_i = [T_{i1} \ T_{i2} \ \dots \ T_{in_i}], T_{ij} = [t_{ij1} \ t_{ij2} \ \dots \ t_{ijn_i}]$$

where  $t_{ij}$  are the eigenvectors of  $A$ :  $A t_{ij} = \lambda_i t_{ij}$  and  $t_{ijk} \neq 0$  defined by the following linear equations for  $k \geq 2$

$$(A - \lambda_i I) t_{ijk} = t_{ij(k-1)}$$

are called the **generalized eigenvectors** of  $A$ .

$A \in \mathbb{R}^{n \times n}$  with distinct eigenvalues can be diagonalized:

$$A \begin{bmatrix} x_1 & x_2 & \dots & x_n \end{bmatrix} = \begin{bmatrix} x_1 & x_2 & \dots & x_n \end{bmatrix} \begin{bmatrix} \lambda_1 & & & \\ & \lambda_2 & & \\ & & \ddots & \\ & & & \lambda_n \end{bmatrix}$$

and has the following spectral decomposition:

$$A = \sum \lambda_i x_i x_i^*$$

where  $y_i \in \mathbb{C}^n$  is given by

$$\begin{bmatrix} y_1^* \\ y_2^* \\ \vdots \\ y_n^* \end{bmatrix} = \begin{bmatrix} x_1 & x_2 & \dots & x_n \end{bmatrix}^{-1}$$

- $A \in \mathbb{R}^{n \times n}$  with real eigenvalue  $\lambda \in \mathbb{R} \Rightarrow$  real eigenvector  $x \in \mathbb{R}^n$   
 □  $A$  is Hermitian, i.e.,  $A = A^* \Rightarrow \exists$  unitary  $U$  such that  $A = U \Lambda U^*$  and  $\Lambda = \text{diag}\{\lambda_1, \lambda_2, \dots, \lambda_n\}$  is real.

## Matrix Inversion Formulas

$$\bullet \begin{bmatrix} A_{11} & A_{12} \\ A_{21} & A_{22} \end{bmatrix} = \begin{bmatrix} I & 0 \\ A_{21} A_{11}^{-1} & I \end{bmatrix} \begin{bmatrix} A_{11} & 0 \\ 0 & \Delta \end{bmatrix} \begin{bmatrix} I & A_{11}^{-1} A_{12} \\ 0 & I \end{bmatrix}$$

$$\Delta := A_{22} - A_{21} A_{11}^{-1} A_{12}$$

$$\bullet \begin{bmatrix} A_{11} & A_{12} \\ A_{21} & A_{22} \end{bmatrix} = \begin{bmatrix} I & A_{12} A_{22}^{-1} \\ 0 & I \end{bmatrix} \hat{\Delta} \begin{bmatrix} I & 0 \\ A_{22}^{-1} A_{21} & I \end{bmatrix}$$

$$\hat{\Delta} := A_{11} - A_{12} A_{22}^{-1} A_{21}$$

$$\bullet \begin{bmatrix} A_{11} & A_{12} \\ A_{21} & A_{22} \end{bmatrix}^{-1} = \begin{bmatrix} A_{11}^{-1} + A_{11}^{-1} A_{12} \hat{\Delta}^{-1} A_{12} A_{11}^{-1} & -A_{11}^{-1} A_{12} \hat{\Delta}^{-1} \\ -\hat{\Delta}^{-1} A_{21} A_{11}^{-1} & \hat{\Delta}^{-1} \end{bmatrix}$$

$$\begin{bmatrix} A_{11} & A_{12} \\ A_{21} & A_{22} \end{bmatrix}^{-1} = \begin{bmatrix} \hat{\Delta}^{-1} & -\hat{\Delta}^{-1} A_{12} A_{22}^{-1} \\ -A_{22}^{-1} A_{21} \hat{\Delta}^{-1} & A_{22}^{-1} + A_{22}^{-1} A_{21} \hat{\Delta}^{-1} A_{12} A_{22}^{-1} \end{bmatrix}$$

$$\begin{bmatrix} A_{11} & 0 \\ A_{21} & A_{22} \end{bmatrix}^{-1} = \begin{bmatrix} A_{11}^{-1} & 0 \\ -A_{22}^{-1} A_{21} A_{11}^{-1} & A_{22}^{-1} \end{bmatrix}$$

$$\begin{bmatrix} A_{11} & A_{12} \\ 0 & A_{22} \end{bmatrix}^{-1} = \begin{bmatrix} A_{11}^{-1} & -A_{11}^{-1} A_{12} A_{22}^{-1} \\ 0 & A_{22}^{-1} \end{bmatrix}$$

$$\det A = \det A_{11} \det(A_{22} - A_{21} A_{11}^{-1} A_{12}) = \det A_{22} \det(A_{11} - A_{12} A_{22}^{-1} A_{21}).$$

In particular, for any  $B \in \mathbb{C}^{m \times n}$  and  $C \in \mathbb{C}^{n \times m}$ , we have

$$\det \begin{bmatrix} I_m & B \\ -C & I_n \end{bmatrix} = \det(I_n + CB) = \det(I_m + BC)$$

and for  $x, y \in \mathbb{C}^n$   $\det(I_n + xy^*) = 1 + y^* x$ .

**matrix inversion lemma :**

$$(A_{11} - A_{12} A_{22}^{-1} A_{21})^{-1} = A_{11}^{-1} + A_{11}^{-1} A_{12} (A_{22} - A_{21} A_{11}^{-1} A_{12})^{-1} A_{21} A_{11}^{-1}$$

## Invariant Subspaces

- A subspace  $S \subset \mathbb{C}^n$  is an **A-invariant subspace** if  $Ax \in S$  for every  $x \in S$ .

For example,  $\{0\}$ ,  $\mathbb{C}^n$ ,  $\text{Ker } A$ , and  $\text{Im } A$  are all A-invariant subspaces.

Let  $\lambda$  and  $x$  be an eigenvalue and a corresponding eigenvector of  $A \in \mathbb{C}^{n \times n}$ . Then  $S := \text{span}\{x\}$  is an A-invariant subspace since

$$Ax = \lambda x \in S.$$

In general, let  $\{\lambda_1, \lambda_2, \dots, \lambda_k\}$  (not necessarily distinct) and  $x_i$  be a set of eigenvalues and a set of corresponding eigenvectors and the generalized eigenvectors. Then  $S = \text{span}\{x_1, \dots, x_k\}$  is an invariant subspace provided that all the lower rank generalized eigenvectors are included.



- An  $A$ -invariant subspace  $S \subset \mathbb{C}^n$  is called a stable invariant subspace if all the eigenvalues of  $A$  constrained to  $S$  have negative real parts.

Stable invariant subspaces are used to compute the stabilizing solutions of the algebraic Riccati equations.

- Example: Let  $A$  be such that

$$A \begin{bmatrix} x_1 & x_2 & x_3 & x_4 \end{bmatrix} = \begin{bmatrix} x_1 & x_2 & x_3 & x_4 \end{bmatrix} \begin{bmatrix} \lambda_1 & 1 & & \\ & \lambda_1 & & \\ & & \lambda_3 & \\ & & & \lambda_4 \end{bmatrix}$$

with  $\text{Re } \lambda_1 < 0$ ,  $\lambda_3 < 0$ , and  $\lambda_4 > 0$ . Then it is easy to verify that

$S_1 = \text{span}\{x_1\}$ ,  $S_{12} = \text{span}\{x_1, x_2\}$ ,  $S_{123} = \text{span}\{x_1, x_2, x_3\}$ ,  $S_3 = \text{span}\{x_3\}$ ,  
 $S_{13} = \text{span}\{x_1, x_3\}$ ,  $S_{124} = \text{span}\{x_1, x_2, x_4\}$ ,  $S_4 = \text{span}\{x_4\}$ ,  
 $S_{14} = \text{span}\{x_1, x_4\}$ ,  $S_{34} = \text{span}\{x_3, x_4\}$

are all  $A$ -invariant subspaces. Moreover,  $S_1$ ,  $S_3$ ,  $S_{12}$ ,  $S_{13}$ , and  $S_{123}$  are stable  $A$ -invariant subspaces.



However, the subspaces  $S_2 = \text{span}\{x_2\}$ ,  $S_{23} = \text{span}\{x_2, x_3\}$ ,  $S_{24} = \text{span}\{x_2, x_4\}$ ,  $S_{234} = \text{span}\{x_2, x_3, x_4\}$  are not  $A$ -invariant subspaces since the lower rank generalized eigenvector  $x_2$  of  $x_1$  is not in these subspaces.

To illustrate, consider the subspace  $S_{23}$ . It is an  $A$ -invariant subspace if  $Ax_2 \in S_{23}$ . Since  $Ax_2 = \lambda_1 x_2 + x_1$ ,  $Ax_2 \in S_{23}$  would require that  $x_1$  be a linear combination of  $x_2$  and  $x_3$ , but this is impossible since  $x_1$  is independent

## Vector Norms and Matrix Norms



- Norm: Let  $X$  be a vector space.  $\|\cdot\|$  is a norm if

- $\|x\| \geq 0$  (positivity);
- $\|x\| = 0$  if and only if  $x = 0$  (positive definiteness);
- $\|\alpha x\| = |\alpha| \|x\|$  for any scalar  $\alpha$  (homogeneity);
- $\|x+y\| \leq \|x\| + \|y\|$  (triangle inequality)

for any  $x \in X$  and  $y \in X$ .

Let  $x \in \mathbb{C}^n$ . Then we define the vector

$$\|x\|_p := \left( \sum_{i=1}^n |x_i|^p \right)^{1/p}, \text{ for } 1 \leq p \leq \infty.$$



In particular, when  $p = 1, 2, \infty$ , we have

$$\|x\|_1 := \sum_{i=1}^n |x_i|; \quad \|x\|_2 := \sqrt{\sum_{i=1}^n |x_i|^2}; \quad \|x\|_\infty := \max_{1 \leq i \leq n} |x_i|.$$

- Induced Matrix Norm: the matrix norm induced by a vector  $p$ -norm is defined as

$$\|A\|_p := \sup_{x \neq 0} \frac{\|Ax\|_p}{\|x\|_p}.$$

In particular, for  $p = 1, 2, \infty$ , the corresponding induced matrix norm can be computed as

$$\|A\|_1 := \max_{1 \leq j \leq n} \sum_{i=1}^m |a_{ij}| \quad (\text{column sum});$$

$$\|A\|_2 = \sqrt{\lambda_{\max}(A^*A)};$$

$$\|A\|_\infty := \max_{1 \leq i \leq m} \sum_{j=1}^n |a_{ij}| \quad (\text{row sum}).$$



- Properties of Euclidean Norm: The Euclidean 2-norm has some very nice properties:

Let  $x \in \mathbb{F}^n$  and  $y \in \mathbb{F}^m$

- Suppose  $n \geq m$ . Then  $\|x\| = \|y\|$  iff there is a matrix  $U \in \mathbb{F}^{n \times m}$  such that  $x = Uy$  and  $U^*U = I$ .
- Suppose  $n = m$ . Then  $\|x^*y\| \leq \|x\| \|y\|$ . Moreover, the equality holds iff  $x = \alpha y$  for some  $\alpha \in \mathbb{F}$  or  $y = 0$ .
- $\|x\| \leq \|y\|$  iff there is a matrix  $A \in \mathbb{F}^{n \times m}$  with  $\|A\| \leq 1$  such that  $x = Ay$ . Furthermore,  $\|x\| < \|y\|$  iff  $\|A\| < 1$ .
- $\|Ux\| = \|x\|$  for any appropriately dimensioned unitary matrices  $U$ .



- Properties of Matrix Norm:

**Frobenius norm**

$$\|A\|_F := \sqrt{\text{Trace}(A^*A)} = \sqrt{\sum_{i=1}^m \sum_{j=1}^n |a_{ij}|^2}.$$

Let  $A$  and  $B$  be any matrices with appropriate dimensions. Then

- $\rho(A) \leq \|A\|$  (This is also true for  $F$  norm and any induced matrix norm).
- $\|AB\| \leq \|A\| \|B\|$ . In particular, this gives  $\|A^{-j}\| \geq \|A\|^{-j}$  if  $A$  is invertible. (This is also true for any induced matrix norm.)
- $\|UAV\| = \|A\|$  and  $\|UAV\|_F = \|A\|_F$  for any appropriately dimensioned unitary matrices  $U$  and  $V$ .
- $\|AB\|_F \leq \|A\| \|B\|_F$ , and  $\|AB\|_F \leq \|B\| \|A\|_F$ .

## Singular Value Decomposition

- Let  $A \in \mathbb{F}^{m \times n}$ . There exist unitary matrices

$$U = [u_1, u_2, \dots, u_m] \in \mathbb{F}^{m \times m}, \quad V = [v_1, v_2, \dots, v_n] \in \mathbb{F}^{n \times n}$$

such that  $A = U \Sigma V^*$  where

$$\text{with } \Sigma = \text{diag}\{\sigma_1, \sigma_2, \dots, \sigma_p\} \text{ and } \Sigma = \begin{bmatrix} \Sigma & 0 \\ 0 & 0 \end{bmatrix},$$

$$\sigma_1 \geq \sigma_2 \geq \dots \geq \sigma_p \geq 0, \quad p = \min\{m, n\}.$$

$$\sigma_{\max}(A) = \sigma_1(A) = \text{the largest singular value of } A;$$

$$\sigma_{\min}(A) = \sigma_p(A) = \text{the smallest singular value of } A.$$

Note that  $\sigma(A)$

$$Av_i = \sigma_i u_i, \quad A^* u_i = \sigma_i v_i \\ A^* A v_i = \sigma_i^2 v_i, \quad A A^* u_i = \sigma_i^2 u_i$$

- Singular values are good measures of the "size" of the matrix singular vectors are good indications of strong/weak input or output directions.

Geometrically, the singular values of a matrix  $A$  are precisely the lengths of the semi-axes of the hyperellipsoid  $E$  defined by

$$E = \{y: y = Ax, x \in \mathbb{C}^n, \|x\| = 1\}.$$

Thus  $v_1$  is the direction in which  $\|y\|$  is largest for all  $\|x\| = 1$ , while  $v_n$  is the direction in which  $\|y\|$  is smallest for all  $\|x\| = 1$

$v_1(v_n)$  is the *highest (lowest) gain input direction*

$u_1(u_m)$  is the *highest (lowest) gain observing direction*

e.g.,

$$A = \begin{bmatrix} \cos \theta_1 & -\sin \theta_1 \\ \sin \theta_1 & \cos \theta_1 \end{bmatrix} \begin{bmatrix} \sigma_1 & 0 \\ 0 & \sigma_2 \end{bmatrix} \begin{bmatrix} \cos \theta_2 & -\sin \theta_2 \\ \sin \theta_2 & \cos \theta_2 \end{bmatrix}$$

$A$  maps a unit disk to an ellipsoid with semi-axes of

- Alternative definitions:

$$\bar{\sigma}(A) := \max_{\|x\|=1} \|Ax\|$$

and for the smallest singular value  $\underline{\sigma}$  of a tall matrix:

$$\underline{\sigma}(A) := \min_{\|y\|=1} \|Ax\|.$$

Suppose  $A$  and  $\Delta$  are square matrices. Then

$$(i) |\underline{\sigma}(A + \Delta) - \underline{\sigma}(A)| \leq \bar{\sigma}(\Delta);$$

$$(ii) \underline{\sigma}(A\Delta) \geq \underline{\sigma}(A)\underline{\sigma}(\Delta);$$

$$(iii) \bar{\sigma}(A^{-1}) = \frac{1}{\underline{\sigma}(A)} \text{ if } A \text{ is invertible.}$$

- Some useful properties

Let  $A \in \mathbb{F}^{m \times n}$  and  $\sigma_1 \geq \sigma_2 \geq \dots \geq \sigma_r > \sigma_{r+1} = \dots = 0$ ,  $r \leq \min\{m, n\}$ . Then

1.  $\text{rank}(A) = r$ ;
2.  $\text{Ker } A = \text{span}\{v_{r+1}, v_{r+2}, \dots, v_n\}$  and  $(\text{Ker } A)^\perp = \text{span}\{v_1, v_2, \dots, v_r\}$ ;
3.  $\text{Im } A = \text{span}\{u_1, u_2, \dots, u_r\}$  and  $(\text{Im } A)^\perp = \text{span}\{u_{r+1}, u_{r+2}, \dots, u_m\}$ ;
4.  $A \in \mathbb{F}^{m \times n}$  has a dyadic expansion:

$$A = \sum_{i=1}^r \sigma_i u_i v_i^* = U_r \Sigma_r V_r^*$$

where  $U_r = [u_1, u_2, \dots, u_r]$ ,  $V_r = [v_1, v_2, \dots, v_r]$ , and  $\Sigma_r = \text{diag}\{\sigma_1, \sigma_2, \dots, \sigma_r\}$ ;

$$5. \|A\|_F^2 = \sigma_1^2 + \sigma_2^2 + \dots + \sigma_r^2;$$

$$6. \|A\| = \sigma_1;$$

$$7. \sigma_i(U_0 A V_0) = \sigma_i(A), \quad i=1, 2, \dots, p, \text{ for any appropriately dimensioned unitary matrices } U_0 \text{ and } V_0.$$

## Generalized Inverses

- Let  $A \in \mathbb{F}^{m \times n}$ .  $X \in \mathbb{F}^{n \times m}$  is a *right inverse* if  $AX = I$ . One of the right inverses is given by  $X = A^*(AA^*)^{-1}$ .  $YA = I$  then  $Y$  is a *left inverse* of  $A$ .

- Pseudo-inverse* or *Moore-Penrose inverse*  $A^+$ :

- (i)  $A A^+ A = A$ ; (ii)  $A^+ A A^+ = A^+$ ; (iii)  $(A A^+)^* = A A^+$ ; (iv)  $(A^+ A)^* = A^+ A$ .

Pseudo-inverse is unique.

Let  $A = BC$  where  $B$  has a full column rank and  $C$  has full row rank. Then  $A^+ = C^*(CC^*)^{-1}(B^*B)^{-1}B^*$ .

or let  $A = U \Sigma V^*$  with  $\Sigma = \begin{bmatrix} \Sigma_r & 0 \\ 0 & 0 \end{bmatrix}$  and  $\Sigma_r = \text{diag}\{\sigma_1, \sigma_2, \dots, \sigma_r\}$ .

$$\text{Then } A^+ = V \Sigma^+ U^* \text{ with } \Sigma^+ = \begin{bmatrix} \Sigma_r^{-1} & 0 \\ 0 & 0 \end{bmatrix}.$$

## Semidefinite Matrices

- $A = A^*$  is *positive definite* (semi-definite) denoted by  $A > 0$  ( $\geq 0$ ), if  $x^* A x > 0$  ( $\geq 0$ ) for all  $x \neq 0$ .

- $A \in \mathbb{F}^{n \times n}$  and  $A = A^* \geq 0$ ,  $\exists B \in \mathbb{F}^{n \times r}$  with  $r \geq \text{rank}(A)$  such that  $A = BB^*$ .

- Let  $B \in \mathbb{F}^{m \times n}$  and  $C \in \mathbb{F}^{l \times n}$ . Suppose  $m \geq k$  and  $B^* B = C^* C$ .  $\exists U \in \mathbb{F}^{m \times k}$  such that  $U^* U = I$  and  $B = UC$ .

- Square root* for a positive semidefinite matrix  $A$ ,  $A^{1/2} = (A^{1/2})^* \geq 0$ , such that  $A = A^{1/2} A^{1/2}$ .

Clearly,  $A^{1/2}$  can be computed by using spectral decomposition or SVD: let  $A = U \Lambda U^*$ , then  $A^{1/2} = U \Lambda^{1/2} U^*$ , where  $\Lambda = \text{diag}\{\lambda_1, \lambda_2, \dots, \lambda_n\}$ ,  $A^{1/2} = \text{diag}\{(\lambda_1)^{1/2}, (\lambda_2)^{1/2}, \dots, (\lambda_n)^{1/2}\}$



□  $A=A^* > 0$  and  $B=B^* \geq 0$ . Then  $A > B$  iff  $\rho(BA^{-1}) < 1$ .

□ Let  $X=X^* \geq 0$  be partitioned as

$$X = \begin{bmatrix} X_{11} & X_{12} \\ X_{12}^* & X_{22} \end{bmatrix}$$

Then  $\text{Ker } X_{22} \subset \text{Ker } X_{12}$ . Consequently, if  $X_{22}^+$  is the pseudo-inverse of  $X_{22}$ , then  $Y = X_{12}X_{22}^+$  solves

$$YX_{22} = X_{12}$$

and

$$\begin{bmatrix} X_{11} & X_{12} \\ X_{12}^* & X_{22} \end{bmatrix} = \begin{bmatrix} I & X_{12}X_{22}^+ \\ 0 & I \end{bmatrix} \begin{bmatrix} X_{11} - X_{12}X_{22}^+X_{12}^* & 0 \\ 0 & X_{22} \end{bmatrix} \begin{bmatrix} I & 0 \\ X_{22}^+X_{12}^* & I \end{bmatrix}$$

## Chapter 3: Linear Systems



- Dynamical systems
- Controllability and stabilizability
- Observability and detectability
- Observer theory
- System interconnections
- Realizations
- Poles and zeros

## Dynamical Systems



- Linear equations:  $\dot{x} = Ax + Bu$ ,  $x(t_0) = x_0$   
 $y = Cx + Du$
- transfer matrix:  $Y(s) = G(s) U(s)$ ,  $G(s) = C(sI - A)^{-1}B + D$
- notation  $\begin{bmatrix} A & B \\ C & D \end{bmatrix} := C(sI - A)^{-1}B + D$ .
- solution: 
$$x(t) = e^{A(t-t_0)}x(t_0) + \int_{t_0}^t e^{A(t-\tau)}Bu(\tau)d\tau$$
  
$$y(t) = Cx(t) + Du(t).$$
- impulse matrix:  $g(t) = L^{-1}\{G(s)\} = Ce^{At}B1_+(t) + D\delta(t)$ .
- input/output relationship:

$$y(t) = (g * u)(t) = \int_{-\infty}^t g(t-\tau)u(\tau)d\tau.$$

## Matlab



```
>> G=ss(A,B,C,D) % state space realization
>> [A,B,C,D] = ssdata(G) % unpack the system matrix
>> [y,t,x] = step(g)
>> [y,t,x] = impulse(g) % impulse response
>> [y,x]=lsim(A,B,C,D,U,T) % U is a length(T) column(B)
matrix input; T is the sampling points.
```

## Controllability



- Controllability:  $(A,B)$  is controllable if, for any initial state  $x(0)=x_0$ ,  $t_1 > 0$  and final state  $x(t_1)$ , there exists a (piecewise continuous) input  $u(\cdot)$  such that  $x(t_1) = x_1$ .
- The matrix  $W_c(t) := \int_0^t e^{A\tau}BB^*e^{A^*\tau}d\tau$  is positive definite for any  $t > 0$ .
- The controllability matrix  $C = [B \ AB \ A^2B \ \dots \ A^{n-1}B]$  has full row rank, i.e.,  $\langle A | \text{Im } B \rangle := \sum_{k=1}^n \text{Im}(A^{k-1}B) = \mathbb{R}^n$ .
- The eigenvalues of  $A+BF$  can be freely assigned by a suitable  $F$ .

## Controllability: PBH test



PBH (Popov-Belevitch-Hautus) test:

- The matrix  $[A - \lambda I \ B]$  has full row rank for all  $\lambda$  in  $\mathbb{C}$ .
- Let  $\lambda$  and  $x$  be any eigenvalue and any corresponding left eigenvector of  $A$ , i.e.,  $x^*A = \lambda x^*$ , then  $x^*B \neq 0$ .

## Stability and Stabilizability

$A$  is stable if  $\text{Re}(\lambda(A)) < 0$ .

- $(A, B)$  is stabilizable.
- $A + BF$  is stable for some  $F$ .

PBH test:

- The matrix  $[A - \lambda I, B]$  has full row rank for all  $\text{Re} \lambda \geq 0$ .
- For all  $\lambda$  and  $x$  such that  $x^* A = x^* \lambda$  and  $\text{Re} \lambda \geq 0$ ,  $x^* B = 0$ .

## Observability

- $(C, A)$  is observable if, for any  $t_1 > 0$ , the initial state  $x(0) = x_0$  can be determined from the time history of the input  $u(t)$  and the output  $y(t)$  in the interval of  $[0, t_1]$ .

- The matrix  $W_0(t) = \int_0^t e^{A\tau} C^* C e^{A\tau} d\tau$

is positive definite for any  $t > 0$ .

- The observability matrix  $O$  has full column rank, i.e.,  $\bigcap_{i=1}^n \text{Ker}(CA^{i-1}) = 0$ .

$$O = \begin{bmatrix} C \\ CA \\ CA^2 \\ \vdots \\ CA^{n-1} \end{bmatrix}$$

- The eigenvalues of  $A + LC$  can be freely assigned by a suitable  $L$ .

## Observability: PBH test

PBH test:

- The matrix  $\begin{bmatrix} A - \lambda I \\ C \end{bmatrix}$  has full column rank for all  $\lambda$  in  $\mathbb{C}$ .
- Let  $\lambda$  and  $y$  be any eigenvalue and any corresponding right eigenvector of  $A$ , i.e.,  $Ay = \lambda y$ , then  $Cy \neq 0$ .

Duality:

- $(C, A)$  is observable if and only if  $(A^*, C^*)$  is controllable.

## Detectability

The following are equivalent:

- $(C, A)$  is detectable.
- $A + LC$  is stable for a suitable  $L$ .
- $(A^*, C^*)$  is stabilizable.

PBH test:

- The matrix  $\begin{bmatrix} A - \lambda I \\ C \end{bmatrix}$  has full column rank for all  $\text{Re} \lambda \geq 0$ .
- For all  $\lambda$  and  $y$  such that  $Ay = \lambda y$ ,  $\text{Re} \lambda \geq 0$ , and  $Cy \neq 0$ .

An example:

$$\left[ \begin{array}{c|c} A & B \\ \hline C & D \end{array} \right] = \left[ \begin{array}{cccc|c} \lambda_1 & 1 & 0 & 0 & 0 \\ 0 & \lambda_1 & 1 & 0 & 1 \\ 0 & 0 & \lambda_1 & 0 & \alpha \\ 0 & 0 & 0 & \lambda_2 & 1 \\ 1 & 0 & 0 & \beta & 0 \end{array} \right]$$

Not controllable if  $\lambda_1 = \lambda_2$  or  $\alpha = 0$ ;

Not observable if  $\lambda_1 = \lambda_2$  or  $\beta = 0$ .

>>  $C = \text{ctrb}(A, B)$ ;  $O = \text{obsv}(A, C)$ ;

>>  $W_c(\infty) = \text{gram}(g, g')$ ; % if  $A$  is stable.

>>  $F = -\text{place}(A, B, P)$  %  $P$  is a vector of desired eigenvalues.

## Observer-Based Controllers

An observer is a dynamical system with input  $(u, y)$  and output, say  $\hat{x}$  which asymptotically estimates the state  $x$ , i.e.,  $\hat{x}(t) - x(t) \rightarrow 0$  as  $t \rightarrow \infty$  for all initial states and for every input.

An observer exists iff  $(C, A)$  is detectable. Further, if  $(C, A)$  is detectable, then a full order Luenberger observer is given by

$$\begin{aligned} \dot{\hat{x}} &= A\hat{x} + Bu + L(C\hat{x} + Du - y) \\ \hat{x} &= q \end{aligned}$$

where  $L$  is a matrix such that  $A + LC$  is stable.

Observer-based controller:  $\hat{\dot{x}} = (A + LC)\hat{x} + Bu + LDu - Ly$   
 $u = F\hat{x}$

$$u = K(s)y$$

and

$$K(s) = \left[ \begin{array}{c|c} A + BF + LC + LDF & -L \\ \hline F & 0 \end{array} \right]$$

### Example

Let  $A = \begin{bmatrix} 1 & 2 \\ 1 & 0 \end{bmatrix}$ ,  $B = \begin{bmatrix} 1 \\ 0 \end{bmatrix}$ , and  $C = [1 \ 0]$

Design  $u = Fx$  so that the closed-loop poles are at  $\{-2, -3\}$ .

$F = [-6 \ -8] \Rightarrow F = -\text{place}(A, B, [-2, -3])$

Suppose observer poles are at  $\{-10, -10\}$

Then  $L = \begin{bmatrix} -21 \\ -51 \end{bmatrix}$  can be obtained by using  $\Rightarrow L = -\text{acker}(A', C', [-10, -10])'$

and the observer-based controller is given by

$$K(s) = \frac{-534(s + 0.6966)}{(s + 34.6564)(s - 8.6564)}$$

which is unstable: this may not be desirable in practice.

### Operations on Systems

$$G_1 = \begin{bmatrix} A_1 & B_1 \\ C_1 & D_1 \end{bmatrix}, \quad G_2 = \begin{bmatrix} A_2 & B_2 \\ C_2 & D_2 \end{bmatrix}$$

• cascade:

$$G_1 G_2 = \begin{bmatrix} A_1 & B_1 C_2 & B_1 D_2 \\ 0 & A_2 & B_2 \\ C_1 & D_1 C_2 & D_1 D_2 \end{bmatrix} = \begin{bmatrix} A_2 & 0 & B_2 \\ B_1 C_2 & A_1 & B_1 D_2 \\ D_1 C_2 & C_1 & D_1 D_2 \end{bmatrix}$$

• addition:

$$G_1 + G_2 = \begin{bmatrix} A_1 & 0 & B_1 \\ 0 & A_2 & B_2 \\ C_1 & C_2 & D_1 + D_2 \end{bmatrix}$$

• feedback:

$$T = \begin{bmatrix} A_1 - B_1 D_2^{-1} C_2 & -B_1 R_{21}^{-1} C_2 & B_1 R_{21}^{-1} \\ B_2 R_{12}^{-1} C_1 & A - B_2 D_1 R_{21}^{-1} C_2 & B_2 D_2 R_{21}^{-1} \\ R_{12}^{-1} C_1 & -R_{12}^{-1} D_1 C_2 & D_1 R_{21}^{-1} \end{bmatrix}$$

where  $R_{21} = I + D_1 D_2$  and  $R_{21} = I + D_2 D_1$ .

• transpose or dual system  $G \mapsto G^T(s) = B^*(sI - A^*)^{-1} C^* + D^*$

or equivalently  $\begin{bmatrix} A & B \\ C & D \end{bmatrix} \mapsto \begin{bmatrix} A^* & C^* \\ B^* & D^* \end{bmatrix}$

• conjugate system  $G \mapsto G^*(s) = G^T(-s) = B^*(-sI - A^*)^{-1} C^* + D^*$

or equivalently  $\begin{bmatrix} A & B \\ C & D \end{bmatrix} \mapsto \begin{bmatrix} -A^* & -C^* \\ B^* & D^* \end{bmatrix}$

In particular, we have  $G^*(j\omega) = [G(j\omega)]^* = G^{\sim}(j\omega)$ .

• inverse system: Let  $D^+$  denote a right (left) inverse of  $D$  if  $D$  has full row (column) rank. Then

$$G^+ = \begin{bmatrix} A - BD^+C & -BD^+ \\ D^+C & D^+ \end{bmatrix}$$

is a right (left) inverse of  $G$ , i.e.,  $GG^+ = I$  ( $G^+G = I$ ).

### State Space Realizations

Given  $G(s)$ , find  $(A, B, C, D)$  such that  $G(s) = \begin{bmatrix} A & B \\ C & D \end{bmatrix}$  which is a state space realization of  $G(s)$ .

A state space realization  $(A, B, C, D)$  of  $G(s)$  is *minimal* if and only if  $(A, B)$  is controllable and  $(C, A)$  is observable.

Let  $(A_1, B_1, C_1, D)$  and  $(A_2, B_2, C_2, D)$  be two minimal realizations of  $G(s)$ . Then there exists a unique nonsingular  $T$  such that

$$A_2 = TA_1 T^{-1}, \quad B_2 = TB_1, \quad C_2 = C_1 T^{-1}.$$

Furthermore,  $T$  can be specified as

$$T = (O_2^* O_2)^{-1} O_2^* O_1 \quad \text{or} \quad T^{-1} = C_1 C_2^* (C_2 C_2^*)^{-1}.$$

where  $C_1$ ,  $C_2$ ,  $O_1$ , and  $O_2$  are the corresponding controllability and observability matrices respectively.

### SIMO and MISO

**SIMO Case:** Let

$$G(s) = \begin{bmatrix} g_1(s) \\ g_2(s) \\ \vdots \\ g_m(s) \end{bmatrix} = \frac{\beta_1 s^{n-1} + \beta_2 s^{n-2} + \dots + \beta_{n-1} s + \beta_n}{s^n + a_1 s^{n-1} + \dots + a_{n-1} s + a_n} + d,$$

where  $\beta_i \in \mathbb{R}^m$  and  $d \in \mathbb{R}^m$ . Then

$$G(s) = \begin{bmatrix} A & b \\ C & d \end{bmatrix}, \quad b \in \mathbb{R}^n, C \in \mathbb{R}^{m \times n}, d \in \mathbb{R}^m$$

$$A := \begin{bmatrix} -a_1 & -a_2 & \dots & -a_{n-1} & -a_n \\ 1 & 0 & \dots & 0 & 0 \\ 0 & 1 & \dots & 0 & 0 \\ \vdots & \vdots & \ddots & \vdots & \vdots \\ 0 & 0 & \dots & 1 & 0 \end{bmatrix}, \quad b := \begin{bmatrix} 1 \\ 0 \\ 0 \\ \vdots \\ 0 \end{bmatrix}$$

$$C = [\beta_1 \ \beta_2 \ \dots \ \beta_{n-1} \ \beta_n]$$

**MISO Case:** Let  $G(s) = (g_1(s) \ g_2(s) \ \dots \ g_m(s))$

$$= \frac{\eta_1 s^{n-1} + \eta_2 s^{n-2} + \dots + \eta_{n-1} s + \eta_n}{s^n + a_1 s^{n-1} + \dots + a_{n-1} s + a_n} + d$$

with  $\eta_i^*$ ,  $d^* \in \mathbb{R}^p$ . Then

$$G(s) = \begin{bmatrix} -a_1 & 1 & 0 & \dots & 0 & \eta_1 \\ -a_2 & 0 & 1 & \dots & 0 & \eta_2 \\ \vdots & \vdots & \vdots & \ddots & \vdots & \vdots \\ -a_{n-1} & 0 & 0 & \dots & 1 & \eta_{n-1} \\ -a_n & 0 & 0 & \dots & 0 & \eta_n \\ 1 & 0 & 0 & \dots & 0 & d \end{bmatrix}$$

## Realizing Each Element

To illustrate, consider a  $2 \times 2$  (block) matrix

$$G(s) = \begin{bmatrix} G_1(s) & G_2(s) \\ G_3(s) & G_4(s) \end{bmatrix}$$

and assume that  $G_i(s)$  has a state space realization of

$$G_i(s) = \begin{bmatrix} A_i & B_i \\ C_i & D_i \end{bmatrix}, \quad i=1, \dots, 4.$$

Note that  $G_i(s)$  may itself be a MIMO transfer matrix.

Then a realization for  $G(s)$  can be given by

$$G(s) = \begin{bmatrix} A_1 & 0 & 0 & 0 & B_1 & 0 \\ 0 & A_2 & 0 & 0 & 0 & B_2 \\ 0 & 0 & A_3 & 0 & B_3 & 0 \\ 0 & 0 & 0 & A_4 & 0 & B_4 \\ C_1 & C_2 & 0 & 0 & D_1 & D_2 \\ 0 & 0 & C_3 & C_4 & D_3 & D_4 \end{bmatrix}$$

Limitation: may not be minimal.

$>> G = \text{tf}(\text{num}, \text{den}); G = \text{zpk}(\text{zeros}, \text{poles}, \text{gain});$

## Gilbert's Realization

Let  $G(s)$  be a  $p \times m$  transfer matrix  $G(s) = N(s)/d(s)$

with  $d(s)$  a scalar polynomial. For simplicity, we shall assume that  $d(s)$  has only real and distinct roots  $\lambda_i \neq \lambda_j$  if  $i \neq j$  and

$$d(s) = (s - \lambda_1)(s - \lambda_2) \cdots (s - \lambda_r).$$

Then  $G(s)$  has the following partial fractional expansion:

$$G(s) = D + \sum_{i=1}^r \frac{W_i}{s - \lambda_i}.$$

Suppose  $\text{rank } W_i = k_i$  and let  $B_i \in \mathbb{R}^{k_i \times m}$  and  $C_i \in \mathbb{R}^{p \times k_i}$  be two constant matrices such that  $W_i = C_i B_i$ .

Then a realization is given by

$$G(s) = \begin{bmatrix} \lambda_1 I_{k_1} & & & B_1 \\ & \ddots & & \\ & & \lambda_r I_{k_r} & B_r \\ C_1 & \cdots & C_r & D \end{bmatrix}$$

This realization is controllable and observable (minimal) by PBH tests.

## System Poles and Zeros

An example:

$$G(s) = \begin{bmatrix} \frac{1}{s+1} & \frac{1}{s+2} \\ \frac{s+1}{2} & \frac{1}{s+1} \end{bmatrix}$$

which is stable and each element of  $G(s)$  has no finite zeros. Let

$$K = \begin{bmatrix} \frac{s+2}{s-\sqrt{2}} & \frac{s+1}{s-\sqrt{2}} \\ 0 & 1 \end{bmatrix}$$

which is unstable.

However,

$$KG = \begin{bmatrix} \frac{s+2}{(s+1)(s+2)} & 0 \\ \frac{2}{s+2} & \frac{1}{s+1} \end{bmatrix}$$

is stable. This implies that  $G(s)$  must have an unstable zero at  $\sqrt{2}$  that cancels the unstable pole of  $K$ .

## Smith Form

• A square polynomial matrix  $Q(s)$  is *unimodular* iff  $\det Q(s)$  is constant.

• Let  $Q(s)$  be a  $(p \times m)$  polynomial matrix. Then the *normal rank* of  $Q(s)$ , denoted  $\text{normalrank}(Q(s))$ , is the maximally possible rank of  $Q(s)$  for at least one  $s \in \mathbb{C}$ .

Example:

$$Q(s) = \begin{bmatrix} s & 1 \\ s^2 & 1 \\ s & 1 \end{bmatrix}$$

$Q(s)$  has normal rank 2 since  $\text{rank } Q(2) = 2$ . However,  $Q(0)$  has rank 1.

• *Smith form*: Let  $P(s)$  be any polynomial matrix, then there exist unimodular matrices  $U(s), V(s) \in \mathbb{R}[s]$  such that

$$U(s)P(s)V(s) = S(s) := \begin{bmatrix} \gamma_1(s) & 0 & \cdots & 0 & 0 \\ 0 & \gamma_2(s) & \cdots & 0 & 0 \\ \vdots & \vdots & \ddots & \vdots & \vdots \\ 0 & 0 & \cdots & \gamma_r(s) & 0 \\ 0 & 0 & \cdots & 0 & 0 \end{bmatrix}$$

where  $\gamma_i(s)$  divides  $\gamma_{i+1}(s)$  and  $r$  is the normal rank of  $P(s)$ .

$S(s)$  is called the *Smith form* of  $P(s)$ .

## Smith-McMillan Form

• Let  $G(s)$  be any proper real transfer matrix, then there exist unimodular matrices  $U(s), V(s) \in \mathbb{R}[s]$  such that

$$U(s)G(s)V(s) = M(s) := \begin{bmatrix} \frac{\alpha_1(s)}{\beta_1(s)} & 0 & \cdots & 0 & 0 \\ 0 & \frac{\alpha_2(s)}{\beta_2(s)} & \cdots & 0 & 0 \\ \vdots & \vdots & \ddots & \vdots & \vdots \\ 0 & 0 & \cdots & \frac{\alpha_r(s)}{\beta_r(s)} & 0 \\ 0 & 0 & \cdots & 0 & 0 \end{bmatrix}$$

and  $\alpha_i(s)$  divides  $\alpha_{i+1}(s)$  and  $\beta_{i+1}(s)$  divides  $\beta_i(s)$ .

• Write  $G(s)$  as  $G(s) = N(s)/d(s)$  such that  $d(s)$  is a scalar polynomial and  $N(s)$  is a  $p \times m$  polynomial matrix.

Let the Smith form of  $N(s)$  be  $S(s) = U(s)N(s)V(s)$ .

Then  $M(s) = S(s)/d(s)$ .

Example:

$$P(s) = \begin{bmatrix} s+1 & (s+1)(2s+1) & s(s+1) \\ s+2 & (s+2)(s^2+5s+3) & s(s+2) \\ 1 & 2s+1 & s \end{bmatrix}$$

$P(s)$  has normal rank 2 since  $\det(P(s)) \neq 0$  and

$$\det \begin{bmatrix} s+1 & (s+1)(2s+1) \\ s+2 & (s+2)(s^2+5s+3) \end{bmatrix} = (s+1)^2(s+2)^2 \neq 0.$$

Let

$$U = \begin{bmatrix} 0 & 0 & 1 \\ 0 & 1 & -(s+2) \\ 1 & 0 & -(s+1) \end{bmatrix} \quad V(s) = \begin{bmatrix} 1 & -(2s+1) & -s \\ 0 & 1 & 0 \\ 0 & 0 & 1 \end{bmatrix}$$

$$S(s) = U(s)P(s)V(s) = \begin{bmatrix} 1 & 0 & 0 \\ 0 & (s+1)(s+2)^2 & 0 \\ 0 & 0 & 0 \end{bmatrix}$$



## Poles and Transmission Zeros

- **McMillan degree** of  $G(s) = \sum \deg(\beta_i(s))$  where  $\deg(\beta_i(s))$  denotes the degree of the polynomial  $\beta_i(s)$ .
- **McMillan degree** of  $G(s)$  = the dimension of a minimal realization of  $G(s)$ .
- **Poles** of  $G(s)$  = roots of  $\beta_i(s)$
- **transmission zeros** of  $G(s)$  = the roots of  $\alpha_i(s)$
- $z_0 \in \mathbb{C}$  is a **blocking zero** of  $G(s)$  if  $G(z_0) = 0$ .

An example:

$$G(s) = \begin{bmatrix} \frac{1}{(s+1)(s+2)} & \frac{2s+1}{(s+1)(s+2)} & \frac{s}{(s+1)(s+2)} \\ \frac{1}{(s+1)^2} & \frac{s^2+5s+3}{(s+1)^2} & \frac{s}{(s+1)^2} \\ \frac{1}{(s+1)^2(s+2)} & \frac{2s+1}{(s+1)^2(s+2)} & \frac{s}{(s+1)^2(s+2)} \end{bmatrix}$$

Then  $G(s)$  can be written as

$$G(s) = \frac{1}{(s+1)^2(s+2)} \begin{bmatrix} s+1 & (s+1)(2s+1) & s(s+1) \\ s+2 & (s^2+5s+3)(s+2) & s(s+2) \\ 1 & 2s+1 & s \end{bmatrix}$$

$G(s)$  has the McMillan form

McMillan degree of  $G(s) = 4$ .

Poles:  $\{-1, -1, -1, -2\}$ .

Transmission zero:  $\{-2\}$ .

The transfer matrix has pole and zero at the same location  $\{-2\}$ ; this is the unique feature of multivariable systems.

$$M(s) = \begin{bmatrix} \frac{1}{(s+1)^2(s+2)} & 0 & 0 \\ 0 & \frac{s+2}{s+1} & 0 \\ 0 & 0 & 0 \end{bmatrix}$$

## Alternative Characterizations

- Let  $G(s)$  have full column normal rank. Then  $z_0 \in \mathbb{C}$  is a transmission zero if and only if there exists a vector  $0 \neq u_0$  such that  $G(z_0)u_0 = 0$ .

not true if  $G(s)$  does not have full column normal rank:

$$G(s) = \frac{1}{s+1} \begin{bmatrix} 1 & 1 \\ 1 & 1 \end{bmatrix}, u_0 = \begin{bmatrix} 1 \\ -1 \end{bmatrix}$$

$G$  has no transmission zero but  $G(s)u_0 = 0$  for all  $s$ .

$z_0$  can be a pole of  $G(s)$  even though  $G(z_0)$  is not defined. (however  $G(z_0)u_0$  may be well defined.)

For example,

$$G(s) = \begin{bmatrix} \frac{s-1}{s+1} & 0 \\ 0 & \frac{s+2}{s-1} \end{bmatrix}, u_0 = \begin{bmatrix} 1 \\ 0 \end{bmatrix}$$

Then  $G(1)u_0 = 0$ . Therefore, 1 is a transmission zero.

- Let  $G(s)$  have full row normal rank. Then  $z_0 \in \mathbb{C}$  is a transmission zero if and only if there exists a vector  $\eta_0 \neq 0$  such that  $\eta_0^* G(z_0) = 0$ .

- Suppose  $z_0 \in \mathbb{C}$  is not a pole of  $G(s)$ . Then  $z_0$  is a transmission zero if and only if

$$\text{rank}(G(z_0)) < \text{normalrank}(G(s)).$$

- Let  $G(s)$  be a square  $m \times m$  matrix and  $\det G(s) \neq 0$ . Suppose  $z_0 \in \mathbb{C}$  is not a pole of  $G(s)$ . Then  $z_0$  is a transmission zero if and only if  $\det G(z_0) = 0$ .

$$\det \begin{bmatrix} \frac{1}{s+1} & \frac{1}{s+2} \\ \frac{s+1}{2} & \frac{1}{s+1} \end{bmatrix} = \frac{2-s^2}{(s+1)^2(s+2)^2}$$

## Invariant Zeros (state space)

- The poles and zeros of a transfer matrix can also be characterized in terms of its state space realizations:

$$G(s) = \begin{bmatrix} A & B \\ C & D \end{bmatrix}$$

Consider the following system matrix

$$Q(s) = \begin{bmatrix} A-sI & B \\ C & D \end{bmatrix}$$

$z_0$  is an invariant zero of the realization if it satisfies

$$\text{rank} \begin{bmatrix} A-z_0I & B \\ C & D \end{bmatrix} < \text{normalrank} \begin{bmatrix} A-sI & B \\ C & D \end{bmatrix}$$

- Suppose  $\begin{bmatrix} A-sI & B \\ C & D \end{bmatrix}$  has full column normal rank. Then  $z_0$  is an invariant zero iff there exist  $0 \neq x \in \mathbb{C}^n$  and  $u \in \mathbb{C}^m$  such that

$$\begin{bmatrix} A-z_0I & B \\ C & D \end{bmatrix} \begin{bmatrix} x \\ u \end{bmatrix} = 0$$

Moreover, if  $u = 0$ , then  $z_0$  is also a non-observable mode.

- Suppose  $\begin{bmatrix} A-sI & B \\ C & D \end{bmatrix}$  has full row normal rank. Then  $z_0$  is an invariant zero iff there exist  $0 \neq y \in \mathbb{C}^n$  and  $v \in \mathbb{C}^p$  such that

$$\begin{bmatrix} y^* & v^* \end{bmatrix} \begin{bmatrix} A-z_0I & B \\ C & D \end{bmatrix} = 0$$

Moreover, if  $v = 0$ , then  $z_0$  is also a non-controllable mode.

- $G(s)$  has full column(row) normal rank if and only if  $\begin{bmatrix} A-sI & B \\ C & D \end{bmatrix}$  has full column(row) normal rank.

This follows by noting that

$$\begin{bmatrix} A-sI & B \\ C & D \end{bmatrix} = \begin{bmatrix} I & 0 \\ C(A-sI)^{-1} & I \end{bmatrix} \begin{bmatrix} A-sI & B \\ 0 & G(s) \end{bmatrix}$$

and

$$\text{normalrank} \begin{bmatrix} A-sI & B \\ C & D \end{bmatrix} = n + \text{normalrank}(G(s)).$$

- Let  $G(s) = \begin{bmatrix} A & B \\ C & D \end{bmatrix}$  be a minimal realization. Then  $z_0$  is a transmission zero of  $G(s)$  iff it is an invariant zero of the minimal realization.



• Let  $G(s)$  be a  $p \times m$  transfer matrix and let  $(A, B, C, D)$  be a minimal realization. Let the input be  $u(t) = u_0 e^{st}$ , where  $s$  is not a pole of  $G(s)$  and  $u_0 \in \mathbb{C}^m$  is an arbitrary constant vector, then the output with the initial state  $x(0) = (sI - A)^{-1} B u_0$  is  $y(t) = G(s) u_0 e^{st}$ .

• Let  $G(s)$  be a  $p \times m$  transfer matrix and let  $(A, B, C, D)$  be a minimal realization. Suppose that  $z_0$  is a transmission zero of  $G(s)$  and is not a pole of  $G(s)$ . Then for any nonzero vector  $u_0 \in \mathbb{C}^m$  such that  $G(z_0) u_0 = 0$ , the output of the system due to the initial state  $x(0) = (z_0 I - A)^{-1} B u_0$  and the input  $u(t) = u_0 e^{z_0 t}$  is identically zero:  $y(t) = G(z_0) u_0 e^{z_0 t} = 0$ .

• Computing Invariant Zeros: generalized eigenvalue problem

$$\underbrace{\begin{bmatrix} A & B \\ C & D \end{bmatrix}}_M \underbrace{\begin{bmatrix} x \\ u \end{bmatrix}}_N = \underbrace{\begin{bmatrix} I & 0 \\ 0 & 0 \end{bmatrix}}_N \underbrace{\begin{bmatrix} x \\ u \end{bmatrix}}_N$$

• MATLAB command: `eig(M,N)`.

## Example



Let

$$G(s) = \begin{bmatrix} A & B \\ C & D \end{bmatrix} = \begin{bmatrix} -1 & -2 & 1 & 1 & 2 & 3 \\ 0 & 2 & -1 & 3 & 2 & 1 \\ -4 & -3 & -2 & 1 & 1 & 1 \\ 1 & 1 & 1 & 0 & 0 & 0 \\ 2 & 3 & 4 & 0 & 0 & 0 \end{bmatrix}$$

invariant zeros:

`>> G=ss(A,B,C,D), z0 = tzero(G), % or`

`>> z0 = tzero(A,B,C,D)`

which gives  $z_0 = 0.2$ . Since  $G(s)$  is full-row rank, we can find  $y$  and  $v$ :

$$\begin{bmatrix} y^* & v^* \end{bmatrix} \begin{bmatrix} A - z_0 I & B \\ C & D \end{bmatrix} = 0,$$

$$\begin{bmatrix} y \\ v \end{bmatrix} = \begin{bmatrix} 0.0466 \\ 0.0466 \\ -0.1866 \\ -0.9702 \\ 0.1399 \end{bmatrix}$$

`>> null([A-z0*eye(3),B;C,D])`

## Chapter 4: $H_2$ and $H_\infty$ Spaces



- Hilbert Space
- $H_2$  and  $H_\infty$  Functions
- State Space Computation of  $H_2$  and  $H_\infty$  norms

## Inner Product



• Inner Product: Let  $V$  be a vector space over  $\mathbb{C}$ . An inner product on  $V$  is a complex valued function,  $\langle \cdot, \cdot \rangle: V \times V \rightarrow \mathbb{C}$

Such that for any  $x, y, z \in V$  and  $a, b \in \mathbb{C}$

- (i)  $\langle x, ay + bz \rangle = a \langle x, y \rangle + b \langle x, z \rangle$
- (ii)  $\langle x, y \rangle = \overline{\langle y, x \rangle}$  (complex conjugate)
- (iii)  $\langle x, x \rangle \geq 0$  if  $x \neq 0$

• Inner product on  $\mathbb{C}^n$ :

$$\langle x, y \rangle := x^* y = \sum_{i=1}^n \bar{x}_i y_i, \quad \forall x = \begin{bmatrix} x_1 \\ \vdots \\ x_n \end{bmatrix}, y = \begin{bmatrix} y_1 \\ \vdots \\ y_n \end{bmatrix} \in \mathbb{C}^n,$$

$$\|x\| = \sqrt{\langle x, x \rangle}, \quad \cos \angle(x, y) = \frac{\langle x, y \rangle}{\|x\| \|y\|}, \quad \angle(x, y) \in [0, \pi].$$

$x$  and  $y$  are orthogonal if  $\angle(x, y) = \frac{1}{2}\pi$

## Properties of Inner Product



A vector space  $V$  with an inner product is called an *inner product space*.

Inner product induced norm  $\|x\| := \sqrt{\langle x, x \rangle}$

Distance between vectors  $x$  and  $y$ :  $d(x, y) = \|x - y\|$ .

Two vectors  $x$  and  $y$  are *orthogonal* if  $\langle x, y \rangle = 0$ , denoted  $x \perp y$ .

• Properties of Inner Product:

- ✧  $|\langle x, y \rangle| \leq \|x\| \|y\|$  (Cauchy-Schwarz inequality). Equality holds iff  $x = \alpha y$  for some constant  $\alpha$  or  $y = 0$ .
- ✧  $\|x+y\|^2 + \|x-y\|^2 = 2(\|x\|^2 + \|y\|^2)$  (Parallelogram law)
- ✧  $\|x+y\|^2 = \|x\|^2 + \|y\|^2$  if  $x \perp y$ .

## Hilbert Spaces



• Hilbert Space: a complete inner product space. (We shall not discuss the completeness here.)

Examples:

- ✧  $\mathbb{C}^n$  with the usual inner product.
- ✧  $\mathbb{C}^n \times \mathbb{C}^m$  with the following inner product  $\langle A, B \rangle := \text{Trace } A^* B, \quad \forall A, B \in \mathbb{C}^n \times \mathbb{C}^m$
- ✧  $L_2[a, b]$ : all square integrable and Lebesgue measurable functions defined on an interval  $[a, b]$  with the inner product

$$\langle f, g \rangle := \int_a^b f(t)^* g(t) dt, \quad \text{Matrix form: } \langle f, g \rangle := \int_a^b \text{Trace}[f(t)^* g(t)] dt.$$

$$\langle f, g \rangle = \langle g, f \rangle^*, \quad \langle f, f \rangle := \int_a^b \text{Trace}[f(t)^* f(t)] dt.$$

$$\langle f, f \rangle = \|f\|^2 \geq 0, \quad \langle f, f \rangle = 0 \iff f = 0.$$

$$\langle f, f \rangle = \|f\|^2 \geq 0, \quad \langle f, f \rangle = 0 \iff f = 0.$$

$$\langle f, f \rangle = \|f\|^2 \geq 0, \quad \langle f, f \rangle = 0 \iff f = 0.$$

## Analytic Functions

- Let  $S \subset \mathbb{C}$  be an open set, and let  $f(s)$  be a complex valued function defined on  $S$ ,  $f(s) : S \rightarrow \mathbb{C}$ . Then  $f(s)$  is *analytic at a point*  $z_0$  in  $S$  if it is differentiable at  $z_0$  and also at each point in some neighborhood of  $z_0$ .

It is a fact that if  $f(s)$  is analytic at  $z_0$  then  $f$  has continuous derivatives of all orders at  $z_0$ . Hence, it has a power series representation at  $z_0$ .

A function  $f(s)$  is said to be *analytic in  $S$*  if it has a derivative or is analytic at each point of  $S$ .

- Maximum Modulus Theorem:** If  $f(s)$  is defined and continuous on a closed-bounded set  $S$  and analytic on the interior of  $S$ , then

$$\max_{s \in S} |f(s)| = \max_{s \in \partial S} |f(s)|$$

where  $\partial S$  denotes the boundary of  $S$ .

## $L_2$ and $H_2$ Spaces

- $L_2(j\mathbb{R})$  Space: all complex matrix functions  $F$  such that the integral below is bounded:

$$\int_{-\infty}^{\infty} \text{Trace}[F^*(j\omega)F(j\omega)]d\omega < \infty$$

with the inner product

$$\langle F, G \rangle := \frac{1}{2\pi} \int_{-\infty}^{\infty} \text{Trace}[F^*(j\omega)G(j\omega)]d\omega.$$

and the inner product induced norm is given by  $\|F\|_2 := \sqrt{\langle F, F \rangle}$ .

$RL_2(j\mathbb{R})$  or simply  $RL_2$ : all real rational strictly proper transfer matrices with no poles on the imaginary axis.

- $H_2$  Space: a (closed) subspace of  $L_2(j\mathbb{R})$  with functions  $F(s)$  analytic in  $\text{Re}(s) > 0$ .

$$\begin{aligned} \|F\|_2^2 &:= \sup_{\sigma > 0} \left\{ \frac{1}{2\pi} \int_{-\infty}^{\infty} \text{Trace}[F^*(\sigma + j\omega)F(\sigma + j\omega)]d\omega \right\} \\ &= \frac{1}{2\pi} \int_{-\infty}^{\infty} \text{Trace}[F^*(j\omega)F(j\omega)]d\omega. \end{aligned}$$

$RH_2$  (real rational subspace of  $H_2$ ): all strictly proper and real rational stable transfer matrices.

- $H_2^\perp$  Space: the orthogonal complement of  $H_2$  in  $L_2$ , i.e., the (closed) subspace of functions in  $L_2$  that are analytic in  $\text{Re}(s) < 0$ .

$RH_2^\perp$  (the real rational subspace of  $H_2^\perp$ ): all strictly proper rational antistable transfer matrices.

- Parseval's relations:** (between time domain and frequency domain)

$$\begin{aligned} L_2(-\infty, \infty) &\cong L_2(j\mathbb{R}) & L_2[0, \infty) &\cong H_2 & L_2(-\infty, 0] &\cong H_2^\perp \\ \|G\|_2 &= \|g\|_2 & \text{where } G(s) &= L[g(t)] \in L_2(j\mathbb{R}) \end{aligned}$$

## $L_\infty$ and $H_\infty$ Spaces

- $L_\infty(j\mathbb{R})$  Space:  $L_\infty(j\mathbb{R})$  or simply  $L_\infty$  is a Banach space of matrix-valued (or scalar-valued) functions that are (essentially) bounded on  $j\mathbb{R}$ , with norm

$$\|F\|_\infty := \text{ess sup}_{\omega \in \mathbb{R}} \bar{\sigma}[F(j\omega)].$$

$RL_\infty(j\mathbb{R})$  or simply  $RL_\infty$ : all proper and real rational transfer matrices with no poles on the imaginary axis.

- $H_\infty$  Space:  $H_\infty$  is a (closed) subspace of  $L_\infty$  with functions that are analytic and bounded in the open right-half plane. The  $H_\infty$  norm is defined as

$$\|F\|_\infty := \sup_{\text{Re}(s) > 0} \bar{\sigma}[F(s)] = \sup_{\omega \in \mathbb{R}} \bar{\sigma}[F(j\omega)].$$

The second equality can be regarded as a generalization of the maximum modulus theorem for matrix functions. See Boyd and Desoer [1985] for a proof.

$RH_\infty$ : all proper and real rational stable transfer matrices.

## $L_\infty$ and $H_\infty$ Spaces

- $H_\infty$  Space:  $H_\infty$  is a (closed) subspace of  $L_\infty$  with functions that are analytic and bounded in the open left-half plane. The  $H_\infty$  norm is defined as

$$\|F\|_\infty := \sup_{\text{Re}(s) < 0} \bar{\sigma}[F(s)] = \sup_{\omega \in \mathbb{R}} \bar{\sigma}[F(j\omega)].$$

$RH_\infty$ : all proper real rational antistable transfer matrices.

Examples:  $H_2$  functions:  $1/s+1$ ,  $e^{-hs}/s+2$ , ...

$H_\infty$  functions:  $5$ ,  $1/s+1$ ,  $5s+1/s+2$ ,  $e^{-hs}/s+2$ ,  $1/s+1+0.1e^{-hs}$ , ...

$L_\infty$  functions:  $5$ ,  $1/s+1$ ,  $1/(s+1)(s-2)$ ,  $1/s-1+0.1e^{-hs}$

## $H_\infty$ Norm: Induced $H_2$ Norm

- Let  $G(s)$  be a  $p \times q$  transfer matrix. Then a *multiplication operator* is defined as  $M_G: L_2 \rightarrow L_2$ ,  $M_G f = Gf$

$$\text{Then } \|M_G\| = \sup_{f \in L_2} \frac{\|Gf\|_2}{\|f\|_2} = \|G\|_\infty.$$

**Proof:** It is clear that  $\|G\|_\infty$  is the upper bound:

$$\begin{aligned} \|Gf\|_2^2 &= \frac{1}{2\pi} \int_{-\infty}^{\infty} f^*(j\omega)G^*(j\omega)G(j\omega)f(j\omega)d\omega \\ &\leq \|G\|_\infty^2 \frac{1}{2\pi} \int_{-\infty}^{\infty} |f(j\omega)|^2 d\omega = \|G\|_\infty^2 \|f\|_2^2 \end{aligned}$$

To show that  $\|G\|_\infty$  is the least upper bound, first choose a frequency  $\omega_0$  where  $\bar{\sigma}[G(j\omega)]$  is maximum, i.e.,

$$\bar{\sigma}[G(j\omega_0)] = \|G\|_\infty$$

and denote the singular value decomposition of  $G(j\omega_0)$  by

$$G(j\omega_0) = \bar{\sigma} u_1(j\omega_0) v_1^*(j\omega_0) + \sum_{i=2}^r \sigma_i u_i(j\omega_0) v_i^*(j\omega_0)$$

where  $r$  is the rank of  $G(j\omega_0)$  and  $u_i, v_i$  have unit length.

If  $\omega_0 < \infty$ , write  $v_1(j\omega_0)$  as

$$v_1(j\omega_0) = \begin{bmatrix} \alpha_1 e^{j\theta_1} \\ \alpha_2 e^{j\theta_2} \\ \vdots \\ \alpha_q e^{j\theta_q} \end{bmatrix}$$

where  $\alpha_i \in \mathbb{R}$  is such that  $\theta_i \in (-\pi, 0]$ . Now let  $\theta \leq \beta_i \leq \infty$  be such that

$$\theta_i = \angle \left( \frac{\beta_i - j\omega_0}{\beta_i + j\omega_0} \right) \quad \text{(with } \beta_i = \infty \text{ if } \theta_i = 0 \text{)} \text{ and let } f \text{ be given by } f(s) = \begin{bmatrix} \alpha_1 \frac{\beta_1 - s}{\beta_1 + s} \\ \alpha_2 \frac{\beta_2 - s}{\beta_2 + s} \\ \vdots \\ \alpha_q \frac{\beta_q - s}{\beta_q + s} \end{bmatrix} \hat{f}(s)$$

(with 1 replacing  $\frac{\beta_i - s}{\beta_i + s}$  if  $\theta_i = 0$ ) where a scalar function is chosen so that

$$|\hat{f}(j\omega)| = \begin{cases} c, & \text{if } |\omega - \omega_0| < \varepsilon \text{ or } |\omega + \omega_0| < \varepsilon \\ 0, & \text{otherwise} \end{cases}$$

where  $\varepsilon$  is a small positive number and  $c$  is chosen so that  $\hat{f}(s)$  has unit 2-norm, i.e.,  $c = \sqrt{\pi/2\varepsilon}$ . This in turn implies that  $f$  has unit 2-norm.

$$\begin{aligned} \|Gf\|_2^2 &= \frac{1}{2\pi} \int_{-\infty}^{\infty} f^*(j\omega) G^*(j\omega) G(j\omega) f(j\omega) d\omega \\ &\approx \bar{\sigma}^2 [G(-j\omega_0)]^2 \frac{1}{2\pi} \int_{-\omega_0-\varepsilon}^{-\omega_0+\varepsilon} \hat{f}^*(j\omega) \hat{f}(j\omega) d\omega \\ &\quad + \bar{\sigma}^2 [G(j\omega_0)]^2 \frac{1}{2\pi} \int_{\omega_0-\varepsilon}^{\omega_0+\varepsilon} \hat{f}^*(j\omega) \hat{f}(j\omega) d\omega \\ &\approx \frac{1}{2\pi} \left[ \bar{\sigma}^2 [G(-j\omega_0)]^2 \pi + \bar{\sigma}^2 [G(j\omega_0)]^2 \pi \right] = \bar{\sigma}^2 [G(j\omega_0)]^2 = \|G\|_{\infty}^2. \end{aligned}$$

Similarly, if  $\omega_0 = \infty$ , the conclusion follows by letting  $\omega_0 \rightarrow \infty$  in the above.

## Computing $L_2$ and $H_2$ Norms

- Let  $G(s) \in L_2$  and  $g(t) = L^{-1} [G(s)]$ . Then

$$\begin{aligned} \|G\|_2^2 &= \frac{1}{2\pi} \int_{-\infty}^{\infty} \text{trace}\{G^*(j\omega) G(j\omega)\} d\omega = \frac{1}{2\pi} \int_{-\infty}^{\infty} \text{trace}\{G^T(-s) G(s)\} ds \\ &= \sum \text{the residues of } \text{trace}\{G^T(-s) G(s)\} \\ &\quad \text{at its poles in the left half plane.} \\ &= \int_{-\infty}^{\infty} \text{trace}\{g^*(t) g(t)\} dt = \|g(t)\|_2^2 \end{aligned}$$

Consider  $G(s) = C(sI - A)^{-1} B \in RH_2$ . Then we have

$$\|G(s)\|_2^2 = \text{trace}(B^* L_B B) = \text{trace}(C L_C C^*)$$

where  $L_B$  and  $L_C$  are observability and controllability Gramians:

$$A L_C + L_C A^* + B B^* = 0 \quad A^* L_B + L_B A + C^* C = 0$$

- Proof: Note that  $g(t) = L^{-1} [G(s)] = C e^{At} B$ ,  $t \geq 0$ , and

$$L_B = \int_0^{\infty} e^{A^* t} C^* C e^{At} dt, \quad L_C = \int_0^{\infty} e^{At} B B^* e^{A^* t} dt$$

Then

$$\begin{aligned} \|G\|_2^2 &= \int_0^{\infty} \text{trace}\{g^*(t) g(t)\} dt = \int_0^{\infty} \text{trace}\{B^* e^{A^* t} C^* C e^{At} B\} dt \\ &= \text{trace}\left\{B^* \int_0^{\infty} e^{A^* t} C^* C e^{At} dt B\right\} = \text{trace}\{B^* L_B B\} \\ &= \int_0^{\infty} \text{trace}\{g(t) g^*(t)\} dt = \text{trace}\left\{C \int_0^{\infty} e^{At} B B^* e^{A^* t} dt C^*\right\} = \text{trace}\{C L_C C^*\} \end{aligned}$$

## Computing $L_2$ and $H_2$ Norms

- Hypothetical input-output experiments:

Apply the impulsive input  $\delta(t) e_i$  ( $\delta(t)$  is the unit impulse and  $e_i$  is the  $i^{\text{th}}$  standard basis vector) and denote the output by  $z_i(t) (= g(t) e_i)$ . Then  $z_i \in L_2$  (assuming  $D = 0$ ) and

$$\|G\|_2^2 = \sum_{i=1}^m \|z_i\|_2^2$$

Can be used for nonlinear time varying systems.

- Example: Consider a transfer matrix

$$G = \begin{bmatrix} \frac{3(s+3)}{(s-1)(s+2)} & \frac{2}{s-1} \\ \frac{s+1}{(s+2)(s+3)} & \frac{1}{s-4} \end{bmatrix} = G_s + G_a$$

with

$$G_s = \begin{bmatrix} -2 & 0 & -1 & 0 \\ 0 & -3 & 2 & 0 \\ 1 & 0 & 0 & 0 \\ 1 & 1 & 0 & 0 \end{bmatrix}, \quad G_a = \begin{bmatrix} 1 & 0 & 4 & 2 \\ 0 & 4 & 0 & 1 \\ 1 & 0 & 0 & 0 \\ 0 & 1 & 0 & 0 \end{bmatrix}$$

Then the command `norm(Gs)` gives  $\|G_s\|_2 = 0.6055$  and `norm(Ga(-s))` gives  $\|G_a\|_2 = 3.182$ . Hence

$$\|G\|_2 = \sqrt{\|G_s\|_2^2 + \|G_a\|_2^2} = 3.2393$$

>> `P = gram(A,B); Q = gram(A',C')`; or `P = lyap(A,B*B')`;

>> `[Gs,Gu] = stabsep(G); % decompose into stable and antistable parts.`

## Computing $L_\infty$ and $H_\infty$ Norms

- Rational Functions: Let  $G(s) \in RL_\infty$ :
  - the farthest distance the Nyquist plot of  $G$  from the origin  $\|G\|_\infty := \sup_{\omega \in \mathbb{R}} \overline{\sigma}(G(j\omega))$ .
  - the peak on the Bode magnitude plot
  - estimation: set up a fine grid of frequency points,  $\{\omega_1, \dots, \omega_N\}$ .

$$\|G\|_\infty \approx \max_{1 \leq k \leq N} \overline{\sigma}(G(j\omega_k)).$$

- Characterization: Let  $\gamma > 0$  and  $G(s) = \begin{bmatrix} A & B \\ C & D \end{bmatrix} \in RL_\infty$ . Then

$$\|G\|_\infty < \gamma \Leftrightarrow \overline{\sigma}(D) < \gamma \text{ \& } H \text{ has no } j\omega \text{ eigenvalues}$$

where

$$H = \begin{bmatrix} A + BR^{-1}D^*C & BR^{-1}B^* \\ -C^*(I + DR^{-1}D^*)C & -(A + BR^{-1}D^*C)^* \end{bmatrix}$$

and  $R = \gamma^2 I - D^*D$ .

- Proof: Let  $\Phi(s) = \gamma^2 I - G^*(s)G(s)$ .

Then  $\|G\|_\infty < \gamma \Leftrightarrow \Phi(j\omega) > 0, \forall \omega \in \mathbb{R} \cup \{\infty\} \Leftrightarrow \det \Phi(j\omega) \neq 0, \forall \omega \in \mathbb{R}$  since  $\Phi(\infty) = R > 0$  and  $\Phi(j\omega)$  is continuous.  $\Leftrightarrow \Phi(s)$  has no imaginary axis zero.  $\Leftrightarrow \Phi^{-1}(s)$  has no imaginary axis pole.

$$\Phi^{-1}(s) = \begin{bmatrix} H & \begin{bmatrix} BR^{-1} \\ -C^*DR^{-1} \end{bmatrix} \\ \begin{bmatrix} R^{-1}D^*C & R^{-1}B^* \end{bmatrix} & R^{-1} \end{bmatrix}$$

$\Leftrightarrow H$  has no  $j\omega$  axis eigenvalues if the above realization has neither uncontrollable modes nor unobservable modes on the imaginary axis.

- We now show that the above realization for  $\Phi^{-1}(s)$  indeed has neither uncontrollable modes nor unobservable modes on the imaginary axis.

Assume that  $j\omega_0$  is an eigenvalue of  $H$  but not a pole of  $\Phi^{-1}(s)$ . Then  $j\omega_0$  must be either an unobservable mode of  $([R^{-1}D^*C \ R^{-1}B^*], H)$  or an uncontrollable mode of  $(H, \begin{bmatrix} BR^{-1} \\ -C^*DR^{-1} \end{bmatrix})$ . Suppose  $j\omega_0$  is an unobservable mode of

$([R^{-1}D^*C \ R^{-1}B^*], H)$ . Then there exists an  $x_0 = \begin{bmatrix} x_1 \\ x_2 \end{bmatrix} \neq 0$  such that

$$Hx_0 = j\omega_0 x_0, [R^{-1}D^*C \ R^{-1}B^*]x_0 = 0.$$

$$(j\omega_0 I - A)x_1 = 0, (j\omega_0 I + A^*)x_2 = -C^*Cx_1, D^*Cx_1 + B^*x_2 = 0.$$

Since  $A$  has no imaginary axis eigenvalues, we have  $x_1 = 0$  and  $x_2 = 0$ . Contradiction!!!

Similarly, a contradiction will also be arrived if  $j\omega_0$  is assumed to be an uncontrollable mode of  $(H, \begin{bmatrix} BR^{-1} \\ -C^*DR^{-1} \end{bmatrix})$ .

## Bisection Algorithm

- (a) select an upper bound  $\gamma_u$  and a lower bound  $\gamma_l$  such that  $\gamma_l \leq \|G\|_\infty \leq \gamma_u$
- (b) if  $(\gamma_u - \gamma_l)/\gamma_l \leq$  specified level, stop;  $\|G\|_\infty \approx (\gamma_u + \gamma_l)/2$ . Otherwise go to next step.
- (c) set  $\gamma = (\gamma_l + \gamma_u)/2$ ;
- (d) test if  $\|G\|_\infty < \gamma$  by calculating the eigenvalues of  $H$  with this  $\gamma$ ;
- (e) if  $H$  has an eigenvalue on  $j\mathbb{R}$  set  $\gamma_l = \gamma$ ; otherwise set  $\gamma_u = \gamma$ ; go back to step (b).
- In all the subsequent discussions, WLOG we can assume  $\gamma = 1$  by a suitable scaling since  $\|G\|_\infty < \gamma \Leftrightarrow \|\gamma^{-1}G\|_\infty < 1$ .

## Estimating the $H_\infty$ Norm

- Estimating the  $H_\infty$  norm experimentally: the maximum magnitude of the steady-state response to all possible unit amplitude sinusoidal input signals.

$$z(t) = |G(j\omega)| \sin(\omega t + \angle G(j\omega)) \quad u(t) = \sin \omega t$$

Let the sinusoidal input  $u(t)$  as shown below. Then the steady-state response of the system can be written as

$$u(t) = \begin{bmatrix} u_1 \sin(\omega_0 t + \phi_1) \\ u_2 \sin(\omega_0 t + \phi_2) \\ \vdots \\ u_p \sin(\omega_0 t + \phi_p) \end{bmatrix}, \quad y(t) = \begin{bmatrix} y_1 \sin(\omega_0 t + \theta_1) \\ y_2 \sin(\omega_0 t + \theta_2) \\ \vdots \\ y_p \sin(\omega_0 t + \theta_p) \end{bmatrix}, \quad \dot{u} = \begin{bmatrix} u_1 \\ u_2 \\ \vdots \\ u_p \end{bmatrix}, \quad \dot{y} = \begin{bmatrix} y_1 \\ y_2 \\ \vdots \\ y_p \end{bmatrix}$$

for some  $y_i, i = 1, 2, \dots, p$ , and furthermore,

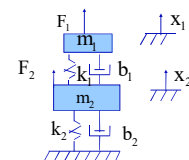
where  $\|\cdot\|$  is the Euclidean norm.

$$\|G\|_\infty = \sup_{\theta_1, \omega_0, \phi_i} \frac{\|\dot{y}\|}{\|\dot{u}\|}$$

## Examples

- Consider a mass/spring/damper system as shown in Figure 4.2.

The dynamical system can be described by the following differential equations:



$$\begin{bmatrix} \dot{x}_1 \\ \dot{x}_2 \end{bmatrix} = A \begin{bmatrix} x_1 \\ x_2 \end{bmatrix} + B \begin{bmatrix} F_1 \\ F_2 \end{bmatrix}, \quad A = \begin{bmatrix} 0 & 0 & 1 & 0 \\ 0 & 0 & 0 & 1 \\ -\frac{k_1}{m_1} & -\frac{k_2}{m_1} & -\frac{b_1}{m_1} & -\frac{b_2}{m_1} \\ \frac{k_2}{m_2} & -\frac{k_2}{m_2} & \frac{b_2}{m_2} & -\frac{b_2}{m_2} \end{bmatrix}, \quad B = \begin{bmatrix} 0 & 0 \\ 0 & 0 \\ \frac{1}{m_1} & 0 \\ 0 & \frac{1}{m_2} \end{bmatrix}$$

Suppose that  $G(s)$  is the transfer matrix from  $(F_1, F_2)$  to  $(x_1, x_2)$ ; that is,

$$C = \begin{bmatrix} 1 & 0 & 0 & 0 \\ 0 & 1 & 0 & 0 \end{bmatrix}, \quad D = 0$$

and suppose  $k_1=1, k_2=4, b_1=0.2, b_2=0.1, m_1=1$ , and  $m_2=2$  with appropriate units.

```
>>G=ss(A,B,C,D);
```

```
>>norm(G,inf,0.0001) % relative error ≤0.0001
```

```
>>w=logspace(-1,1,200); %200 points between 0.1=10-1 and 10=101;
```

```
>>Gf=freqresp(G,w); %computing frequency response;
```

```
>>sigma(G,w), grid %plot both singular values and grid.
```

$\|G\|_\infty=11.47$ =the peak of the largest singular value Bode plot in Figure 4.3.

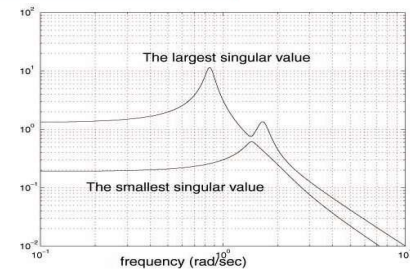


Figure 4.3:  $\|G\|_\infty$  is the peak of the largest singular value of  $G(j\omega)$

$$\|G\|_\infty=11.47, \quad \omega_{max}=0.8483$$

Since the peak is achieved at  $\omega_{max}=0.8483$ , exciting the system using the following sinusoidal input

$$\begin{bmatrix} F_1 \\ F_2 \end{bmatrix} = \begin{bmatrix} 0.9614 \sin(0.8483t) \\ 0.2753 \sin(0.8483t - 0.12) \end{bmatrix}$$

gives the steady-state response of the system as

$$\begin{bmatrix} x_1 \\ x_2 \end{bmatrix} = \begin{bmatrix} 11.47 \times 0.9614 \sin(0.8483t - 1.5483) \\ 11.47 \times 0.2753 \sin(0.8483t - 1.4283) \end{bmatrix}$$

This shows that the system response will be amplified 11.47 times for an input signal at the frequency  $\omega_{max}$ , which could be undesirable if  $F_1$  and  $F_2$  are disturbance force and  $x_1$  and  $x_2$  are the positions to be kept steady.

▪ Example 2: Consider a two-by-two transfer matrix

$$G(s) = \begin{bmatrix} \frac{10(s+1)}{s^2+0.2s+100} & \frac{1}{s+1} \\ \frac{s+2}{s^2+0.1s+10} & \frac{5(s+1)}{(s+2)(s+3)} \end{bmatrix}$$

A state-space realization of  $G$  can be obtained by using the following MATLAB commands:

```
>>G11=tf([10,10],[1,0.2,100]);
```

```
>>G12=tf([1,1],[1,1]);
```

```
>>G21=tf([1,2],[1,0.1,10]);
```

```
>>G22=tf([5,5],[1,5,6]);
```

```
>>G=[G11,G12;G21,G22];
```

Next, we setup a frequency grid to compute the frequency response of  $G$  and the singular values of  $G(j\omega)$  over a suitable range of frequency.

```
>>w=logspace(0,2,200); % 200 points between 1=100 and 100=102;
```

```
>>sigma(G,w), grid %plot both singular values and grid;
```

The singular values of  $G(j\omega)$  are plotted in Figure 4.4, which gives an estimate of  $\|G\|_\infty \approx 32.861$ . The state-space bisection algorithm described previously leads to  $\|G\|_\infty = 50.25 \pm 0.01$  and the corresponding MATLAB command is

```
>>norm(G,inf,0.0001) % relative error ≤0.0001.
```

The preceding computational results show clearly that the graphical method can lead to a wrong answer for a lightly damped system if the frequency grid is not sufficiently dense. Indeed, we would get  $\|G\|_\infty \approx 43.525, 48.286$  and  $49.737$  from the graphical method if 400, 800, and 1600 frequency points are used respectively.

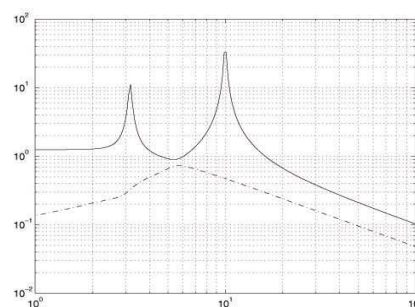


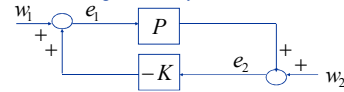
Figure 4.4 The largest and the smallest singular values of  $G(j\omega)$

## Chapter 5: Internal Stability

- Internal stability
- Coprime factorization over  $RH_\infty$

## Internal Stability

Consider the following feedback system:



- well-posed if  $I + K(\infty)P(\infty)$  is invertible.

• **Internal Stability:** if

$$\begin{bmatrix} I & K \\ -P & I \end{bmatrix}^{-1} = \begin{bmatrix} (I + KP)^{-1} & -K(I + PK)^{-1} \\ P(I + KP)^{-1} & (I + PK)^{-1} \end{bmatrix} \in RH_\infty$$

- Need to check all Four transfer matrices. For example,

$$P = \frac{s-1}{s+1}, \quad K = \frac{1}{s-1}, \quad \begin{bmatrix} I & K \\ -P & I \end{bmatrix}^{-1} = \begin{bmatrix} \frac{s+1}{s+2} & -\frac{s+1}{(s-1)(s+2)} \\ \frac{s-1}{s+2} & \frac{s+1}{s+2} \end{bmatrix}$$

## Special Cases

- Suppose  $K \in RH_\infty$ . Internal stability  $\Leftrightarrow P(I+KP)^{-1} \in RH_\infty$   
This is because  $K \in RH_\infty$  and  $P(I+KP)^{-1} \in RH_\infty \Leftrightarrow KP(I+KP)^{-1} \in RH_\infty \Leftrightarrow I-KP(I+KP)^{-1} = (I+KP)^{-1} \in RH_\infty \Leftrightarrow K(I+PK)^{-1} \in RH_\infty$  and  $P(I+KP)^{-1} \in RH_\infty \Leftrightarrow (I+PK)^{-1} = I-P(I+KP)^{-1}K \in RH_\infty$
- Suppose  $P \in RH_\infty$ . Internal stability  $\Leftrightarrow K(I+PK)^{-1} \in RH_\infty$
- Suppose  $P, K \in RH_\infty$ . Internal stability  $\Leftrightarrow (I+PK)^{-1} \in RH_\infty \Leftrightarrow P(I+KP)^{-1} \in RH_\infty \Leftrightarrow K(I+PK)^{-1} \in RH_\infty$
- Suppose no unstable pole-zero cancellation in  $PK$ . (#PK=#P+#K)  
Internal stability  $\Leftrightarrow (I+PK)^{-1} \in RH_\infty$ .  
(note  $[1,0] [1;1/s-1]=1$  but no unstable pole-zero cancellation)

## Example

Let  $P$  and  $K$  be two-by-two transfer matrices

$$P = \begin{bmatrix} \frac{1}{s-1} & 0 \\ 0 & \frac{1}{s+1} \end{bmatrix}, \quad K = \begin{bmatrix} \frac{s-1}{s+1} & 1 \\ 0 & 1 \end{bmatrix}$$

Then

$$PK = \begin{bmatrix} \frac{1}{s+1} & \frac{1}{s-1} \\ 0 & \frac{1}{s+1} \end{bmatrix}, \quad (I + PK)^{-1} = \begin{bmatrix} \frac{s+1}{s+2} & -\frac{(s+1)^2}{(s-1)(s+2)^2} \\ 0 & \frac{s+1}{s+2} \end{bmatrix}$$

So the closed-loop system is not stable even though

$$\det(I + PK) = \frac{(s+2)^2}{(s+1)^2}$$

has no zero in the closed right-half plane and the number of unstable poles of  $PK = n_k + n_p = 1$ . Hence, in general,  $\det(I + PK)$  having no zeros in the closed right-half plane does not necessarily imply  $(I + PK)^{-1} \in RH_\infty$ .

## Coprime Factorization

- Two polynomials  $m(s)$  and  $n(s)$  are coprime if the only common factors are constants.
- Two transfer functions  $m(s)$  and  $n(s)$  in  $RH_\infty$  are coprime if the only common factors are stable and invertible transfer functions (units): I.e.,  $h, mh^{-1}, nh^{-1} \in RH_\infty \Leftrightarrow h^{-1} \in RH_\infty$

Equivalent, there exists  $x, y \in RH_\infty$  such that

$$xm + yn = I.$$

- Matrices  $M$  and  $N$  in  $RH_\infty$  are right coprime if there exist matrices  $X_r$  and  $Y_r$  in  $RH_\infty$  such that

$$\begin{bmatrix} X_r & Y_r \end{bmatrix} \begin{bmatrix} M \\ N \end{bmatrix} = X_r M + Y_r N = I.$$

- Matrices  $\tilde{M}$  and  $\tilde{N}$  in  $RH_\infty$  are left coprime if there exist matrices  $X_l$  and  $Y_l$  in  $RH_\infty$  such that

$$\begin{bmatrix} \tilde{M} & \tilde{N} \end{bmatrix} \begin{bmatrix} X_l \\ Y_l \end{bmatrix} = \tilde{M} X_l + \tilde{N} Y_l = I.$$

## State Space Formula

- Let  $P = \begin{bmatrix} A & B \\ C & D \end{bmatrix}$  be a stabilizable and detectable realization, and let  $F$  and  $L$  be such that  $A + BF$  and  $A + LC$  are both stable.

$$\text{Define } \begin{bmatrix} M & -Y_l \\ N & X_l \end{bmatrix} = \begin{bmatrix} A + BF & B & -L \\ F & I & 0 \\ C + DF & D & I \end{bmatrix} \begin{bmatrix} X_r & Y_r \\ -\tilde{N} & \tilde{M} \end{bmatrix} = \begin{bmatrix} A + LC & -(B + LD) & L \\ F & I & 0 \\ C & -D & I \end{bmatrix}$$

$$\text{Then } \begin{bmatrix} X_r & Y_r \\ -\tilde{N} & \tilde{M} \end{bmatrix} \begin{bmatrix} M & -Y_l \\ N & X_l \end{bmatrix} = I$$

- Hence  $P = NM^{-1} = \tilde{M}^{-1}\tilde{N}$  are rcf and lcf, respectively.

## Closed-loop Stability

- Let  $P = NM^{-1} = \tilde{M}^{-1}\tilde{N}$  and  $-K = UV^{-1} = \tilde{V}^{-1}\tilde{U}$  be rcf and lcf, respectively. Then the following conditions are equivalent:

1. The feedback system is internally stable.

2.  $\begin{bmatrix} M & U \\ N & V \end{bmatrix}$  is invertible in  $RH_\infty$  3.  $\begin{bmatrix} \tilde{V} & -\tilde{U} \\ -\tilde{N} & \tilde{M} \end{bmatrix}$  is invertible in  $RH_\infty$

4.  $\tilde{M}V - \tilde{N}U$  is invertible in  $RH_\infty$  5.  $\tilde{V}M - \tilde{U}N$  is invertible in  $RH_\infty$

$$\begin{bmatrix} I & K \\ -P & I \end{bmatrix}^{-1} = \begin{bmatrix} I & -UV^{-1} \\ -NM^{-1} & I \end{bmatrix}^{-1} = \begin{bmatrix} -M & 0 \\ 0 & V \end{bmatrix} \begin{bmatrix} M & U \\ N & V \end{bmatrix}^{-1} \begin{bmatrix} -I & 0 \\ 0 & I \end{bmatrix}$$

$$\begin{bmatrix} I & K \\ -P & I \end{bmatrix}^{-1} = \begin{bmatrix} I & -\tilde{V}^{-1}\tilde{U} \\ -\tilde{M}^{-1}\tilde{N} & I \end{bmatrix}^{-1} = \begin{bmatrix} \tilde{V} & -\tilde{U} \\ -\tilde{N} & \tilde{M} \end{bmatrix}^{-1} \begin{bmatrix} \tilde{V} & 0 \\ 0 & \tilde{M} \end{bmatrix}$$

$$\begin{bmatrix} \tilde{V} & -\tilde{U} \\ -\tilde{N} & \tilde{M} \end{bmatrix} \begin{bmatrix} M & U \\ N & V \end{bmatrix} = \begin{bmatrix} \tilde{V}M - \tilde{U}N & \tilde{V}U - \tilde{U}V \\ -\tilde{N}M + \tilde{M}N & -\tilde{N}U + \tilde{M}V \end{bmatrix} = \begin{bmatrix} \tilde{V}M - \tilde{U}N & 0 \\ 0 & -\tilde{N}U + \tilde{M}V \end{bmatrix}$$

## Example

Let  $P(s) = \frac{s-2}{s(s+3)}$  and  $\alpha = (s+1)(s+3)$ . Then  $P(s) = n(s)/m(s)$  with

$$n(s) = \frac{s-2}{(s+1)(s+3)} \text{ and } m(s) = \frac{s}{(s+1)}$$

forms a coprime factorization. To find an  $x(s)$  and a  $y(s)$  such that

$x(s)n(s) + y(s)m(s) = 1$ , consider a stabilizing controller for  $P$ :

$$K = \frac{s-1}{s+10}$$

Then  $-K = u/v$  with  $u = -K$  and  $v = 1$  is a coprime factorization and

$$m(s)v(s) - n(s)u(s) = \frac{(s+11.7085)(s+2.214)(s+0.077)}{(s+1)(s+3)(s+10)} =: \beta(s)$$

Then we can take

$$x(s) = -u(s) / \beta(s) = \frac{(s-1)(s+1)(s+3)}{(s+11.7085)(s+2.214)(s+0.077)}$$

$$y(s) = v(s) / \beta(s) = \frac{(s+1)(s+3)(s+10)}{(s+11.7085)(s+2.214)(s+0.077)}$$

MATLAB programs can be used to find the appropriate  $F$  and  $L$  matrices in state-space so that the desired coprime factorization can be obtained. Let  $A \in \mathbf{R}^{n \times n}$ ,  $B \in \mathbf{R}^{n \times m}$  and  $C \in \mathbf{R}^{p \times n}$ . Then an  $F$  and an  $L$  can be obtained from

- $F = -\text{lqr}(A, B, \text{eye}(n), \text{eye}(m)); \% \text{ or}$
- $F = -\text{place}(A, B, \text{Pf}); \% \text{ Pf} = \text{poles of } A+BF$
- $L = -\text{lqr}(A, C, \text{eye}(n), \text{eye}(p)); \% \text{ or}$
- $L = -\text{place}(A, C, \text{Pl}); \% \text{ Pl} = \text{poles of } A+LC$

## Chapter 6: Perf Specs & Lim

- Feedback Properties
- Weighted and Performance
- Selection of Weighting Performance
- Bode's Gain and Phase Relation
- Bode's Sensitivity Integral
- Analyticity Constraints

## Feedback Properties

Consider a feedback system

and define

$$S = (I + KP)^{-1}, \quad S_o = (I + PK)^{-1}$$

$$T_i = I - S_i = KP(I + KP)^{-1}, \quad T_o = I - S_o = PK(I + PK)^{-1}$$

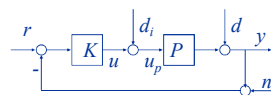
$$Y = T_o(r - n) + S_o P d_i + S_o d$$

$$U = KS_o(r - n) - KS_o d - T_i d_i \quad U_p = KS_o(r - n) - KS_o d + S_i d_i$$

- Disturbance rejection at the plant output (low

$$\bar{\sigma}(S_o) = \bar{\sigma}((I + PK)^{-1}) = \frac{1}{\underline{\sigma}(I + PK)} \quad (< 1)$$

$$\bar{\sigma}(S_o P) = \bar{\sigma}((I + PK)^{-1} P) = \bar{\sigma}(P S_i) \quad (< 1)$$



- Disturbance rejection at the plant input (low frequency):

$$\bar{\sigma}(S_i) = \bar{\sigma}((I + KP)^{-1}) = \frac{1}{\underline{\sigma}(I + KP)} \quad (< 1)$$

$$\bar{\sigma}(S_i K) = \bar{\sigma}(K(I + PK)^{-1}) = \bar{\sigma}(K S_o) \quad (< 1)$$

- Sensor noise rejection and robust stability (high frequency):

$$\bar{\sigma}(T_o) = \bar{\sigma}(PK(I + PK)^{-1}) \quad (< 1)$$

Note that

$$\bar{\sigma}(S_o) < 1 \Leftrightarrow \underline{\sigma}(PK) > 1$$

$$\bar{\sigma}(S_i) < 1 \Leftrightarrow \underline{\sigma}(KP) > 1$$

$$\bar{\sigma}(T_o) < 1 \Leftrightarrow \bar{\sigma}(PK) < 1$$

Now suppose  $P$  and  $K$  are invertible, then

$$\underline{\sigma}(PK) > 1 \text{ or } \underline{\sigma}(KP) > 1$$

$$\Leftrightarrow \begin{cases} \bar{\sigma}(S_o P) = \bar{\sigma}((I + PK)^{-1} P) \approx \bar{\sigma}(K^{-1}) = \frac{1}{\underline{\sigma}(K)} \\ \bar{\sigma}(K S_o) = \bar{\sigma}(K(I + PK)^{-1}) \approx \bar{\sigma}(P^{-1}) = \frac{1}{\underline{\sigma}(P)} \end{cases}$$



## Desired Loop Shape

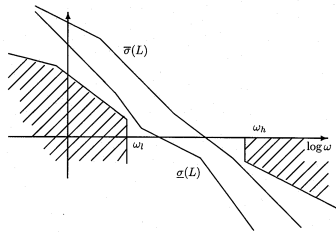
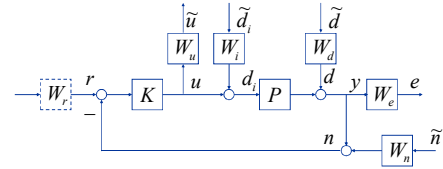


Figure 6.2: Desired loop gain

## Weighted $H_2$ and $H_\infty$



**$H_2$  Performance:** Assume  $d_i(t) = \eta \delta(t)$  and  $E(\eta \eta^*) = I$

Minimize the expected energy of the error e:

$$\mathbb{E} \left\{ \|e\|_2^2 + \rho^2 \|u\|_2^2 \right\} = \mathbb{E} \left\{ \|W_e S_o W_d\|_2^2 + \rho^2 \|W_u K S_o W_d\|_2^2 \right\}$$

Include the control signal u in the cost function:

$$\mathbb{E} \left\{ \|e\|_2^2 + \rho^2 \|u\|_2^2 \right\} = \mathbb{E} \left\{ \|W_e S_o W_d\|_2^2 + \rho^2 \|W_u K S_o W_d\|_2^2 \right\}$$

Robustness problem????

**$H_\infty$  Performance:** under worst possible case

$$\sup_{\|d\|_\infty \leq 1} \|e\|_2 = \|W_e S_o W_d\|_\infty$$

restrictions on the control energy or control bandwidth:

$$\sup_{\|d\|_\infty \leq 1} \|u\|_2 = \|W_u K S_o W_d\|_\infty$$

Combined cost:

$$\sup_{\|d\|_\infty \leq 1} \left\{ \|e\|_2^2 + \rho^2 \|u\|_2^2 \right\} = \mathbb{E} \left\{ \|W_e S_o W_d\|_2^2 + \rho^2 \|W_u K S_o W_d\|_2^2 \right\}$$

## Bode's Gain and Phase

$L$  stable and minimum phase:

$$\angle L(j\omega_0) = \frac{1}{\pi} \int_{-\infty}^{\infty} \frac{d \ln |L|}{dv} \ln \coth \frac{|v|}{2} dv \quad v := \ln(\omega / \omega_0)$$

$$|1 + L(j\omega_c)| = |1 + L^{-1}(j\omega_c)| = 2 \left| \sin \frac{\pi + \angle L(j\omega_c)}{2} \right|,$$

which must not be too small for good stability robustness. It is important to keep the slope of  $L$  near the crossover frequency not much smaller than -1 for a reasonably wide range of frequencies in order to guarantee some reasonable performance.

$L$  stable and nonminimum phase with RHP zeros:  $z_1, \dots, z_k$ :

$$L(s) = \frac{-s + z_1}{s + z_1} \frac{-s + z_2}{s + z_2} \dots \frac{-s + z_k}{s + z_k} L_{mp}(s)$$

$$\angle L(j\omega_0) = \frac{1}{\pi} \int_{-\infty}^{\infty} \frac{d \ln |L|}{dv} \ln \coth \frac{|v|}{2} dv + \sum_{i=1}^k \angle \frac{-j\omega_0 + z_i}{j\omega_0 + z_i},$$

In this case we conclude that the crossover frequency must satisfy the following in order to guarantee the closed-loop stability and some reasonable closed-loop performance.

$$\omega_c < \begin{cases} |z|/4, \Re(z) \gg \Im(z) \\ |z|/3, \Re(z) \approx \Im(z) \\ |z|, \Re(z) \ll \Im(z) \end{cases}$$

## Bode's Sensitivity Integral

Let  $p_1, p_2, \dots, p_m$  be the open right-half plane poles of  $L$

$$\int_0^\infty \ln |S(j\omega)| d\omega = \pi \sum_{i=1}^m \Re(p_i)$$

In the case where  $L$  is stable, the integral simplifies to

$$\int_0^\infty \ln |S(j\omega)| d\omega = 0$$

## Analyticity Constraints



Let  $p_1, p_2, \dots, p_m$  and  $z_1, z_2, \dots, z_k$  be the open right-half plane poles and zeros of  $L$ , respectively.

$$S(p_i) = 0, T(p_i) = 1, i = 1, 2, \dots, m$$

and  $S(z_j) = 1, T(z_j) = 0, j = 1, 2, \dots, k$

Suppose  $S = (I + L)^{-1}$  and  $T = L(I + L)^{-1}$  are stable. Then  $p_1, p_2, \dots, p_m$  are the right-half plane zeros of  $S$  and  $z_1, z_2, \dots, z_k$  are the right-half plane zeros of  $T$ . Let

$$B_p(s) = \prod_{i=1}^m \frac{s - p_i}{s + p_i}, \quad B_z(s) = \prod_{j=1}^k \frac{s - z_j}{s + z_j}$$



Then  $|B_p(j\omega)| = 1$  and  $|B_z(j\omega)| = 1$  for all frequencies and, moreover,

$$B_p^{-1}(s)S(s) \in RH_\infty, \quad B_z^{-1}(s)T(s) \in RH_\infty$$

Hence, by the maximum modulus theorem, we have

$$\|S(s)\|_\infty = \|B_p^{-1}(s)S(s)\|_\infty \geq |B_p^{-1}(z)S(z)| = |B_p^{-1}(z)|$$

for any  $z$  with  $\text{Re } z > 0$ . Let  $z$  be a right-half plane zero of  $L$ ; then

$$\|S(s)\|_\infty \geq |B_p^{-1}(z)| = \prod_{i=1}^m \left| \frac{z + p_i}{z - p_i} \right|$$