



*The Open Source CFD Toolbox*

## Programmer's Guide

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9th July 2008

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# Contents

<b>Copyright Notice</b>	<b>P-2</b>
<b>GNU Free Documentation Licence</b>	<b>P-3</b>
1. APPLICABILITY AND DEFINITIONS . . . . .	P-3
2. VERBATIM COPYING . . . . .	P-4
3. COPYING IN QUANTITY . . . . .	P-4
4. MODIFICATIONS . . . . .	P-5
5. COMBINING DOCUMENTS . . . . .	P-6
6. COLLECTIONS OF DOCUMENTS . . . . .	P-7
7. AGGREGATION WITH INDEPENDENT WORKS . . . . .	P-7
8. TRANSLATION . . . . .	P-7
9. TERMINATION . . . . .	P-7
10. FUTURE REVISIONS OF THIS LICENSE . . . . .	P-7
<b>Trademarks</b>	<b>P-9</b>
<b>Contents</b>	<b>P-11</b>
<b>1 Tensor mathematics</b>	<b>P-15</b>
1.1 Coordinate system . . . . .	P-15
1.2 Tensors . . . . .	P-15
1.2.1 Tensor notation . . . . .	P-17
1.3 Algebraic tensor operations . . . . .	P-17
1.3.1 The inner product . . . . .	P-18
1.3.2 The double inner product of two tensors . . . . .	P-19
1.3.3 The triple inner product of two third rank tensors . . . . .	P-19
1.3.4 The outer product . . . . .	P-19
1.3.5 The cross product of two vectors . . . . .	P-19
1.3.6 Other general tensor operations . . . . .	P-20
1.3.7 Geometric transformation and the identity tensor . . . . .	P-20
1.3.8 Useful tensor identities . . . . .	P-21
1.3.9 Operations exclusive to tensors of rank 2 . . . . .	P-21
1.3.10 Operations exclusive to scalars . . . . .	P-22
1.4 OpenFOAM tensor classes . . . . .	P-23
1.4.1 Algebraic tensor operations in OpenFOAM . . . . .	P-23
1.5 Dimensional units . . . . .	P-25
<b>2 Discretisation procedures</b>	<b>P-27</b>
2.1 Differential operators . . . . .	P-27
2.1.1 Gradient . . . . .	P-27
2.1.2 Divergence . . . . .	P-28

2.1.3	Curl . . . . .	P-28
2.1.4	Laplacian . . . . .	P-28
2.1.5	Temporal derivative . . . . .	P-28
2.2	Overview of discretisation . . . . .	P-29
2.2.1	OpenFOAM lists and fields . . . . .	P-29
2.3	Discretisation of the solution domain . . . . .	P-29
2.3.1	Defining a mesh in OpenFOAM . . . . .	P-31
2.3.2	Defining a <code>geometricField</code> in OpenFOAM . . . . .	P-32
2.4	Equation discretisation . . . . .	P-33
2.4.1	The Laplacian term . . . . .	P-38
2.4.2	The convection term . . . . .	P-38
2.4.3	First time derivative . . . . .	P-39
2.4.4	Second time derivative . . . . .	P-39
2.4.5	Divergence . . . . .	P-39
2.4.6	Gradient . . . . .	P-40
2.4.7	Grad-grad squared . . . . .	P-41
2.4.8	Curl . . . . .	P-41
2.4.9	Source terms . . . . .	P-41
2.4.10	Other explicit discretisation schemes . . . . .	P-41
2.5	Temporal discretisation . . . . .	P-42
2.5.1	Treatment of temporal discretisation in OpenFOAM . . . . .	P-43
2.6	Boundary Conditions . . . . .	P-43
2.6.1	Physical boundary conditions . . . . .	P-44
<b>3</b>	<b>Examples of the use of OpenFOAM</b>	<b>P-45</b>
3.1	Flow around a cylinder . . . . .	P-45
3.1.1	Problem specification . . . . .	P-46
3.1.2	Note on <code>potentialFoam</code> . . . . .	P-47
3.1.3	Mesh generation . . . . .	P-47
3.1.4	Boundary conditions and initial fields . . . . .	P-49
3.1.5	Running the case . . . . .	P-49
3.1.6	Generating the analytical solution . . . . .	P-50
3.1.7	Exercise . . . . .	P-53
3.2	Steady turbulent flow over a backward-facing step . . . . .	P-53
3.2.1	Problem specification . . . . .	P-54
3.2.2	Mesh generation . . . . .	P-55
3.2.3	Boundary conditions and initial fields . . . . .	P-57
3.2.4	Case control . . . . .	P-58
3.2.5	Running the case and post-processing . . . . .	P-58
3.3	Supersonic flow over a forward-facing step . . . . .	P-58
3.3.1	Problem specification . . . . .	P-59
3.3.2	Mesh generation . . . . .	P-60
3.3.3	Running the case . . . . .	P-62
3.3.4	Exercise . . . . .	P-62
3.4	Decompression of a tank internally pressurised with water . . . . .	P-62
3.4.1	Problem specification . . . . .	P-62
3.4.2	Mesh Generation . . . . .	P-64
3.4.3	Preparing the Run . . . . .	P-65
3.4.4	Running the case . . . . .	P-66
3.4.5	Improving the solution by refining the mesh . . . . .	P-67
3.5	Magnetohydrodynamic flow of a liquid . . . . .	P-67

Contents	P-13
3.5.1 Problem specification . . . . .	P-67
3.5.2 Mesh generation . . . . .	P-69
3.5.3 Running the case . . . . .	P-70
<b>Index</b>	<b>P-73</b>



# Chapter 1

## Tensor mathematics

This Chapter describes tensors and their algebraic operations and how they are represented in mathematical text in this book. It then explains how tensors and tensor algebra are programmed in OpenFOAM.

### 1.1 Coordinate system

OpenFOAM is primarily designed to solve problems in continuum mechanics, *i.e.* the branch of mechanics concerned with the stresses in solids, liquids and gases and the deformation or flow of these materials. OpenFOAM is therefore based in 3 dimensional space and time and deals with physical entities described by tensors. The coordinate system used by OpenFOAM is the right-handed rectangular Cartesian axes as shown in [Figure 1.1](#). This system of axes is constructed by defining an origin  $O$  from which three lines are drawn at right angles to each other, termed the  $Ox$ ,  $Oy$ ,  $Oz$  axes. A right-handed set of axes is defined such that to an observer looking down the  $Oz$  axis (with  $O$  nearest them), the arc from a point on the  $Ox$  axis to a point on the  $Oy$  axis is in a clockwise sense.

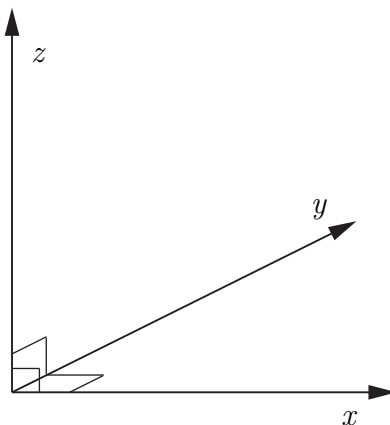


Figure 1.1: Right handed axes

### 1.2 Tensors

The term tensor describes an entity that belongs to a particular space and obeys certain mathematical rules. Briefly, tensors are represented by a set of *component values* relating to a set of unit base vectors; in OpenFOAM the unit base vectors  $\mathbf{i}_x$ ,  $\mathbf{i}_y$  and  $\mathbf{i}_z$  are

aligned with the right-handed rectangular Cartesian axes  $x$ ,  $y$  and  $z$  respectively. The base vectors are therefore orthogonal, *i.e.* at right-angles to one another. Every tensor has the following attributes:

**Dimension**  $d$  of the particular space to which they belong, *i.e.*  $d = 3$  in OpenFOAM;

**Rank** An integer  $r \geq 0$ , such that the number of component values  $= d^r$ .

While OpenFOAM 1.x is set to 3 dimensions, it offers tensors of ranks 0 to 3 as standard while being written in such a way to allow this basic set of ranks to be extended indefinitely. Tensors of rank 0 and 1, better known as scalars and vectors, should be familiar to readers; tensors of rank 2 and 3 may not be so familiar. For completeness all ranks of tensor offered as standard in OpenFOAM 1.x are reviewed below.

**Rank 0 ‘scalar’** Any property which can be represented by a single real number, denoted by characters in italics, *e.g.* mass  $m$ , volume  $V$ , pressure  $p$  and viscosity  $\mu$ .

**Rank 1 ‘vector’** An entity which can be represented physically by both magnitude and direction. In component form, the vector  $\mathbf{a} = (a_1, a_2, a_3)$  relates to a set of Cartesian axes  $x, y, z$  respectively. The *index notation* presents the same vector as  $a_i$ ,  $i = 1, 2, 3$ , although the list of indices  $i = 1, 2, 3$  will be omitted in this book, as it is intuitive since we are always dealing with 3 dimensions.

**Rank 2 ‘tensor’** or second rank tensor,  $\mathbf{T}$  has 9 components which can be expressed in array notation as:

$$\mathbf{T} = T_{ij} = \begin{pmatrix} T_{11} & T_{12} & T_{13} \\ T_{21} & T_{22} & T_{23} \\ T_{31} & T_{32} & T_{33} \end{pmatrix} \quad (1.1)$$

The components  $T_{ij}$  are now represented using 2 indices since  $r = 2$  and the list of indices  $i, j = 1, 2, 3$  is omitted as before. The components for which  $i = j$  are referred to as the diagonal components, and those for which  $i \neq j$  are referred to as the off-diagonal components. The *transpose* of  $\mathbf{T}$  is produced by exchanging components across the diagonal such that

$$\mathbf{T}^T = T_{ji} = \begin{pmatrix} T_{11} & T_{21} & T_{31} \\ T_{12} & T_{22} & T_{32} \\ T_{13} & T_{23} & T_{33} \end{pmatrix} \quad (1.2)$$

Note: a rank 2 tensor is often colloquially termed ‘tensor’ since the occurrence of higher order tensors is fairly rare.

**Symmetric rank 2** The term ‘symmetric’ refers to components being symmetric about the diagonal, *i.e.*  $T_{ij} = T_{ji}$ . In this case, there are only 6 independent components since  $T_{12} = T_{21}$ ,  $T_{13} = T_{31}$  and  $T_{23} = T_{32}$ . OpenFOAM distinguishes between symmetric and non-symmetric tensors to save memory by storing 6 components rather than 9 if the tensor is symmetric. Most tensors encountered in continuum mechanics are symmetric.

**Rank 3** has 27 components and is represented in index notation as  $P_{ijk}$  which is too long to represent in array notation as in [Equation 1.1](#).

**Symmetric rank 3** Symmetry of a rank 3 tensor is defined in OpenFOAM to mean that  $P_{ijk} = P_{ikj} = P_{jik} = P_{jki} = P_{kij} = P_{kji}$  and therefore has 10 independent components. More specifically, it is formed by the outer product of 3 identical vectors, where the outer product operation is described in [Section 1.3.4](#).



### 1.2.1 Tensor notation

This is a book on computational continuum mechanics that deals with problems involving complex PDEs in 3 spatial dimensions and in time. It is vital from the beginning to adopt a notation for the equations which is compact yet unambiguous. To make the equations easy to follow, we must use a notation that encapsulates the idea of a tensor as an entity in its own right, rather than a list of scalar components. Additionally, any tensor operation should be perceived as an operation on the entire tensor entity rather than a series of operations on its components.

Consequently, in this book the *tensor notation* is preferred in which any tensor of rank 1 and above, *i.e.* all tensors other than scalars, are represented by letters in bold face, *e.g.* **a**. This actively promotes the concept of a tensor as an entity in its own right since it is denoted by a single symbol, and it is also extremely compact. The potential drawback is that the rank of a bold face symbol is not immediately apparent, although it is clearly not zero. However, in practice this presents no real problem since we are aware of the property each symbol represents and therefore intuitively know its rank, *e.g.* we know velocity **U** is a tensor of rank 1.

A further, more fundamental idea regarding the choice of notation is that the mathematical representation of a tensor should not change depending on our coordinate system, *i.e.* the vector **a** is the same vector irrespective of where we view it from. The tensor notation supports this concept as it implies nothing about the coordinate system. However, other notations, *e.g.*  $a_i$ , expose the individual components of the tensor which naturally implies the choice of coordinate system. The unsatisfactory consequence of this is that the tensor is then represented by a set of values which are not unique — they depend on the coordinate system.

That said, the index notation, introduced in Section 1.2, is adopted from time to time in this book mainly to expand tensor operations into the constituent components. When using the index notation, we adopt the *summation convention* which states that whenever the same letter subscript occurs twice in a term, the that subscript is to be given all values, *i.e.* 1, 2, 3, and the results added together, *e.g.*

$$a_i b_i = \sum_{i=1}^3 a_i b_i = a_1 b_1 + a_2 b_2 + a_3 b_3 \quad (1.3)$$

In the remainder of the book the symbol  $\sum$  is omitted since the repeated subscript indicates the summation.

## 1.3 Algebraic tensor operations

This section describes all the algebraic operations for tensors that are available in OpenFOAM. Let us first review the most simple tensor operations: addition, subtraction, and scalar multiplication and division. Addition and subtraction are both commutative and associative and are only valid between tensors of the same rank. The operations are performed by addition/subtraction of respective components of the tensors, *e.g.* the subtraction of two vectors **a** and **b** is

$$\mathbf{a} - \mathbf{b} = a_i - b_i = (a_1 - b_1, a_2 - b_2, a_3 - b_3) \quad (1.4)$$

Multiplication of any tensor **a** by a scalar  $s$  is also commutative and associative and is performed by multiplying all the tensor components by the scalar. For example,

$$s\mathbf{a} = sa_i = (sa_1, sa_2, sa_3) \quad (1.5)$$

Division between a tensor  $\mathbf{a}$  and a scalar is only relevant when the scalar is the second argument of the operation, *i.e.*

$$\mathbf{a}/s = a_i/s = (a_1/s, a_2/s, a_3/s) \quad (1.6)$$

Following these operations are a set of more complex products between tensors of rank 1 and above, described in the following Sections.

### 1.3.1 The inner product

The inner product operates on any two tensors of rank  $r_1$  and  $r_2$  such that the rank of the result  $r = r_1 + r_2 - 2$ . Inner product operations with tensors up to rank 3 are described below:

- The inner product of two vectors  $\mathbf{a}$  and  $\mathbf{b}$  is commutative and produces a scalar  $s = \mathbf{a} \cdot \mathbf{b}$  where

$$s = a_i b_i = a_1 b_1 + a_2 b_2 + a_3 b_3 \quad (1.7)$$

- The inner product of a tensor  $\mathbf{T}$  and vector  $\mathbf{a}$  produces a vector  $\mathbf{b} = \mathbf{T} \cdot \mathbf{a}$ , represented below as a column array for convenience

$$b_i = T_{ij} a_j = \begin{pmatrix} T_{11}a_1 + T_{12}a_2 + T_{13}a_3 \\ T_{21}a_1 + T_{22}a_2 + T_{23}a_3 \\ T_{31}a_1 + T_{32}a_2 + T_{33}a_3 \end{pmatrix} \quad (1.8)$$

It is non-commutative if  $\mathbf{T}$  is non-symmetric such that  $\mathbf{b} = \mathbf{a} \cdot \mathbf{T} = \mathbf{T}^T \cdot \mathbf{a}$  is

$$b_i = a_j T_{ji} = \begin{pmatrix} a_1 T_{11} + a_2 T_{21} + a_3 T_{31} \\ a_1 T_{12} + a_2 T_{22} + a_3 T_{32} \\ a_1 T_{13} + a_2 T_{23} + a_3 T_{33} \end{pmatrix} \quad (1.9)$$

- The inner product of two tensors  $\mathbf{T}$  and  $\mathbf{S}$  produces a tensor  $\mathbf{P} = \mathbf{T} \cdot \mathbf{S}$  whose components are evaluated as:

$$P_{ij} = T_{ik} S_{kj} \quad (1.10)$$

It is non-commutative such that  $\mathbf{T} \cdot \mathbf{S} = (\mathbf{S}^T \cdot \mathbf{T}^T)^T$

- The inner product of a vector  $\mathbf{a}$  and third rank tensor  $\mathbf{P}$  produces a second rank tensor  $\mathbf{T} = \mathbf{a} \cdot \mathbf{P}$  whose components are

$$T_{ij} = a_k P_{kij} \quad (1.11)$$

Again this is non-commutative so that  $\mathbf{T} = \mathbf{P} \cdot \mathbf{a}$  is

$$T_{ij} = P_{ijk} a_k \quad (1.12)$$

- The inner product of a second rank tensor  $\mathbf{T}$  and third rank tensor  $\mathbf{P}$  produces a third rank tensor  $\mathbf{Q} = \mathbf{T} \cdot \mathbf{P}$  whose components are

$$Q_{ijk} = T_{il} P_{ljk} \quad (1.13)$$

Again this is non-commutative so that  $\mathbf{Q} = \mathbf{P} \cdot \mathbf{T}$  is

$$Q_{ijk} = P_{ijl} T_{lk} \quad (1.14)$$

### 1.3.2 The double inner product of two tensors

The double inner product of two second-rank tensors  $\mathbf{T}$  and  $\mathbf{S}$  produces a scalar  $s = \mathbf{T}:\mathbf{S}$  which can be evaluated as the sum of the 9 products of the tensor components

$$s = T_{ij}S_{ij} = T_{11}S_{11} + T_{12}S_{12} + T_{13}S_{13} + T_{21}S_{21} + T_{22}S_{22} + T_{23}S_{23} + T_{31}S_{31} + T_{32}S_{32} + T_{33}S_{33} \quad (1.15)$$

The double inner product between a second rank tensor  $\mathbf{T}$  and third rank tensor  $\mathbf{P}$  produces a vector  $\mathbf{a} = \mathbf{T}:\mathbf{P}$  with components

$$a_i = T_{jk}P_{jki} \quad (1.16)$$

This is non-commutative so that  $\mathbf{a} = \mathbf{P}:\mathbf{T}$  is

$$a_i = P_{ijk}T_{jk} \quad (1.17)$$

### 1.3.3 The triple inner product of two third rank tensors

The triple inner product of two third rank tensors  $\mathbf{P}$  and  $\mathbf{Q}$  produces a scalar  $s = \mathbf{P}:\mathbf{Q}$  which can be evaluated as the sum of the 27 products of the tensor components

$$s = P_{ijk}Q_{ijk} \quad (1.18)$$

### 1.3.4 The outer product

The outer product operates between vectors and tensors as follows:

- The outer product of two vectors  $\mathbf{a}$  and  $\mathbf{b}$  is non-commutative and produces a tensor  $\mathbf{T} = \mathbf{ab} = (\mathbf{ba})^T$  whose components are evaluated as:

$$T_{ij} = a_i b_j = \begin{pmatrix} a_1 b_1 & a_1 b_2 & a_1 b_3 \\ a_2 b_1 & a_2 b_2 & a_2 b_3 \\ a_3 b_1 & a_3 b_2 & a_3 b_3 \end{pmatrix} \quad (1.19)$$

- An outer product of a vector  $\mathbf{a}$  and second rank tensor  $\mathbf{T}$  produces a third rank tensor  $\mathbf{P} = \mathbf{aT}$  whose components are

$$P_{ijk} = a_i T_{jk} \quad (1.20)$$

This is non-commutative so that  $\mathbf{P} = \mathbf{Ta}$  produces

$$P_{ijk} = T_{ij} a_k \quad (1.21)$$

### 1.3.5 The cross product of two vectors

The cross product operation is exclusive to vectors only. For two vectors  $\mathbf{a}$  with  $\mathbf{b}$ , it produces a vector  $\mathbf{c} = \mathbf{a} \times \mathbf{b}$  whose components are

$$c_i = e_{ijk} a_j b_k = (a_2 b_3 - a_3 b_2, a_3 b_1 - a_1 b_3, a_1 b_2 - a_2 b_1) \quad (1.22)$$

where the *permutation symbol* is defined by

$$e_{ijk} = \begin{cases} 0 & \text{when any two indices are equal} \\ +1 & \text{when } i,j,k \text{ are an even permutation of } 1,2,3 \\ -1 & \text{when } i,j,k \text{ are an odd permutation of } 1,2,3 \end{cases} \quad (1.23)$$

in which the even permutations are 123, 231 and 312 and the odd permutations are 132, 213 and 321.

### 1.3.6 Other general tensor operations

Some less common tensor operations and terminology used by OpenFOAM are described below.

**Square** of a tensor is defined as the outer product of the tensor with itself, *e.g.* for a vector  $\mathbf{a}$ , the square  $\mathbf{a}^2 = \mathbf{a}\mathbf{a}$ .

**$n$ th power** of a tensor is evaluated by  $n$  outer products of the tensor, *e.g.* for a vector  $\mathbf{a}$ , the 3rd power  $\mathbf{a}^3 = \mathbf{a}\mathbf{a}\mathbf{a}$ .

**Magnitude squared** of a tensor is the  $r$ th inner product of the tensor of rank  $r$  with itself, to produce a scalar. For example, for a second rank tensor  $\mathbf{T}$ ,  $|\mathbf{T}|^2 = \mathbf{T}:\mathbf{T}$ .

**Magnitude** is the square root of the magnitude squared, *e.g.* for a tensor  $\mathbf{T}$ ,  $|\mathbf{T}| = \sqrt{\mathbf{T}:\mathbf{T}}$ . Vectors of unit magnitude are referred to as *unit vectors*.

**Component maximum** is the component of the tensor with greatest value, inclusive of sign, *i.e.* not the largest magnitude.

**Component minimum** is the component of the tensor with smallest value.

**Component average** is the mean of all components of a tensor.

**Scale** As the name suggests, the scale function is a tool for scaling the components of one tensor by the components of another tensor of the same rank. It is evaluated as the product of corresponding components of 2 tensors, *e.g.*, scaling vector  $\mathbf{a}$  by vector  $\mathbf{b}$  would produce vector  $\mathbf{c}$  whose components are

$$c_i = \text{scale}(\mathbf{a}, \mathbf{b}) = (a_1b_1, a_2b_2, a_3b_3) \quad (1.24)$$

### 1.3.7 Geometric transformation and the identity tensor

A second rank tensor  $\mathbf{T}$  is strictly defined as a linear vector function, *i.e.* it is a function which associates an argument vector  $\mathbf{a}$  to another vector  $\mathbf{b}$  by the inner product  $\mathbf{b} = \mathbf{T} \cdot \mathbf{a}$ . The components of  $\mathbf{T}$  can be chosen to perform a specific geometric transformation of a tensor from the  $x, y, z$  coordinate system to a new coordinate system  $x^*, y^*, z^*$ ;  $\mathbf{T}$  is then referred to as the *transformation tensor*. While a scalar remains unchanged under a transformation, the vector  $\mathbf{a}$  is transformed to  $\mathbf{a}^*$  by

$$\mathbf{a}^* = \mathbf{T} \cdot \mathbf{a} \quad (1.25)$$

A second rank tensor  $\mathbf{S}$  is transformed to  $\mathbf{S}^*$  according to

$$\mathbf{S}^* = \mathbf{T} \cdot \mathbf{S} \cdot \mathbf{T}^T \quad (1.26)$$

The *identity tensor*  $\mathbf{I}$  is defined by the requirement that it transforms another tensor onto itself. For all vectors  $\mathbf{a}$

$$\mathbf{a} = \mathbf{I} \cdot \mathbf{a} \quad (1.27)$$

and therefore

$$\mathbf{I} = \delta_{ij} = \begin{pmatrix} 1 & 0 & 0 \\ 0 & 1 & 0 \\ 0 & 0 & 1 \end{pmatrix} \quad (1.28)$$

where  $\delta_{ij}$  is known as the *Kronecker delta* symbol.

### 1.3.8 Useful tensor identities

Several identities are listed below which can be verified by under the assumption that all the relevant derivatives exist and are continuous. The identities are expressed for scalar  $s$  and vector  $\mathbf{a}$ .

$$\begin{aligned}
\nabla \cdot (\nabla \times \mathbf{a}) &\equiv 0 \\
\nabla \times (\nabla s) &\equiv \mathbf{0} \\
\nabla \cdot (s\mathbf{a}) &\equiv s\nabla \cdot \mathbf{a} + \mathbf{a} \cdot \nabla s \\
\nabla \times (s\mathbf{a}) &\equiv s\nabla \times \mathbf{a} + \nabla s \times \mathbf{a} \\
\nabla(\mathbf{a} \cdot \mathbf{b}) &\equiv \mathbf{a} \times (\nabla \times \mathbf{b}) + \mathbf{b} \times (\nabla \times \mathbf{a}) + (\mathbf{a} \cdot \nabla)\mathbf{b} + (\mathbf{b} \cdot \nabla)\mathbf{a} \\
\nabla \cdot (\mathbf{a} \times \mathbf{b}) &\equiv \mathbf{b} \cdot (\nabla \times \mathbf{a}) - \mathbf{a} \cdot (\nabla \times \mathbf{b}) \\
\nabla \times (\mathbf{a} \times \mathbf{b}) &\equiv \mathbf{a}(\nabla \cdot \mathbf{b}) - \mathbf{b}(\nabla \cdot \mathbf{a}) + (\mathbf{b} \cdot \nabla)\mathbf{a} - (\mathbf{a} \cdot \nabla)\mathbf{b} \\
\nabla \times (\nabla \times \mathbf{a}) &\equiv \nabla(\nabla \cdot \mathbf{a}) - \nabla^2 \mathbf{a} \\
(\nabla \times \mathbf{a}) \times \mathbf{a} &\equiv \mathbf{a} \cdot (\nabla \mathbf{a}) - \nabla(\mathbf{a} \cdot \mathbf{a})
\end{aligned} \tag{1.29}$$

It is sometimes useful to know the  $e - \delta$  identity to help to manipulate equations in index notation:

$$e_{ijk}e_{irs} = \delta_{jr}\delta_{ks} - \delta_{js}\delta_{kr} \tag{1.30}$$

### 1.3.9 Operations exclusive to tensors of rank 2

There are several operations that manipulate the components of tensors of rank 2 that are listed below:

**Transpose** of a tensor  $\mathbf{T} = T_{ij}$  is  $\mathbf{T}^T = T_{ji}$  as described in [Equation 1.2](#).

**Symmetric and skew (antisymmetric) tensors** As discussed in [section 1.2](#), a tensor is said to be symmetric if its components are symmetric about the diagonal, i.e.  $\mathbf{T} = \mathbf{T}^T$ . A skew or antisymmetric tensor has  $\mathbf{T} = -\mathbf{T}^T$  which intuitively implies that  $T_{11} = T_{22} = T_{33} = 0$ . Every second order tensor can be decomposed into symmetric and skew parts by

$$\mathbf{T} = \underbrace{\frac{1}{2}(\mathbf{T} + \mathbf{T}^T)}_{\text{symmetric}} + \underbrace{\frac{1}{2}(\mathbf{T} - \mathbf{T}^T)}_{\text{skew}} = \text{symm } \mathbf{T} + \text{skew } \mathbf{T} \tag{1.31}$$

**Trace** The trace of a tensor  $\mathbf{T}$  is a scalar, evaluated by summing the diagonal components

$$\text{tr } \mathbf{T} = T_{11} + T_{22} + T_{33} \tag{1.32}$$

**Diagonal** returns a vector whose components are the diagonal components of the second rank tensor  $\mathbf{T}$

$$\text{diag } \mathbf{T} = (T_{11}, T_{22}, T_{33}) \tag{1.33}$$

**Deviatoric and hydrostatic tensors** Every second rank tensor  $\mathbf{T}$  can be decomposed into a deviatoric component, for which  $\text{tr } \mathbf{T} = 0$  and a hydrostatic component of the form  $\mathbf{T} = s\mathbf{I}$  where  $s$  is a scalar. Every second rank tensor can be decomposed into deviatoric and hydrostatic parts as follows:

$$\mathbf{T} = \underbrace{\mathbf{T} - \frac{1}{3}(\text{tr } \mathbf{T})\mathbf{I}}_{\text{deviatoric}} + \underbrace{\frac{1}{3}(\text{tr } \mathbf{T})\mathbf{I}}_{\text{hydrostatic}} = \text{dev } \mathbf{T} + \text{hyd } \mathbf{T} \tag{1.34}$$

**Determinant** The determinant of a second rank tensor is evaluated by

$$\begin{aligned} \det \mathbf{T} &= \begin{vmatrix} T_{11} & T_{12} & T_{13} \\ T_{21} & T_{22} & T_{23} \\ T_{31} & T_{32} & T_{33} \end{vmatrix} = \begin{aligned} &T_{11}(T_{22}T_{33} - T_{23}T_{32}) - \\ &T_{12}(T_{21}T_{33} - T_{23}T_{31}) + \\ &T_{13}(T_{21}T_{32} - T_{22}T_{31}) \end{aligned} \\ &= \frac{1}{6} e_{ijk} e_{pqr} T_{ip} T_{jq} T_{kr} \end{aligned} \quad (1.35)$$

**Cofactors** The *minors* of a tensor are evaluated for each component by deleting the row and column in which the component is situated and evaluating the resulting entries as a  $2 \times 2$  *determinant*. For example, the minor of  $T_{12}$  is

$$\begin{vmatrix} T_{11} & T_{13} \\ T_{21} & T_{23} \\ T_{31} & T_{33} \end{vmatrix} = \begin{vmatrix} T_{21} & T_{23} \\ T_{31} & T_{33} \end{vmatrix} = T_{21}T_{33} - T_{23}T_{31} \quad (1.36)$$

The cofactors are *signed minors* where each minor is component is given a sign based on the rule

$$\begin{aligned} &+ve \text{ if } i + j \text{ is even} \\ &-ve \text{ if } i + j \text{ is odd} \end{aligned} \quad (1.37)$$

The cofactors of  $\mathbf{T}$  can be evaluated as

$$\text{cof } \mathbf{T} = \frac{1}{2} e_{jkr} e_{ist} T_{sk} T_{tr} \quad (1.38)$$

**Inverse** The inverse of a tensor can be evaluated as

$$\text{inv } \mathbf{T} = \frac{\text{cof } \mathbf{T}^T}{\det \mathbf{T}} \quad (1.39)$$

**Hodge dual** of a tensor is a vector whose components are

$$*\mathbf{T} = (T_{23}, -T_{13}, T_{12}) \quad (1.40)$$

### 1.3.10 Operations exclusive to scalars

OpenFOAM supports most of the well known functions that operate on scalars, *e.g.* square root, exponential, logarithm, sine, cosine *etc.*, a list of which can be found in Table 1.2. There are 3 additional functions defined within OpenFOAM that are described below:

**Sign** of a scalar  $s$  is

$$\text{sgn}(s) = \begin{cases} 1 & \text{if } s \geq 0, \\ -1 & \text{if } s < 0. \end{cases} \quad (1.41)$$

**Positive** of a scalar  $s$  is

$$\text{pos}(s) = \begin{cases} 1 & \text{if } s \geq 0, \\ 0 & \text{if } s < 0. \end{cases} \quad (1.42)$$

**Limit** of a scalar  $s$  by the scalar  $n$

$$\text{limit}(s, n) = \begin{cases} s & \text{if } s < n, \\ 0 & \text{if } s \geq n. \end{cases} \quad (1.43)$$

## 1.4 OpenFOAM tensor classes

OpenFOAM contains a C++ class library **primitive** that contains the classes for the tensor mathematics described so far. The basic tensor classes that are available as standard in OpenFOAM are listed in Table 1.1. The Table also lists the functions that allow the user to access individual components of a tensor, known as access functions.

Rank	Common name	Basic class	Access functions
0	Scalar	<b>scalar</b>	
1	Vector	<b>vector</b>	<b>x()</b> , <b>y()</b> , <b>z()</b>
2	Tensor	<b>tensor</b>	<b>xx()</b> , <b>xy()</b> , <b>xz()</b> ...

Table 1.1: Basic tensor classes in OpenFOAM

We can declare the tensor

$$\mathbf{T} = \begin{pmatrix} 1 & 2 & 3 \\ 4 & 5 & 6 \\ 7 & 8 & 9 \end{pmatrix} \quad (1.44)$$

in OpenFOAM by the line:

```
tensor T(1, 2, 3, 4, 5, 6, 7, 8, 9);
```

We can then access the component  $T_{13}$ , or  $T_{xz}$  using the **xz()** access function. For instance the code

```
Info << "Txz = " << T.xz() << endl;
```

outputs to the screen:

```
Txz = 3
```

### 1.4.1 Algebraic tensor operations in OpenFOAM

The algebraic operations described in Section 1.3 are all available to the OpenFOAM tensor classes using syntax which closely mimics the notation used in written mathematics. Some functions are represented solely by descriptive functions, *e.g.* **symm()**, but others can also be executed using symbolic operators, *e.g.* **\***. All functions are listed in Table 1.2.

Operation	Comment	Mathematical Description	Description in OpenFOAM
Addition		$\mathbf{a} + \mathbf{b}$	$\mathbf{a} + \mathbf{b}$
Subtraction		$\mathbf{a} - \mathbf{b}$	$\mathbf{a} - \mathbf{b}$
Scalar multiplication		$s\mathbf{a}$	$\mathbf{s} * \mathbf{a}$
Scalar division		$\mathbf{a}/s$	$\mathbf{a} / \mathbf{s}$
Outer product	rank $\mathbf{a}, \mathbf{b} \geq 1$	$\mathbf{a}\mathbf{b}$	$\mathbf{a} * \mathbf{b}$
Inner product	rank $\mathbf{a}, \mathbf{b} \geq 1$	$\mathbf{a} \cdot \mathbf{b}$	$\mathbf{a} \& \mathbf{b}$
Double inner product	rank $\mathbf{a}, \mathbf{b} \geq 2$	$\mathbf{a} : \mathbf{b}$	$\mathbf{a} \&\& \mathbf{b}$
Cross product	rank $\mathbf{a}, \mathbf{b} = 1$	$\mathbf{a} \times \mathbf{b}$	$\mathbf{a} \wedge \mathbf{b}$
Square		$\mathbf{a}^2$	<b>sqr(a)</b>

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Operation	Comment	Mathematical Description	Description in OpenFOAM
Magnitude squared		$ \mathbf{a} ^2$	magSqr(a)
Magnitude		$ \mathbf{a} $	mag(a)
Power	$n = 0, 1, \dots, 4$	$\mathbf{a}^n$	pow(a,n)
Component average	$i = 1, \dots, N$	$\overline{a_i}$	cmptAv(a)
Component maximum	$i = 1, \dots, N$	$\max(a_i)$	max(a)
Component minimum	$i = 1, \dots, N$	$\min(a_i)$	min(a)
Scale		scale( <b>a</b> , <b>b</b> )	scale(a,b)
Geometric transformation	transforms <b>a</b> using tensor <b>T</b>		transform(T,a)

### Operations exclusive to tensors of rank 2

Transpose		$\mathbf{T}^T$	T.T()
Diagonal		diag <b>T</b>	diag(T)
Trace		tr <b>T</b>	tr(T)
Deviatoric component		dev <b>T</b>	dev(T)
Symmetric component		symm <b>T</b>	symm(T)
Skew-symmetric component		skew <b>T</b>	skew(T)
Determinant		det <b>T</b>	det(T)
Cofactors		cof <b>T</b>	cof(T)
Inverse		inv <b>T</b>	inv(T)
Hodge dual		* <b>T</b>	*T

### Operations exclusive to scalars

Sign (boolean)		sgn( $s$ )	sign(s)
Positive (boolean)		$s \geq 0$	pos(s)
Negative (boolean)		$s < 0$	neg(s)
Limit	$n$ scalar	limit( $s, n$ )	limit(s,n)
Square root		$\sqrt{s}$	sqrt(s)
Exponential		exp $s$	exp(s)
Natural logarithm		ln $s$	log(s)
Base 10 logarithm		$\log_{10} s$	log10(s)
Sine		sin $s$	sin(s)
Cosine		cos $s$	cos(s)
Tangent		tan $s$	tan(s)
Arc sine		asin $s$	asin(s)
Arc cosine		acos $s$	acos(s)
Arc tangent		atan $s$	atan(s)
Hyperbolic sine		sinh $s$	sinh(s)
Hyperbolic cosine		cosh $s$	cosh(s)
Hyperbolic tangent		tanh $s$	tanh(s)
Hyperbolic arc sine		asinh $s$	asinh(s)
Hyperbolic arc cosine		acosh $s$	acosh(s)
Hyperbolic arc tangent		atanh $s$	atanh(s)
Error function		erf $s$	erf(s)
Complement error function		erfc $s$	erfc(s)
Logarithm gamma function		ln $\Gamma s$	lgamma(s)
Type 1 Bessel function of order 0		$J_0 s$	j0(s)
Type 1 Bessel function of order 1		$J_1 s$	j1(s)

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Operation	Comment	Mathematical Description	Description in OpenFOAM
Type 2 Bessel function of order 0		$Y_0 s$	<code>y0(s)</code>
Type 2 Bessel function of order 1		$Y_1 s$	<code>y1(s)</code>

---

**a, b** are tensors of arbitrary rank unless otherwise stated  
*s* is a scalar, *N* is the number of tensor components

Table 1.2: Algebraic tensor operations in OpenFOAM

## 1.5 Dimensional units

In continuum mechanics, properties are represented in some chosen units, *e.g.* mass in kilograms (kg), volume in cubic metres (m<sup>3</sup>), pressure in Pascals (kg m s<sup>-2</sup>). Algebraic operations must be performed on these properties using consistent units of measurement; in particular, addition, subtraction and equality are only physically meaningful for properties of the same dimensional units. As a safeguard against implementing a meaningless operation, OpenFOAM encourages the user to attach dimensional units to any tensor and will then perform dimension checking of any tensor operation.

Units are defined using the `dimensionSet` class, *e.g.*

```
dimensionSet pressureDims(1, -1, -2, 0, 0, 0, 0);
```

No.	Property	Unit	Symbol
1	Mass	kilogram	k
2	Length	metre	m
3	Time	second	s
4	Temperature	Kelvin	K
5	Quantity	moles	mol
6	Current	ampere	A
7	Luminous intensity	candela	cd

Table 1.3: S.I. base units of measurement

where each of the values corresponds to the power of each of the S.I. base units of measurement listed in Table 1.3. The line of code declares `pressureDims` to be the `dimensionSet` for pressure kg m s<sup>-2</sup> since the first entry in the `pressureDims` array, 1, corresponds to k<sup>1</sup>, the second entry, -1, corresponds to m<sup>-1</sup> *etc.*. A tensor with units is defined using the `dimensioned<Type>` template class, the `<Type>` being `scalar`, `vector`, `tensor`, *etc.*. The `dimensioned<Type>` stores a variable name of class `word`, the value `<Type>` and a `dimensionSet`

```
dimensionedTensor sigma
(
    "sigma",
    dimensionSet(1, -1, -2, 0, 0, 0, 0),
    tensor(1e6,0,0,0,1e6,0,0,0,1e6),
);
```

creates a tensor with correct dimensions of pressure, or stress

$$\boldsymbol{\sigma} = \begin{pmatrix} 10^6 & 0 & 0 \\ 0 & 10^6 & 0 \\ 0 & 0 & 10^6 \end{pmatrix} \quad (1.45)$$

# Chapter 2

## Discretisation procedures

So far we have dealt with algebra of tensors at a point. The PDEs we wish to solve involve derivatives of tensors with respect to time and space. We therefore need to extend our description to a *tensor field*, *i.e.* a tensor that varies across time and spatial domains. In this Chapter we will first present a mathematical description of all the differential operators we may encounter. We will then show how a tensor field is constructed in OpenFOAM and how the derivatives of these fields are discretised into a set of algebraic equations.

### 2.1 Differential operators

Before defining the spatial derivatives we first introduce the nabla *vector operator*  $\nabla$ , represented in index notation as  $\partial_i$ :

$$\nabla \equiv \partial_i \equiv \frac{\partial}{\partial x_i} \equiv \left( \frac{\partial}{\partial x_1}, \frac{\partial}{\partial x_2}, \frac{\partial}{\partial x_3} \right) \quad (2.1)$$

The nabla operator is a useful notation that obeys the following rules:

- it operates on the tensors to its right and the conventional rules of a derivative of a product, *e.g.*  $\partial_i ab = (\partial_i a) b + a (\partial_i b)$ ;
- otherwise the nabla operator behaves like any other vector in an algebraic operation.

#### 2.1.1 Gradient

If a scalar field  $s$  is defined and continuously differentiable then the gradient of  $s$ ,  $\nabla s$  is a vector field

$$\nabla s = \partial_i s = \left( \frac{\partial s}{\partial x_1}, \frac{\partial s}{\partial x_2}, \frac{\partial s}{\partial x_3} \right) \quad (2.2)$$

The gradient can operate on any tensor field to produce a tensor field that is one rank higher. For example, the gradient of a vector field  $\mathbf{a}$  is a second rank tensor field

$$\nabla \mathbf{a} = \partial_i a_j = \begin{pmatrix} \partial a_1/\partial x_1 & \partial a_2/\partial x_1 & \partial a_3/\partial x_1 \\ \partial a_1/\partial x_2 & \partial a_2/\partial x_2 & \partial a_3/\partial x_2 \\ \partial a_1/\partial x_3 & \partial a_2/\partial x_3 & \partial a_3/\partial x_3 \end{pmatrix} \quad (2.3)$$

### 2.1.2 Divergence

If a vector field  $\mathbf{a}$  is defined and continuously differentiable then the divergence of  $\mathbf{a}$  is a scalar field

$$\nabla \cdot \mathbf{a} = \partial_i a_i = \frac{\partial a_1}{\partial x_1} + \frac{\partial a_2}{\partial x_2} + \frac{\partial a_3}{\partial x_3} \quad (2.4)$$

The divergence can operate on any tensor field of rank 1 and above to produce a tensor that is one rank lower. For example the divergence of a second rank tensor field  $\mathbf{T}$  is a vector field (expanding the vector as a column array for convenience)

$$\nabla \cdot \mathbf{T} = \partial_i T_{ij} = \begin{pmatrix} \partial T_{11}/\partial x_1 + \partial T_{12}/\partial x_2 + \partial T_{13}/\partial x_3 \\ \partial T_{21}/\partial x_1 + \partial T_{22}/\partial x_2 + \partial T_{23}/\partial x_3 \\ \partial T_{31}/\partial x_1 + \partial T_{32}/\partial x_2 + \partial T_{33}/\partial x_3 \end{pmatrix} \quad (2.5)$$

### 2.1.3 Curl

If a vector field  $\mathbf{a}$  is defined and continuously differentiable then the curl of  $\mathbf{a}$ ,  $\nabla \times \mathbf{a}$  is a vector field

$$\nabla \times \mathbf{a} = e_{ijk} \partial_j a_k = \left( \frac{\partial a_3}{\partial x_2} - \frac{\partial a_2}{\partial x_3}, \frac{\partial a_1}{\partial x_3} - \frac{\partial a_3}{\partial x_1}, \frac{\partial a_2}{\partial x_1} - \frac{\partial a_1}{\partial x_2} \right) \quad (2.6)$$

The curl is related to the gradient by

$$\nabla \times \mathbf{a} = 2 (* \text{skew } \nabla \mathbf{a}) \quad (2.7)$$

### 2.1.4 Laplacian

The Laplacian is an operation that can be defined mathematically by a combination of the divergence and gradient operators by  $\nabla^2 \equiv \nabla \cdot \nabla$ . However, the Laplacian should be considered as a single operation that transforms a tensor field into another tensor field of the same rank, rather than a combination of two operations, one which raises the rank by 1 and one which reduces the rank by 1.

In fact, the Laplacian is best defined as a *scalar operator*, just as we defined nabla as a vector operator, by

$$\nabla^2 \equiv \partial^2 \equiv \frac{\partial^2}{\partial x_1^2} + \frac{\partial^2}{\partial x_2^2} + \frac{\partial^2}{\partial x_3^2} \quad (2.8)$$

For example, the Laplacian of a scalar field  $s$  is the scalar field

$$\nabla^2 s = \partial^2 s = \frac{\partial^2 s}{\partial x_1^2} + \frac{\partial^2 s}{\partial x_2^2} + \frac{\partial^2 s}{\partial x_3^2} \quad (2.9)$$

### 2.1.5 Temporal derivative

There is more than one definition of temporal, or time, derivative of a tensor. To describe the temporal derivatives we must first recall that the tensor relates to a property of a volume of material that may be moving. If we track an infinitesimally small volume of material, or particle, as it moves and observe the change in the tensorial property  $\phi$  in time, we have the *total*, or *material* time derivative denoted by

$$\frac{D\phi}{Dt} = \lim_{\Delta t \rightarrow 0} \frac{\Delta\phi}{\Delta t} \quad (2.10)$$

However in continuum mechanics, particularly fluid mechanics, we often observe the change of a  $\phi$  in time at a fixed point in space as different particles move across that point. This change at a point in space is termed the *spatial* time derivative which is denoted by  $\partial/\partial t$  and is related to the material derivative by:

$$\frac{D\phi}{Dt} = \frac{\partial\phi}{\partial t} + \mathbf{U} \cdot \nabla\phi \quad (2.11)$$

where  $\mathbf{U}$  is the velocity field of property  $\phi$ . The second term on the right is known as the convective rate of change of  $\phi$ .

## 2.2 Overview of discretisation

The term discretisation means *approximation of a problem into discrete quantities*. The FV method and others, such as the finite element and finite difference methods, all discretise the problem as follows:

**Spatial discretisation** Defining the solution domain by a set of points that fill and bound a region of space when connected;

**Temporal discretisation** (For transient problems) dividing the time domain into into a finite number of time intervals, or steps;

**Equation discretisation** Generating a system of algebraic equations in terms of discrete quantities defined at specific locations in the domain, from the PDEs that characterise the problem.

### 2.2.1 OpenFOAM lists and fields

OpenFOAM frequently needs to store sets of data and perform functions, such as mathematical operations, on the data. OpenFOAM therefore provides an array template class `List<Type>`, making it possible to create a list of any object of class `Type` that inherits the functions of the `Type`. For example a List of `vector` is `List<vector>`.

Lists of the tensor classes are defined as standard in OpenFOAM by the template class `Field<Type>`. For better code legibility, all instances of `Field<Type>`, *e.g.* `Field<vector>`, are renamed using `typedef` declarations as `scalarField`, `vectorField`, `tensorField`, `symmTensorField`, `tensorThirdField` and `symmTensorThirdField`. Algebraic operations can be performed between `Fields` subject to obvious restrictions such as the fields having the same number of elements. OpenFOAM also supports operations between a field and single tensor, *e.g.* all values of a `Field U` can be multiplied by the scalar 2 with the operation `U = 2.0 * U`.

## 2.3 Discretisation of the solution domain

Discretisation of the solution domain is shown in [Figure 2.1](#). The space domain is discretised into computational mesh on which the PDEs are subsequently discretised. Discretisation of time, if required, is simple: it is broken into a set of time steps  $\Delta t$  that may change during a numerical simulation, perhaps depending on some condition calculated during the simulation.

On a more detailed level, discretisation of space requires the subdivision of the domain into a number of cells, or control volumes. The cells are contiguous, *i.e.* they do not overlap one another and completely fill the domain. A typical cell is shown in [Figure 2.2](#).

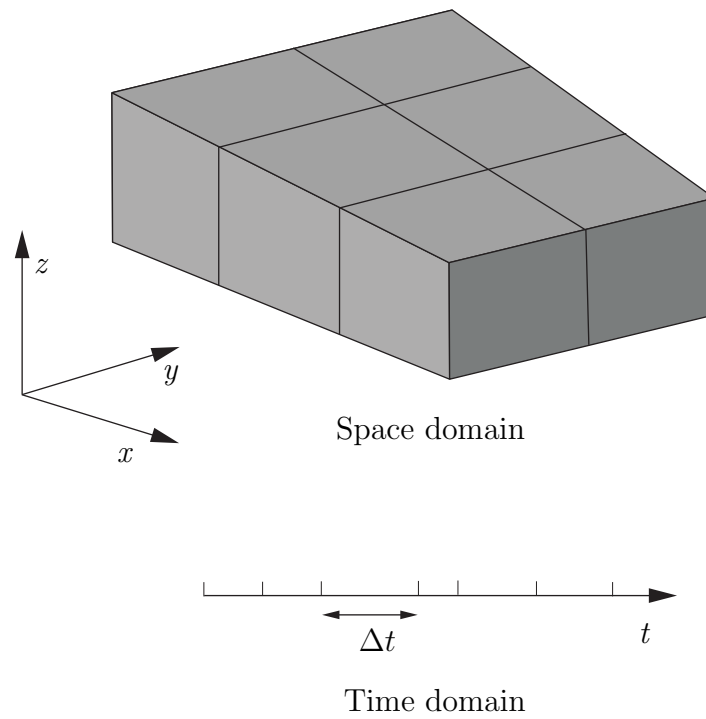


Figure 2.1: Discretisation of the solution domain

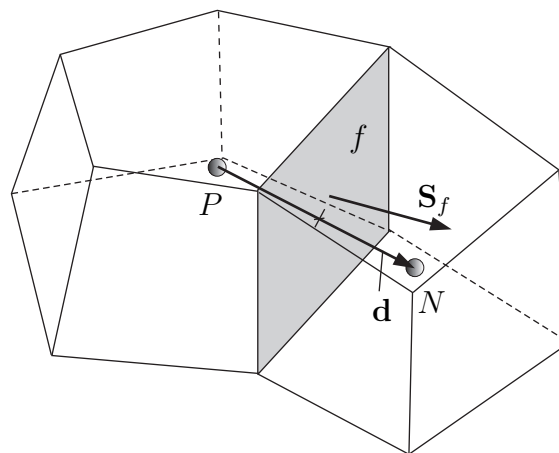


Figure 2.2: Parameters in finite volume discretisation

Dependent variables and other properties are principally stored at the cell centroid  $P$  although they may be stored on faces or vertices. The cell is bounded by a set of flat faces, given the generic label  $f$ . In OpenFOAM there is no limitation on the number of faces bounding each cell, nor any restriction on the alignment of each face. This kind of mesh is often referred to as “arbitrarily unstructured” to differentiate it from meshes in which the cell faces have a prescribed alignment, typically with the coordinate axes. Codes with arbitrarily unstructured meshes offer greater freedom in mesh generation and manipulation in particular when the geometry of the domain is complex or changes over time.

Whilst most properties are defined at the cell centroids, some are defined at cell faces. There are two types of cell face.

**Internal faces** Those faces that connect two cells (and it can never be more than two).

For each internal face, OpenFOAM designates one adjoining cell to be the face *owner* and the other to be the *neighbour*;

**Boundary faces** Those belonging to one cell since they coincide with the boundary of the domain. These faces simply have an owner cell.

### 2.3.1 Defining a mesh in OpenFOAM

There are different levels of mesh description in OpenFOAM, beginning with the most basic mesh class, named `polyMesh` since it is based on polyhedra. A `polyMesh` is constructed using the minimum information required to define the mesh geometry described below and presented in [Figure 2.3](#):

**Points** A list of cell vertex point coordinate vectors, *i.e.* a `vectorField`, that is renamed `pointField` using a `typedef` declaration;

**Faces** A list of cell faces `List<face>`, or `faceList`, where the `face` class is defined by a list of vertex numbers, corresponding to the `pointField`;

**Cells** a list of cells `List<cell>`, or `cellList`, where the `cell` class is defined by a list of face numbers, corresponding to the `faceList` described previously.

**Boundary** a `polyBoundaryMesh` decomposed into a list of patches, `polyPatchList` representing different regions of the boundary. The boundary is subdivided in this manner to allow different boundary conditions to be specified on different patches during a solution. All the faces of any `polyPatch` are stored as a single block of the `faceList`, so that its faces can be easily accessed using the `slice` class which stores references to the first and last face of the block. Each `polyPatch` is then constructed from

- a `slice`;
- a `word` to assign it a name.

FV discretisation uses specific data that is derived from the mesh geometry stored in `polyMesh`. OpenFOAM therefore extends the `polyMesh` class to `fvMesh` which stores the additional data needed for FV discretisation. `fvMesh` is constructed from `polyMesh` and stores the data in [Table 2.1](#) which can be updated during runtime in cases where the mesh moves, is refined *etc.*

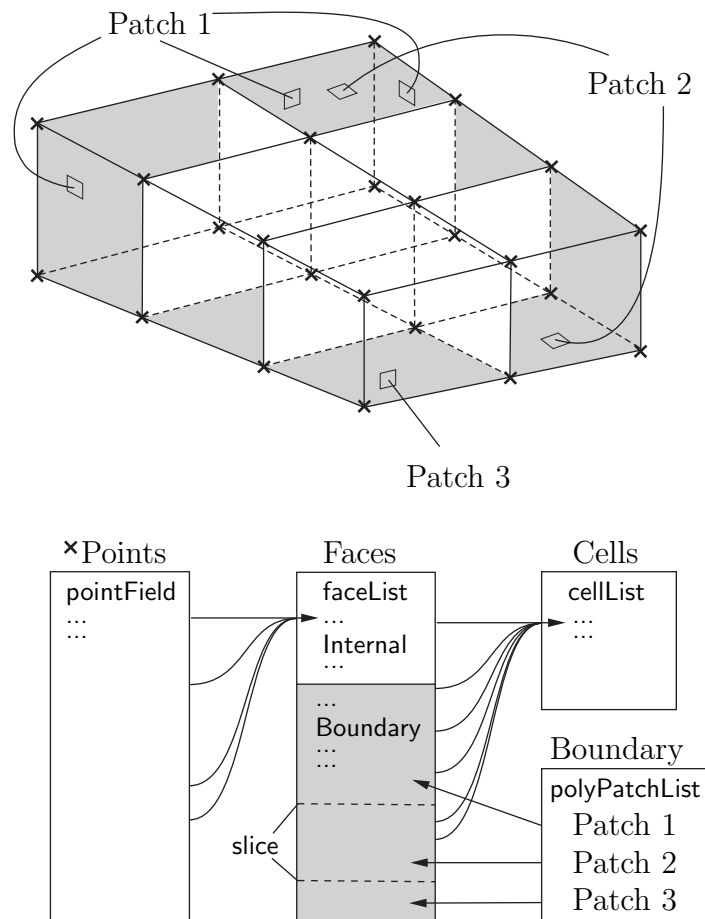


Figure 2.3: Schematic of the basic mesh description used in OpenFOAM

### 2.3.2 Defining a geometricField in OpenFOAM

So far we can define a field, *i.e.* a list of tensors, and a mesh. These can be combined to define a tensor field relating to discrete points in our domain, specified in OpenFOAM by the template class `geometricField<Type>`. The Field values are separated into those defined within the internal region of the domain, *e.g.* at the cell centres, and those defined on the domain boundary, *e.g.* on the boundary faces. The `geometricField<Type>` stores the following information:

**Internal field** This is simply a `Field<Type>`, described in Section 2.2.1;

**BoundaryField** This is a `GeometricBoundaryField`, in which a `Field` is defined for the faces of each patch and a `Field` is defined for the patches of the boundary. This is then a field of fields, stored within an object of the `FieldField<Type>` class. A reference to the `fvBoundaryMesh` is also stored [\*\*].

**Mesh** A reference to an `fvMesh`, with some additional detail as to the whether the field is defined at cell centres, faces, *etc.*

**Dimensions** A `dimensionSet`, described in Section 4.2.6.

**Old values** Discretisation of time derivatives requires field data from previous time steps. The `geometricField<Type>` will store references to stored fields from the previous, or old, time step and its previous, or old-old, time step where necessary.



Class	Description	Symbol	Access function
volScalarField	Cell volumes	$V$	<code>V()</code>
surfaceVectorField	Face area vectors	$\mathbf{S}_f$	<code>Sf()</code>
surfaceScalarField	Face area magnitudes	$ \mathbf{S}_f $	<code>magSf()</code>
volVectorField	Cell centres	$\mathbf{C}$	<code>C()</code>
surfaceVectorField	Face centres	$\mathbf{C}_f$	<code>Cf()</code>
surfaceScalarField	Face motion fluxes **	$\phi_g$	<code>phi()</code>

Table 2.1: fvMesh stored data.

**Previous iteration values** The iterative solution procedures can use under-relaxation which requires access to data from the previous iteration. Again, if required, `geometricField<Type>` stores a reference to the data from the previous iteration.

As discussed in Section 2.3, we principally define a property at the cell centres but quite often it is stored at the cell faces and on occasion it is defined on cell vertices. The `geometricField<Type>` is renamed using `typedef` declarations to indicate where the field variable is defined as follows:

`volField<Type>` A field defined at cell centres;

`surfaceField<Type>` A field defined on cell faces;

`pointField<Type>` A field defined on cell vertices.

These `typedef` field classes of `geometricField<Type>` are illustrated in Figure 2.4. A `geometricField<Type>` inherits all the tensor algebra of `Field<Type>` and has all operations subjected to dimension checking using the `dimensionSet`. It can also be subjected to the FV discretisation procedures described in the following Section. The class structure used to build `geometricField<Type>` is shown in Figure 2.5<sup>1</sup>.

## 2.4 Equation discretisation

Equation discretisation converts the PDEs into a set of algebraic equations that are commonly expressed in matrix form as:

$$[A][x] = [b] \quad (2.12)$$

where  $[A]$  is a square matrix,  $[x]$  is the column vector of dependent variable and  $[b]$  is the source vector. The description of  $[x]$  and  $[b]$  as ‘vectors’ comes from matrix terminology rather than being a precise description of what they truly are: a list of values defined at locations in the geometry, *i.e.* a `geometricField<Type>`, or more specifically a `volField<Type>` when using FV discretisation.

$[A]$  is a list of coefficients of a set of algebraic equations, and cannot be described as a `geometricField<Type>`. It is therefore given a class of its own: `fvMatrix`. `fvMatrix<Type>` is created through discretisation of a `geometric<Type>Field` and therefore inherits the `<Type>`. It supports many of the standard algebraic matrix operations of addition  $+$ , subtraction  $-$  and multiplication  $*$ .

Each term in a PDE is represented individually in OpenFOAM code using the classes of static functions `finiteVolumeMethod` and `finiteVolumeCalculus`, abbreviated by a `typedef`

<sup>1</sup>The diagram is not an exact description of the class hierarchy, rather a representation of the general structure leading from some primitive classes to `geometric<Type>Field`.

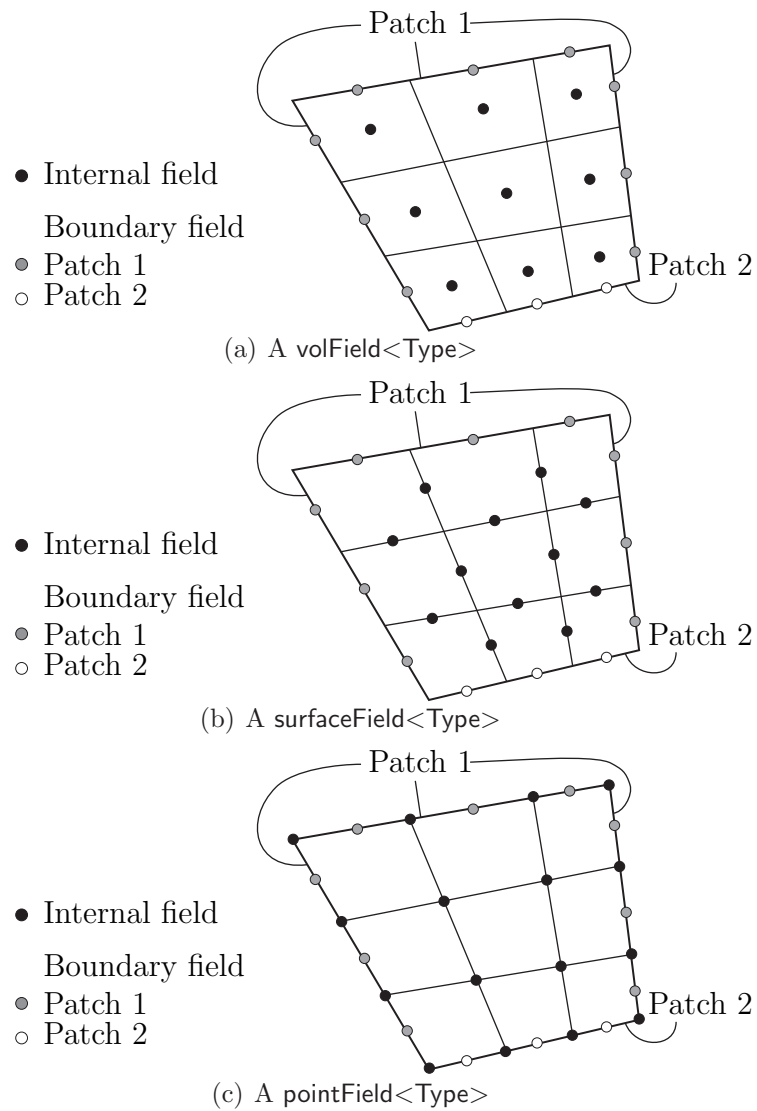


Figure 2.4: Types of `geometricField<Type>` defined on a mesh with 2 boundary patches (in 2 dimensions for simplicity)

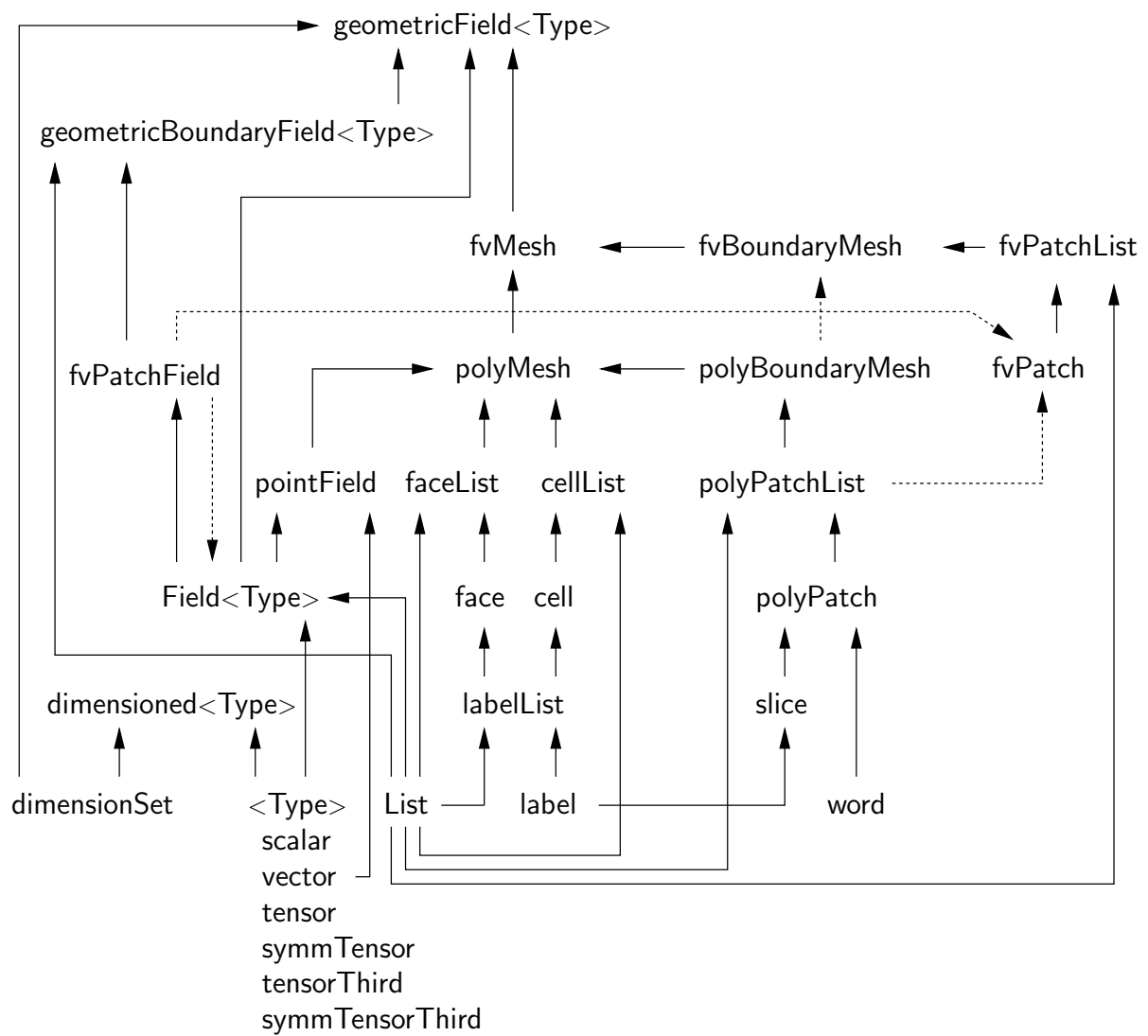


Figure 2.5: Basic class structure leading to `geometricField<Type>`

to `fvm` and `fvc` respectively. `fvm` and `fvc` contain static functions, representing differential operators, *e.g.*  $\nabla^2$ ,  $\nabla \cdot$  and  $\partial/\partial t$ , that discretise `geometricField<Type>`s. The purpose of defining these functions within two classes, `fvm` and `fvc`, rather than one, is to distinguish:

- functions of `fvm` that calculate implicit derivatives of and return an `fvMatrix<Type>`
- some functions of `fvc` that calculate explicit derivatives and other explicit calculations, returning a `geometricField<Type>`.

Figure 2.6 shows a `geometricField<Type>` defined on a mesh with 2 boundary patches and illustrates the explicit operations merely transform one field to another and drawn in 2D for simplicity.

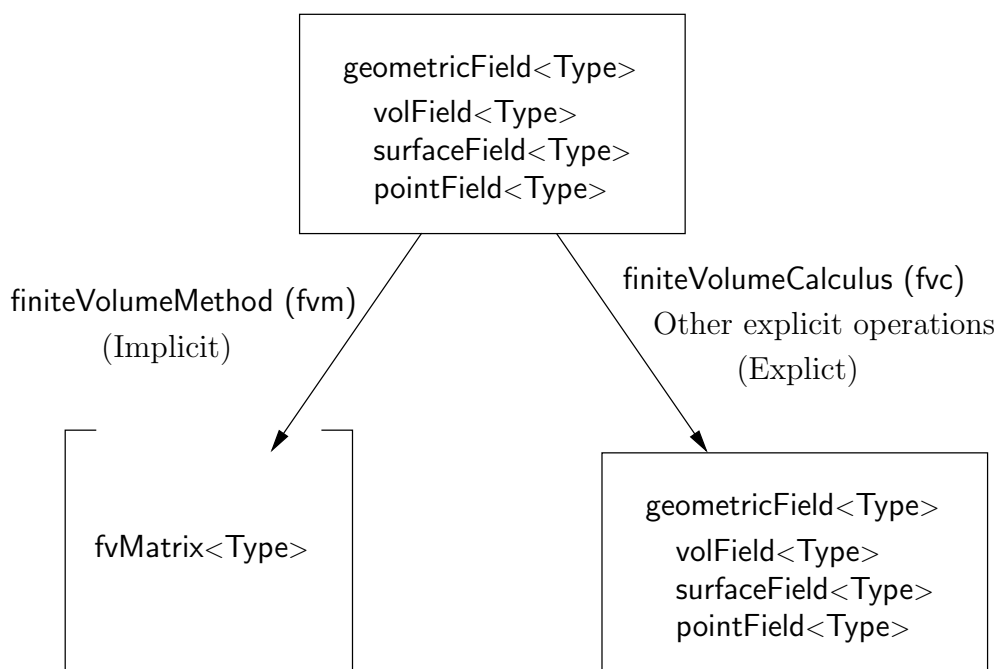


Figure 2.6: A `geometricField<Type>` and its operators

Table 2.2 lists the main functions that are available in `fvm` and `fvc` to discretise terms that may be found in a PDE. FV discretisation of each term is formulated by first integrating the term over a cell volume  $V$ . Most spatial derivative terms are then converted to integrals over the cell surface  $S$  bounding the volume using Gauss's theorem

$$\int_V \nabla \star \phi \, dV = \int_S d\mathbf{S} \star \phi \quad (2.13)$$

where  $\mathbf{S}$  is the surface area vector,  $\phi$  can represent any tensor field and the star notation  $\star$  is used to represent any tensor product, *i.e.* inner, outer and cross and the respective derivatives: divergence  $\nabla \cdot \phi$ , gradient  $\nabla \phi$  and  $\nabla \times \phi$ . Volume and surface integrals are then linearised using appropriate schemes which are described for each term in the following Sections. Some terms are always discretised using one scheme, a selection of schemes is offered in OpenFOAM for the discretisation of other terms. The choice of scheme is either made by a direct specification within the code or it can be read from an input file at job run-time and stored within an `fvSchemes` class object.

Term description	Implicit / Explicit	Text expression	fvm::/fvc:: functions
Laplacian	Imp/Exp	$\nabla^2 \phi$ $\nabla \cdot \Gamma \nabla \phi$	laplacian(phi) laplacian(Gamma, phi)
Time derivative	Imp/Exp	$\frac{\partial \phi}{\partial t}$ $\frac{\partial \rho \phi}{\partial t}$	ddt(phi) ddt(rho, phi)
Second time derivative	Imp/Exp	$\frac{\partial}{\partial t} \left( \rho \frac{\partial \phi}{\partial t} \right)$	d2dt2(rho, phi)
Convection	Imp/Exp	$\nabla \cdot (\psi)$ $\nabla \cdot (\psi \phi)$	div(psi, scheme)* div(psi, phi, word)* div(psi, phi)
Divergence	Exp	$\nabla \cdot \chi$	div(chi)
Gradient	Exp	$\nabla \chi$ $\nabla \phi$	grad(chi) gGrad(phi) lsGrad(phi) snGrad(phi) snGradCorrection(phi)
Grad-grad squared	Exp	$ \nabla \nabla \phi ^2$	sqrGradGrad(phi)
Curl	Exp	$\nabla \times \phi$	curl(phi)
Source	Imp Imp/Exp†	$\rho \phi$	Sp(rho, phi) SuSp(rho, phi)

†fvm::SuSp source is discretised implicit or explicit depending on the sign of rho.

†An explicit source can be introduced simply as a vol<Type>Field, e.g. rho\*phi.

Function arguments can be of the following classes:

phi: vol<Type>Field

Gamma: scalar volScalarField, surfaceScalarField, volTensorField, surfaceTensorField.

rho: scalar, volScalarField

psi: surfaceScalarField.

chi: surface<Type>Field, vol<Type>Field.

Table 2.2: Discretisation of PDE terms in OpenFOAM

### 2.4.1 The Laplacian term

The Laplacian term is integrated over a control volume and linearised as follows:

$$\int_V \nabla \cdot (\Gamma \nabla \phi) dV = \int_S d\mathbf{S} \cdot (\Gamma \nabla \phi) = \sum_f \Gamma_f \mathbf{S}_f \cdot (\nabla \phi)_f \quad (2.14)$$

The face gradient discretisation is implicit when the length vector  $\mathbf{d}$  between the centre of the cell of interest  $P$  and the centre of a neighbouring cell  $N$  is orthogonal to the face plane, *i.e.* parallel to  $\mathbf{S}_f$ :

$$\mathbf{S}_f \cdot (\nabla \phi)_f = |S_f| \frac{\phi_N - \phi_P}{|\mathbf{d}|} \quad (2.15)$$

In the case of non-orthogonal meshes, an additional explicit term is introduced [?] which is evaluated by interpolating cell centre gradients, themselves calculated by central differencing cell centre values.

### 2.4.2 The convection term

The convection term is integrated over a control volume and linearised as follows:

$$\int_V \nabla \cdot (\rho \mathbf{U} \phi) dV = \int_S d\mathbf{S} \cdot (\rho \mathbf{U} \phi) = \sum_f \mathbf{S}_f \cdot (\rho \mathbf{U})_f \phi_f = \sum_f F \phi_f \quad (2.16)$$

The face field  $\phi_f$  can be evaluated using a variety of schemes:

**Central differencing (CD)** is second-order accurate but unbounded

$$\phi_f = f_x \phi_P + (1 - f_x) \phi_N \quad (2.17)$$

where  $f_x \equiv \overline{fN} / \overline{PN}$  where  $\overline{fN}$  is the distance between  $f$  and cell centre  $N$  and  $\overline{PN}$  is the distance between cell centres  $P$  and  $N$ .

**Upwind differencing (UD)** determines  $\phi_f$  from the direction of flow and is bounded at the expense of accuracy

$$\phi_f = \begin{cases} \phi_P & \text{for } F \geq 0 \\ \phi_N & \text{for } F < 0 \end{cases} \quad (2.18)$$

**Blended differencing (BD)** schemes combine UD and CD in an attempt to preserve boundedness with reasonable accuracy,

$$\phi_f = (1 - \gamma) (\phi_f)_{UD} + \gamma (\phi_f)_{CD} \quad (2.19)$$

OpenFOAM has several implementations of the Gamma differencing scheme to select the blending coefficient  $\gamma$  [?] but it offers other well-known schemes such as van Leer, SUPERBEE, MINMOD *etc.*

### 2.4.3 First time derivative

The first time derivative  $\partial/\partial t$  is integrated over a control volume as follows:

$$\frac{\partial}{\partial t} \int_V \rho \phi \, dV \quad (2.20)$$

The term is discretised by simple differencing in time using:

**new values**  $\phi^n \equiv \phi(t + \Delta t)$  at the time step we are solving for;

**old values**  $\phi^o \equiv \phi(t)$  that were stored from the previous time step;

**old-old values**  $\phi^{oo} \equiv \phi(t - \Delta t)$  stored from a time step previous to the last.

One of two discretisation schemes can be declared using the `timeScheme` keyword in the appropriate input file, described in detail in [section 4.4](#) of the User Guide.

**Euler implicit** scheme, `timeScheme EulerImplicit`, that is first order accurate in time:

$$\frac{\partial}{\partial t} \int_V \rho \phi \, dV = \frac{(\rho_P \phi_P V)^n - (\rho_P \phi_P V)^o}{\Delta t} \quad (2.21)$$

**Backward differencing** scheme, `timeScheme BackwardDifferencing`, that is second order accurate in time by storing the old-old values and therefore with a larger overhead in data storage than `EulerImplicit`:

$$\frac{\partial}{\partial t} \int_V \rho \phi \, dV = \frac{3(\rho_P \phi_P V)^n - 4(\rho_P \phi_P V)^o + (\rho_P \phi_P V)^{oo}}{2\Delta t} \quad (2.22)$$

### 2.4.4 Second time derivative

The second time derivative is integrated over a control volume and linearised as follows:

$$\frac{\partial}{\partial t} \int_V \rho \frac{\partial \phi}{\partial t} \, dV = \frac{(\rho_P \phi_P V)^n - 2(\rho_P \phi_P V)^o + (\rho_P \phi_P V)^{oo}}{\Delta t^2} \quad (2.23)$$

It is first order accurate in time.

### 2.4.5 Divergence

The divergence term described in this Section is strictly an explicit term that is distinguished from the convection term of [Section 2.4.2](#), *i.e.* in that it is not the divergence of the product of a velocity and dependent variable. The term is integrated over a control volume and linearised as follows:

$$\int_V \nabla \cdot \phi \, dV = \int_S d\mathbf{S} \cdot \phi = \sum_f \mathbf{S}_f \cdot \phi_f \quad (2.24)$$

The `fvc::div` function can take as its argument either a `surface<Type>Field`, in which case  $\phi_f$  is specified directly, or a `vol<Type>Field` which is interpolated to the face by central differencing as described in [Section 2.4.10](#):

### 2.4.6 Gradient

The gradient term is an explicit term that can be evaluated in a variety of ways. The scheme can be evaluated either by selecting the particular grad function relevant to the discretisation scheme, *e.g.* `fvc::gGrad`, `fvc::lsGrad` *etc.*, or by using the `fvc::grad` function combined with the appropriate `timeScheme` keyword in an input file

**Gauss integration** is invoked using the `fvc::grad` function with `timeScheme Gauss` or directly using the `fvc::gGrad` function. The discretisation is performed using the standard method of applying Gauss's theorem to the volume integral:

$$\int_V \nabla \phi \, dV = \int_S d\mathbf{S} \, \phi = \sum_f \mathbf{S}_f \phi_f \quad (2.25)$$

As with the `fvc::div` function, the Gaussian integration `fvc::grad` function can take either a `surfaceField<Type>` or a `volField<Type>` as an argument.

**Least squares method** is based on the following idea:

1. a value at point  $P$  can be extrapolated to neighbouring point  $N$  using the gradient at  $P$ ;
2. the extrapolated value at  $N$  can be compared to the actual value at  $N$ , the difference being the error;
3. if we now minimise the sum of the square of weighted errors at all neighbours of  $P$  with the respect to the gradient, then the gradient should be a good approximation.

Least squares is invoked using the `fvc::grad` function with `timeScheme leastSquares` or directly using the `fvc::lsGrad` function. The discretisation is performed as by first calculating the tensor  $\mathbf{G}$  at every point  $P$  by summing over neighbours  $N$ :

$$\mathbf{G} = \sum_N w_N^2 \mathbf{d} \mathbf{d} \quad (2.26)$$

where  $\mathbf{d}$  is the vector from  $P$  to  $N$  and the weighting function  $w_N = 1/|\mathbf{d}|$ . The gradient is then evaluated as:

$$(\nabla \phi)_P = \sum_N w_N^2 \mathbf{G}^{-1} \cdot \mathbf{d} (\phi_N - \phi_P) \quad (2.27)$$

**Surface normal gradient** The gradient normal to a surface  $\mathbf{n}_f \cdot (\nabla \phi)_f$  can be evaluated at cell faces using the scheme

$$(\nabla \phi)_f = \frac{\phi_N - \phi_P}{|\mathbf{d}|} \quad (2.28)$$

This gradient is called by the function `fvc::snGrad` and returns a `surfaceField<Type>`. The scheme is directly analogous to that evaluated for the Laplacian discretisation scheme in Section 2.4.1, and in the same manner, a correction can be introduced to improve the accuracy of this face gradient in the case of non-orthogonal meshes. This correction is called using the function `fvc::snGradCorrection [Check**]`.



### 2.4.7 Grad-grad squared

The grad-grad squared term is evaluated by: taking the gradient of the field; taking the gradient of the resulting gradient field; and then calculating the magnitude squared of the result. The mathematical expression for grad-grad squared of  $\phi$  is  $|\nabla(\nabla\phi)|^2$ .

### 2.4.8 Curl

The curl is evaluated from the gradient term described in Section 2.4.6. First, the gradient is discretised and then the curl is evaluated using the relationship from Equation 2.7, repeated here for convenience

$$\nabla \times \phi = 2 * (\text{skew } \nabla \phi)$$

### 2.4.9 Source terms

Source terms can be specified in 3 ways

**Explicit** Every explicit term is a `volField<Type>`. Hence, an explicit source term can be incorporated into an equation simply as a field of values. For example if we wished to solve Poisson's equation  $\nabla^2\phi = f$ , we would define `phi` and `f` as `volScalarField` and then do

```
solve(fvm::laplacian(phi) == f)
```

**Implicit** An implicit source term is integrated over a control volume and linearised by

$$\int_V \rho \phi \, dV = \rho_P V_P \phi_P \quad (2.29)$$

**Implicit/Explicit** The implicit source term changes the coefficient of the diagonal of the matrix. Depending on the sign of the coefficient and matrix terms, this will either increase or decrease diagonal dominance of the matrix. Decreasing the diagonal dominance could cause instability during iterative solution of the matrix equation. Therefore OpenFOAM provides a mixed source discretisation procedure that is implicit when the coefficients that are greater than zero, and explicit for the coefficients less than zero. In mathematical terms the matrix coefficient for node  $P$  is  $V_P \max(\rho_P, 0)$  and the source term is  $V_P \phi_P \min(\rho_P, 0)$ .

### 2.4.10 Other explicit discretisation schemes

There are some other discretisation procedures that convert `volField<Type>`s into `surface<Type>Fields` and visa versa.

**Surface integral** `fvc::surfaceIntegrate` performs a summation of `surface<Type>Field` face values bounding each cell and dividing by the cell volume, *i.e.*  $(\sum_f \phi_f)/V_P$ . It returns a `volField<Type>`.

**Surface sum** `fvc::surfaceSum` performs a summation of `surface<Type>Field` face values bounding each cell, *i.e.*  $\sum_f \phi_f$  returning a `volField<Type>`.

**Average** `fvc::average` produces an area weighted average of `surface<Type>Field` face values, *i.e.*  $(\sum_f S_f \phi_f) / \sum_f S_f$ , and returns a `volField<Type>`.

## Reconstruct

**Face interpolate** The `geometric<Type>Field` function `faceInterpolate()` interpolates `volField<Type>` cell centre values to cell faces using central differencing, returning a `surface<Type>Field`.

## 2.5 Temporal discretisation

Although we have described the discretisation of temporal derivatives in Sections 2.4.3 and 2.4.4, we need to consider how to treat the spatial derivatives in a transient problem. If we denote all the spatial terms as  $\mathcal{A}\phi$  where  $\mathcal{A}$  is any spatial operator, *e.g.* Laplacian, then we can express a transient PDE in integral form as

$$\int_t^{t+\Delta t} \left[ \frac{\partial}{\partial t} \int_V \rho \phi \, dV + \int_V \mathcal{A} \phi \, dV \right] dt = 0 \quad (2.30)$$

Using the Euler implicit method of Equation 2.21, the first term can be expressed as

$$\begin{aligned} \int_t^{t+\Delta t} \left[ \frac{\partial}{\partial t} \int_V \rho \phi \, dV \right] dt &= \int_t^{t+\Delta t} \frac{(\rho_P \phi_P V)^n - (\rho_P \phi_P V)^o}{\Delta t} dt \\ &= \frac{(\rho_P \phi_P V)^n - (\rho_P \phi_P V)^o}{\Delta t} \Delta t \end{aligned} \quad (2.31)$$

The second term can be expressed as

$$\int_t^{t+\Delta t} \left[ \int_V \mathcal{A} \phi \, dV \right] dt = \int_t^{t+\Delta t} \mathcal{A}^* \phi \, dt \quad (2.32)$$

where  $\mathcal{A}^*$  represents the spatial discretisation of  $\mathcal{A}$ . The time integral can be discretised in three ways:

**Euler implicit** uses implicit discretisation of the spatial terms, thereby taking current values  $\phi^n$ .

$$\int_t^{t+\Delta t} \mathcal{A}^* \phi \, dt = \mathcal{A}^* \phi^n \Delta t \quad (2.33)$$

It is first order accurate in time, guarantees boundedness and is unconditionally stable.

**Explicit** uses explicit discretisation of the spatial terms, thereby taking old values  $\phi^o$ .

$$\int_t^{t+\Delta t} \mathcal{A}^* \phi \, dt = \mathcal{A}^* \phi^o \Delta t \quad (2.34)$$

It is first order accurate in time and is unstable if the Courant number  $Co$  is greater than 1. The Courant number is defined as

$$Co = \frac{\mathbf{U}_f \cdot \mathbf{d}}{|\mathbf{d}|^2 \Delta t} \quad (2.35)$$

where  $\mathbf{U}_f$  is a characteristic velocity, *e.g.* velocity of a wave front, velocity of flow.

**Crank Nicholson** uses the trapezoid rule to discretise the spatial terms, thereby taking a mean of current values  $\phi^n$  and old values  $\phi^o$ .

$$\int_t^{t+\Delta t} \mathcal{A}^* \phi \, dt = \mathcal{A}^* \left( \frac{\phi^n + \phi^o}{2} \right) \Delta t \quad (2.36)$$

It is second order accurate in time, is unconditionally stable but does not guarantee boundedness.

### 2.5.1 Treatment of temporal discretisation in OpenFOAM

At present the treatment of the temporal discretisation is controlled by the implementation of the spatial derivatives in the PDE we wish to solve. For example, let us say we wish to solve a transient diffusion equation

$$\frac{\partial \phi}{\partial t} = \kappa \nabla^2 \phi \quad (2.37)$$

An Euler implicit implementation of this would read

```
solve(fvm::ddt(phi) == kappa*fvm::laplacian(phi))
```

where we use the `fvm` class to discretise the `Laplacian` term implicitly. An explicit implementation would read

```
solve(fvm::ddt(phi) == kappa*fvc::laplacian(phi))
```

where we now use the `fvc` class to discretise the `Laplacian` term explicitly. The Crank Nicholson scheme can be implemented by the mean of implicit and explicit terms:

```
solve
(
  fvm::ddt(phi)
  ==
  kappa*0.5*(fvm::laplacian(phi) + fvc::laplacian(phi))
)
```

## 2.6 Boundary Conditions

Boundary conditions are required to complete the problem we wish to solve. We therefore need to specify boundary conditions on all our boundary faces. Boundary conditions can be divided into 2 types:

**Dirichlet** prescribes the value of the dependent variable on the boundary and is therefore termed ‘fixed value’ in this guide;

**Neumann** prescribes the gradient of the variable normal to the boundary and is therefore termed ‘fixed gradient’ in this guide.

When we perform discretisation of terms that include the sum over faces  $\sum_f$ , we need to consider what happens when one of the faces is a boundary face.

**Fixed value** We specify a fixed value at the boundary  $\phi_b$

- We can simply substitute  $\phi_b$  in cases where the discretisation requires the value on a boundary face  $\phi_f$ , *e.g.* in the convection term in [Equation 2.16](#).
- In terms where the face gradient  $(\nabla \phi)_f$  is required, *e.g.* Laplacian, it is calculated using the boundary face value and cell centre value,

$$\mathbf{S}_f \cdot (\nabla \phi)_f = |S_f| \frac{\phi_b - \phi_P}{|\mathbf{d}|} \quad (2.38)$$

**Fixed gradient** The fixed gradient boundary condition  $g_b$  is a specification on inner product of the gradient and unit normal to the boundary, or

$$g_b = \left( \frac{\mathbf{S}}{|\mathbf{S}|} \cdot \nabla \phi \right)_f \quad (2.39)$$

- When discretisation requires the value on a boundary face  $\phi_f$  we must interpolate the cell centre value to the boundary by

$$\begin{aligned} \phi_f &= \phi_P + \mathbf{d} \cdot (\nabla \phi)_f \\ &= \phi_P + |\mathbf{d}| g_b \end{aligned} \quad (2.40)$$

- $\phi_b$  can be directly substituted in cases where the discretisation requires the face gradient to be evaluated,

$$\mathbf{S}_f \cdot (\nabla \phi)_f = |S_f| g_b \quad (2.41)$$

### 2.6.1 Physical boundary conditions

The specification of boundary conditions is usually an engineer's interpretation of the true behaviour. Real boundary conditions are generally defined by some physical attributes rather than the numerical description as described of the previous Section. In incompressible fluid flow there are the following physical boundaries

**Inlet** The velocity field at the inlet is supplied and, for consistency, the boundary condition on pressure is zero gradient.

**Outlet** The pressure field at the outlet is supplied and a zero gradient boundary condition on velocity is specified.

**No-slip impermeable wall** The velocity of the fluid is equal to that of the wall itself, *i.e.* a fixed value condition can be specified. The pressure is specified zero gradient since the flux through the wall is zero.

In a problem whose solution domain and boundary conditions are symmetric about a plane, we only need to model half the domain to one side of the symmetry plane. The boundary condition on the plane must be specified according to

**Symmetry plane** The symmetry plane condition specifies the component of the gradient normal to the plane should be zero. [Check\*\*]

# Chapter 3

## Examples of the use of OpenFOAM

In this section we shall describe several test cases supplied with the OpenFOAM distribution. The intention is to provide example cases, including those in the tutorials in [chapter 2](#) of the User Guide, for every standard solver. The examples are designed to introduce certain tools and features of OpenFOAM, *e.g.* within pre-/post-processing, numerical schemes, algorithms. They also provide a means for validation of solvers although that is not their principal function.

Each example contains a description of the problem: the geometry, initial and boundary conditions, a brief description of the equations being solved, models used, and physical properties required. The solution domain is selected which may be a portion of the original geometry, *e.g.* if we introduce symmetry planes. The method of meshing, usually **blockMesh**, is specified; of course the user can simply view the mesh since every example is distributed with the *polyMesh* directory containing the data files that describe the mesh.

The examples coexist with the tutorials in the *tutorials* subdirectory of the OpenFOAM installation. They are organised into a set of subdirectories by solver, *e.g.* all the *icoFoam* cases are stored within a subdirectory *icoFoam*. Before running a particular example, the user is urged to copy it into their user account. We recommend that the user stores all OpenFOAM cases in a directory we recommend that the tutorials are copied into a directory *\$FOAM\_RUN*. If this directory structure has not yet been created in the user's account, it can be created with

```
mkdir -p $FOAM_RUN
```

The tutorials can then be copied into this directory with

```
cp -r $FOAM_TUTORIALS/* $FOAM_RUN
```

### 3.1 Flow around a cylinder

In this example we shall investigate potential flow around a cylinder using **potentialFoam**. This example introduces the following OpenFOAM features:

- non-orthogonal meshes;
- generating an analytical solution to a problem in OpenFOAM.

### 3.1.1 Problem specification

The problem is defined as follows:

**Solution domain** The domain is 2 dimensional and consists of a square domain with a cylinder collocated with the centre of the square as shown in [Figure 3.1](#).

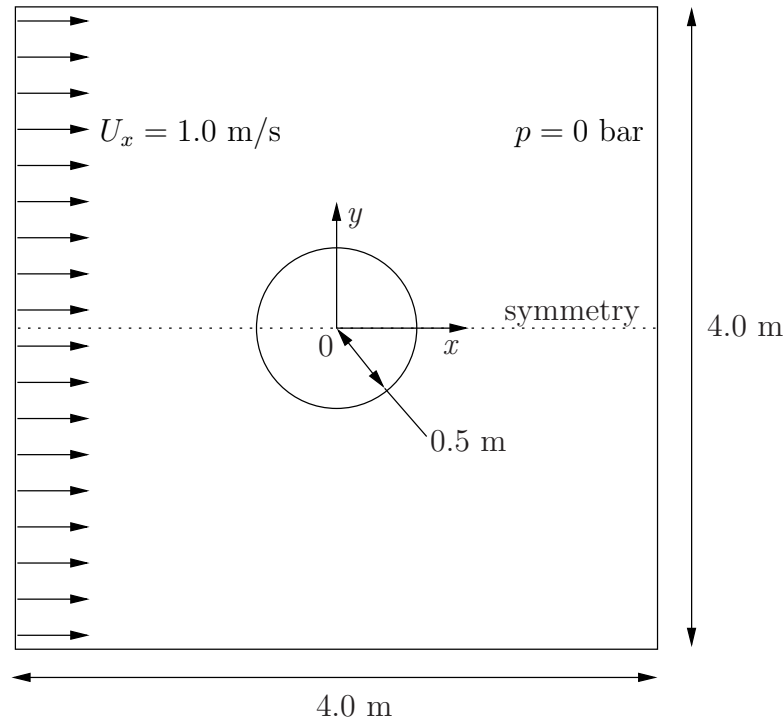


Figure 3.1: Geometry of flow round a cylinder

#### Governing equations

- Mass continuity for an incompressible fluid

$$\nabla \cdot \mathbf{U} = 0 \quad (3.1)$$

- Pressure equation for an incompressible, irrotational fluid assuming steady-state conditions

$$\nabla^2 p = 0 \quad (3.2)$$

#### Boundary conditions

- Inlet (left) with fixed velocity  $\mathbf{U} = (1, 0, 0)$  m/s.
- Outlet (right) with a fixed pressure  $p = 0$  Pa.
- No-slip wall (bottom);
- Symmetry plane (top).

**Initial conditions**  $U = 0$  m/s,  $p = 0$  Pa — required in OpenFOAM input files but not necessary for the solution since the problem is steady-state.

**Solver name** potentialFoam: a potential flow code, *i.e.* assumes the flow is incompressible, steady, irrotational, inviscid and it ignores gravity.

**Case name** cylinder case located in the `$FOAM_TUTORIALS/potentialFoam` directory.

### 3.1.2 Note on potentialFoam

**potentialFoam** is a useful solver to validate OpenFOAM since the assumptions of potential flow are such that an analytical solution exists for cases whose geometries are relatively simple. In this example of flow around a cylinder an analytical solution exists with which we can compare our numerical solution. **potentialFoam** can also be run more like a utility to provide a (reasonably) conservative initial **U** field for a problem. When running certain cases, this can be useful for avoiding instabilities due to the initial field being unstable. In short, **potentialFoam** creates a conservative field from a non-conservative initial field supplied by the user.

### 3.1.3 Mesh generation

Mesh generation using **blockMesh** has been described in tutorials in the User Guide. In this case, the mesh consists of 10 blocks as shown in **Figure 3.2**. Remember that all

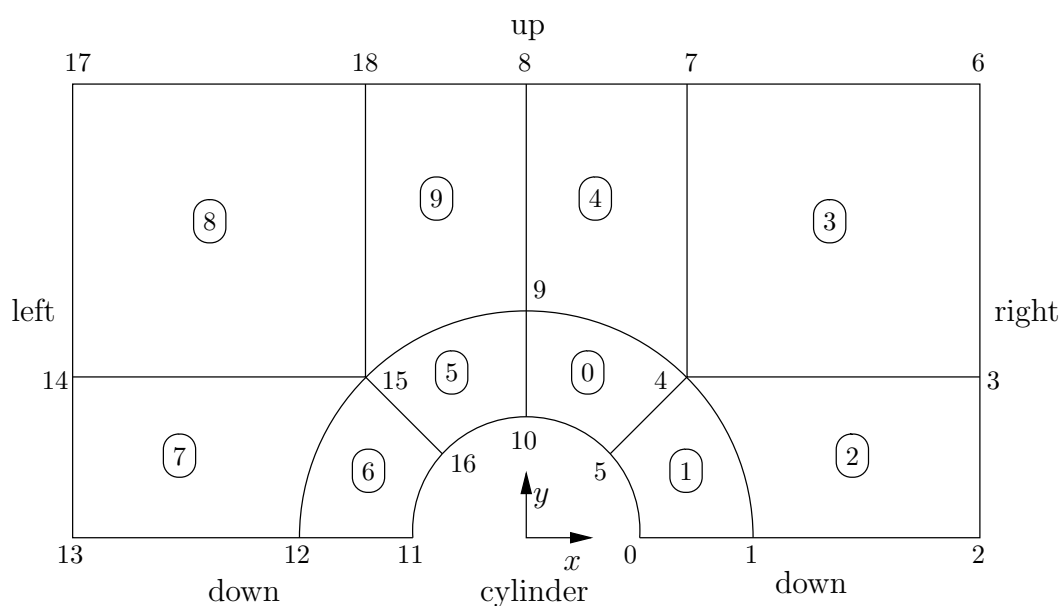


Figure 3.2: Blocks in cylinder geometry

meshes are treated as 3 dimensional in OpenFOAM. If we wish to solve a 2 dimensional problem, we must describe a 3 dimensional mesh that is only one cell thick in the third direction that is not solved. In **Figure 3.2** we show only the back plane of the geometry, along  $z = -0.5$ , in which the vertex numbers are numbered 0-18. The other 19 vertices in the front plane,  $z = +0.5$ , are numbered in the same order as the back plane, as shown in the mesh description file below:

```

1  /*-----*-- C++ -----*/
2  |=====|
3  | \      / | F ield      | OpenFOAM: The Open Source CFD Toolbox
4  |  \    /  | O peration  | Version: 1.5
5  |   \  /   | A nd        | Web: http://www.OpenFOAM.org
6  |    \/    | M anipulation|
7  |-----*--*/
8  FoamFile
9  {
10     version      2.0;
11     format        ascii;
12     class         dictionary;
13     object        blockMeshDict;
14 }
15 // *****
16
17 convertToMeters 1;
```

```

18
19 vertices
20 (
21     (0.5 0 -0.5)
22     (1 0 -0.5)
23     (2 0 -0.5)
24     (2 0.707107 -0.5)
25     (0.707107 0.707107 -0.5)
26     (0.353553 0.353553 -0.5)
27     (2 2 -0.5)
28     (0.707107 2 -0.5)
29     (0 2 -0.5)
30     (0 1 -0.5)
31     (0 0.5 -0.5)
32     (-0.5 0 -0.5)
33     (-1 0 -0.5)
34     (-2 0 -0.5)
35     (-2 0.707107 -0.5)
36     (-0.707107 0.707107 -0.5)
37     (-0.353553 0.353553 -0.5)
38     (-2 2 -0.5)
39     (-0.707107 2 -0.5)
40     (0.5 0 0.5)
41     (1 0 0.5)
42     (2 0 0.5)
43     (2 0.707107 0.5)
44     (0.707107 0.707107 0.5)
45     (0.353553 0.353553 0.5)
46     (2 2 0.5)
47     (0.707107 2 0.5)
48     (0 2 0.5)
49     (0 1 0.5)
50     (0 0.5 0.5)
51     (-0.5 0 0.5)
52     (-1 0 0.5)
53     (-2 0 0.5)
54     (-2 0.707107 0.5)
55     (-0.707107 0.707107 0.5)
56     (-0.353553 0.353553 0.5)
57     (-2 2 0.5)
58     (-0.707107 2 0.5)
59 );
60
61 blocks
62 (
63     hex (5 4 9 10 24 23 28 29) (10 10 1) simpleGrading (1 1 1)
64     hex (0 1 4 5 19 20 23 24) (10 10 1) simpleGrading (1 1 1)
65     hex (1 2 3 4 20 21 22 23) (20 10 1) simpleGrading (1 1 1)
66     hex (4 3 6 7 23 22 25 26) (20 20 1) simpleGrading (1 1 1)
67     hex (9 4 7 8 28 23 26 27) (10 20 1) simpleGrading (1 1 1)
68     hex (15 16 10 9 34 35 29 28) (10 10 1) simpleGrading (1 1 1)
69     hex (12 11 16 15 31 30 35 34) (10 10 1) simpleGrading (1 1 1)
70     hex (13 12 15 14 32 31 34 33) (20 10 1) simpleGrading (1 1 1)
71     hex (14 15 18 17 33 34 37 36) (20 20 1) simpleGrading (1 1 1)
72     hex (15 9 8 18 34 28 27 37) (10 20 1) simpleGrading (1 1 1)
73 );
74
75 edges
76 (
77     arc 0 5 (0.469846 0.17101 -0.5)
78     arc 5 10 (0.17101 0.469846 -0.5)
79     arc 1 4 (0.939693 0.34202 -0.5)
80     arc 4 9 (0.34202 0.939693 -0.5)
81     arc 19 24 (0.469846 0.17101 0.5)
82     arc 24 29 (0.17101 0.469846 0.5)
83     arc 20 23 (0.939693 0.34202 0.5)
84     arc 23 28 (0.34202 0.939693 0.5)
85     arc 11 16 (-0.469846 0.17101 -0.5)
86     arc 16 10 (-0.17101 0.469846 -0.5)
87     arc 12 15 (-0.939693 0.34202 -0.5)
88     arc 15 9 (-0.34202 0.939693 -0.5)
89     arc 30 35 (-0.469846 0.17101 0.5)
90     arc 35 29 (-0.17101 0.469846 0.5)
91     arc 31 34 (-0.939693 0.34202 0.5)
92     arc 34 28 (-0.34202 0.939693 0.5)
93 );
94
95 patches
96 (
97     symmetryPlane down
98     (
99         (0 1 20 19)
100        (1 2 21 20)
101        (12 11 30 31)

```



```

102         (13 12 31 32)
103     )
104     patch right
105     (
106         (2 3 22 21)
107         (3 6 25 22)
108     )
109     symmetryPlane up
110     (
111         (7 8 27 26)
112         (6 7 26 25)
113         (8 18 37 27)
114         (18 17 36 37)
115     )
116     patch left
117     (
118         (14 13 32 33)
119         (17 14 33 36)
120     )
121     symmetryPlane cylinder
122     (
123         (10 5 24 29)
124         (5 0 19 24)
125         (16 10 29 35)
126         (11 16 35 30)
127     )
128 );
129
130 mergePatchPairs
131 (
132 );
133
134 // *****

```

### 3.1.4 Boundary conditions and initial fields

Using **FoamX** or editing case files by hand, set the boundary conditions in accordance with the problem description in [Figure 3.1](#), *i.e.* the left boundary should be an **Inlet**, the right boundary should be an **Outlet** and the down and cylinder boundaries should be **symmetryPlane**. The top boundary conditions is chosen so that we can make the most genuine comparison with our analytical solution which uses the assumption that the domain is infinite in the  $y$  direction. The result is that the normal gradient of  $\mathbf{U}$  is small along a plane coinciding with our boundary. We therefore impose the condition that the normal component is zero, *i.e.* specify the boundary as a **symmetryPlane**, thereby ensuring that the comparison with the analytical is reasonable.

### 3.1.5 Running the case

No fluid properties need be specified in this problem since the flow is assumed to be incompressible and inviscid. In the **system** subdirectory, the **controlDict** specifies the control parameters for the run. Note that since we assume steady flow, we only run for 1 time step:

```

1  /*-----*-- C++ -*-----*/
2  |=====|
3  |  \ \  /  F ield      | OpenFOAM: The Open Source CFD Toolbox |
4  |  \ \  /  O peration   | Version: 1.5                        |
5  |  \ \  /  A nd         | Web:      http://www.OpenFOAM.org    |
6  |  \ \  /  M anipulation |                                     |
7  |-----*--*/
8  FoamFile
9  {
10     version      2.0;
11     format        ascii;
12     class         dictionary;
13     object        controlDict;
14 }
15 // *****
16
17 application potentialFoam;
18

```

```

19  startFrom      startTime;
20
21  startTime      0;
22
23  stopAt         endTime;
24
25  endTime        1;
26
27  deltaT         1;
28
29  writeControl    timeStep;
30
31  writeInterval   1;
32
33  purgeWrite     0;
34
35  writeFormat     ascii;
36
37  writePrecision  6;
38
39  writeCompression uncompressed;
40
41  timeFormat      general;
42
43  timePrecision   6;
44
45  runTimeModifiable yes;
46
47  // ***** //

```

potentialFoam executes an iterative loop around the pressure equation which it solves in order that explicit terms relating to non-orthogonal correction in the Laplacian term may be updated in successive iterations. The number of iterations around the pressure equation is controlled by the `nNonOrthogonalCorrectors` keyword in *controlDict*. In the first instance we can set `nNonOrthogonalCorrectors` to 0 so that no loops are performed, *i.e.* the pressure equation is solved once, and there is no non-orthogonal correction. The solution is shown in [Figure 3.3\(a\)](#) (at  $t = 1$ , when the steady-state simulation is complete). We expect the solution to show smooth streamlines passing across the domain as in the analytical solution in [Figure 3.3\(c\)](#), yet there is clearly some error in the regions where there is high non-orthogonality in the mesh, *e.g.* at the join of blocks 0, 1 and 3. The case can be run a second time with some non-orthogonal correction by setting `nNonOrthogonalCorrectors` to 3. The solution shows smooth streamlines with no significant error due to non-orthogonality as shown in [Figure 3.3\(b\)](#).

### 3.1.6 Generating the analytical solution

Source code is included in the `$FOAM_TUTORIALS/potentialFoam/analyticalCylinder` directory to generate the analytical solution for the potential flow case. The velocity at any point at a distance  $d$  and angle  $\theta$  from the cylinder centre is described analytically as

$$U_x = U_\infty \left[ 1 - \left( \frac{r}{d} \right)^2 \cos 2\theta \right]$$

$$U_y = U_\infty \left( \frac{r}{d} \right)^2 \sin 2\theta \quad (3.3)$$

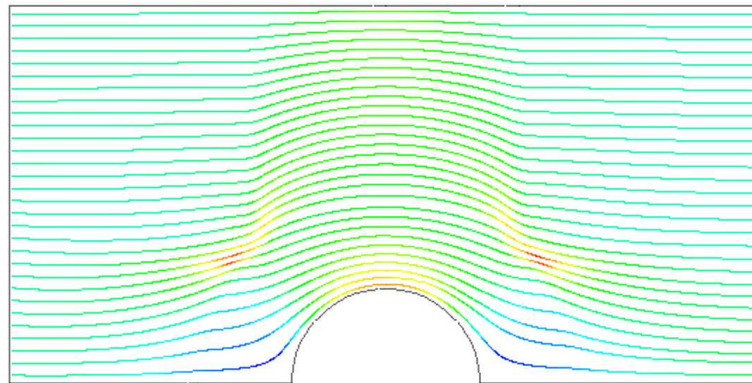
where  $r$  is the cylinder radius and  $U_\infty$  is the inlet flow velocity. Here,  $\theta$  describes the angle subtended from the  $x$ -axis.

Let us examine some details of the source code in the *analyticalCylinder* directory. In *createFields.H*, the velocity field is read in using the `IOobject::NO_WRITE` option to ensure that the field data can never be overwritten during execution of *analyticalCylinder*. The inlet velocity and cylinder radius are taken from data read from the mesh and a field `UA` is set up to store the analytical solution:

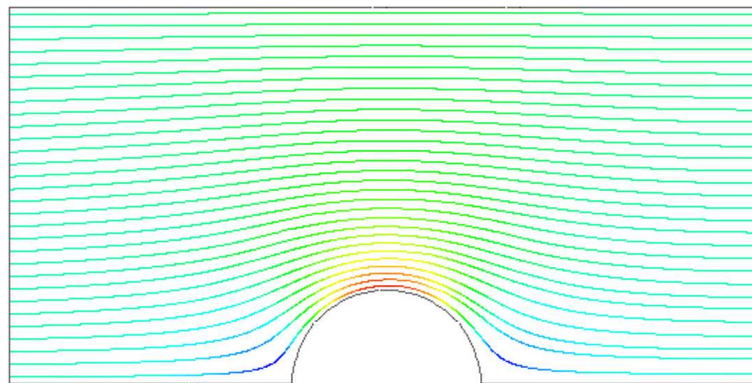
```

1  Info<< "Reading field U\n" << endl;
2  volVectorField U

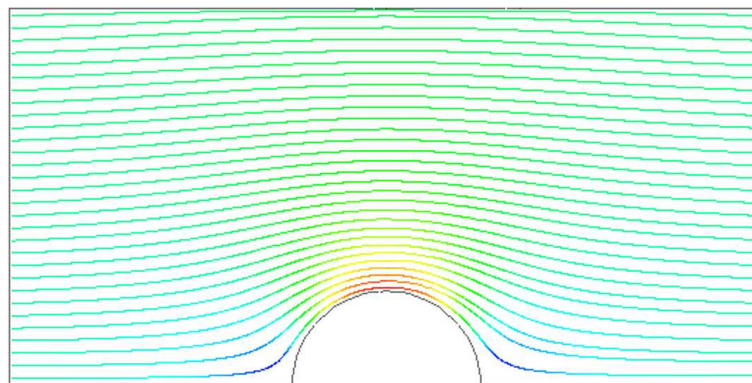
```



(a) With no non-orthogonal correction



(b) With non-orthogonal correction



(c) Analytical solution

Figure 3.3: Streamlines of potential flow

```

3  (
4      IObject
5      (
6          "U",
7          runTime.timeName(),
8          mesh,
9          IObject::MUST_READ,
10         IObject::NO_WRITE
11     ),
12     mesh
13 );
14
15 Info<< "Reading inlet velocity  uInfX\n" << endl;
16
17 dimensionedScalar uInfX
18 (
19     "uInfX",
20     dimensionSet(0, 1, -1, 0, 0),
21     U.boundaryField()[3][0].x()
22 );
23 Info << "U at inlet = " << uInfX.value() << " m/s" << endl;
24
25 dimensionedScalar radius
26 (
27     "radius",
28     dimensionSet(0, 1, 0, 0, 0),
29     mag(U.mesh().boundary()[4].Cf()[0])
30 );
31
32 Info << "Cylinder radius = " << radius.value() << " m" << endl;
33
34 volVectorField UA
35 (
36     IObject
37     (
38         "UA",
39         runTime.timeName(),
40         mesh,
41         IObject::NO_READ,
42         IObject::AUTO_WRITE
43     ),
44     U
45 );

```

The main code *analyticalCylinder.C* performs the following tasks:

- increments the time step by `runTime++`;
- generates the analytical solution for field UA using tensor arithmetic;
- writes the solution to file by `runTime.writeObjects()`.

```

1  /*-----*\
2  =====
3  \ \      /  F i e l d      |  OpenFOAM: The Open Source CFD Toolbox
4  \ \      /  O p e r a t i o n  |
5  \ \      /  A n d      |  Copyright (C) 1991-2008 OpenCFD Ltd.
6  \ \      /  M a n i p u l a t i o n  |
7  -----*/
8  License
9      This file is part of OpenFOAM.
10
11      OpenFOAM is free software; you can redistribute it and/or modify it
12      under the terms of the GNU General Public License as published by the
13      Free Software Foundation; either version 2 of the License, or (at your
14      option) any later version.
15
16      OpenFOAM is distributed in the hope that it will be useful, but WITHOUT
17      ANY WARRANTY; without even the implied warranty of MERCHANTABILITY or
18      FITNESS FOR A PARTICULAR PURPOSE. See the GNU General Public License
19      for more details.
20
21      You should have received a copy of the GNU General Public License
22      along with OpenFOAM; if not, write to the Free Software Foundation,
23      Inc., 51 Franklin St, Fifth Floor, Boston, MA 02110-1301 USA
24
25  Application
26      analyticalCylinder
27
28  Description
29      Generates an analytical solution for potential flow around a cylinder.

```

```

30      Can be compared with the solution from the potentialFlow/cylinder example.
31
32      \*-----*/
33
34      #include "fvCFD.H"
35
36
37      // * * * * *
38
39      int main(int argc, char *argv[])
40      {
41
42          #   include "setRootCase.H"
43
44          #   include "createTime.H"
45          #   include "createMesh.H"
46          #   include "createFields.H"
47
48          // * * * * *
49
50          Info << "\nEvaluating analytical solution" << endl;
51
52          volVectorField centres = UA.mesh().C();
53          volScalarField magCentres = mag(centres);
54          volScalarField theta = acos((centres & vector(1,0,0))/magCentres);
55
56          volVectorField cs2theta =
57              cos(2*theta)*vector(1,0,0)
58              + sin(2*theta)*vector(0,1,0);
59
60          UA = uInfx*(dimensionedVector(vector(1,0,0))
61              - pow((radius/magCentres),2)*cs2theta);
62
63          runTime.write();
64
65          Info<< "end" << endl;
66
67          return(0);
68      }
69
70      // *****

```

The utility must be compiled with `wmake` as normal. It can then be run by typing

```
analyticalCylinder $FOAM_RUN/potentialFoam cylinder
```

The analytical solution is plotted as streamlines as shown in [Figure 3.3\(c\)](#). Note that differences in the analytical and numerical solutions at the top plane are due to the fact that the analytical solution assumes an infinite boundary and the numerical solution specifies a `zeroGradient` boundary condition at that boundary.

### 3.1.7 Exercise

Investigate the accuracy of the numerical solution by implementing some measure of comparison between the numerical and analytical in `analyticalCylinder`.

## 3.2 Steady turbulent flow over a backward-facing step

In this example we shall investigate steady turbulent flow over a backward-facing step. The problem description is taken from one used by Pitz and Daily in an experimental investigation [\[\\*\\*\]](#) against which the computed solution can be compared. This example introduces the following OpenFOAM features for the first time:

- generation of a mesh using `blockMesh` using full mesh grading capability;
- steady turbulent flow.

### 3.2.1 Problem specification

The problem is defined as follows:

**Solution domain** The domain is 2 dimensional, consisting of a short inlet, a backward-facing step and converging nozzle at outlet as shown in [Figure 3.4](#).

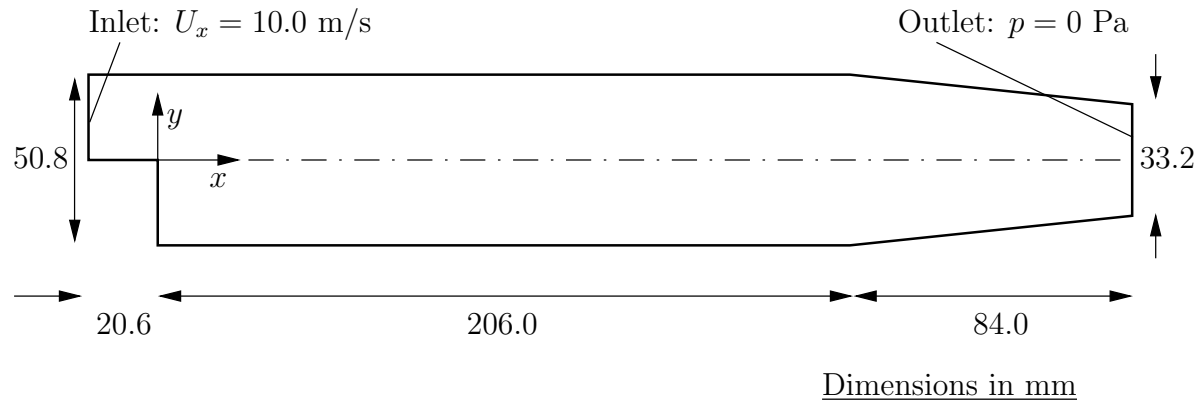


Figure 3.4: Geometry of backward-facing step

#### Governing equations

- Mass continuity for incompressible flow

$$\nabla \cdot \mathbf{U} = 0 \quad (3.4)$$

- Steady flow momentum equation

$$\nabla \cdot (\mathbf{U}\mathbf{U}) + \nabla \cdot \mathbf{R} = -\nabla p \quad (3.5)$$

where  $p$  is kinematic pressure and (in slightly over-simplistic terms)  $\mathbf{R} = \nu_{eff} \nabla \mathbf{U}$  is the viscous stress term with an effective kinematic viscosity  $\nu_{eff}$ , calculated from selected transport and turbulence models.

**Initial conditions**  $U = 0$  m/s,  $p = 0$  Pa — required in OpenFOAM input files but not necessary for the solution since the problem is steady-state.

#### Boundary conditions

- Inlet (left) with fixed velocity  $\mathbf{U} = (10, 0, 0)$  m/s;
- Outlet (right) with fixed pressure  $p = 0$  Pa;
- No-slip walls on other boundaries.

#### Transport properties

- Kinematic viscosity of air  $\nu = \mu/\rho = 18.1 \times 10^{-6}/1.293 = 14.0 \mu\text{m}^2/\text{s}$

#### Turbulence model

- Standard  $k - \epsilon$ ;
- Coefficients:  $C_\mu = 0.09$ ;  $C_1 = 1.44$ ;  $C_2 = 1.92$ ;  $\alpha_k = 1$ ;  $\alpha_\epsilon = 0.76923$ .

**Solver name** simpleFoam: an implementation for steady incompressible flow.





```

24      (-20.6 25.4 -0.5)
25      (0 -25.4 -0.5)
26      (0 -5 -0.5)
27      (0 0 -0.5)
28      (0 3 -0.5)
29      (0 12.7 -0.5)
30      (0 25.4 -0.5)
31      (206 -25.4 -0.5)
32      (206 -8.5 -0.5)
33      (206 0 -0.5)
34      (206 6.5 -0.5)
35      (206 17 -0.5)
36      (206 25.4 -0.5)
37      (290 -16.6 -0.5)
38      (290 -6.3 -0.5)
39      (290 0 -0.5)
40      (290 4.5 -0.5)
41      (290 11 -0.5)
42      (290 16.6 -0.5)
43      (-20.6 0 0.5)
44      (-20.6 3 0.5)
45      (-20.6 12.7 0.5)
46      (-20.6 25.4 0.5)
47      (0 -25.4 0.5)
48      (0 -5 0.5)
49      (0 0 0.5)
50      (0 3 0.5)
51      (0 12.7 0.5)
52      (0 25.4 0.5)
53      (206 -25.4 0.5)
54      (206 -8.5 0.5)
55      (206 0 0.5)
56      (206 6.5 0.5)
57      (206 17 0.5)
58      (206 25.4 0.5)
59      (290 -16.6 0.5)
60      (290 -6.3 0.5)
61      (290 0 0.5)
62      (290 4.5 0.5)
63      (290 11 0.5)
64      (290 16.6 0.5)
65  );
66
67  blocks
68  (
69      hex (0 6 7 1 22 28 29 23) (18 7 1) simpleGrading (0.5 1.8 1)
70      hex (1 7 8 2 23 29 30 24) (18 10 1) simpleGrading (0.5 4 1)
71      hex (2 8 9 3 24 30 31 25) (18 13 1) simpleGrading (0.5 0.25 1)
72      hex (4 10 11 5 26 32 33 27) (180 18 1) simpleGrading (4 1 1)
73      hex (5 11 12 6 27 33 34 28) (180 9 1) edgeGrading (4 4 4 4 0.5 1 1 0.5 1 1 1 1)
74      hex (6 12 13 7 28 34 35 29) (180 7 1) edgeGrading (4 4 4 4 1.8 1 1 1.8 1 1 1 1)
75      hex (7 13 14 8 29 35 36 30) (180 10 1) edgeGrading (4 4 4 4 1 1 4 1 1 1 1)
76      hex (8 14 15 9 30 36 37 31) (180 13 1) simpleGrading (4 0.25 1)
77      hex (10 16 17 11 32 38 39 33) (25 18 1) simpleGrading (2.5 1 1)
78      hex (11 17 18 12 33 39 40 34) (25 9 1) simpleGrading (2.5 1 1)
79      hex (12 18 19 13 34 40 41 35) (25 7 1) simpleGrading (2.5 1 1)
80      hex (13 19 20 14 35 41 42 36) (25 10 1) simpleGrading (2.5 1 1)
81      hex (14 20 21 15 36 42 43 37) (25 13 1) simpleGrading (2.5 0.25 1)
82  );
83
84  edges
85  (
86  );
87
88  patches
89  (
90      patch inlet
91      (
92          (0 22 23 1)
93          (1 23 24 2)
94          (2 24 25 3)
95      )
96      patch outlet
97      (
98          (16 17 39 38)
99          (17 18 40 39)
100         (18 19 41 40)
101         (19 20 42 41)
102         (20 21 43 42)
103     )
104     wall upperWall
105     (
106         (3 25 31 9)

```



```

107         (9 31 37 15)
108         (15 37 43 21)
109     )
110     wall lowerWall
111     (
112         (0 6 28 22)
113         (6 5 27 28)
114         (5 4 26 27)
115         (4 10 32 26)
116         (10 16 38 32)
117     )
118     empty frontAndBack
119     (
120         (22 28 29 23)
121         (23 29 30 24)
122         (24 30 31 25)
123         (26 32 33 27)
124         (27 33 34 28)
125         (28 34 35 29)
126         (29 35 36 30)
127         (30 36 37 31)
128         (32 38 39 33)
129         (33 39 40 34)
130         (34 40 41 35)
131         (35 41 42 36)
132         (36 42 43 37)
133         (0 1 7 6)
134         (1 2 8 7)
135         (2 3 9 8)
136         (4 5 11 10)
137         (5 6 12 11)
138         (6 7 13 12)
139         (7 8 14 13)
140         (8 9 15 14)
141         (10 11 17 16)
142         (11 12 18 17)
143         (12 13 19 18)
144         (13 14 20 19)
145         (14 15 21 20)
146     )
147 );
148
149 mergePatchPairs
150 (
151 );
152
153 // *****

```

A major feature of this problem is the use of the full mesh grading capability of **blockMesh** that is described in [section 5.3.1](#) of the User Guide. The user can see that blocks 4,5 and 6 use the full list of 12 expansion ratios. The expansion ratios correspond to each edge of the block, the first 4 to the edges aligned in the local  $x_1$  direction, the second 4 to the edges in the local  $x_2$  direction and the last 4 to the edges in the local  $x_3$  direction. In blocks 4, 5, and 6, the ratios are equal for all edges in the local  $x_1$  and  $x_3$  directions but not for the edges in the  $x_2$  direction that corresponds in all blocks to the global  $y$ . If we consider the ratios used in relation to the block definition in [section 5.3.1](#) of the User Guide, we realize that different gradings have been prescribed along the left and right edges in blocks 4,5 and 6 in [Figure 3.5](#). The purpose of this differential grading is to generate a fine mesh close to the most critical region of flow, the corner of the step, and allow it to expand into the rest of the domain.

The mesh can be generated using **blockMesh** from the command line or from within **FoamX** and viewed as described in previous examples.

### 3.2.3 Boundary conditions and initial fields

The case files can be viewed, or edited from within **FoamX** or by hand. In this case, we are required to set the initial and boundary fields for velocity  $\mathbf{U}$ , pressure  $p$ , turbulent kinetic energy  $k$  and dissipation rate  $\varepsilon$ . The boundary conditions can be specified by setting the physical patch types in **FoamX**: the upper and lower walls are set to **Wall**, the left patch to **Inlet** and the right patch to **Outlet**. These physical boundary conditions

require us to specify a `fixedValue` at the inlet on  $\mathbf{U}$ ,  $k$  and  $\varepsilon$ .  $\mathbf{U}$  is given in the problem specification, but the values of  $k$  and  $\varepsilon$  must be chosen by the user in a similar manner to that described in [section 2.1.8.1](#) of the User Guide. We assume that the inlet turbulence is isotropic and estimate the fluctuations to be 5% of  $\mathbf{U}$  at the inlet. We have

$$U'_x = U'_y = U'_z = \frac{5}{100}10 = 0.5 \text{ m/s} \quad (3.6)$$

and

$$k = \frac{3}{2}(0.5)^2 = 0.375 \text{ m}^2/\text{s}^2 \quad (3.7)$$

If we estimate the turbulent length scale  $l$  to be 10% of the width of the inlet then

$$\varepsilon = \frac{C_\mu^{0.75} k^{1.5}}{l} = \frac{0.09^{0.75} 0.375^{1.5}}{0.1 \times 25.4 \times 10^{-3}} = 14.855 \text{ m}^2/\text{s}^3 \quad (3.8)$$

At the outlet we need only specify the pressure  $p = 0\text{Pa}$ .

### 3.2.4 Case control

The choices of `fvSchemes` are as follows: the `timeScheme` should be `SteadyState`; the `gradScheme` and `laplacianScheme` should be set as default to `Gauss`; and, the `divScheme` should be set to `UD` to ensure boundedness.

Special attention should be paid to the settings of `fvTolerances`. Although the top level `simpleFoam` code contains only equations for  $p$  and  $\mathbf{U}$ , the turbulent model solves equations for  $k$ ,  $\varepsilon$  and  $\mathbf{R}$ , and tolerance settings are required for all 5 equations. A `solverTolerance` of  $10^{-5}$  and `solverRelativeTolerance` of 0.1 are acceptable for all variables with the exception of  $p$  when  $10^{-6}$  and 0.01 are recommended. Under-relaxation of the solution is required since the problem is steady. A `relaxationFactor` of 0.7 is acceptable for  $\mathbf{U}$ ,  $k$ ,  $\varepsilon$  and  $\mathbf{R}$  but 0.3 is required for  $p$  to avoid numerical instability.

Finally, in `controlDict`, the time step `deltaT` should be set to 1 since in steady state cases such as this is effectively an iteration counter. With benefit of hindsight we know that the solution requires 1000 iterations reach reasonable convergence, hence `endTime` is set to 1000. Ensure that the `writeFrequency` is sufficiently high, *e.g.* 50, that you will not fill the hard disk with data during run time.

### 3.2.5 Running the case and post-processing

Run the case and post-process the results. After a few iterations, *e.g.* 50, a vortex develops beneath the corner of the step that is the height of the step but narrow in the  $x$ -direction as shown by the vector plot of velocities is shown [Figure 3.6\(a\)](#). Over several iterations the vortex stretches in the  $x$ -direction from the step to the outlet until at 1000 iterations the system reaches a steady-state in which the vortex is fully developed as shown in [Figure 3.6\(b-c\)](#).

## 3.3 Supersonic flow over a forward-facing step

In this example we shall investigate supersonic flow over a forward-facing step. The problem description involves a flow of Mach 3 at an inlet to a rectangular geometry with a step near the inlet region that generates shock waves.

This example introduces the following OpenFOAM features for the first time:

- supersonic flow;

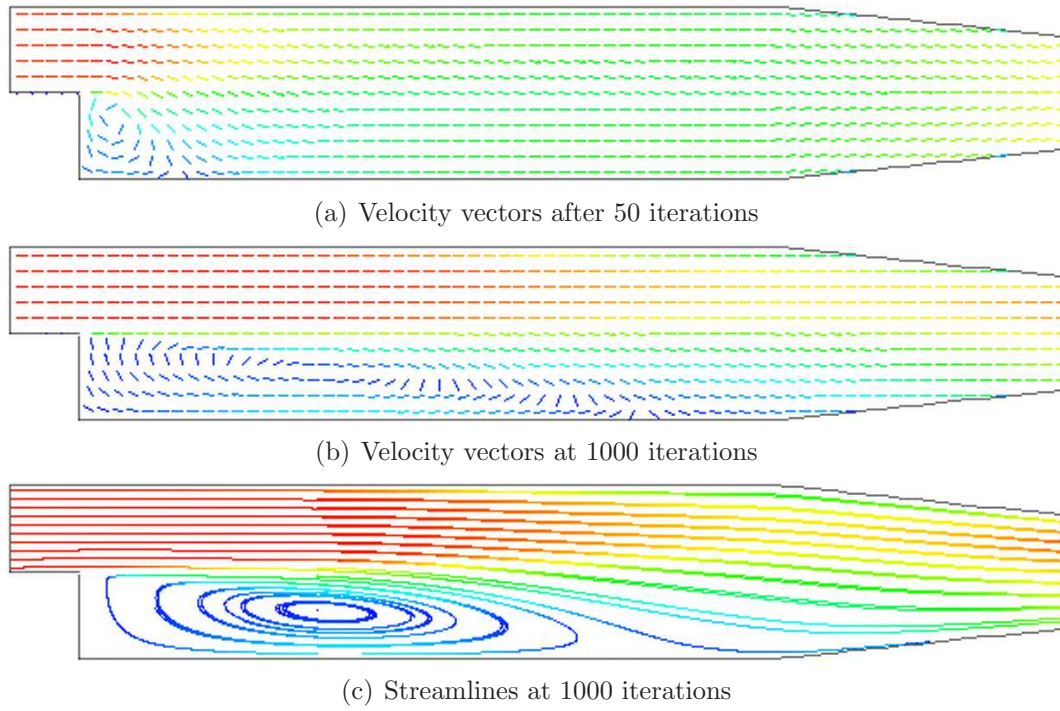


Figure 3.6: Development of a vortex in the backward-facing step.

### 3.3.1 Problem specification

The problem is defined as follows:

**Solution domain** The domain is 2 dimensional and consists of a short inlet section followed by a forward-facing step of 20% the height of the section as shown in [Figure 3.7](#)

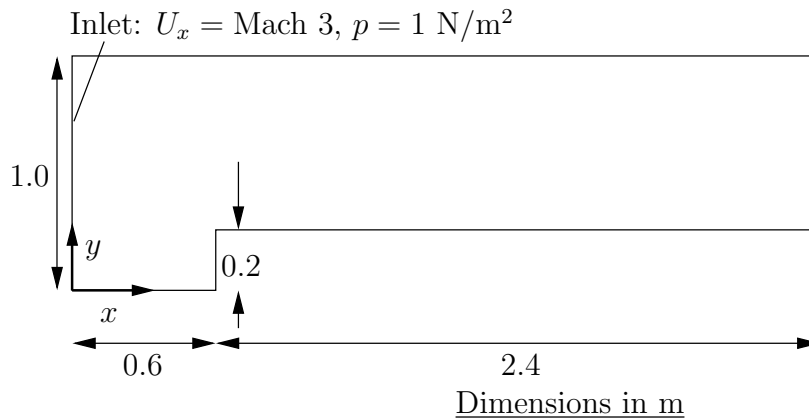


Figure 3.7: Geometry of the forward step geometry

#### Governing equations

- Mass continuity

$$\frac{\partial \rho}{\partial t} + \nabla \cdot (\rho \mathbf{U}) = 0 \quad (3.9)$$

- Ideal gas

$$p = \rho RT \quad (3.10)$$

- Momentum equation for Newtonian fluid

$$\frac{\partial \rho \mathbf{U}}{\partial t} + \nabla \cdot (\rho \mathbf{U} \mathbf{U}) - \nabla \cdot \mu \nabla \mathbf{U} = -\nabla p \quad (3.11)$$

- Energy equation for fluid (ignoring some viscous terms),  $e = C_v T$ , with Fourier's Law  $\mathbf{q} = -k \nabla T$

$$\frac{\partial \rho e}{\partial t} + \nabla \cdot (\rho \mathbf{U} e) - \nabla \cdot \left( \frac{k}{C_v} \right) \nabla e = p \nabla \cdot \mathbf{U} \quad (3.12)$$

**Initial conditions**  $U = 0$  m/s,  $p = 1$  Pa,  $T = 1$  K.

### **Boundary conditions**

- Inlet (left) with `fixedValue` for velocity  $U = 3$  m/s = Mach 3, pressure  $p = 1$  Pa and temperature  $T = 1$  K;
- Outlet (right) with `zeroGradient` on  $U$ ,  $p$  and  $T$ ;
- No-slip adiabatic wall (bottom);
- Symmetry plane (top).

### **Transport properties**

- Dynamic viscosity of air  $\mu = 18.1 \mu\text{Pa s}$

### **Thermodynamic properties**

- Specific heat at constant volume  $C_v = 1.78571$  J/kg K
- Gas constant  $R = 0.714286$  J/kg K
- Conductivity  $k = 32.3 \mu\text{W/m K}$

**Case name** `forwardStep` case located in the `$FOAM_TUTORIALS/sonicFoam` directory.

**Solver name** `sonicFoam`: an implementation for compressible trans-sonic/supersonic laminar gas flow.

The case is designed such that the speed of sound of the gas  $c = \sqrt{\gamma R T} = 1$  m/s, the consequence being that the velocities are directly equivalent to the Mach number, *e.g.* the inlet velocity of 3 m/s is equivalent to Mach 3. This speed of sound calculation can be verified using the relationship for a perfect gas,  $C_p - C_v = R$ , *i.e.* the ratio of specific heats

$$\gamma = C_p / C_v = \frac{R}{C_v} + 1 \quad (3.13)$$

## **3.3.2 Mesh generation**

The mesh used in this case is relatively simple, specified with uniform rectangular cells of length 0.06 m in the  $x$  direction and 0.05 m in the  $y$  direction. The geometry can simply be divided into 3 blocks, one below the top of the step, and two above the step, one either side of the step front. The full set of vertices and blocks are given in the mesh description file below:

```

1  /*-----*-- C++ -----*\
2  |=====|
3  |  \ \  /  | F ield      | OpenFOAM: The Open Source CFD Toolbox
4  |  \ \  /  | O peration  | Version: 1.5
5  |  \ \  /  | A nd        | Web:      http://www.OpenFOAM.org
6  |  \ \  /  | M anipulation|
7  /*-----*--\
8  FoamFile
9  {
10     version      2.0;
11     format        ascii;
12     class          dictionary;
13     object         blockMeshDict;
14 }
15 // * * * * *
16
17 convertToMeters 1;
18
19 vertices
20 (
21     (0 0 -0.05)
22     (0.6 0 -0.05)
23     (0 0.2 -0.05)
24     (0.6 0.2 -0.05)
25     (3 0.2 -0.05)
26     (0 1 -0.05)
27     (0.6 1 -0.05)
28     (3 1 -0.05)
29     (0 0 0.05)
30     (0.6 0 0.05)
31     (0 0.2 0.05)
32     (0.6 0.2 0.05)
33     (3 0.2 0.05)
34     (0 1 0.05)
35     (0.6 1 0.05)
36     (3 1 0.05)
37 );
38
39 blocks
40 (
41     hex (0 1 3 2 8 9 11 10) (25 10 1) simpleGrading (1 1 1)
42     hex (2 3 6 5 10 11 14 13) (25 40 1) simpleGrading (1 1 1)
43     hex (3 4 7 6 11 12 15 14) (100 40 1) simpleGrading (1 1 1)
44 );
45
46 edges
47 (
48 );
49
50 patches
51 (
52     patch inlet
53     (
54         (0 8 10 2)
55         (2 10 13 5)
56     )
57     patch outlet
58     (
59         (4 7 15 12)
60     )
61     symmetryPlane bottom
62     (
63         (0 1 9 8)
64     )
65     symmetryPlane top
66     (
67         (5 13 14 6)
68         (6 14 15 7)
69     )
70     patch obstacle
71     (
72         (1 3 11 9)
73         (3 4 12 11)
74     )
75 );
76
77 mergePatchPairs
78 (
79 );
80
81 // *****

```

### 3.3.3 Running the case

The case approaches a steady-state at some time after 5 s. The results for pressure at 10 s are shown in [Figure 3.8](#). The results clearly show discontinuities in pressure, *i.e.* shock waves, emanating from ahead of the base of the step.

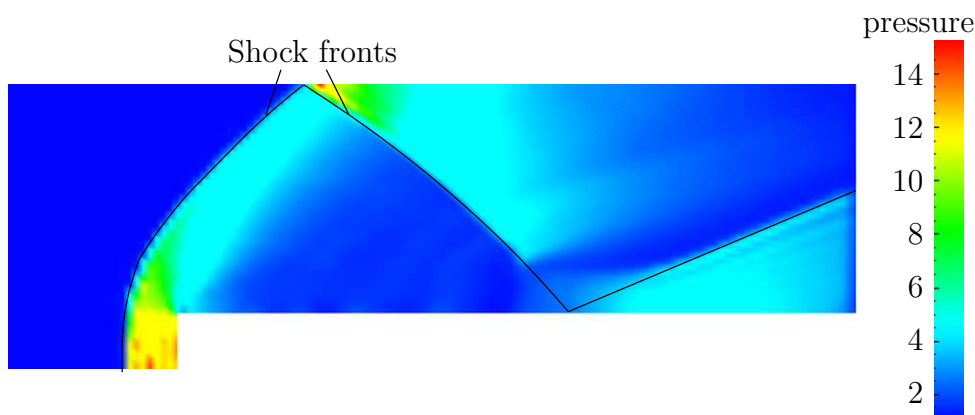


Figure 3.8: Shock fronts in the forward step problem

### 3.3.4 Exercise

The user can examine the effect on the solution of increasing the inlet velocity.

## 3.4 Decompression of a tank internally pressurised with water

In this example we shall investigate a problem of rapid opening of a pipe valve close to a pressurised liquid-filled tank. The prominent feature of the result in such cases is the propagation of pressure waves which must therefore be modelled as a compressible liquid.

This tutorial introduces the following OpenFOAM features for the first time:

- Mesh refinement
- Pressure waves in liquids

### 3.4.1 Problem specification

**Solution domain** The domain is 2 dimensional and consists of a tank with a small outflow pipe as shown in [Figure 3.9](#)

**Governing equations** This problem requires a model for compressibility  $\psi$  in the fluid in order to be able to resolve waves propagating at a finite speed. A barotropic relationship is used to relate density  $\rho$  and pressure  $p$  are related to  $\psi$ .

- Mass continuity

$$\frac{\partial \rho}{\partial t} + \nabla \cdot (\rho \mathbf{U}) = 0 \quad (3.14)$$

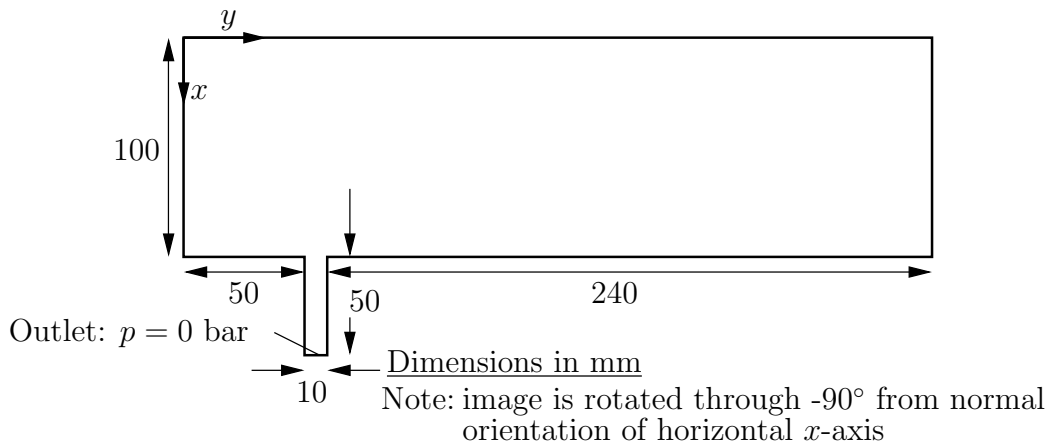


Figure 3.9: Geometry of a tank with outflow pipe

- The barotropic relationship

$$\frac{\partial \rho}{\partial p} = \frac{\rho}{K} = \psi \quad (3.15)$$

where  $K$  is the bulk modulus

- Equation 3.15 is linearised as

$$\rho \approx \rho_0 + \psi (p - p_0) \quad (3.16)$$

where  $\rho_0$  and  $p_0$  are the reference density and pressure respectively such that  $\rho(p_0) = \rho_0$ .

- Momentum equation for Newtonian fluid

$$\frac{\partial \rho \mathbf{U}}{\partial t} + \nabla \cdot (\rho \mathbf{U} \mathbf{U}) - \nabla \cdot \mu \nabla \mathbf{U} = -\nabla p \quad (3.17)$$

**Boundary conditions** Using FoamX the following physical boundary conditions can be set:

- `outerWall` is specified the `wall` condition;
- `axis` is specified as the `symmetryPlane`;
- `nozzle` is specified as a `pressureOutlet` where  $p = 0$  bar.
- `front` and `back` boundaries are specified as `empty`.

**Initial conditions**  $\mathbf{U} = 0$  m/s,  $p = 100$  bar.

**Transport properties**

- Dynamic viscosity of water  $\mu = 1.0$  mPa s

**Thermodynamic properties**

- Density of water  $\rho = 1000$  kg/m<sup>3</sup>
- Reference pressure  $p_0 = 1$  bar
- Compressibility of water  $\psi = 4.54 \times 10^{-7}$  s<sup>2</sup>/m<sup>2</sup>

**Solver name** `sonicLiquidFoam`: a compressible sonic laminar liquid flow code.

**Case name** `decompressionTank` case located in the `$FOAM_TUTORIALS/sonicLiquidFoam` directory.

### 3.4.2 Mesh Generation

The full geometry is modelled in this case; the set of vertices and blocks are given in the mesh description file below:

```

1  /*-----*-- C++ -*-----*\
2  |=====|
3  | \\\ / F ield      | OpenFOAM: The Open Source CFD Toolbox
4  |  \\  O peration   | Version: 1.5
5  |   \\  A nd        | Web:      http://www.OpenFOAM.org
6  |  \\ / M anipulation|
7  /*-----*--\
8  FoamFile
9  {
10     version      2.0;
11     format        ascii;
12     class         dictionary;
13     object        blockMeshDict;
14 }
15 // * * * * *
16
17 convertToMeters 0.1;
18
19 vertices
20 (
21     (0 0 -0.1)
22     (1 0 -0.1)
23     (0 0.5 -0.1)
24     (1 0.5 -0.1)
25     (1.5 0.5 -0.1)
26     (0 0.6 -0.1)
27     (1 0.6 -0.1)
28     (1.5 0.6 -0.1)
29     (0 3 -0.1)
30     (1 3 -0.1)
31     (0 0 0.1)
32     (1 0 0.1)
33     (0 0.5 0.1)
34     (1 0.5 0.1)
35     (1.5 0.5 0.1)
36     (0 0.6 0.1)
37     (1 0.6 0.1)
38     (1.5 0.6 0.1)
39     (0 3 0.1)
40     (1 3 0.1)
41 );
42
43 blocks
44 (
45     hex (0 1 3 2 10 11 13 12) (30 20 1) simpleGrading (1 1 1)
46     hex (2 3 6 5 12 13 16 15) (30 5 1) simpleGrading (1 1 1)
47     hex (3 4 7 6 13 14 17 16) (25 5 1) simpleGrading (1 1 1)
48     hex (5 6 9 8 15 16 19 18) (30 95 1) simpleGrading (1 1 1)
49 );
50
51 edges
52 (
53 );
54
55 patches
56 (
57     wall outerWall
58     (
59         (0 1 11 10)
60         (1 3 13 11)
61         (3 4 14 13)
62         (7 6 16 17)
63         (6 9 19 16)
64         (9 8 18 19)
65     )
66     symmetryPlane axis
67     (
68         (0 10 12 2)
69         (2 12 15 5)
70         (5 15 18 8)
71     )
72     patch nozzle
73     (
74         (4 7 17 14)
75     )
76     empty back
77     (

```



```

78         (0 2 3 1)
79         (2 5 6 3)
80         (3 6 7 4)
81         (5 8 9 6)
82     )
83     empty front
84     (
85         (10 11 13 12)
86         (12 13 16 15)
87         (13 14 17 16)
88         (15 16 19 18)
89     )
90 );
91
92 mergePatchPairs
93 (
94 );
95
96 // *****

```

In order to improve the numerical accuracy, we shall use the reference level of 1 bar for the pressure field. Note that both the internal field level and the boundary conditions are offset by the reference level.

### 3.4.3 Preparing the Run

Before we commence the setup of the calculation, we need to consider the characteristic velocity of the phenomenon we are trying to capture. In the case under consideration, the fluid velocity will be very small, but the pressure wave will propagate with the speed of sound in water. The speed of sound is calculated as:

$$c = \sqrt{\frac{1}{\psi}} = \sqrt{\frac{1}{4.54 \times 10^{-7}}} = 1483.2 \text{ m/s}. \quad (3.18)$$

For the mesh described above, the characteristic mesh size is approximately 2 mm (note the scaling factor of 0.1 in the *blockMeshDict* file). Using

$$Co = \frac{U \Delta t}{\Delta x} \quad (3.19)$$

a reasonable time step is around  $\Delta t = 5 \times 10^{-7}$  s, giving the *Co* number of 0.35, based on the speed of sound. Also, note that the reported *Co* number by the code (associated with the convective velocity) will be two orders of magnitude smaller. As we are interested in the pressure wave propagation, we shall set the simulation time to 0.25 ms. For reference, the *controlDict* file is quoted below.

```

1  /*-----* C++ -*-----*\
2  |=====|
3  | \\\ /  F ield      | OpenFOAM: The Open Source CFD Toolbox
4  | \\\ /  O peration  | Version: 1.5
5  | \\\ /  A nd        | Web: http://www.OpenFOAM.org
6  | \\\ /  M anipulation |
7  /*-----*\
8  FoamFile
9  {
10     version      2.0;
11     format        ascii;
12     class         dictionary;
13     object        controlDict;
14 }
15 // *****
16
17 application sonicLiquidFoam;
18
19 startFrom      startTime;
20
21 startTime      0;
22
23 stopAt         endTime;

```

```

24
25 endTime      0.0001;
26
27 deltaT        5e-07;
28
29 writeControl   timeStep;
30
31 writeInterval  20;
32
33 purgeWrite     0;
34
35 writeFormat    ascii;
36
37 writePrecision 6;
38
39 writeCompression compressed;
40
41 timeFormat     general;
42
43 timePrecision  6;
44
45 runTimeModifiable yes;
46
47 // ***** //

```

### 3.4.4 Running the case

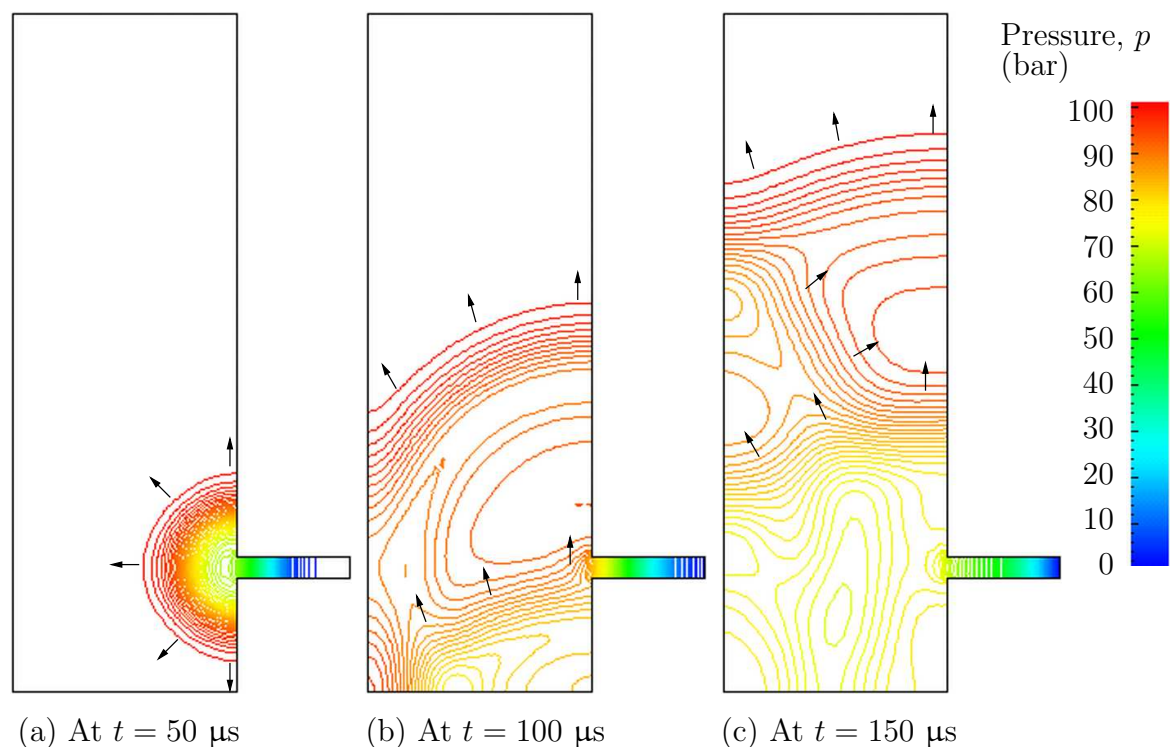


Figure 3.10: Propagation of pressure waves

The user can run the case and view results in `dxFoam`. The liquid flows out through the nozzle causing a wave to move along the nozzle. As it reaches the inlet to the tank, some of the wave is transmitted into the tank and some of it is reflected. While a wave is reflected up and down the inlet pipe, the waves transmitted into the tank expand and propagate through the tank. In [Figure 3.10](#), the pressures are shown as contours so that the wave fronts are more clearly defined than if plotted as a normal isoline plot.

If the simulation is run for a long enough time for the reflected wave to return to the pipe, we can see that negative absolute pressure is detected. The modelling permits this and has some physical basis since liquids can support tension, *i.e.* negative pressures. In reality, however, impurities or dissolved gases in liquids act as sites for cavitation,

or vapourisation/boiling, of the liquid due to the low pressure. Therefore in practical situations, we generally do not observe pressures falling below the vapourisation pressure of the liquid; not at least for longer than it takes for the cavitation process to occur.

### 3.4.5 Improving the solution by refining the mesh

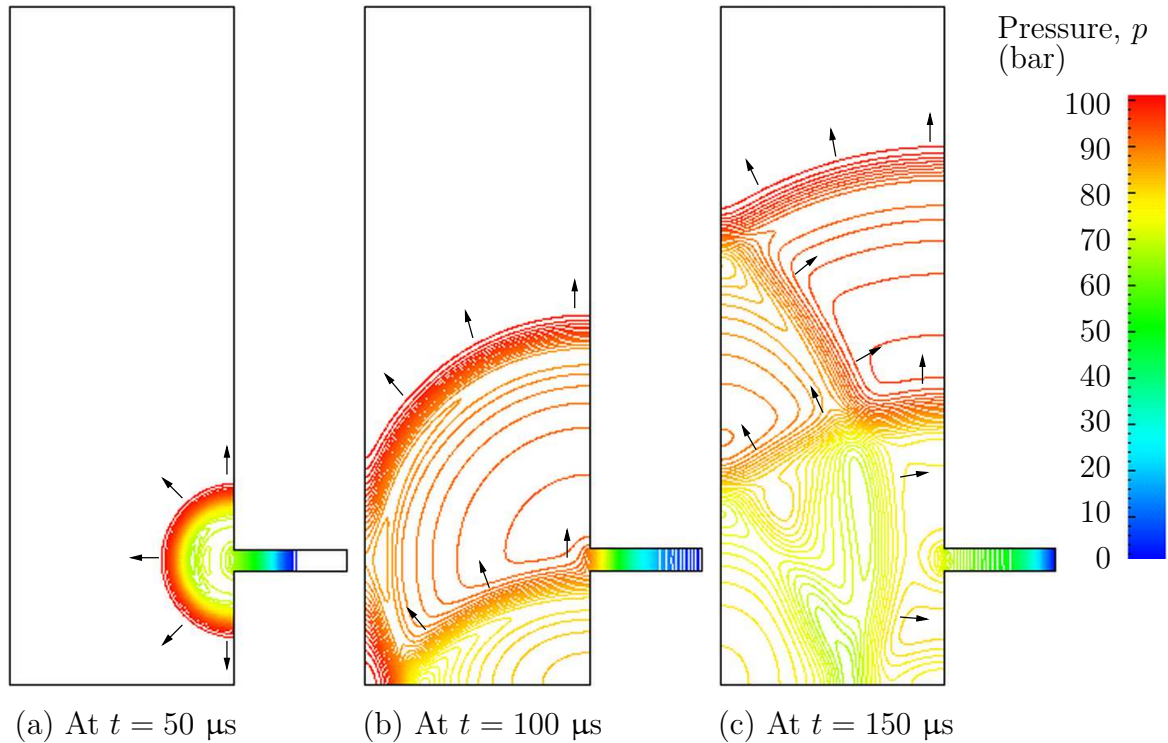


Figure 3.11: Propagation of pressure waves with refined mesh

Looking at the evolution of the resulting pressure field in time, we can clearly see the propagation of the pressure wave into the tank and numerous reflections from the inside walls. It is also obvious that the pressure wave is smeared over a number of cells. We shall now refine the mesh and reduce the time step to obtain a sharper front resolution. Simply edit the `blockMeshDict` and increase the number of cells by a factor of 4 in the  $x$  and  $y$  directions, *i.e.* block 0 becomes (120 80 1) from (30 20 1) and so on. Run `blockMesh` on this file. In addition, in order to maintain a Courant number below 1, the time step must be reduced accordingly to  $\Delta t = 10^{-7}$  s. The second simulation gives considerably better resolution of the pressure waves as shown in [Figure 3.11](#).

## 3.5 Magnetohydrodynamic flow of a liquid

In this example we shall investigate an flow of an electrically-conducting liquid through a magnetic field. The problem is one belonging to the branch of fluid dynamics known as magnetohydrodynamics (MHD) that uses `mhdFoam`.

### 3.5.1 Problem specification

The problem is known as the Hartmann problem, chosen as it contains an analytical solution with which `mhdFoam` can be validated. It is defined as follows:

**Solution domain** The domain is 2 dimensional and consists of flow along two parallel plates as shown in Fig. 3.12.

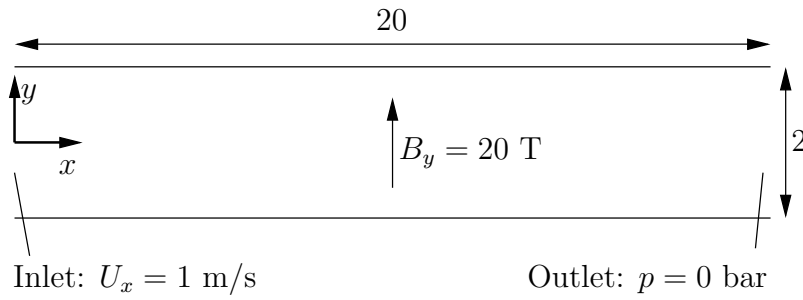


Figure 3.12: Geometry of the Hartmann problem

### Governing equations

- Mass continuity for incompressible fluid

$$\nabla \cdot \mathbf{U} = 0 \quad (3.20)$$

- Momentum equation for incompressible fluid

$$\frac{\partial \mathbf{U}}{\partial t} + \nabla \cdot (\mathbf{U}\mathbf{U}) + \nabla \cdot (2\mathbf{B}\Gamma_{\mathbf{B}\mathbf{U}}\mathbf{B}) + \nabla \cdot (\nu\mathbf{U}) + \nabla (\Gamma_{\mathbf{B}\mathbf{U}}\mathbf{B}:\mathbf{B}) = -\nabla p \quad (3.21)$$

where  $\mathbf{B}$  is the magnetic flux density,  $\Gamma_{\mathbf{B}\mathbf{U}} = (2\mu\rho)^{-1}$ .

- Maxwell's equations

$$\nabla \times \mathbf{E} = -\frac{\partial \mathbf{B}}{\partial t} \quad (3.22)$$

where  $\mathbf{E}$  is the electric field strength.

$$\nabla \cdot \mathbf{B} = 0 \quad (3.23)$$

$$\nabla \times \mathbf{H} = \mathbf{J} + \frac{\partial \mathbf{D}}{\partial t} = \mathbf{J} \quad (3.24)$$

assuming  $\partial \mathbf{D} / \partial t \ll \mathbf{J}$ . Here,  $\mathbf{H}$  is the magnetic field strength,  $\mathbf{J}$  is the current density and  $\mathbf{D}$  is the electric flux density.

- Charge continuity

$$\nabla \cdot \mathbf{J} = 0 \quad (3.25)$$

- Constitutive law

$$\mathbf{B} = \mu \mathbf{H} \quad (3.26)$$

- Ohm's law

$$\mathbf{J} = \sigma (\mathbf{E} + \mathbf{U} \times \mathbf{B}) \quad (3.27)$$

- Combining Equation 3.22, Equation 3.24, Equation 3.27, and taking the curl

$$\frac{\partial \mathbf{B}}{\partial t} + \nabla \cdot (\mathbf{U}\mathbf{B}) - \nabla \cdot (\phi_{\mathbf{B}}\mathbf{U}) - \nabla \cdot (\Gamma_{\mathbf{B}}\mathbf{B}) = 0 \quad (3.28)$$

**Boundary conditions**

- inlet is specified the inlet condition with fixed velocity  $\mathbf{U} = (1, 0, 0)$  m/s;
- outlet is specified as the outlet with fixed pressure  $p = 0$  Pa;
- upperWall is specified as a wall where  $\mathbf{B} = (0, 20, 0)$  T.
- lowerWall is specified as a wall where  $\mathbf{B} = (0, 20, 0)$  T.
- front and back boundaries are specified as empty.

**Initial conditions**  $\mathbf{U} = 0$  m/s,  $p = 100$  Pa,  $\mathbf{B} = (0, 20, 0)$  T.

**Transport properties**

- Kinematic viscosity  $\nu = 1$  Pa s
- Density  $\rho = 1$  kg m/s
- Electrical conductivity  $\sigma = 1$  ( $\Omega$  m) $^{-1}$
- Permeability  $\mu = 1$  H/m

**Solver name** mhdFoam: an incompressible laminar magneto-hydrodynamics code.

**Case name** hartmann case located in the `$FOAM_TUTORIALS/mhdFoam` directory.

**3.5.2 Mesh generation**

The geometry is simply modelled with 100 cells in the  $x$ -direction and 40 cells in the  $y$ -direction; the set of vertices and blocks are given in the mesh description file below:

```

1  /*----- C++ -----*/
2  |=====|
3  | \\\ /  F ield      | OpenFOAM: The Open Source CFD Toolbox
4  | \\\ /  O peration   | Version: 1.5
5  | \\\ /  A nd         | Web: http://www.OpenFOAM.org
6  | \\\ /  M anipulation |
7  /*-----*/
8  FoamFile
9  {
10     version      2.0;
11     format        ascii;
12     class         dictionary;
13     object        blockMeshDict;
14 }
15 // *****
16
17 convertToMeters 1;
18
19 vertices
20 (
21     (0 -1 0)
22     (20 -1 0)
23     (20 1 0)
24     (0 1 0)
25     (0 -1 0.1)
26     (20 -1 0.1)
27     (20 1 0.1)
28     (0 1 0.1)
29 );
30
31 blocks
32 (
33     hex (0 1 2 3 4 5 6 7) (100 40 1) simpleGrading (1 1 1)
34 );
35
36 edges
37 (
38 );
39
40 patches
41 (

```

```

42     patch inlet
43     (
44         (0 4 7 3)
45     )
46     patch outlet
47     (
48         (2 6 5 1)
49     )
50     patch lowerWall
51     (
52         (1 5 4 0)
53     )
54     patch upperWall
55     (
56         (3 7 6 2)
57     )
58     empty frontAndBack
59     (
60         (0 3 2 1)
61         (4 5 6 7)
62     )
63 );
64
65     mergePatchPairs
66     (
67     );
68
69 // *****

```

### 3.5.3 Running the case

The user can run the case and view results in **dxFoam**. It is also useful at this stage to run the **Ucomponents** utility to convert the **U** vector field into individual scalar components. MHD flow is governed by, amongst other things, the Hartmann number which is a measure of the ratio of electromagnetic body force to viscous force

$$M = BL\sqrt{\frac{\sigma}{\rho\nu}} \quad (3.29)$$

where  $L$  is the characteristic length scale. In this case with  $B_y = 20$  T,  $M = 20$  and the electromagnetic body forces dominate the viscous forces. Consequently with the flow fairly steady at  $t = 2$  s the velocity profile is almost planar, viewed at a cross section midway along the domain  $x = 10$  m. The user can plot a graph of the profile of  $U_x$  in **dxFoam**. Now the user should reduce the magnetic flux density **B** to 1 T and re-run the code and **Ucomponents**. In this case,  $M = 1$  and the electromagnetic body forces no longer dominate. The velocity profile consequently takes on the parabolic form, characteristic of Poiseuille flow as shown in [Figure 3.13](#). To validate the code the analytical solution for the velocity profile  $U_x$  is superimposed in [Figure 3.13](#), given by:

$$\frac{U_x(y)}{U_x(0)} = \frac{\cosh M - \cosh M(y/L)}{\cosh M - 1} \quad (3.30)$$

where the characteristic length  $L$  is half the width of the domain, *i.e.* 1 m.

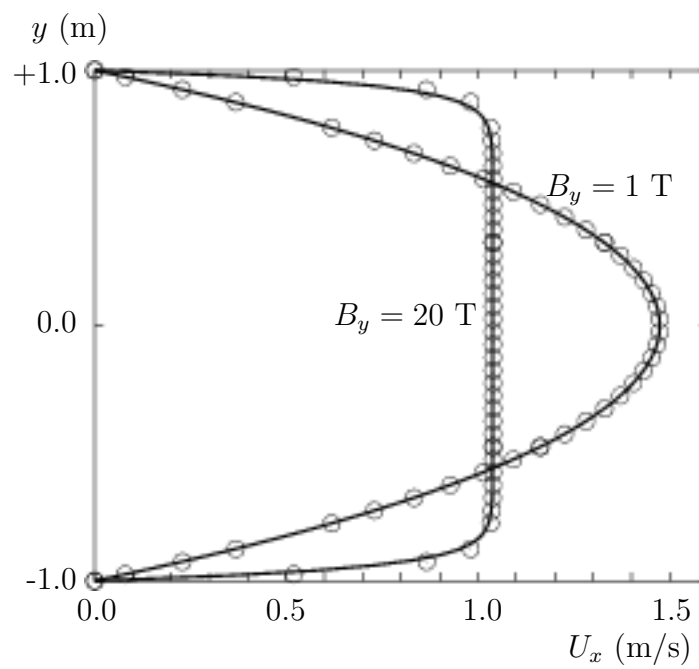


Figure 3.13: Velocity profile in the Hartmann problem for  $B_y = 1$  T and  $B_y = 20$  T.





# Index

**Symbols Numbers A B C D E F G H I J K L M N O P Q R S T U V W X Z**

## Symbols

**\***  
 tensor member function, [P-25](#)

**+**  
 tensor member function, [P-25](#)

**-**  
 tensor member function, [P-25](#)

**/**  
 tensor member function, [P-25](#)

**/\*...\*/**  
 C++ syntax, [U-76](#)

**//**  
 C++ syntax, [U-76](#)  
 OpenFOAM file syntax, [U-98](#)

**# include**  
 C++ syntax, [U-70](#), [U-76](#)

**&**  
 tensor member function, [P-25](#)

**&&**  
 tensor member function, [P-25](#)

**~**  
 tensor member function, [P-25](#)

**<LESmodel>Coeffs** keyword, [U-174](#)

**<RASModel>Coeffs** keyword, [U-174](#)

**<delta>Coeffs** keyword, [U-174](#)

**0.000000e+00** directory, [U-98](#)

**1-dimensional mesh**, [U-122](#)

**1D mesh**, [U-122](#)

**2-dimensional mesh**, [U-122](#)

**2D mesh**, [U-122](#)

## Numbers

**0** directory, [U-98](#)

## A

**access** functions, [P-23](#)

**addLayersControls** keyword, [U-138](#)

**adiabaticFlameT** utility, [U-90](#)

**adjustableRunTime**  
 keyword entry, [U-59](#), [U-104](#)

**adjustPhi** tools, [U-91](#)

**adjustTimeStep** keyword, [U-59](#)

**agglomerator** keyword, [U-115](#)

**algorithms** tools, [U-91](#)

**allTime**  
 menu entry, [U-184](#)

**analytical** solution, [P-45](#)

**anisotropicFilter** model, [U-94](#)

**Annotation** window panel, [U-25](#), [U-159](#)

**ansysToFoam** utility, [U-86](#)

**APIfunctions** model, [U-93](#)

**applications**, [U-67](#)

**Apply** button, [U-156](#), [U-160](#)

**arbitrarily unstructured**, [P-31](#)

**arc**  
 keyword entry, [U-132](#)

**arc** keyword, [U-131](#)

**ascii**  
 keyword entry, [U-105](#)

**attachMesh** utility, [U-87](#)

**Auto Accept** button, [U-159](#)

**autoPatch** utility, [U-87](#)

**axes**  
 right-handed, [U-130](#)  
 right-handed rectangular Cartesian, [P-15](#), [U-20](#)

**axi-symmetric** cases, [U-127](#), [U-135](#)

**axi-symmetric** mesh, [U-122](#)

## B

**background**  
 process, [U-26](#), [U-79](#)

**backward**  
 keyword entry, [U-112](#)

**Backward** differencing, [P-39](#)

**basicThermophysicalModels**  
 library, [U-92](#)

**binary**  
 keyword entry, [U-105](#)

**BirdCarreau** model, [U-95](#)

**blended** differencing, [P-38](#)

**block**  
 expansion ratio, [U-132](#)

**block** keyword, [U-131](#)

**blockMesh** solver, [P-47](#)

- blockMesh utility, [U-38](#), [U-86](#), [U-127](#)
  - blockMesh executable
    - vertex numbering, [U-132](#)
  - blockMeshDict*
    - dictionary, [U-20](#), [U-22](#), [U-36](#), [U-48](#), [U-127](#), [U-136](#)
  - blocks keyword, [U-22](#), [U-32](#), [U-132](#)
  - bound tools, [U-91](#)
  - boundaries, [U-124](#)
  - boundary, [U-124](#)
  - boundary*
    - dictionary, [U-121](#), [U-127](#)
  - boundary condition
    - calculated, [U-128](#)
    - cyclic, [U-127](#)
    - directionMixed, [U-128](#)
    - empty, [P-63](#), [P-69](#), [U-20](#), [U-122](#), [U-127](#)
    - fixedGradient, [U-128](#)
    - fixedValue, [U-128](#)
    - fluxCorrectedVelocity, [U-129](#)
    - gammaContactAngle, [U-57](#)
    - inlet, [P-69](#)
    - inletOutlet, [U-129](#)
    - mixed, [U-128](#)
    - movingWallVelocity, [U-129](#)
    - outlet, [P-69](#)
    - outletInlet, [U-129](#)
    - partialSlip, [U-129](#)
    - patch, [U-126](#)
    - pressureDirectedInletVelocity, [U-129](#)
    - pressureInletVelocity, [U-129](#)
    - pressureOutlet, [P-63](#)
    - pressureTransmissive, [U-129](#)
    - processor, [U-127](#)
    - setup, [U-22](#)
    - slip, [U-129](#)
    - supersonicFreeStream, [U-129](#)
    - surfaceNormalFixedValue, [U-129](#)
    - symmetryPlane, [P-63](#), [U-126](#)
    - totalPressure, [U-129](#)
    - turbulentInlet, [U-129](#)
    - wall, [U-40](#)
    - wall, [P-63](#), [P-69](#), [U-57](#), [U-126](#)
    - wallBuoyantPressure, [U-129](#)
    - wedge, [U-122](#), [U-127](#), [U-135](#)
    - zeroGradient, [U-128](#)
  - boundary conditions, [P-43](#)
    - Dirichlet, [P-43](#)
    - inlet, [P-44](#)
    - Neumann, [P-43](#)
    - no-slip impermeable wall, [P-44](#)
    - outlet, [P-44](#)
    - physical, [P-44](#)
    - symmetry plane, [P-44](#)
  - boundary type
    - empty, [U-187](#)
  - boundaryField keyword, [U-22](#), [U-102](#)
  - boundaryFoam solver, [U-83](#)
  - bounded
    - keyword entry, [U-110](#), [U-111](#)
  - boxToCell keyword, [U-58](#)
  - boxTurb utility, [U-86](#)
  - breaking of a dam, [U-55](#)
  - bubbleFoam solver, [U-84](#)
  - buoyantFoam solver, [U-85](#)
  - buoyantSimpleRadiationFoam solver, [U-85](#)
  - buoyantSimpleFoam solver, [U-85](#)
  - button
    - Apply, [U-156](#), [U-160](#)
    - Auto Accept, [U-159](#)
    - Choose Preset, [U-158](#)
    - Compact, [U-187](#)
    - Delete, [U-156](#)
    - Edit Color Map, [U-157](#)
    - Info, [U-187](#)
    - My Jobs, [U-187](#)
    - Orientation Axes, [U-25](#), [U-159](#)
    - Rescale to Data Range, [U-28](#)
    - Reset, [U-156](#)
    - Set Solid Color, [U-158](#)
    - Update GUI, [U-28](#), [U-157](#)
    - Use Parallel Projection, [U-25](#)
    - Use parallel projection, [U-159](#)
    - cont, [U-187](#)
    - endNow, [U-187](#)
    - end, [U-187](#)
    - kill, [U-187](#)
    - purge, [U-187](#)
    - read, [U-187](#)
    - status, [U-187](#)
    - suspend, [U-187](#)
- ## C
- C++ syntax
    - `/*...*/`, [U-76](#)
    - `//`, [U-76](#)
    - `# include`, [U-70](#), [U-76](#)
  - cacheAgglomeration keyword, [U-115](#)
  - calculated
    - boundary condition, [U-128](#)
  - case
    - browser, [U-180](#)
    - server, [U-186](#)
  - case manager
    - FoamX (obsolete), [U-177](#)
  - Case Name text box, [U-182](#)
  - Case Root text box, [U-182](#)
  - cases, [U-97](#)

- castellatedMesh keyword, [U-138](#)
- castellatedMeshControls*
  - dictionary, [U-139](#), [U-141](#)
- castellatedMeshControls keyword, [U-138](#)
- cavity flow, [U-19](#)
- ccm26ToFoam utility, [U-86](#)
- CEI\_ARCH
  - environment variable, [U-164](#)
- CEI\_HOME
  - environment variable, [U-164](#)
- cell
  - expansion ratio, [U-132](#)
- cell class, [P-31](#)
- cell
  - keyword entry, [U-166](#)
- cellDecompFiniteElement
  - library, [U-91](#)
- cellPoint
  - keyword entry, [U-166](#)
- cellPointFace
  - keyword entry, [U-166](#)
- cells
  - dictionary, [U-127](#)
- cellSet utility, [U-87](#)
- central differencing, [P-38](#)
- cfTools
  - library, [U-91](#)
- cfxToFoam utility, [U-86](#), [U-145](#)
- cGamma keyword, [U-61](#)
- channelOodles solver, [U-83](#)
- Chart Options window, [U-35](#)
- checkMesh utility, [U-87](#), [U-146](#)
- checkYPlus utility, [U-89](#)
- chemistryModel
  - library, [U-93](#)
- chemistryModel model, [U-93](#)
- chemistrySolver model, [U-93](#)
- chemkinMixture model, [U-93](#), [U-172](#)
- chemkinToFoam utility, [U-90](#)
- Choose Preset button, [U-158](#)
- chtMultiRegionFoam solver, [U-85](#)
- Class menu, [U-182](#)
- class
  - cell, [P-31](#)
  - dimensionSet, [P-25](#), [P-32](#), [P-33](#)
  - face, [P-31](#)
  - finiteVolumeCalculus, [P-33](#)
  - finiteVolumeMethod, [P-33](#)
  - fvMesh, [P-31](#)
  - fvSchemes, [P-36](#)
  - fvc, [P-36](#)
  - fvm, [P-36](#)
  - pointField, [P-31](#)
  - polyBoundaryMesh, [P-31](#)
  - polyMesh, [P-31](#), [U-119](#), [U-121](#)
  - polyPatchList, [P-31](#)
  - polyPatch, [P-31](#)
  - scalarField, [P-29](#)
  - scalar, [P-23](#)
  - slice, [P-31](#)
  - symmTensorField, [P-29](#)
  - symmTensorThirdField, [P-29](#)
  - tensorField, [P-29](#)
  - tensorThirdField, [P-29](#)
  - tensor, [P-23](#)
  - vectorField, [P-29](#)
  - vector, [P-23](#), [U-101](#)
  - word, [P-25](#), [P-31](#)
- class keyword, [U-99](#)
- clockTime
  - keyword entry, [U-105](#)
- cloud keyword, [U-167](#)
- cmptAv
  - tensor member function, [P-25](#)
- Co utility, [U-88](#)
- cofactors
  - tensor member function, [P-25](#)
- coldEngineFoam solver, [U-85](#)
- Color By menu, [U-158](#)
- Color Legend window, [U-30](#)
- Color Legend window panel, [U-158](#)
- Color Scale window panel, [U-158](#)
- combustionThermophysicalModels
  - library, [U-92](#)
- comments, [U-76](#)
- Compact button, [U-187](#)
- compressed
  - keyword entry, [U-105](#)
- compressible tools, [U-91](#)
- compressibleLesInterFoam solver, [U-84](#)
- compressibleLESModels
  - library, [U-95](#)
- compressibleRASModels
  - library, [U-94](#)
- constant* directory, [U-98](#), [U-171](#)
- constLaminarFlameSpeed model, [U-93](#)
- constTransport model, [U-93](#), [U-172](#)
- cont button, [U-187](#)
- containers tools, [U-91](#)
- continuum
  - mechanics, [P-15](#)
- control
  - of time, [U-104](#)
- controlDict*
  - dictionary, [P-65](#), [U-23](#), [U-32](#), [U-41](#), [U-50](#), [U-59](#), [U-98](#), [U-151](#)
- controlDict* file, [P-49](#)
- convection, *see* divergence, [P-38](#)

convergence, [U-39](#)  
 convertToMeters keyword, [U-131](#)  
 coodles solver, [U-84](#)  
 coordinate  
     system, [P-15](#)  
 coordinate system, [U-20](#)  
 CORBA, [U-92](#), [U-177](#)  
 corrected  
     keyword entry, [U-110](#), [U-111](#)  
 couplePatches utility, [U-87](#)  
 Courant number, [P-42](#), [U-24](#)  
 cpuTime  
     keyword entry, [U-105](#)  
 Crank Nicholson  
     temporal discretisation, [P-42](#)  
 CrankNicholson  
     keyword entry, [U-112](#)  
 createPatch utility, [U-87](#)  
 cross product, *see* tensor, vector cross product  
 CrossPowerLaw  
     keyword entry, [U-58](#)  
 CrossPowerLaw model, [U-95](#)  
 cubeRootVolDelta model, [U-94](#)  
 cubicCorrected  
     keyword entry, [U-112](#)  
 cubicCorrection  
     keyword entry, [U-109](#)  
 curl, [P-37](#)  
 curl  
     fvc member function, [P-37](#)  
 Current Time Controls menu, [U-28](#), [U-157](#)  
 curve keyword, [U-167](#)  
 cyclic  
     boundary condition, [U-127](#)  
 cyclic  
     keyword entry, [U-127](#)  
 cylinder  
     flow around a, [P-45](#)

## D

d2dt2  
     fvc member function, [P-37](#)  
     fvm member function, [P-37](#)  
 dam  
     breaking of a, [U-55](#)  
 db tools, [U-91](#)  
 ddt  
     fvc member function, [P-37](#)  
     fvm member function, [P-37](#)  
 DeardorffDiffStress model, [U-95](#)  
 debug keyword, [U-138](#)  
 decomposePar utility, [U-79](#), [U-80](#), [U-90](#)  
 decomposeParDict  
     dictionary, [U-79](#)

decomposition  
     of field, [U-79](#)  
     of mesh, [U-79](#)  
 decompression of a tank, [P-62](#)  
 defaultFieldValues keyword, [U-58](#)  
 deformedGeom utility, [U-87](#)  
 Delete button, [U-156](#)  
 delta keyword, [U-81](#), [U-174](#)  
 deltaT keyword, [U-104](#)  
 dependencies, [U-70](#)  
 dependency lists, [U-70](#)  
 det  
     tensor member function, [P-25](#)  
 determinant, *see* tensor, determinant  
 dev  
     tensor member function, [P-25](#)  
 diag  
     tensor member function, [P-25](#)  
 diagonal  
     keyword entry, [U-115](#)  
 DIC  
     keyword entry, [U-115](#)  
 DICGaussSeidel  
     keyword entry, [U-115](#)  
 Dictionaries dictionary tree, [U-188](#)  
 dictionary  
     *LESProperties*, [U-174](#)  
     *PISO*, [U-25](#)  
     *RASProperties*, [U-41](#), [U-174](#)  
     *blockMeshDict*, [U-20](#), [U-22](#), [U-36](#), [U-48](#),  
         [U-127](#), [U-136](#)  
     *boundary*, [U-121](#), [U-127](#)  
     *castellatedMeshControls*, [U-139](#), [U-141](#)  
     *cells*, [U-127](#)  
     *controlDict*, [P-65](#), [U-23](#), [U-32](#), [U-41](#), [U-50](#),  
         [U-59](#), [U-98](#), [U-151](#)  
     *decomposeParDict*, [U-79](#)  
     *faces*, [U-121](#), [U-127](#)  
     *fvSchemes*, [U-60](#), [U-98](#), [U-106](#)  
     *fvSolution*, [U-98](#), [U-113](#)  
     *mechanicalProperties*, [U-49](#)  
     *neighbour*, [U-121](#)  
     *owner*, [U-121](#)  
     *points*, [U-121](#), [U-127](#)  
     *thermalProperties*, [U-50](#)  
     *thermophysicalProperties*, [U-171](#)  
     *transportProperties*, [U-23](#), [U-39](#), [U-41](#)  
 dictionary tree  
     Dictionaries, [U-188](#)  
     Fields, [U-187](#)  
 dieselEngineFoam solver, [U-85](#)  
 dieselFoam solver, [U-85](#)  
 dieselMixture model, [U-92](#), [U-172](#)  
 dieselSpray

- library, [U-92](#)
  - diEthylEther model, [U-93](#)
  - differencing
    - Backward, [P-39](#)
    - blended, [P-38](#)
    - central, [P-38](#)
    - Euler implicit, [P-39](#)
    - Gamma, [P-38](#)
    - MINMOD, [P-38](#)
    - SUPERBEE, [P-38](#)
    - upwind, [P-38](#)
    - van Leer, [P-38](#)
  - DILU
    - keyword entry, [U-115](#)
  - dimension
    - checking in OpenFOAM, [P-25](#), [U-101](#)
  - dimensional units, [U-101](#)
  - dimensioned<Type> template class, [P-25](#)
  - dimensionedTypes tools, [U-91](#)
  - dimensions keyword, [U-22](#), [U-102](#)
  - dimensionSet class, [P-25](#), [P-32](#), [P-33](#)
  - dimensionSet tools, [U-91](#)
  - diMethylEther model, [U-93](#)
  - direct numerical simulation, [U-60](#)
  - directionMixed
    - boundary condition, [U-128](#)
  - directory
    - 0.000000e+00*, [U-98](#)
    - 0*, [U-98](#)
    - Make*, [U-71](#)
    - constant*, [U-98](#), [U-171](#)
    - fluentInterface*, [U-162](#)
    - polyMesh*, [U-98](#), [U-121](#)
    - processorN*, [U-80](#)
    - run*, [U-97](#)
    - system*, [P-49](#), [U-98](#)
    - tutorials*, [P-45](#), [U-19](#)
  - discretisation
    - equation, [P-33](#)
  - Display window panel, [U-25](#), [U-28](#), [U-156](#), [U-157](#)
  - distance
    - keyword entry, [U-141](#), [U-167](#)
  - distributed keyword, [U-81](#), [U-82](#)
  - div
    - fvc member function, [P-37](#)
    - fvm member function, [P-37](#)
  - divergence, [P-37](#), [P-39](#)
  - divSchemes keyword, [U-107](#)
  - divU utility, [U-88](#)
  - dnsFoam solver, [U-85](#)
  - doLayers keyword, [U-138](#)
  - double inner product, *see* tensor, double inner product
  - dx
    - keyword entry, [U-166](#)
  - dynamicMesh
    - library, [U-91](#)
  - dynMixedSmagorinsky model, [U-94](#)
  - dynOneEqEddy model, [U-94](#), [U-95](#)
  - dynSmagorinsky model, [U-94](#)
- ## E
- edgeGrading keyword, [U-133](#)
  - edgeMesh
    - library, [U-92](#)
  - edges keyword, [U-131](#)
  - Edit menu, [U-159](#)
  - Edit Color Map button, [U-157](#)
  - electrostaticFoam solver, [U-85](#)
  - empty
    - boundary condition, [P-63](#), [P-69](#), [U-20](#), [U-122](#), [U-127](#)
  - empty boundary type, [U-187](#)
  - empty
    - keyword entry, [U-127](#)
  - end button, [U-187](#)
  - endNow button, [U-187](#)
  - endTime keyword, [U-24](#), [U-104](#)
  - engine
    - library, [U-92](#)
  - engineCompRatio utility, [U-90](#)
  - engineFoam solver, [U-85](#)
  - engineSwirl utility, [U-86](#)
  - ensight74FoamExec utility, [U-164](#)
  - ensight76FoamExec utility, [U-88](#)
  - ENSIGHT7\_INPUT
    - environment variable, [U-164](#)
  - ENSIGHT7\_READER
    - environment variable, [U-164](#)
  - entrophy utility, [U-88](#)
  - environment variable
    - CEI\_ARCH, [U-164](#)
    - CEI\_HOME, [U-164](#)
    - ENSIGHT7\_INPUT, [U-164](#)
    - ENSIGHT7\_READER, [U-164](#)
    - FOAMX\_PATH, [U-192](#)
    - FOAMX\_SYSTEM\_CONFIG, [U-192](#)
    - FOAMX\_USER\_CONFIG, [U-192](#)
    - FOAM\_RUN, [U-97](#), [U-192](#)
    - JAVA\_HOME, [U-192](#)
    - WM\_ARCH, [U-74](#)
    - WM\_COMPILER\_BIN, [U-74](#)
    - WM\_COMPILER\_DIR, [U-74](#)
    - WM\_COMPILER\_LIB, [U-74](#)
    - WM\_COMPILER, [U-74](#)
    - WM\_COMPILE\_OPTION, [U-74](#)
    - WM\_DIR, [U-74](#)

- WM\_JAVAC\_OPTION, [U-74](#)
  - WM\_LINK\_LANGUAGE, [U-74](#)
  - WM\_MPLIB, [U-74](#)
  - WM\_OPTIONS, [U-74](#)
  - WM\_PROJECT\_DIR, [U-74](#)
  - WM\_PROJECT\_INST\_DIR, [U-74](#)
  - WM\_PROJECT\_LANGUAGE, [U-74](#)
  - WM\_PROJECT\_USER\_DIR, [U-74](#)
  - WM\_PROJECT\_VERSION, [U-74](#)
  - WM\_PROJECT, [U-74](#)
  - WM\_SHELL, [U-74](#)
  - wmake, [U-73](#)
  - environmentalProperties* file, [U-58](#)
  - equilibriumCO utility, [U-90](#)
  - equilibriumFlameT utility, [U-90](#)
  - errorEstimation
    - library, [U-92](#)
  - errorReduction keyword, [U-145](#)
  - estimateScalarError utility, [U-90](#)
  - Euler
    - keyword entry, [U-112](#)
  - Euler implicit
    - differencing, [P-39](#)
    - temporal discretisation, [P-42](#)
  - examples
    - decompression of a tank, [P-62](#)
    - flow around a cylinder, [P-45](#)
    - flow over backward step, [P-53](#)
    - Hartmann problem, [P-67](#)
    - supersonic flow over forward step, [P-58](#)
  - expansionRatio keyword, [U-144](#)
  - explicit
    - temporal discretisation, [P-42](#)
  - exponential model, [U-93](#)
  - extrudeMesh utility, [U-86](#)
- ## F
- face class, [P-31](#)
  - face keyword, [U-167](#)
  - faceAreaPair
    - keyword entry, [U-115](#)
  - faceDecompFiniteElement
    - library, [U-92](#)
  - faces
    - dictionary, [U-121](#), [U-127](#)
  - faceSet utility, [U-87](#)
  - FDIC
    - keyword entry, [U-115](#)
  - featureAngle keyword, [U-144](#)
  - features keyword, [U-139](#)
  - field
    - U, [U-24](#)
    - p, [U-24](#)
    - decomposition, [U-79](#)
  - FieldField<Type> template class, [P-32](#)
  - Fields dictionary tree, [U-187](#)
  - fields, [P-29](#)
    - mapping, [U-151](#)
  - fields tools, [U-91](#)
  - fields keyword, [U-166](#)
  - Field<Type> template class, [P-29](#)
  - fieldValues keyword, [U-58](#)
  - file
    - FoamX.cfg*, [U-191](#)
    - FoamXClient.cfg*, [U-178](#), [U-191](#)
    - Make/files*, [U-72](#)
    - controlDict*, [P-49](#)
    - environmentalProperties*, [U-58](#)
    - files*, [U-71](#)
    - options*, [U-71](#)
    - snappyHexMeshDict*, [U-137](#)
    - transportProperties*, [U-58](#)
  - file format, [U-98](#)
  - files file, [U-71](#)
  - finalLayerRatio keyword, [U-144](#)
  - financialFoam solver, [U-86](#)
  - finite volume
    - discretisation, [P-27](#)
    - mesh, [P-31](#)
  - finiteVolume tools, [U-91](#)
  - finiteVolumeCalculus class, [P-33](#)
  - finiteVolumeMethod class, [P-33](#)
  - firstTime
    - menu entry, [U-184](#)
  - firstTime keyword, [U-104](#)
  - fixed
    - keyword entry, [U-105](#)
  - fixedGradient
    - boundary condition, [U-128](#)
  - fixedValue
    - boundary condition, [U-128](#)
  - flattenMesh utility, [U-87](#)
  - flow
    - free surface, [U-55](#)
    - laminar, [U-19](#)
    - steady, turbulent, [P-53](#)
    - supersonic, [P-58](#)
    - turbulent, [U-19](#)
  - flow around a cylinder, [P-45](#)
  - flow over backward step, [P-53](#)
  - flowType utility, [U-88](#)
  - fluentInterface* directory, [U-162](#)
  - fluentMeshToFoam utility, [U-87](#), [U-144](#)
  - fluxCorrectedVelocity
    - boundary condition, [U-129](#)
  - fluxRequired keyword, [U-107](#)
  - OpenFOAM
    - cases, [U-97](#)



FOAM\_RUN  
     environment variable, [U-97](#), [U-192](#)  
 foamCalc utility, [U-33](#)  
 foamCorrectVrt script/alias, [U-150](#)  
 foamDataToFluent utility, [U-88](#), [U-162](#)  
 foamDebugSwitches utility, [U-90](#)  
 FoamFile keyword, [U-99](#)  
 foamFile  
     keyword entry, [U-166](#)  
 foamInfoExec utility, [U-90](#)  
 foamJob script/alias, [U-169](#)  
 foamLog script/alias, [U-169](#)  
 foamMeshToFluent utility, [U-87](#), [U-162](#)  
 foamToEnight utility, [U-88](#)  
 foamToFieldview9 utility, [U-88](#)  
 foamToGMV utility, [U-88](#)  
 foamToVTK utility, [U-88](#)  
 foamUser  
     library, [U-78](#)  
 FoamX (obsolete)  
     case browser, [U-180](#)  
     case manager, [U-177](#)  
     case server, [U-186](#)  
     OpenFOAM case manager, [U-177](#)  
     host browser, [U-178](#)  
     JAVA GUI, [U-179](#)  
     name server, [U-178](#)  
 FoamX utility, [U-86](#)  
 FoamX.cfg file, [U-191](#)  
 FOAMX\_PATH  
     environment variable, [U-192](#)  
 FOAMX\_SYSTEM\_CONFIG  
     environment variable, [U-192](#)  
 FOAMX\_USER\_CONFIG  
     environment variable, [U-192](#)  
 FoamXClient.cfg file, [U-178](#), [U-191](#)  
 foreground  
     process, [U-26](#)  
 format keyword, [U-99](#)  
 fourth  
     keyword entry, [U-110](#), [U-111](#)  
 functions keyword, [U-106](#)  
 fvc class, [P-36](#)  
 fvc member function  
     curl, [P-37](#)  
     d2dt2, [P-37](#)  
     ddt, [P-37](#)  
     div, [P-37](#)  
     gGrad, [P-37](#)  
     grad, [P-37](#)  
     laplacian, [P-37](#)  
     lsGrad, [P-37](#)  
     snGrad, [P-37](#)  
     snGradCorrection, [P-37](#)

    sqrGradGrad, [P-37](#)  
 fvm class, [P-36](#)  
 fvm member function  
     d2dt2, [P-37](#)  
     ddt, [P-37](#)  
     div, [P-37](#)  
     laplacian, [P-37](#)  
     Su, [P-37](#)  
     SuSp, [P-37](#)  
 fvMatrix template class, [P-33](#)  
 fvMesh class, [P-31](#)  
 fvSchemes  
     dictionary, [U-60](#), [U-98](#), [U-106](#)  
 fvSchemes class, [P-36](#)  
 fvSchemes  
     menu entry, [U-51](#)  
 fvSolution  
     dictionary, [U-98](#), [U-113](#)

## G

gambitToFoam utility, [U-87](#), [U-144](#)  
 GAMG  
     keyword entry, [U-114](#), [U-115](#)  
 Gamma  
     keyword entry, [U-109](#)  
 Gamma differencing, [P-38](#)  
 gammaContactAngle  
     boundary condition, [U-57](#)  
 Gauss  
     keyword entry, [U-110](#)  
 Gauss's theorem, [P-36](#)  
 GaussSeidel  
     keyword entry, [U-115](#)  
 General window panel, [U-159](#)  
 general model, [U-93](#)  
 general  
     keyword entry, [U-105](#)  
 geometric-algebraic multi-grid, [U-115](#)  
 GeometricBoundaryField template class, [P-32](#)  
 geometricField<Type> template class, [P-32](#)  
 geometry keyword, [U-138](#)  
 gGrad  
     fvc member function, [P-37](#)  
 global tools, [U-91](#)  
 gmshToFoam utility, [U-87](#)  
 gnemdFoam solver, [U-86](#)  
 gnuplot  
     keyword entry, [U-105](#), [U-166](#)  
 grad  
     fvc member function, [P-37](#)  
 (Grad Grad) squared, [P-37](#)  
 gradient, [P-37](#), [P-40](#)  
     Gauss scheme, [P-40](#)  
     Gauss's theorem, [U-51](#)

- least square fit, [U-51](#)
- least squares method, [P-40](#), [U-51](#)
- surface normal, [P-40](#)
- gradSchemes keyword, [U-107](#)
- graphFormat keyword, [U-105](#)
- Gstream
  - library, [U-92](#)
- guldersLaminarFlameSpeed model, [U-93](#)

## H

- hConstThermo model, [U-93](#), [U-171](#)
- Help menu, [U-159](#)
- hhuMixtureThermo model, [U-92](#), [U-172](#)
- hierarchical
  - keyword entry, [U-80](#), [U-81](#)
- hMixtureThermo model, [U-92](#), [U-172](#)
- homogeneousMixture model, [U-92](#), [U-172](#)
- host
  - browser, [U-178](#)
- hThermo model, [U-92](#), [U-172](#)

## I

- I
  - tensor member function, [P-25](#)
- icoDyMFoam solver, [U-83](#)
- icoErrorEstimate utility, [U-90](#)
- icoFoam solver, [U-19](#), [U-23](#), [U-24](#), [U-26](#), [U-83](#)
- icoMomentError utility, [U-90](#)
- ideasToFoam utility, [U-145](#)
- ideasUnvToFoam utility, [U-87](#)
- identities, *see* tensor, identities
- identity, *see* tensor, identity
- incompressible tools, [U-91](#)
- incompressibleLESModels
  - library, [U-94](#)
- incompressiblePostProcessing
  - library, [U-91](#)
- incompressibleRASModels
  - library, [U-94](#)
- incompressibleTransportModels
  - library, [P-55](#), [U-95](#)
- incompressibleTurbulenceModels
  - library, [P-55](#)
- index
  - notation, [P-16](#), [P-17](#)
- Info button, [U-187](#)
- Information window panel, [U-156](#)
- inhomogeneousMixture model, [U-92](#), [U-172](#)
- inlet
  - boundary condition, [P-69](#)
- inletOutlet
  - boundary condition, [U-129](#)
- inner product, *see* tensor, inner product
- inside

- keyword entry, [U-141](#)
- insideCells utility, [U-87](#)
- interDyMFoam solver, [U-84](#)
- interFoam solver, [U-84](#)
- internalField keyword, [U-22](#), [U-102](#), [U-187](#)
- interPhaseChangeFoam solver, [U-84](#)
- interpolationScheme keyword, [U-166](#)
- interpolations tools, [U-91](#)
- interpolationSchemes keyword, [U-107](#)
- inv
  - tensor member function, [P-25](#)
- isoOctane model, [U-93](#)

## J

- janafThermo model, [U-93](#), [U-171](#)
- JAVA\_HOME
  - environment variable, [U-192](#)
- jplot
  - keyword entry, [U-105](#), [U-166](#)

## K

- kappa keyword, [U-174](#)
- kEpsilon model, [U-94](#)
- keyword
  - FoamFile, [U-99](#)
  - LESmodel, [U-174](#)
  - RASModel, [U-174](#)
  - addLayersControls, [U-138](#)
  - adjustTimeStep, [U-59](#)
  - agglomerator, [U-115](#)
  - arc, [U-131](#)
  - blocks, [U-22](#), [U-32](#), [U-132](#)
  - block, [U-131](#)
  - boundaryField, [U-22](#), [U-102](#)
  - boxToCell, [U-58](#)
  - cGamma, [U-61](#)
  - cacheAgglomeration, [U-115](#)
  - castellatedMeshControls, [U-138](#)
  - castellatedMesh, [U-138](#)
  - class, [U-99](#)
  - cloud, [U-167](#)
  - convertToMeters, [U-131](#)
  - curve, [U-167](#)
  - debug, [U-138](#)
  - defaultFieldValues, [U-58](#)
  - deltaT, [U-104](#)
  - delta, [U-81](#), [U-174](#)
  - dimensions, [U-22](#), [U-102](#)
  - distributed, [U-81](#), [U-82](#)
  - divSchemes, [U-107](#)
  - doLayers, [U-138](#)
  - edgeGrading, [U-133](#)
  - edges, [U-131](#)
  - endTime, [U-24](#), [U-104](#)



errorReduction, [U-145](#)  
expansionRatio, [U-144](#)  
face, [U-167](#)  
featureAngle, [U-144](#)  
features, [U-139](#)  
fieldValues, [U-58](#)  
fields, [U-166](#)  
finalLayerRatio, [U-144](#)  
firstTime, [U-104](#)  
fluxRequired, [U-107](#)  
format, [U-99](#)  
functions, [U-106](#)  
geometry, [U-138](#)  
gradSchemes, [U-107](#)  
graphFormat, [U-105](#)  
internalField, [U-22](#), [U-102](#), [U-187](#)  
interpolationSchemes, [U-107](#)  
interpolationScheme, [U-166](#)  
kappa, [U-174](#)  
laplacianSchemes, [U-107](#)  
latestTime, [U-39](#)  
layers, [U-144](#)  
leastSquares, [U-51](#)  
levels, [U-142](#)  
libs, [U-105](#)  
locationInMesh, [U-139](#), [U-141](#)  
location, [U-99](#)  
manualCoeffs, [U-81](#)  
maxBoundarySkewness, [U-145](#)  
maxConcave, [U-145](#)  
maxCo, [U-59](#)  
maxDeltaT, [U-59](#)  
maxFaceThicknessRatio, [U-144](#)  
maxGlobalCells, [U-139](#)  
maxInternalSkewness, [U-145](#)  
maxLocalCells, [U-139](#)  
maxNonOrtho, [U-145](#)  
maxThicknessToMedialRatio, [U-144](#)  
mergeLevels, [U-116](#)  
mergeTolerance, [U-138](#)  
meshQualityControls, [U-138](#)  
method, [U-81](#)  
metisCoeffs, [U-81](#)  
midPointAndFace, [U-167](#)  
midPoint, [U-167](#)  
minArea, [U-145](#)  
minDeterminant, [U-145](#)  
minFaceWeight, [U-145](#)  
minFlatness, [U-145](#)  
minMedianAxisAngle, [U-144](#)  
minRefinementCells, [U-139](#)  
minThickness, [U-144](#)  
minTriangleTwist, [U-145](#)  
minTwist, [U-145](#)  
minVolRatio, [U-145](#)  
minVol, [U-145](#)  
mode, [U-141](#)  
nBufferCellsNoExtrude, [U-144](#)  
nCellsBetweenLevels, [U-139](#)  
nFaces, [U-122](#)  
nFinestSweeps, [U-115](#), [U-116](#)  
nGammaSubCycles, [U-61](#)  
nGrow, [U-144](#)  
nPostSweeps, [U-115](#), [U-116](#)  
nPreSweeps, [U-115](#)  
nRelaxIter, [U-142](#), [U-144](#)  
nSmoothNormals, [U-144](#)  
nSmoothPatch, [U-142](#)  
nSmoothScale, [U-145](#)  
nSmoothSurfaceNormals, [U-144](#)  
nSmoothThickness, [U-144](#)  
nSolveIter, [U-142](#)  
numberOfSubdomains, [U-81](#)  
n, [U-81](#)  
object, [U-99](#)  
order, [U-81](#)  
pRefCell, [U-25](#), [U-117](#)  
pRefValue, [U-25](#), [U-117](#)  
patchMap, [U-152](#)  
patches, [U-131](#), [U-133](#)  
pdRefCell, [U-117](#)  
pdRefValue, [U-117](#)  
preconditioner, [U-114](#)  
pressure, [U-49](#)  
processorWeights, [U-81](#)  
purgeWrite, [U-105](#)  
refGradient, [U-128](#)  
referenceLevel, [U-187](#)  
refinementRegions, [U-139](#), [U-142](#)  
refinementSurfaces, [U-139](#)  
refinementRegions, [U-141](#)  
regions, [U-58](#)  
relTol, [U-52](#), [U-114](#)  
resolveFeatureAngle, [U-139](#), [U-140](#)  
roots, [U-81](#), [U-82](#)  
runTimeModifiable, [U-105](#)  
setFormat, [U-166](#)  
sets, [U-166](#)  
simpleGrading, [U-133](#)  
smoother, [U-115](#)  
snGradSchemes, [U-107](#)  
snapControls, [U-138](#)  
snap, [U-138](#)  
solvers, [U-113](#)  
spline, [U-131](#)  
startFace, [U-122](#)  
startFrom, [U-23](#), [U-104](#)  
startTime, [U-23](#), [U-104](#)

- stopAt, [U-104](#)
- surfaceFormat, [U-166](#)
- surfaces, [U-166](#)
- thermoType, [U-171](#)
- timeFormat, [U-105](#)
- timePrecision, [U-105](#)
- timeScheme, [U-107](#)
- tolerance, [U-52](#), [U-114](#), [U-142](#)
- topoSetSource, [U-58](#)
- traction, [U-49](#)
- turbulence, [U-174](#)
- type, [U-124](#), [U-125](#)
- uniform, [U-167](#)
- valueFraction, [U-128](#)
- value, [U-23](#), [U-128](#)
- version, [U-99](#)
- vertices, [U-22](#), [U-131](#)
- wallFunctionCoeffs, [U-174](#)
- writeCompression, [U-105](#)
- writeControl, [U-24](#), [U-59](#), [U-104](#)
- writeFormat, [U-54](#), [U-105](#)
- writeInterval, [U-24](#), [U-33](#), [U-105](#)
- writePrecision, [U-105](#)
- <LESmodel>Coeffs, [U-174](#)
- <RASModel>Coeffs, [U-174](#)
- <delta>Coeffs, [U-174](#)
- keyword entry
  - CrankNicholson, [U-112](#)
  - CrossPowerLaw, [U-58](#)
  - DICGaussSeidel, [U-115](#)
  - DIC, [U-115](#)
  - DILU, [U-115](#)
  - Euler, [U-112](#)
  - FDIC, [U-115](#)
  - GAMG, [U-114](#), [U-115](#)
  - Gamma, [U-109](#)
  - GaussSeidel, [U-115](#)
  - Gauss, [U-110](#)
  - MGridGen, [U-115](#)
  - MUSCL, [U-109](#)
  - Newtonian, [U-58](#)
  - PBiCG, [U-114](#)
  - PCG, [U-114](#)
  - QUICK, [U-109](#), [U-112](#)
  - SFCD, [U-109](#), [U-112](#)
  - UMIST, [U-108](#)
  - adjustableRunTime, [U-59](#), [U-104](#)
  - arc, [U-132](#)
  - ascii, [U-105](#)
  - backward, [U-112](#)
  - binary, [U-105](#)
  - bounded, [U-110](#), [U-111](#)
  - cellPointFace, [U-166](#)
  - cellPoint, [U-166](#)
  - cell, [U-166](#)
  - clockTime, [U-105](#)
  - compressed, [U-105](#)
  - corrected, [U-110](#), [U-111](#)
  - cpuTime, [U-105](#)
  - cubicCorrected, [U-112](#)
  - cubicCorrection, [U-109](#)
  - cyclic, [U-127](#)
  - diagonal, [U-115](#)
  - distance, [U-141](#), [U-167](#)
  - dx, [U-166](#)
  - empty, [U-127](#)
  - faceAreaPair, [U-115](#)
  - fixed, [U-105](#)
  - foamFile, [U-166](#)
  - fourth, [U-110](#), [U-111](#)
  - general, [U-105](#)
  - gnuplot, [U-105](#), [U-166](#)
  - hierarchical, [U-80](#), [U-81](#)
  - inside, [U-141](#)
  - jplot, [U-105](#), [U-166](#)
  - latestTime, [U-104](#)
  - leastSquares, [U-110](#)
  - limitedCubic, [U-109](#)
  - limitedLinear, [U-109](#)
  - limited, [U-110](#), [U-111](#)
  - linearUpwind, [U-109](#), [U-112](#)
  - linear, [U-109](#), [U-112](#)
  - line, [U-132](#)
  - manual, [U-80](#), [U-81](#)
  - metis, [U-80](#), [U-81](#)
  - midPoint, [U-109](#)
  - nextWrite, [U-104](#)
  - noWriteNow, [U-104](#)
  - none, [U-108](#), [U-115](#)
  - null, [U-166](#)
  - outside, [U-141](#)
  - patch, [U-127](#), [U-168](#)
  - polyLine, [U-132](#)
  - polySpline, [U-132](#)
  - processor, [U-127](#)
  - raw, [U-105](#), [U-166](#)
  - runTime, [U-33](#), [U-104](#)
  - scientific, [U-105](#)
  - simpleSpline, [U-132](#)
  - simple, [U-80](#), [U-81](#)
  - skewLinear, [U-109](#), [U-112](#)
  - smoothSolver, [U-114](#)
  - startTime, [U-23](#), [U-104](#)
  - steadyState, [U-112](#)
  - stl, [U-166](#)
  - symmetryPlane, [U-127](#)
  - timeStep, [U-24](#), [U-33](#), [U-104](#)
  - uncompressed, [U-105](#)

- uncorrected, [U-110](#), [U-111](#)
  - upwind, [U-109](#), [U-112](#)
  - vanLeer, [U-109](#)
  - vtk, [U-166](#)
  - wall, [U-127](#)
  - wedge, [U-127](#)
  - writeControl, [U-104](#)
  - writeNow, [U-104](#)
  - xmgr, [U-105](#), [U-166](#)
  - xyz, [U-167](#)
  - x, [U-167](#)
  - y, [U-167](#)
  - z, [U-167](#)
  - kill button, [U-187](#)
  - kivaToFoam utility, [U-87](#)
  - Kronecker delta, [P-20](#)
- ## L
- lagrangian
    - library, [U-92](#)
  - Lambda2 utility, [U-89](#)
  - LamBremhorstKE model, [U-94](#)
  - laminar model, [U-94](#)
  - laminarFlameSpeedModels
    - library, [U-93](#)
  - laplaceFilter model, [U-94](#)
  - Laplacian, [P-38](#)
  - laplacian, [P-37](#)
  - laplacian
    - fvc member function, [P-37](#)
    - fvm member function, [P-37](#)
  - laplacianFoam solver, [U-83](#)
  - laplacianSchemes keyword, [U-107](#)
  - latestTime
    - keyword entry, [U-104](#)
    - menu entry, [U-184](#)
  - latestTime keyword, [U-39](#)
  - LaunderGibsonRSTM model, [U-94](#)
  - LaunderSharmaKE model, [U-94](#)
  - layers keyword, [U-144](#)
  - leastSquares
    - keyword entry, [U-110](#)
  - leastSquares keyword, [U-51](#)
  - lesBuoyantFoam solver, [U-85](#)
  - lesCavitatingFoam solver, [U-84](#)
  - LESdeltas
    - library, [U-94](#)
  - LESfilters
    - library, [U-94](#)
  - lesInterFoam solver, [U-84](#)
  - LESmodel keyword, [U-174](#)
  - LESProperties*
    - dictionary, [U-174](#)
  - levels keyword, [U-142](#)
  - libraries, [U-67](#)
  - library
    - Gstream, [U-92](#)
    - LESdeltas, [U-94](#)
    - LESfilters, [U-94](#)
    - ODE, [U-92](#)
    - OpenFOAM, [U-91](#)
    - PV3FoamReader, [U-155](#)
    - PVFoamReader, [U-155](#)
    - basicThermophysicalModels, [U-92](#)
    - cellDecompFiniteElement, [U-91](#)
    - cfTools, [U-91](#)
    - chemistryModel, [U-93](#)
    - combustionThermophysicalModels, [U-92](#)
    - compressibleLESModels, [U-95](#)
    - compressibleRASModels, [U-94](#)
    - dieselSpray, [U-92](#)
    - dynamicMesh, [U-91](#)
    - edgeMesh, [U-92](#)
    - engine, [U-92](#)
    - errorEstimation, [U-92](#)
    - faceDecompFiniteElement, [U-92](#)
    - foamUser, [U-78](#)
    - incompressibleLESModels, [U-94](#)
    - incompressiblePostProcessing, [U-91](#)
    - incompressibleRASModels, [U-94](#)
    - incompressibleTransportModels, [P-55](#), [U-95](#)
    - incompressibleTurbulenceModels, [P-55](#)
    - lagrangian, [U-92](#)
    - laminarFlameSpeedModels, [U-93](#)
    - liquids, [U-93](#)
    - meshTools, [U-92](#)
    - mico-2.3.13, [U-92](#)
    - mpich-1.2.4, [U-92](#)
    - openmpi-1.2.6, [U-92](#)
    - pdf, [U-93](#)
    - primitive, [P-23](#)
    - randomProcesses, [U-92](#)
    - sampling, [U-91](#)
    - shapeMeshTools, [U-92](#)
    - specie, [U-93](#)
    - thermophysicalFunctions, [U-93](#)
    - thermophysical, [U-171](#)
    - triSurface, [U-92](#)
    - vtkFoam, [U-155](#)
    - vtkPV3Foam, [U-155](#)
    - zlib-1.2.3, [U-92](#)
  - libs keyword, [U-105](#)
  - lid-driven cavity flow, [U-19](#)
  - LienCubicKE model, [U-94](#)
  - LienCubicKELowRE model, [U-94](#)
  - LienLeschzinerLowRE model, [U-94](#)
  - Lights window panel, [U-159](#)
  - limited

- keyword entry, [U-110](#), [U-111](#)
- limitedCubic
  - keyword entry, [U-109](#)
- limitedLinear
  - keyword entry, [U-109](#)
- line
  - keyword entry, [U-132](#)
- linear
  - keyword entry, [U-109](#), [U-112](#)
- linearUpwind
  - keyword entry, [U-109](#), [U-112](#)
- liquid
  - electrically-conducting, [P-67](#)
- liquids
  - library, [U-93](#)
- lists, [P-29](#)
- List<Type> template class, [P-29](#)
- location keyword, [U-99](#)
- locationInMesh keyword, [U-139](#), [U-141](#)
- locDynOneEqEddy model, [U-94](#)
- lowReOneEqEddy model, [U-95](#)
- LRDDiffStress model, [U-95](#)
- LRR model, [U-94](#)
- lsGrad
  - fvc member function, [P-37](#)

## M

- Mach utility, [U-89](#)
- mag
  - tensor member function, [P-25](#)
- magGradU utility, [U-89](#)
- magnetohydrodynamics, [P-67](#)
- magSqr
  - tensor member function, [P-25](#)
- magU utility, [U-89](#)
- Make directory, [U-71](#)
- make script/alias, [U-69](#)
- Make/files file, [U-72](#)
- manual
  - keyword entry, [U-80](#), [U-81](#)
- manualCoeffs keyword, [U-81](#)
- mapFields utility, [U-32](#), [U-38](#), [U-42](#), [U-54](#), [U-86](#), [U-151](#)
- mapping
  - fields, [U-151](#)
- matrices tools, [U-91](#)
- max
  - tensor member function, [P-25](#)
- maxBoundarySkewness keyword, [U-145](#)
- maxCo keyword, [U-59](#)
- maxConcave keyword, [U-145](#)
- maxDeltaT keyword, [U-59](#)
- maxFaceThicknessRatio keyword, [U-144](#)
- maxGlobalCells keyword, [U-139](#)

- maxInternalSkewness keyword, [U-145](#)
- maxLocalCells keyword, [U-139](#)
- maxNonOrtho keyword, [U-145](#)
- maxThicknessToMedialRatio keyword, [U-144](#)
- mdEquilibrationFoam solver, [U-86](#)
- mechanicalProperties
  - dictionary, [U-49](#)
- menu
  - Class, [U-182](#)
  - Color By, [U-158](#)
  - Current Time Controls, [U-28](#), [U-157](#)
  - Edit, [U-159](#)
  - Help, [U-159](#)
  - Plot Type, [U-35](#)
  - VCR Controls, [U-28](#), [U-157](#)
  - View, [U-159](#)
- menu entry
  - Plot Over Line, [U-35](#)
  - Save Animation, [U-161](#)
  - Save Screenshot, [U-161](#)
  - Settings, [U-159](#)
  - Show Color Legend, [U-28](#)
  - Solid Color, [U-158](#)
  - Toolbars, [U-159](#)
  - View Settings..., [U-25](#)
  - View Settings, [U-25](#), [U-159](#)
  - Wireframe, [U-158](#)
  - allTime, [U-184](#)
  - firstTime, [U-184](#)
  - fvSchemes, [U-51](#)
  - latestTime, [U-184](#)
  - noTime, [U-184](#)
- mergeLevels keyword, [U-116](#)
- mergeMeshes utility, [U-87](#)
- mergeTolerance keyword, [U-138](#)
- mesh
  - 1-dimensional, [U-122](#)
  - 1D, [U-122](#)
  - 2-dimensional, [U-122](#)
  - 2D, [U-122](#)
  - axi-symmetric, [U-122](#)
  - basic, [P-31](#)
  - block structured, [U-127](#)
  - decomposition, [U-79](#)
  - description, [U-119](#)
  - finite volume, [P-31](#)
  - generation, [U-127](#), [U-136](#)
  - grading, [U-127](#), [U-132](#)
  - grading, example of, [P-53](#)
  - non-orthogonal, [P-45](#)
  - refinement, [P-62](#)
  - resolution, [U-30](#)
  - specification, [U-119](#)
  - split-hex, [U-136](#)

- Stereolithography (STL), [U-136](#)
- surface, [U-136](#)
- validity constraints, [U-119](#)
- meshes tools, [U-91](#)
- meshQualityControls keyword, [U-138](#)
- meshTools
  - library, [U-92](#)
- message passing interface
  - MPICH, [U-193](#)
  - openMPI, [U-81](#)
- method keyword, [U-81](#)
- metis
  - keyword entry, [U-80](#), [U-81](#)
- metisCoeffs keyword, [U-81](#)
- MGridGen
  - keyword entry, [U-115](#)
- mhdFoam solver, [P-69](#), [U-85](#)
- mico-2.3.13
  - library, [U-92](#)
- midPoint
  - keyword entry, [U-109](#)
- midPoint keyword, [U-167](#)
- midPointAndFace keyword, [U-167](#)
- min
  - tensor member function, [P-25](#)
- minArea keyword, [U-145](#)
- minDeterminant keyword, [U-145](#)
- minFaceWeight keyword, [U-145](#)
- minFlatness keyword, [U-145](#)
- minMedianAxisAngle keyword, [U-144](#)
- MINMOD differencing, [P-38](#)
- minRefinementCells keyword, [U-139](#)
- minThickness keyword, [U-144](#)
- minTriangleTwist keyword, [U-145](#)
- minTwist keyword, [U-145](#)
- minVol keyword, [U-145](#)
- minVolRatio keyword, [U-145](#)
- mirrorMesh utility, [U-87](#)
- mixed
  - boundary condition, [U-128](#)
- mixedSmagorinsky model, [U-94](#)
- mixtureAdiabaticFlameT utility, [U-90](#)
- mode keyword, [U-141](#)
- model
  - APIfunctions, [U-93](#)
  - BirdCarreau, [U-95](#)
  - CrossPowerLaw, [U-95](#)
  - DeardorffDiffStress, [U-95](#)
  - LRDDiffStress, [U-95](#)
  - LRR, [U-94](#)
  - LamBremhorstKE, [U-94](#)
  - LaunderGibsonRSTM, [U-94](#)
  - LaunderSharmaKE, [U-94](#)
  - LienCubicKELowRE, [U-94](#)
  - LienCubicKE, [U-94](#)
  - LienLeschzinerLowRE, [U-94](#)
  - NSRDSfunctions, [U-93](#)
  - Newtonian, [U-95](#)
  - NonlinearKEShah, [U-94](#)
  - PrandtlDelta, [U-94](#)
  - QZeta, [U-94](#)
  - RNGkEpsilon, [U-94](#)
  - RosinRammler, [U-93](#)
  - Smagorinsky2, [U-94](#)
  - Smagorinsky, [U-94](#), [U-95](#)
  - SpalartAllmaras, [U-94](#), [U-95](#)
  - anisotropicFilter, [U-94](#)
  - chemistryModel, [U-93](#)
  - chemistrySolver, [U-93](#)
  - chemkinMixture, [U-93](#), [U-172](#)
  - constLaminarFlameSpeed, [U-93](#)
  - constTransport, [U-93](#), [U-172](#)
  - cubeRootVolDelta, [U-94](#)
  - diEthylEther, [U-93](#)
  - diMethylEther, [U-93](#)
  - dieselMixture, [U-92](#), [U-172](#)
  - dynMixedSmagorinsky, [U-94](#)
  - dynOneEqEddy, [U-94](#), [U-95](#)
  - dynSmagorinsky, [U-94](#)
  - exponential, [U-93](#)
  - general, [U-93](#)
  - guldersonLaminarFlameSpeed, [U-93](#)
  - hConstThermo, [U-93](#), [U-171](#)
  - hMixtureThermo, [U-92](#), [U-172](#)
  - hThermo, [U-92](#), [U-172](#)
  - hhuMixtureThermo, [U-92](#), [U-172](#)
  - homogeneousMixture, [U-92](#), [U-172](#)
  - inhomogeneousMixture, [U-92](#), [U-172](#)
  - isoOctane, [U-93](#)
  - janafThermo, [U-93](#), [U-171](#)
  - kEpsilon, [U-94](#)
  - laminar, [U-94](#)
  - laplaceFilter, [U-94](#)
  - locDynOneEqEddy, [U-94](#)
  - lowReOneEqEddy, [U-95](#)
  - mixedSmagorinsky, [U-94](#)
  - multiComponentMixture, [U-93](#), [U-172](#)
  - nDecane, [U-93](#)
  - nDodecane, [U-93](#)
  - nHeptane, [U-93](#)
  - nOctane, [U-93](#)
  - normal, [U-93](#)
  - oneEqEddy, [U-94](#), [U-95](#)
  - perfectGas, [U-93](#), [U-171](#)
  - pureMixture, [U-92](#), [U-172](#)
  - scaleSimilarity, [U-94](#)
  - simpleFilter, [U-94](#)
  - smoothDelta, [U-94](#)

specieThermo, [U-93](#), [U-171](#)  
 spectEddyVisc, [U-95](#)  
 sutherlandTransport, [U-93](#), [U-172](#)  
 uniform, [U-93](#)  
 veryInhomogeneousMixture, [U-92](#), [U-172](#)  
 water, [U-93](#)  
 momentScalarError utility, [U-90](#)  
 moveDynamicMesh utility, [U-87](#)  
 moveEngineMesh utility, [U-87](#)  
 moveMesh utility, [U-87](#)  
 movingWallVelocity  
   boundary condition, [U-129](#)  
 MPI  
   MPICH, [U-193](#)  
   openMPI, [U-81](#)  
 MPICH  
   message passing interface, [U-193](#)  
   MPI, [U-193](#)  
 mpich-1.2.4  
   library, [U-92](#)  
 mshToFoam utility, [U-87](#)  
 multiComponentMixture model, [U-93](#), [U-172](#)  
 multigrid  
   geometric-algebraic, [U-115](#)  
 multiphaseInterFoam solver, [U-84](#)  
 MUSCL  
   keyword entry, [U-109](#)  
 My Jobs button, [U-187](#)

## N

n keyword, [U-81](#)  
 nabla  
   operator, [P-27](#)  
 name  
   server, [U-178](#)  
 nBufferCellsNoExtrude keyword, [U-144](#)  
 nCellsBetweenLevels keyword, [U-139](#)  
 nDecane model, [U-93](#)  
 nDodecane model, [U-93](#)  
 neighbour  
   dictionary, [U-121](#)  
 netgenNeutralToFoam utility, [U-87](#)  
 Newtonian  
   keyword entry, [U-58](#)  
 Newtonian model, [U-95](#)  
 nextWrite  
   keyword entry, [U-104](#)  
 nFaces keyword, [U-122](#)  
 nFinestSweeps keyword, [U-115](#), [U-116](#)  
 nGammaSubCycles keyword, [U-61](#)  
 nGrow keyword, [U-144](#)  
 nHeptane model, [U-93](#)  
 nOctane model, [U-93](#)  
 non-orthogonal mesh, [P-45](#)

none  
   keyword entry, [U-108](#), [U-115](#)  
 NonlinearKEShik model, [U-94](#)  
 nonNewtonianIcoFoam solver, [U-83](#)  
 normal model, [U-93](#)  
 noTime  
   menu entry, [U-184](#)  
 noWriteNow  
   keyword entry, [U-104](#)  
 nPostSweeps keyword, [U-115](#), [U-116](#)  
 nPreSweeps keyword, [U-115](#)  
 nRelaxIter keyword, [U-142](#), [U-144](#)  
 nSmoothNormals keyword, [U-144](#)  
 nSmoothPatch keyword, [U-142](#)  
 nSmoothScale keyword, [U-145](#)  
 nSmoothSurfaceNormals keyword, [U-144](#)  
 nSmoothThickness keyword, [U-144](#)  
 nSolveIter keyword, [U-142](#)  
 NSRDSfunctions model, [U-93](#)  
 null  
   keyword entry, [U-166](#)  
 numberOfSubdomains keyword, [U-81](#)

## O

object keyword, [U-99](#)  
 objToVTK utility, [U-87](#)  
 ODE  
   library, [U-92](#)  
 oneEqEddy model, [U-94](#), [U-95](#)  
 oodles solver, [U-83](#)  
 Opacity text box, [U-159](#)  
 OpenFOAM  
   applications, [U-67](#)  
   file format, [U-98](#)  
   libraries, [U-67](#)  
 OpenFOAM  
   library, [U-91](#)  
 OpenFOAM file syntax  
   //, [U-98](#)  
 openMPI  
   message passing interface, [U-81](#)  
   MPI, [U-81](#)  
 openmpi-1.2.6  
   library, [U-92](#)  
 operator  
   scalar, [P-28](#)  
   vector, [P-27](#)  
 Options window, [U-159](#)  
 options file, [U-71](#)  
 order keyword, [U-81](#)  
 Orientation Axes button, [U-25](#), [U-159](#)  
 outer product, *see* tensor, outer product  
 outlet  
   boundary condition, [P-69](#)



outletInlet  
     boundary condition, [U-129](#)  
 outside  
     keyword entry, [U-141](#)  
 owner  
     dictionary, [U-121](#)  
  
**P**  
 p field, [U-24](#)  
 paraFoam, [U-25](#), [U-155](#)  
 paraFoam utility, [U-88](#)  
 parallel  
     running, [U-79](#)  
 partialSlip  
     boundary condition, [U-129](#)  
 patch  
     boundary condition, [U-126](#)  
 patch  
     keyword entry, [U-127](#), [U-168](#)  
 patchAverage utility, [U-89](#)  
 patches keyword, [U-131](#), [U-133](#)  
 patchIntegrate utility, [U-89](#)  
 patchMap keyword, [U-152](#)  
 patchTool utility, [U-87](#)  
 PBiCG  
     keyword entry, [U-114](#)  
 PCG  
     keyword entry, [U-114](#)  
 pdf  
     library, [U-93](#)  
 pdRefCell keyword, [U-117](#)  
 pdRefValue keyword, [U-117](#)  
 PDRFoam solver, [U-85](#)  
 Pe utility, [U-89](#)  
 perfectGas model, [U-93](#), [U-171](#)  
 permutation symbol, [P-19](#)  
 Pipeline Browser window, [U-25](#), [U-156](#)  
 PISO  
     dictionary, [U-25](#)  
 Plot Over Line  
     menu entry, [U-35](#)  
 Plot Type menu, [U-35](#)  
 plot3dToFoam utility, [U-87](#)  
 pointField class, [P-31](#)  
 pointField<Type> template class, [P-33](#)  
 points  
     dictionary, [U-121](#), [U-127](#)  
 pointSet utility, [U-87](#)  
 polyBoundaryMesh class, [P-31](#)  
 polyDualMesh utility, [U-87](#)  
 polyLine  
     keyword entry, [U-132](#)  
 polyMesh directory, [U-98](#), [U-121](#)  
 polyMesh class, [P-31](#), [U-119](#), [U-121](#)

polyPatch class, [P-31](#)  
 polyPatchList class, [P-31](#)  
 polySpline  
     keyword entry, [U-132](#)  
 post-processing, [U-155](#)  
     post-processing  
         paraFoam, [U-155](#)  
 postChannel utility, [U-90](#)  
 potentialFoam solver, [P-46](#), [U-83](#)  
 pow  
     tensor member function, [P-25](#)  
 PrandtlDelta model, [U-94](#)  
 preconditioner keyword, [U-114](#)  
 pRefCell keyword, [U-25](#), [U-117](#)  
 pRefValue keyword, [U-25](#), [U-117](#)  
 pressure keyword, [U-49](#)  
 pressure waves  
     in liquids, [P-62](#)  
 pressureDirectedInletVelocity  
     boundary condition, [U-129](#)  
 pressureInletVelocity  
     boundary condition, [U-129](#)  
 pressureOutlet  
     boundary condition, [P-63](#)  
 pressureTransmissive  
     boundary condition, [U-129](#)  
 primitive  
     library, [P-23](#)  
 primitives tools, [U-91](#)  
 process  
     background, [U-26](#), [U-79](#)  
     foreground, [U-26](#)  
 processor  
     boundary condition, [U-127](#)  
 processor  
     keyword entry, [U-127](#)  
 processorN directory, [U-80](#)  
 processorWeights keyword, [U-81](#)  
 Properties window panel, [U-26](#), [U-156](#)  
 ptot utility, [U-90](#)  
 pureMixture model, [U-92](#), [U-172](#)  
 purge button, [U-187](#)  
 purgeWrite keyword, [U-105](#)  
 PV3FoamReader  
     library, [U-155](#)  
 PVFoamReader  
     library, [U-155](#)

## Q

Q utility, [U-89](#)  
 QUICK  
     keyword entry, [U-109](#), [U-112](#)  
 QZeta model, [U-94](#)

## R

R utility, [U-89](#)  
 randomProcesses  
     library, [U-92](#)  
 rasCavitatingFoam solver, [U-84](#)  
 rasInterFoam solver, [U-84](#)  
 RASModel keyword, [U-174](#)  
 RASProperties  
     dictionary, [U-41](#), [U-174](#)  
 raw  
     keyword entry, [U-105](#), [U-166](#)  
 Rcomponents utility, [U-89](#)  
 reactingFoam solver, [U-85](#)  
 read button, [U-187](#)  
 reconstructPar utility, [U-83](#), [U-90](#)  
 reconstructParMesh utility, [U-90](#)  
 referenceLevel keyword, [U-187](#)  
 refGradient keyword, [U-128](#)  
 refinementRegions keyword, [U-141](#)  
 refinementRegions keyword, [U-139](#), [U-142](#)  
 refinementSurfaces keyword, [U-139](#)  
 refineMesh utility, [U-87](#)  
 Region Status window panel, [U-25](#)  
 regions keyword, [U-58](#)  
 relative tolerance, [U-114](#)  
 relTol keyword, [U-52](#), [U-114](#)  
 Render View window, [U-160](#)  
 Render View window panel, [U-159](#)  
 Render View Options window, [U-159](#)  
 renumberMesh utility, [U-87](#)  
 Rescale to Data Range button, [U-28](#)  
 Reset button, [U-156](#)  
 resolveFeatureAngle keyword, [U-139](#), [U-140](#)  
 restart, [U-39](#)  
 Reynolds number, [U-19](#), [U-23](#)  
 rhoCentralFoam solver, [U-84](#)  
 rhoPimpleFoam solver, [U-84](#)  
 rhoPorousSimpleFoam solver, [U-84](#)  
 rhoPsonicFoam solver, [U-84](#)  
 rhoSimpleFoam solver, [U-84](#)  
 rhoSonicFoam solver, [U-84](#)  
 rhoTurbFoam solver, [U-84](#)  
 rmdepall script/alias, [U-74](#)  
 RNGkEpsilon model, [U-94](#)  
 roots keyword, [U-81](#), [U-82](#)  
 RosinRammler model, [U-93](#)  
 rotateMesh utility, [U-88](#)  
 run  
     parallel, [U-79](#)  
     run directory, [U-97](#)  
     runFoamX script/alias, [U-177–U-179](#)  
     runFoamXHB script/alias, [U-177](#), [U-178](#)  
 runTime  
     keyword entry, [U-33](#), [U-104](#)

runTimeModifiable keyword, [U-105](#)

## S

sammToFoam utility, [U-87](#)  
 sample utility, [U-90](#), [U-165](#)  
 sampleSurface utility, [U-90](#)  
 sampling  
     library, [U-91](#)  
 Save Animation  
     menu entry, [U-161](#)  
 Save Screenshot  
     menu entry, [U-161](#)  
 scalar, [P-16](#)  
     operator, [P-28](#)  
 scalar class, [P-23](#)  
 scalarField class, [P-29](#)  
 scalarTransportFoam solver, [U-83](#)  
 scale  
     tensor member function, [P-25](#)  
 scalePoints utility, [U-148](#)  
 scaleSimilarity model, [U-94](#)  
 scientific  
     keyword entry, [U-105](#)  
 script/alias  
     foamCorrectVrt, [U-150](#)  
     foamJob, [U-169](#)  
     foamLog, [U-169](#)  
     make, [U-69](#)  
     rmdepall, [U-74](#)  
     runFoamXHB, [U-177](#), [U-178](#)  
     runFoamX, [U-177–U-179](#)  
     wclean, [U-73](#)  
     wmake, [U-69](#)  
 second time derivative, [P-37](#)  
 Seed window, [U-160](#)  
 Set Solid Color button, [U-158](#)  
 setFields utility, [U-57](#), [U-58](#), [U-86](#)  
 setFormat keyword, [U-166](#)  
 sets keyword, [U-166](#)  
 Settings  
     menu entry, [U-159](#)  
 settlingFoam solver, [U-85](#)  
 SFCD  
     keyword entry, [U-109](#), [U-112](#)  
 shape, [U-132](#)  
 shapeMeshTools  
     library, [U-92](#)  
 Show Color Legend  
     menu entry, [U-28](#)  
 SI units, [U-101](#)  
 simple  
     keyword entry, [U-80](#), [U-81](#)  
 simpleFilter model, [U-94](#)  
 simpleFoam solver, [P-54](#), [U-83](#)



- simpleGrading keyword, [U-133](#)
- simpleSpline
  - keyword entry, [U-132](#)
- skew
  - tensor member function, [P-25](#)
- skewLinear
  - keyword entry, [U-109](#), [U-112](#)
- slice class, [P-31](#)
- slip
  - boundary condition, [U-129](#)
- Smagorinsky model, [U-94](#), [U-95](#)
- Smagorinsky2 model, [U-94](#)
- smapToFoam utility, [U-88](#)
- smoothDelta model, [U-94](#)
- smoother keyword, [U-115](#)
- smoothSolver
  - keyword entry, [U-114](#)
- snap keyword, [U-138](#)
- snapControls keyword, [U-138](#)
- snappyHexMesh utility
  - background mesh, [U-138](#)
  - cell removal, [U-140](#)
  - cell splitting, [U-139](#)
  - mesh layers, [U-142](#)
  - meshing process, [U-137](#)
  - snapping to surfaces, [U-142](#)
- snappyHexMesh utility, [U-136](#)
- snappyHexMeshDict* file, [U-137](#)
- snGrad
  - fvc member function, [P-37](#)
- snGradCorrection
  - fvc member function, [P-37](#)
- snGradSchemes keyword, [U-107](#)
- Solid Color
  - menu entry, [U-158](#)
- solidDisplacementFoam solver, [U-50](#), [U-85](#)
- solidEquilibriumDisplacementFoam solver, [U-86](#)
- solver
  - PDRFoam, [U-85](#)
  - XiFoam, [U-85](#)
  - Xoodles, [U-85](#)
  - blockMesh, [P-47](#)
  - boundaryFoam, [U-83](#)
  - bubbleFoam, [U-84](#)
  - buoyantFoam, [U-85](#)
  - buoyantSimpleFoam, [U-85](#)
  - buoyantSimpleRadiationFoam, [U-85](#)
  - channelOodles, [U-83](#)
  - chtMultiRegionFoam, [U-85](#)
  - coldEngineFoam, [U-85](#)
  - compressibleLesInterFoam, [U-84](#)
  - coodles, [U-84](#)
  - dieselEngineFoam, [U-85](#)
  - dieselFoam, [U-85](#)
  - dnsFoam, [U-85](#)
  - electrostaticFoam, [U-85](#)
  - engineFoam, [U-85](#)
  - financialFoam, [U-86](#)
  - gnemDFoam, [U-86](#)
  - icoDyMFoam, [U-83](#)
  - icoFoam, [U-19](#), [U-23](#), [U-24](#), [U-26](#), [U-83](#)
  - interDyMFoam, [U-84](#)
  - interFoam, [U-84](#)
  - interPhaseChangeFoam, [U-84](#)
  - laplacianFoam, [U-83](#)
  - lesBuoyantFoam, [U-85](#)
  - lesCavitatingFoam, [U-84](#)
  - lesInterFoam, [U-84](#)
  - mdEquilibrationFoam, [U-86](#)
  - mhdFoam, [P-69](#), [U-85](#)
  - multiphaseInterFoam, [U-84](#)
  - nonNewtonianIcoFoam, [U-83](#)
  - oodles, [U-83](#)
  - potentialFoam, [P-46](#), [U-83](#)
  - rasCavitatingFoam, [U-84](#)
  - rasInterFoam, [U-84](#)
  - reactingFoam, [U-85](#)
  - rhoCentralFoam, [U-84](#)
  - rhoPimpleFoam, [U-84](#)
  - rhoPorousSimpleFoam, [U-84](#)
  - rhoSimpleFoam, [U-84](#)
  - rhoSonicFoam, [U-84](#)
  - rhoTurbFoam, [U-84](#)
  - rhoPsonicFoam, [U-84](#)
  - scalarTransportFoam, [U-83](#)
  - settlingFoam, [U-85](#)
  - simpleFoam, [P-54](#), [U-83](#)
  - solidDisplacementFoam, [U-50](#), [U-85](#)
  - solidEquilibriumDisplacementFoam, [U-86](#)
  - sonicFoamAutoMotion, [U-84](#)
  - sonicFoam, [P-60](#), [U-84](#)
  - sonicLiquidFoam, [P-63](#), [U-84](#)
  - sonicTurbFoam, [U-84](#)
  - turbDyMFoam, [U-84](#)
  - turbFoam, [U-19](#), [U-84](#)
  - twoLiquidMixingFoam, [U-85](#)
  - twoPhaseEulerFoam, [U-85](#)
- solver relative tolerance, [U-114](#)
- solver tolerance, [U-114](#)
- solvers keyword, [U-113](#)
- sonicFoam solver, [P-60](#), [U-84](#)
- sonicFoamAutoMotion solver, [U-84](#)
- sonicLiquidFoam solver, [P-63](#), [U-84](#)
- sonicTurbFoam solver, [U-84](#)
- source, [P-37](#)
- SpalartAllmaras model, [U-94](#), [U-95](#)
- specie
  - library, [U-93](#)

specieThermo model, [U-93](#), [U-171](#)  
 spectEddyVisc model, [U-95](#)  
 spline keyword, [U-131](#)  
 splitMesh utility, [U-88](#)  
 splitMeshRegions utility, [U-88](#)  
 sqr  
     tensor member function, [P-25](#)  
 sqrGradGrad  
     fvc member function, [P-37](#)  
 startFace keyword, [U-122](#)  
 startFrom keyword, [U-23](#), [U-104](#)  
 starToFoam utility, [U-87](#), [U-144](#)  
 startTime  
     keyword entry, [U-23](#), [U-104](#)  
 startTime keyword, [U-23](#), [U-104](#)  
 status button, [U-187](#)  
 steady flow  
     turbulent, [P-53](#)  
 steadyState  
     keyword entry, [U-112](#)  
 Stereolithography (STL), [U-136](#)  
 stitchMesh utility, [U-88](#)  
 stl  
     keyword entry, [U-166](#)  
 stopAt keyword, [U-104](#)  
 streamFunction utility, [U-89](#)  
 stress analysis of plate with hole, [U-45](#)  
 stressComponents utility, [U-89](#)  
 Style window panel, [U-25](#), [U-158](#)  
 Su  
     fvm member function, [P-37](#)  
 subsetMesh utility, [U-88](#)  
 summation convention, [P-17](#)  
 SUPERBEE differencing, [P-38](#)  
 supersonic flow, [P-58](#)  
 supersonic flow over forward step, [P-58](#)  
 supersonicFreeStream  
     boundary condition, [U-129](#)  
 surface mesh, [U-136](#)  
 surfaceField<Type> template class, [P-33](#)  
 surfaceFormat keyword, [U-166](#)  
 surfaceNormalFixedValue  
     boundary condition, [U-129](#)  
 surfaces keyword, [U-166](#)  
 SuSp  
     fvm member function, [P-37](#)  
 suspend button, [U-187](#)  
 sutherlandTransport model, [U-93](#), [U-172](#)  
 symm  
     tensor member function, [P-25](#)  
 symmetryPlane  
     boundary condition, [P-63](#), [U-126](#)  
 symmetryPlane  
     keyword entry, [U-127](#)

symmTensorField class, [P-29](#)  
 symmTensorThirdField class, [P-29](#)  
 system directory, [P-49](#), [U-98](#)

## T

T()  
     tensor member function, [P-25](#)  
 template class  
     GeometricBoundaryField, [P-32](#)  
     fvMatrix, [P-33](#)  
     dimensioned<Type>, [P-25](#)  
     FieldField<Type>, [P-32](#)  
     Field<Type>, [P-29](#)  
     geometricField<Type>, [P-32](#)  
     List<Type>, [P-29](#)  
     pointField<Type>, [P-33](#)  
     surfaceField<Type>, [P-33](#)  
     volField<Type>, [P-33](#)  
 temporal discretisation, [P-42](#)  
     Crank Nicholson, [P-42](#)  
     Euler implicit, [P-42](#)  
     explicit, [P-42](#)  
     in OpenFOAM, [P-43](#)  
 tensor, [P-15](#)  
     addition, [P-17](#)  
     algebraic operations, [P-17](#)  
     algebraic operations in OpenFOAM, [P-23](#)  
     antisymmetric, *see* tensor, skew  
     calculus, [P-27](#)  
     classes in OpenFOAM, [P-23](#)  
     cofactors, [P-22](#)  
     component average, [P-20](#)  
     component maximum, [P-20](#)  
     component minimum, [P-20](#)  
     determinant, [P-22](#)  
     deviatoric, [P-21](#)  
     diagonal, [P-21](#)  
     dimension, [P-16](#)  
     double inner product, [P-19](#)  
     geometric transformation, [P-20](#)  
     Hodge dual, [P-22](#)  
     hydrostatic, [P-21](#)  
     identities, [P-21](#)  
     identity, [P-20](#)  
     inner product, [P-18](#)  
     inverse, [P-22](#)  
     magnitude, [P-20](#)  
     magnitude squared, [P-20](#)  
     mathematics, [P-15](#)  
     notation, [P-17](#)  
     nth power, [P-20](#)  
     outer product, [P-19](#)  
     rank, [P-16](#)  
     rank 3, [P-16](#)

- scalar division, [P-18](#)
- scalar multiplication, [P-17](#)
- scale function, [P-20](#)
- second rank, [P-16](#)
- skew, [P-21](#)
- square of, [P-20](#)
- subtraction, [P-17](#)
- symmetric, [P-21](#)
- symmetric rank 2, [P-16](#)
- symmetric rank 3, [P-16](#)
- trace, [P-21](#)
- transformation, [P-20](#)
- transpose, [P-16](#), [P-21](#)
- triple inner product, [P-19](#)
- vector cross product, [P-19](#)
- tensor class, [P-23](#)
- tensor member function
  - [\\*](#), [P-25](#)
  - [+](#), [P-25](#)
  - [-](#), [P-25](#)
  - [/](#), [P-25](#)
  - [&](#), [P-25](#)
  - [&&](#), [P-25](#)
  - [^](#), [P-25](#)
  - [cmptAv](#), [P-25](#)
  - [cofactors](#), [P-25](#)
  - [det](#), [P-25](#)
  - [dev](#), [P-25](#)
  - [diag](#), [P-25](#)
  - [I](#), [P-25](#)
  - [inv](#), [P-25](#)
  - [mag](#), [P-25](#)
  - [magSqr](#), [P-25](#)
  - [max](#), [P-25](#)
  - [min](#), [P-25](#)
  - [pow](#), [P-25](#)
  - [scale](#), [P-25](#)
  - [skew](#), [P-25](#)
  - [sqr](#), [P-25](#)
  - [symm](#), [P-25](#)
  - [T\(\)](#), [P-25](#)
  - [tr](#), [P-25](#)
  - [transform](#), [P-25](#)
- tensorField class, [P-29](#)
- tensorThirdField class, [P-29](#)
- tetDecomposition utility, [U-88](#)
- tetgenToFoam utility, [U-87](#)
- text box
  - Case Name, [U-182](#)
  - Case Root, [U-182](#)
  - Opacity, [U-159](#)
- thermalProperties*
  - dictionary, [U-50](#)
- thermophysical
  - library, [U-171](#)
- thermophysicalFunctions
  - library, [U-93](#)
- thermophysicalProperties*
  - dictionary, [U-171](#)
- thermoType keyword, [U-171](#)
- time
  - control, [U-104](#)
- time derivative, [P-37](#)
  - first, [P-39](#)
  - second, [P-37](#), [P-39](#)
- time step, [U-24](#)
- timeFormat keyword, [U-105](#)
- timePrecision keyword, [U-105](#)
- timeScheme keyword, [U-107](#)
- timeStep
  - keyword entry, [U-24](#), [U-33](#), [U-104](#)
- tolerance
  - solver, [U-114](#)
  - solver relative, [U-114](#)
- tolerance keyword, [U-52](#), [U-114](#), [U-142](#)
- Toolbars
  - menu entry, [U-159](#)
- tools
  - [adjustPhi](#), [U-91](#)
  - [algorithms](#), [U-91](#)
  - [bound](#), [U-91](#)
  - [compressible](#), [U-91](#)
  - [containers](#), [U-91](#)
  - [db](#), [U-91](#)
  - [dimensionSet](#), [U-91](#)
  - [dimensionedTypes](#), [U-91](#)
  - [fields](#), [U-91](#)
  - [finiteVolume](#), [U-91](#)
  - [global](#), [U-91](#)
  - [incompressible](#), [U-91](#)
  - [interpolations](#), [U-91](#)
  - [matrices](#), [U-91](#)
  - [meshes](#), [U-91](#)
  - [primitives](#), [U-91](#)
  - [wallDist](#), [U-91](#)
- topoSetSource keyword, [U-58](#)
- totalPressure
  - boundary condition, [U-129](#)
- tr
  - tensor member function, [P-25](#)
- trace, *see* tensor, trace
- traction keyword, [U-49](#)
- transform
  - tensor member function, [P-25](#)
- transformPoints utility, [U-88](#)
- transportProperties*
  - dictionary, [U-23](#), [U-39](#), [U-41](#)
- transportProperties* file, [U-58](#)

triple inner product, [P-19](#)  
 triSurface  
   library, [U-92](#)  
 turbDyMFoam solver, [U-84](#)  
 turbFoam solver, [U-19](#), [U-84](#)  
 turbulence  
   dissipation, [U-40](#)  
   kinetic energy, [U-40](#)  
   length scale, [U-41](#)  
   model, [U-41](#)  
 turbulence keyword, [U-174](#)  
 turbulence model  
   RAS, [U-40](#)  
 turbulent flow  
   steady, [P-53](#)  
 turbulentInlet  
   boundary condition, [U-129](#)  
 tutorials  
   breaking of a dam, [U-55](#)  
   lid-driven cavity flow, [U-19](#)  
   stress analysis of plate with hole, [U-45](#)  
*tutorials* directory, [P-45](#), [U-19](#)  
 twoLiquidMixingFoam solver, [U-85](#)  
 twoPhaseEulerFoam solver, [U-85](#)  
 type keyword, [U-124](#), [U-125](#)

## U

U field, [U-24](#)  
 Ucomponents utility, [P-70](#), [U-89](#)  
 UMIST  
   keyword entry, [U-108](#)  
 uncompressed  
   keyword entry, [U-105](#)  
 uncorrected  
   keyword entry, [U-110](#), [U-111](#)  
 uniform model, [U-93](#)  
 uniform keyword, [U-167](#)  
 units  
   base, [U-101](#)  
   of measurement, [P-25](#), [U-101](#)  
   S.I. base, [P-25](#)  
   SI, [U-101](#)  
   Système International, [U-101](#)  
   United States Customary System, [U-101](#)  
   USCS, [U-101](#)  
 Update GUI button, [U-28](#), [U-157](#)  
 uprime utility, [U-89](#)  
 upwind  
   keyword entry, [U-109](#), [U-112](#)  
 upwind differencing, [P-38](#), [U-60](#)  
 USCS units, [U-101](#)  
 Use Parallel Projection button, [U-25](#)  
 Use parallel projection button, [U-159](#)  
 utility

Co, [U-88](#)  
 FoamX, [U-86](#)  
 Lambda2, [U-89](#)  
 Mach, [U-89](#)  
 Pe, [U-89](#)  
 Q, [U-89](#)  
 Rcomponents, [U-89](#)  
 R, [U-89](#)  
 Ucomponents, [P-70](#), [U-89](#)  
 adiabaticFlameT, [U-90](#)  
 ansysToFoam, [U-86](#)  
 attachMesh, [U-87](#)  
 autoPatch, [U-87](#)  
 blockMesh, [U-38](#), [U-86](#), [U-127](#)  
 boxTurb, [U-86](#)  
 ccm26ToFoam, [U-86](#)  
 cellSet, [U-87](#)  
 cfxToFoam, [U-86](#), [U-145](#)  
 checkMesh, [U-87](#), [U-146](#)  
 checkYPlus, [U-89](#)  
 chemkinToFoam, [U-90](#)  
 couplePatches, [U-87](#)  
 createPatch, [U-87](#)  
 decomposePar, [U-79](#), [U-80](#), [U-90](#)  
 deformedGeom, [U-87](#)  
 divU, [U-88](#)  
 engineCompRatio, [U-90](#)  
 engineSwirl, [U-86](#)  
 ensight74FoamExec, [U-164](#)  
 ensight76FoamExec, [U-88](#)  
 enstrophy, [U-88](#)  
 equilibriumCO, [U-90](#)  
 equilibriumFlameT, [U-90](#)  
 estimateScalarError, [U-90](#)  
 extrudeMesh, [U-86](#)  
 faceSet, [U-87](#)  
 flattenMesh, [U-87](#)  
 flowType, [U-88](#)  
 fluentMeshToFoam, [U-87](#), [U-144](#)  
 foamCalc, [U-33](#)  
 foamDataToFluent, [U-88](#), [U-162](#)  
 foamDebugSwitches, [U-90](#)  
 foamInfoExec, [U-90](#)  
 foamMeshToFluent, [U-87](#), [U-162](#)  
 foamToEnight, [U-88](#)  
 foamToFieldview9, [U-88](#)  
 foamToGMV, [U-88](#)  
 foamToVTK, [U-88](#)  
 gambitToFoam, [U-87](#), [U-144](#)  
 gmshToFoam, [U-87](#)  
 icoErrorEstimate, [U-90](#)  
 icoMomentError, [U-90](#)  
 ideasToFoam, [U-145](#)  
 ideasUnvToFoam, [U-87](#)

insideCells, [U-87](#)  
 kivaToFoam, [U-87](#)  
 magGradU, [U-89](#)  
 magU, [U-89](#)  
 mapFields, [U-32](#), [U-38](#), [U-42](#), [U-54](#), [U-86](#),  
     [U-151](#)  
 mergeMeshes, [U-87](#)  
 mirrorMesh, [U-87](#)  
 mixtureAdiabaticFlameT, [U-90](#)  
 momentScalarError, [U-90](#)  
 moveDynamicMesh, [U-87](#)  
 moveEngineMesh, [U-87](#)  
 moveMesh, [U-87](#)  
 mshToFoam, [U-87](#)  
 netgenNeutralToFoam, [U-87](#)  
 objToVTK, [U-87](#)  
 paraFoam, [U-88](#)  
 patchAverage, [U-89](#)  
 patchIntegrate, [U-89](#)  
 patchTool, [U-87](#)  
 plot3dToFoam, [U-87](#)  
 pointSet, [U-87](#)  
 polyDualMesh, [U-87](#)  
 postChannel, [U-90](#)  
 ptot, [U-90](#)  
 reconstructParMesh, [U-90](#)  
 reconstructPar, [U-83](#), [U-90](#)  
 refineMesh, [U-87](#)  
 renumberMesh, [U-87](#)  
 rotateMesh, [U-88](#)  
 sammToFoam, [U-87](#)  
 sampleSurface, [U-90](#)  
 sample, [U-90](#), [U-165](#)  
 scalePoints, [U-148](#)  
 setFields, [U-57](#), [U-58](#), [U-86](#)  
 smapToFoam, [U-88](#)  
 snappyHexMesh, [U-136](#)  
 splitMeshRegions, [U-88](#)  
 splitMesh, [U-88](#)  
 starToFoam, [U-87](#), [U-144](#)  
 stitchMesh, [U-88](#)  
 streamFunction, [U-89](#)  
 stressComponents, [U-89](#)  
 subsetMesh, [U-88](#)  
 tetDecomposition, [U-88](#)  
 tetgenToFoam, [U-87](#)  
 transformPoints, [U-88](#)  
 uprime, [U-89](#)  
 vorticity, [U-89](#)  
 wallGradU, [U-89](#)  
 wallHeatFlux, [U-89](#)  
 wallShearStress, [U-89](#)  
 wdot, [U-90](#)  
 writeCellCentres, [U-90](#)

writeMeshObj, [U-87](#)  
 yPlusLES, [U-89](#)  
 zipUpMesh, [U-88](#)

## V

value keyword, [U-23](#), [U-128](#)  
 valueFraction keyword, [U-128](#)  
 van Leer differencing, [P-38](#)  
 vanLeer  
     keyword entry, [U-109](#)  
 VCR Controls menu, [U-28](#), [U-157](#)  
 vector, [P-16](#)  
     operator, [P-27](#)  
     unit, [P-20](#)  
 vector class, [P-23](#), [U-101](#)  
 vector product, *see* tensor, vector cross product  
 vectorField class, [P-29](#)  
 version keyword, [U-99](#)  
 vertices keyword, [U-22](#), [U-131](#)  
 veryInhomogeneousMixture model, [U-92](#), [U-172](#)  
 View menu, [U-159](#)  
 View Settings  
     menu entry, [U-25](#), [U-159](#)  
 View Settings...  
     menu entry, [U-25](#)  
 viscosity  
     kinematic, [U-23](#), [U-41](#)  
 volField<Type> template class, [P-33](#)  
 vorticity utility, [U-89](#)  
 vtk  
     keyword entry, [U-166](#)  
 vtkFoam  
     library, [U-155](#)  
 vtkPV3Foam  
     library, [U-155](#)

## W

wall  
     boundary condition, [P-63](#), [P-69](#), [U-57](#),  
         [U-126](#)  
 wall  
     keyword entry, [U-127](#)  
 wall function, [U-94](#)  
 wallBuoyantPressure  
     boundary condition, [U-129](#)  
 wallDist tools, [U-91](#)  
 wallFunctionCoeffs keyword, [U-174](#)  
 wallGradU utility, [U-89](#)  
 wallHeatFlux utility, [U-89](#)  
 wallShearStress utility, [U-89](#)  
 water model, [U-93](#)  
 wclean script/alias, [U-73](#)  
 wdot utility, [U-90](#)  
 wedge

- boundary condition, [U-122](#), [U-127](#), [U-135](#)
  - wedge
    - keyword entry, [U-127](#)
  - window
    - Chart Options*, [U-35](#)
    - Color Legend*, [U-30](#)
    - Options*, [U-159](#)
    - Pipeline Browser*, [U-25](#), [U-156](#)
    - Render View Options*, [U-159](#)
    - Render View*, [U-160](#)
    - Seed*, [U-160](#)
  - window panel
    - Annotation*, [U-25](#), [U-159](#)
    - Color Legend*, [U-158](#)
    - Color Scale*, [U-158](#)
    - Display*, [U-25](#), [U-28](#), [U-156](#), [U-157](#)
    - General*, [U-159](#)
    - Information*, [U-156](#)
    - Lights*, [U-159](#)
    - Properties*, [U-26](#), [U-156](#)
    - Region Status*, [U-25](#)
    - Render View*, [U-159](#)
    - Style*, [U-25](#), [U-158](#)
  - Wireframe
    - menu entry, [U-158](#)
  - WM\_ARCH
    - environment variable, [U-74](#)
  - WM\_COMPILE\_OPTION
    - environment variable, [U-74](#)
  - WM\_COMPILER
    - environment variable, [U-74](#)
  - WM\_COMPILER\_BIN
    - environment variable, [U-74](#)
  - WM\_COMPILER\_DIR
    - environment variable, [U-74](#)
  - WM\_COMPILER\_LIB
    - environment variable, [U-74](#)
  - WM\_DIR
    - environment variable, [U-74](#)
  - WM\_JAVAC\_OPTION
    - environment variable, [U-74](#)
  - WM\_LINK\_LANGUAGE
    - environment variable, [U-74](#)
  - WM\_MPLIB
    - environment variable, [U-74](#)
  - WM\_OPTIONS
    - environment variable, [U-74](#)
  - WM\_PROJECT
    - environment variable, [U-74](#)
  - WM\_PROJECT\_DIR
    - environment variable, [U-74](#)
  - WM\_PROJECT\_INST\_DIR
    - environment variable, [U-74](#)
  - WM\_PROJECT\_LANGUAGE
    - environment variable, [U-74](#)
  - WM\_PROJECT\_USER\_DIR
    - environment variable, [U-74](#)
  - WM\_PROJECT\_VERSION
    - environment variable, [U-74](#)
  - WM\_SHELL
    - environment variable, [U-74](#)
  - wmake
    - platforms, [U-71](#)
  - wmake script/alias, [U-69](#)
  - word class, [P-25](#), [P-31](#)
  - writeCellCentres utility, [U-90](#)
  - writeCompression keyword, [U-105](#)
  - writeControl
    - keyword entry, [U-104](#)
  - writeControl keyword, [U-24](#), [U-59](#), [U-104](#)
  - writeFormat keyword, [U-54](#), [U-105](#)
  - writeInterval keyword, [U-24](#), [U-33](#), [U-105](#)
  - writeMeshObj utility, [U-87](#)
  - writeNow
    - keyword entry, [U-104](#)
  - writePrecision keyword, [U-105](#)
- ## X
- x
    - keyword entry, [U-167](#)
  - XiFoam solver, [U-85](#)
  - xmgr
    - keyword entry, [U-105](#), [U-166](#)
  - Xoodles solver, [U-85](#)
  - xyz
    - keyword entry, [U-167](#)
- ## Y
- y
    - keyword entry, [U-167](#)
  - yPlusLES utility, [U-89](#)
- ## Z
- z
    - keyword entry, [U-167](#)
  - zeroGradient
    - boundary condition, [U-128](#)
  - zipUpMesh utility, [U-88](#)
  - zlib-1.2.3
    - library, [U-92](#)