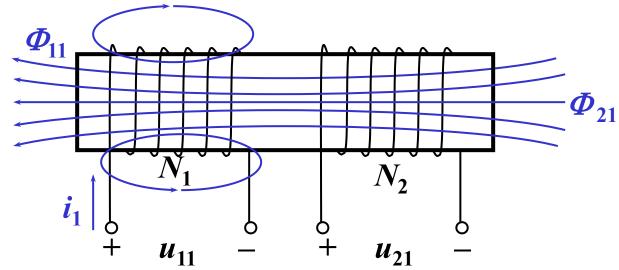
Chapter 13

含磁耦合的电路

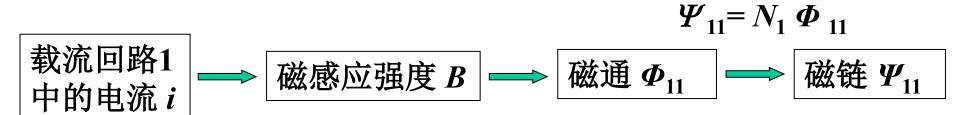
- 13.1 耦合电感 Coupled inductors
- 13. 2 含耦合电感电路的分析 Analysis of coupled circuits
- 13.3 变压器 Transformers

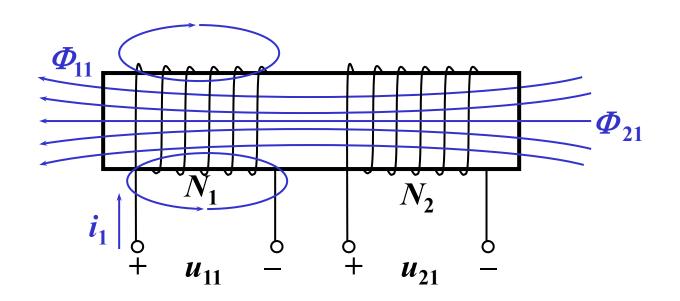
13.1 耦合电感

一、 互感(mutual inductance)和互感电压(mutual voltage)



当线圈1中通入电流i₁时

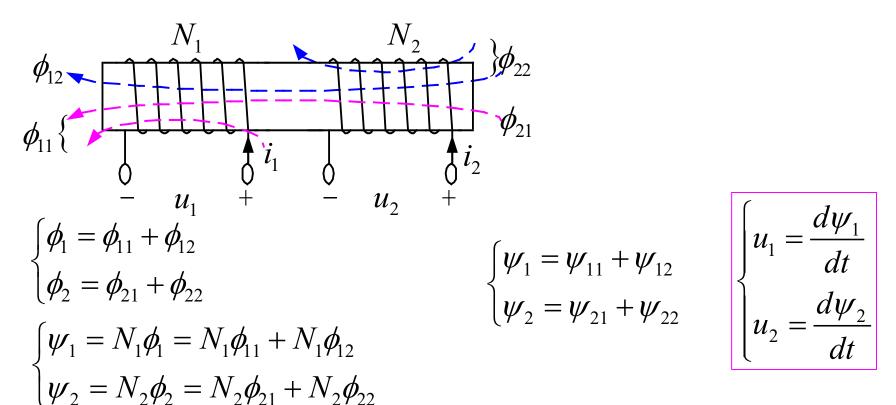




由电磁感应定律(Farady's law)和楞次定律(Lenz's law)可得

$$u_{11} = \frac{d\Psi_{11}}{dt} = N_1 \frac{d\Phi_{11}}{dt}$$
 —自感电压 $u_{21} = \frac{d\Psi_{21}}{dt} = N_2 \frac{d\Phi_{21}}{dt}$ —互感电压

当两个线圈同时通以电流时



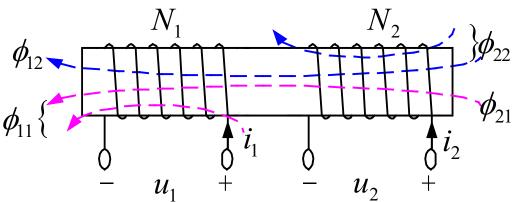
$$\begin{cases} u_{1} = u_{11} + u_{12} = L_{1} \frac{di_{1}}{dt} + M \frac{di_{2}}{dt} \\ u_{2} = u_{21} + u_{22} = M \frac{di_{1}}{dt} + L_{2} \frac{di_{2}}{dt} \end{cases} \begin{cases} \dot{U}_{1} = j\omega L_{1}\dot{I}_{1} + j\omega M\dot{I}_{2} \\ \dot{U}_{2} = j\omega M\dot{I}_{1} + j\omega L_{2}\dot{I}_{2} \end{cases}$$

二、耦合系数(coupling coefficient)k

k表示两个线圈磁耦合(magnetic coupling)的紧密程度。

$$k \stackrel{\text{def}}{=} \frac{M}{\sqrt{L_1 L_2}}$$

可以证明, *k*≤1



全耦合时: $\Phi_{11} = \Phi_{21}$, $\Phi_{22} = \Phi_{12}$

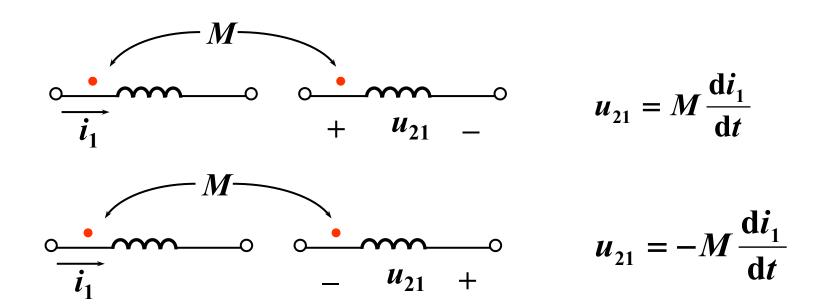
$$\therefore L_{1} = \frac{N_{1}\Phi_{11}}{i_{1}}, L_{2} = \frac{N_{2}\Phi_{22}}{i_{2}}$$

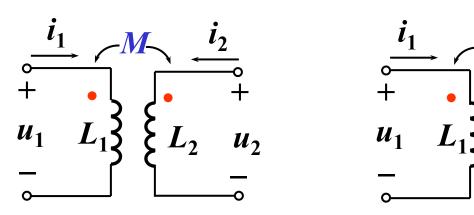
$$M_{21} = \frac{N_{2}\Phi_{21}}{i_{1}}, M_{12} = \frac{N_{1}\Phi_{12}}{i_{2}}$$

 $\therefore M_{12}M_{21} = L_1L_2, M^2 = L_1L_2, k = 1$

三、互感线圈的同名端(Dot convention)

当两个电流分别从这两个端点流入或流出,两个电感的磁链耦合互相加强,为加强型耦合。

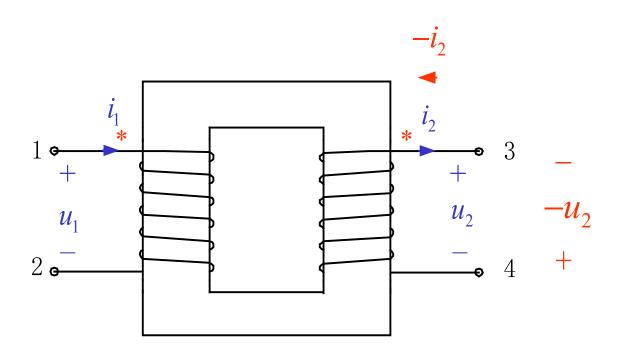




时域形式

$$\begin{cases} u_1 = L_1 \frac{\mathrm{d}i_1}{\mathrm{d}t} + M \frac{\mathrm{d}i_2}{\mathrm{d}t} \\ u_2 = M \frac{\mathrm{d}i_1}{\mathrm{d}t} + L_2 \frac{\mathrm{d}i_2}{\mathrm{d}t} \end{cases} \qquad \begin{cases} u_1 = L_1 \frac{\mathrm{d}i_1}{\mathrm{d}t} - M \frac{\mathrm{d}i_2}{\mathrm{d}t} \\ u_2 = -M \frac{\mathrm{d}i_1}{\mathrm{d}t} + L_2 \frac{\mathrm{d}i_2}{\mathrm{d}t} \end{cases}$$

在正弦交流电路中,其相量形式的电路模型和方程分别为

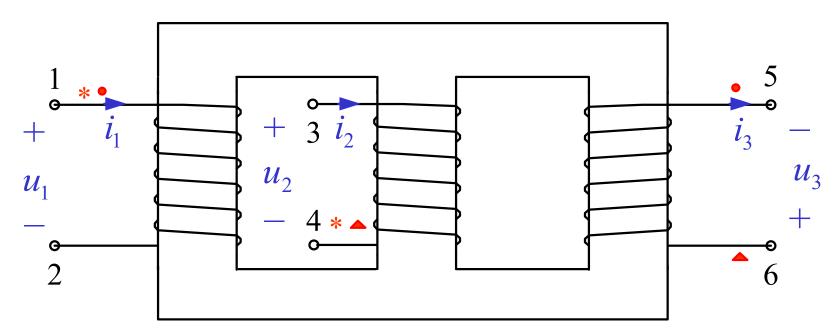


$$u_{1} = L_{1} \frac{di_{1}}{dt} + M \frac{d(-i_{2})}{dt}$$

$$u_{1} = L_{1} \frac{di_{1}}{dt} - M \frac{di_{2}}{dt}$$

$$u_{2} = +M \frac{di_{1}}{dt} + L_{2} \frac{d(-i_{2})}{dt}$$

$$-u_{2} = -M \frac{di_{1}}{dt} + L_{2} \frac{di_{2}}{dt}$$



$$u_{1} = L_{1} \frac{di_{1}}{dt} - M_{12} \frac{di_{2}}{dt} - M_{13} \frac{di_{3}}{dt}$$

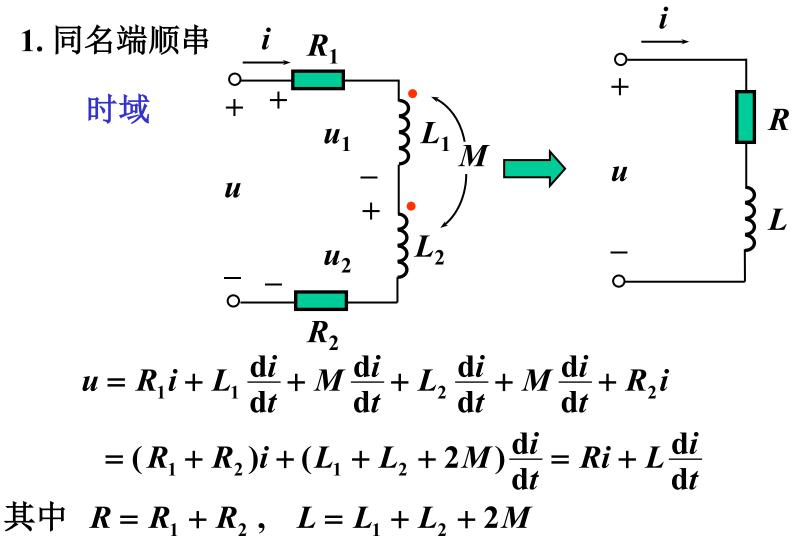
$$u_{2} = L_{2} \frac{di_{2}}{dt} - M_{12} \frac{di_{1}}{dt} - M_{23} \frac{di_{3}}{dt}$$

$$u_{3} = L_{3} \frac{di_{3}}{dt} - M_{13} \frac{di_{1}}{dt} - M_{23} \frac{di_{2}}{dt}$$

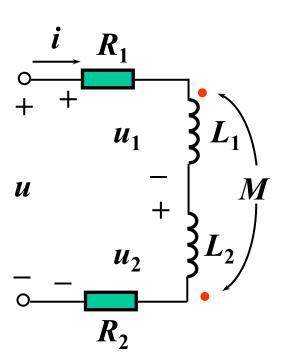
$$\begin{bmatrix} u_{1} \\ u_{2} \\ u_{3} \end{bmatrix} = \begin{bmatrix} L_{1} & -M_{12} & -M_{13} \\ -M_{12} & L_{2} & -M_{23} \\ -M_{13} & -M_{23} & L_{3} \end{bmatrix} \begin{bmatrix} \frac{di_{1}}{dt} \\ \frac{di_{2}}{dt} \\ \frac{di_{3}}{dt} \end{bmatrix}$$

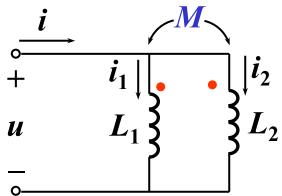
13.2 互感线圈的串并联

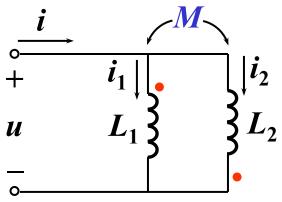
一、互感线圈的串联











$$\begin{array}{c}
\stackrel{i}{\longrightarrow} & \stackrel{M}{\longrightarrow} \\
+ & i_1 \downarrow \\
u & L_1
\end{array}$$

$$\begin{array}{c}
u = L_1 \frac{\mathrm{d}i_1}{\mathrm{d}t} + M \frac{\mathrm{d}i_2}{\mathrm{d}t} \\
u = L_2 \frac{\mathrm{d}i_2}{\mathrm{d}t} + M \frac{\mathrm{d}i_1}{\mathrm{d}t} \\
i = i_1 + i_2
\end{array}$$

解得u, i的关系

$$u = \frac{(L_1 L_2 - M^2)}{L_1 + L_2 - 2M} \frac{\mathrm{d}i}{\mathrm{d}t} \longrightarrow L_{\mathrm{eq}} = \frac{(L_1 L_2 - M^2)}{L_1 + L_2 - 2M} \ge 0$$

故
$$M \leq \sqrt{L_1 L_2}$$

互感小于两元件自感的几何平均值。

解得u, i的关系

$$u = \frac{(L_1 L_2 - M^2)}{L_1 + L_2 + 2M} \frac{di}{dt}$$

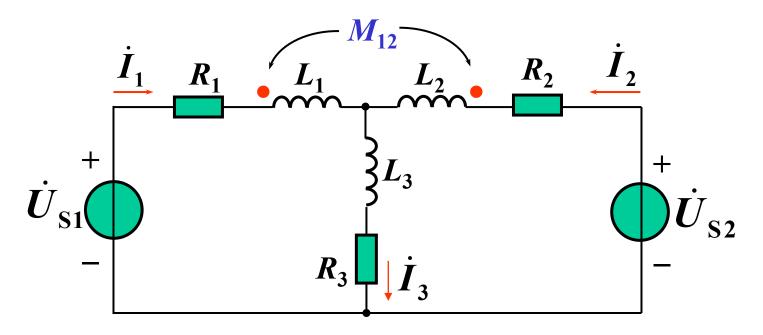
$$L_{eq} = \frac{(L_1 L_2 - M^2)}{L_1 + L_2 + 2M} \ge 0$$

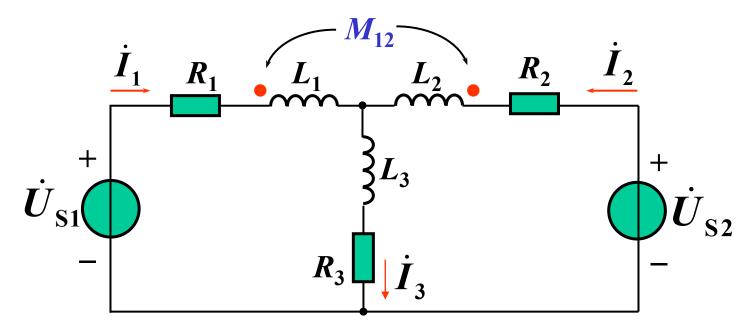
13.3 含耦合电感电路分析

有互感的电路的计算仍属正弦稳态分析,前面介绍的相量分析的的方法均适用。只需注意互感线圈上的电压除自感电压外,还应包含互感电压。

1.网孔分析法

例1 列写下图电路的方程。





网孔分析法:

$$\begin{cases} R_{1}\dot{I}_{1} + j\omega L_{1}\dot{I}_{1} + j\omega M\dot{I}_{2} + j\omega L_{3}\dot{I}_{3} + R_{3}\dot{I}_{3} = \dot{U}_{S1} \\ R_{2}\dot{I}_{2} + j\omega L_{2}\dot{I}_{2} + j\omega M\dot{I}_{1} + j\omega L_{3}\dot{I}_{3} + R_{3}\dot{I}_{3} = \dot{U}_{S2} \\ \dot{I}_{3} = \dot{I}_{1} + \dot{I}_{2} \end{cases}$$

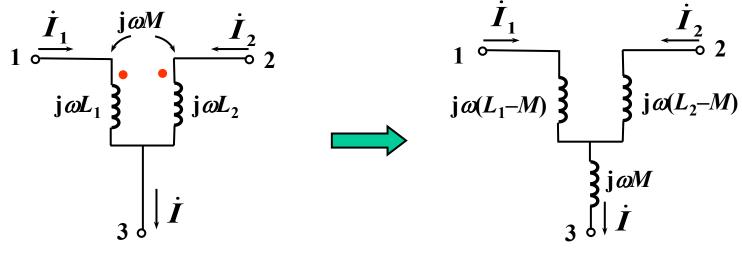
注意:线圈上互感电压的表示式及正负号。

含互感的电路,直接用节点法列写方程不方便。

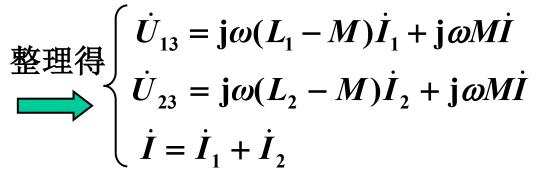
2.互感的去耦等效 (两电感有公共端)

当耦合的两个线圈有一个公共端时,可以等效为非耦合的三个电感,称为去耦等效电路

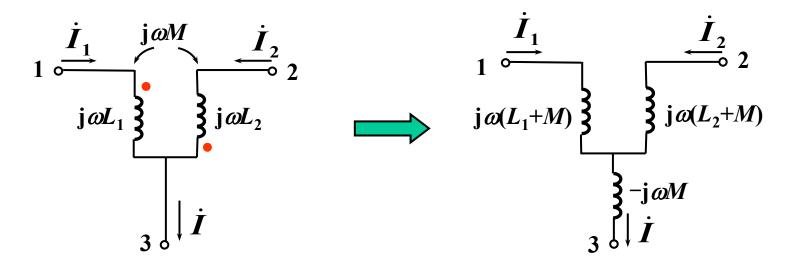
(a) 两个线圈的同名端接在公共端



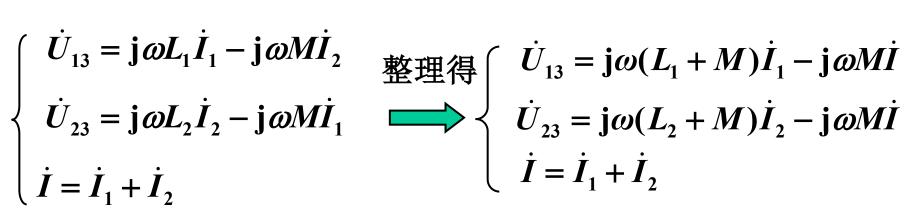
$$\begin{cases} \dot{U}_{13} = \mathbf{j}\omega L_1 \dot{I}_1 + \mathbf{j}\omega M \dot{I}_2 \\ \dot{U}_{23} = \mathbf{j}\omega L_2 \dot{I}_2 + \mathbf{j}\omega M \dot{I}_1 \\ \dot{I} = \dot{I}_1 + \dot{I}_2 \end{cases}$$



(b) 两个线圈的异名端接在公共端

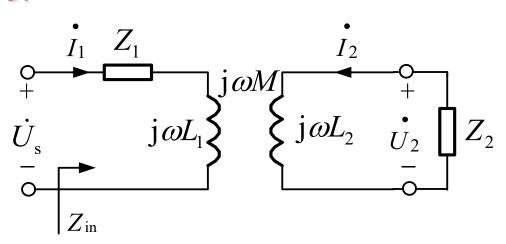


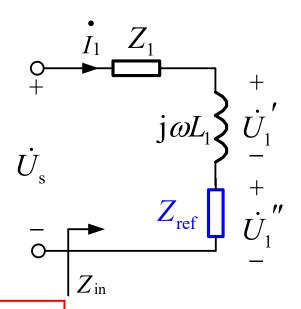
$$\begin{cases} \dot{U}_{13} = \mathbf{j}\omega L_1 \dot{I}_1 - \mathbf{j}\omega M \dot{I}_2 \\ \dot{U}_{23} = \mathbf{j}\omega L_2 \dot{I}_2 - \mathbf{j}\omega M \dot{I}_1 \\ \dot{I} = \dot{I}_1 + \dot{I}_2 \end{cases}$$



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3. 映射阻抗





负载回路对电源回路的影响可用 Z_{ref} 表示,称 Z_{ref} 为负载回路在电源回路的映射阻抗。

$$Z_{\text{in}} = \frac{\dot{U}_{\text{S}}}{\dot{I}_{1}} = Z_{1} + \frac{\dot{j}\omega L_{1}\dot{I}_{1} \pm \dot{j}\omega M\dot{I}_{2}}{\dot{I}_{1}} = (Z_{1} + \dot{j}\omega L_{1}) + (\pm \dot{j}\omega M)\frac{\dot{I}_{2}}{\dot{I}_{1}}$$

$$\dot{U}_2 = j\omega L_2 \dot{I}_2 \pm j\omega M \dot{I}_1 = -Z_2 \dot{I}_2$$

$$\frac{I_2}{\dot{I}_1} = -\frac{(\pm j\omega M)}{Z_2 + j\omega L_2}$$

$$Z_{\text{in}} = (Z_1 + j\omega L_1) + \frac{(\omega M)^2}{Z_2 + j\omega L_2}$$

$$= Z_{11} + \frac{(\omega M)^2}{Z_{22}}$$

$$= Z_{11} + Z_{\text{ref}}$$

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3. 映射阻抗

$$\dot{U}_{s} = [Z_{11} + \frac{(\omega M)^{2}}{Z_{22}}]\dot{I}_{1}$$

$$100 \angle 0^{\circ} = [(20 + j30) + \frac{10^{2}}{(10 + 10 + j20)}]\dot{I}_{1}$$

$$10\dot{I}_{2} + 10\dot{I}_{2} + (j20\dot{I}_{2} - j10\dot{I}_{1}) = 0$$

$$j10\Omega \longrightarrow j10\Omega \longrightarrow j10\Omega \longrightarrow j10\Omega$$

$$j20\Omega \longrightarrow j10\Omega \longrightarrow j20\Omega$$

$$Z_{eq} \longrightarrow i2$$

如何先求 \dot{I}_2 ?

$$\dot{U}_{\text{oc}} = j\omega M \dot{I}_{1} = j\omega M \frac{\dot{U}_{\text{s}}}{Z_{11}} = j10 \times \frac{100 \angle 0^{\circ}}{20 + j30}$$

$$Z_{\text{eq}} = (10 + j20) + \frac{10^{2}}{20 + j30} \qquad \dot{I}_{2} = \frac{\dot{U}_{\text{oc}}}{10 + Z_{\text{eq}}}$$

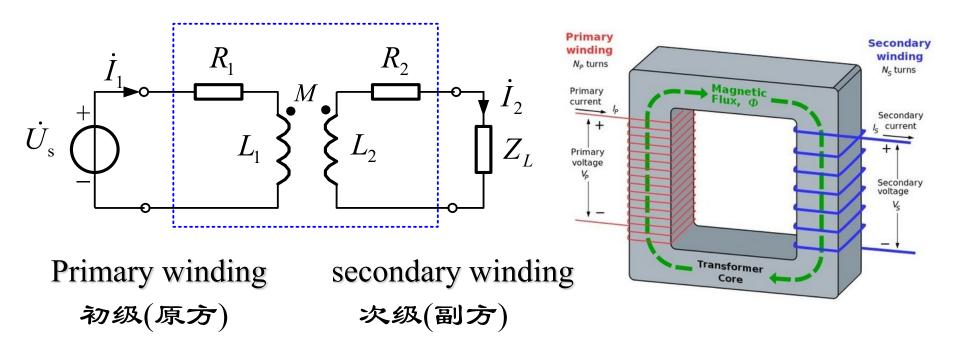
 $20\dot{I}_{1} + j30\dot{I}_{1} - j10\dot{I}_{2}$ $= 100 \angle 0^{\circ}$

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13.4 变压器 Transformers

1. 变压器模型



• 交流变压、变流

• 电隔离

• 传送功率

• 阻抗匹配

2. 全耦合变压器

$$\begin{cases} \dot{U}_1 = j\omega L_1 \dot{I}_1 + j\omega M \dot{I}_2 \\ \dot{U}_2 = j\omega L_2 \dot{I}_2 + j\omega M \dot{I}_1 \end{cases}$$

全耦合时 $M = \sqrt{L_1 L_2}$, k = 1

$$\dot{I}_{1} = \frac{\dot{U}_{2} - j\omega L_{2}\dot{I}_{2}}{j\omega M}$$

$$\dot{U}_{1} = \frac{L_{1}}{M}(\dot{U}_{2} - j\omega L_{2}\dot{I}_{2}) + j\omega M\dot{I}_{2} = \frac{L_{1}}{M}\dot{U}_{2}$$

$$\frac{\dot{U}_{1}}{\dot{U}_{2}} = \sqrt{\frac{L_{1}}{L_{2}}}$$

$$\boldsymbol{\Phi} = \boldsymbol{\Phi}_{11} + \boldsymbol{\Phi}_{22}$$

$$u_1 = N_1 \frac{\mathrm{d}\Phi}{\mathrm{d}t} \quad , \quad u_2 = N_2 \frac{\mathrm{d}\Phi}{\mathrm{d}t}$$

$$\frac{u_1}{u_2} = \frac{N_1}{N_2} = n$$

则

$$\frac{u_1}{u_2} = \frac{N_1}{N_2} = n = \frac{L_1}{M} = \frac{M}{L_2} = \sqrt{\frac{L_1}{L_2}}$$

全耦合变压器的电压、电流关系

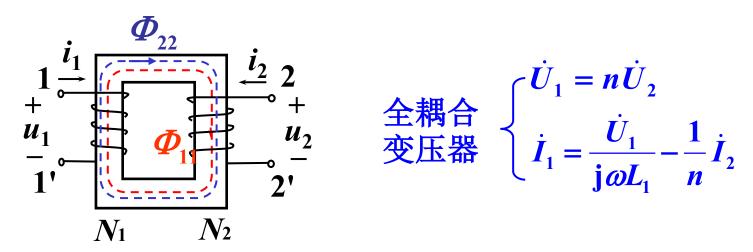
上州日文
$$\hat{U}_1 = n\hat{U}_2$$

$$\hat{I}_1 = \frac{\hat{U}_1 - j\omega M \hat{I}_2}{j\omega L_1} = \frac{\hat{U}_1}{j\omega L_1} - \frac{j\omega M}{j\omega L_1} \hat{I}_2 = \frac{\hat{U}_1}{j\omega L_1} - \frac{1}{n} \hat{I}_2$$

$$\frac{2023/5/15}{2023} = \frac{1}{2} \hat{U}_1 + \frac{1}{2} \hat{U}_2 + \frac{1}{2} \hat{U}_3 + \frac{1}{2} \hat{U}_4 + \frac{1}{2} \hat{U}_4 + \frac{1}{2} \hat{U}_5 +$$

22

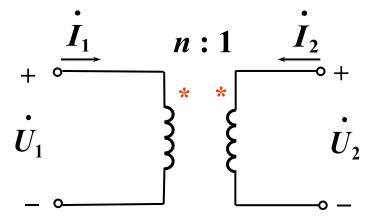
3. 理想变压器



当 L_1 , M, $L_2 \rightarrow \infty$, L_1/L_2 比值不变 (磁导率 $\mu \rightarrow \infty$) ,则有

$$\begin{cases} \dot{U}_1 = n\dot{U}_2 \\ \dot{I}_1 = -\frac{1}{n}\dot{I}_2 \end{cases}$$

理想变压器的元件特性



理想变压器的电路模型

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$$k=1$$
 $\mu o \infty$ $L_1, L_2, M o \infty$ $+$ $R_1=0=R_2$ 没有损耗 u_1

$$u_1 = \frac{d\psi_1}{dt} = \frac{d(N_1\phi)}{dt} = N_1 \frac{d\phi}{dt}$$
$$u_2 = \frac{d\psi_2}{dt} = \frac{d(N_2\phi)}{dt} = N_2 \frac{d\phi}{dt}$$

$$\oint \vec{H} \cdot d\vec{l} = \sum i = N_1 i_1 + N_2 i_2 = 0$$

$$\frac{u_1}{u_2} = \frac{N_1}{N_2} = n$$

$$i_1 = -\frac{N_2}{N_1}i_2 = -\frac{1}{n}i_2$$

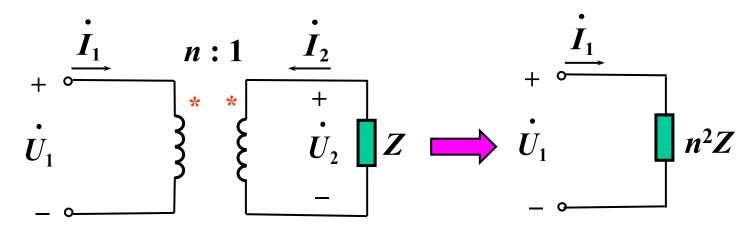
$$\begin{array}{c}
i_1 \\
u_1 \\
\mu >> \mu_0
\end{array}$$

$$H=0$$

$$u_1 i_1 + u_2 i_2 = 0$$

理想变压器的性质:

(a) 阻抗变换性质



$$\frac{\dot{U}_1}{\dot{I}_1} = \frac{n\dot{U}_2}{-1/n\dot{I}_2} = n^2(-\frac{\dot{U}_2}{\dot{I}_2}) = n^2Z$$

(b) 功率传输

理想变压器的特性方程为代数关系,因此无记忆作用。

$$\begin{cases} u_{1} = nu_{2} \\ i_{1} = -\frac{1}{n}i_{2} \\ p = u_{1}i_{1} + u_{2}i_{2} = u_{1}i_{1} + \frac{1}{n}u_{1} \times (-ni_{1}) = 0 \end{cases}$$

由此可以看出,理想变压器既不储能,也不耗能,在电路中只起传递信号和能量的作用。

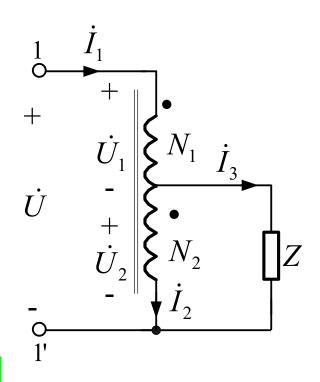
4. 自耦变压器

自耦变压器是闭合铁心上只有一个线圈,从线圈中间接出一个抽头,线圈的一部分为一次绕组(或二次绕组),线圈的全部为二次绕组(或一次绕组)。

$$\frac{\dot{U}_1}{\dot{U}_2} = \frac{N_1}{N_2} \longrightarrow \frac{\dot{U}}{\dot{U}_2} = \frac{N_1 + N_2}{N_2}$$

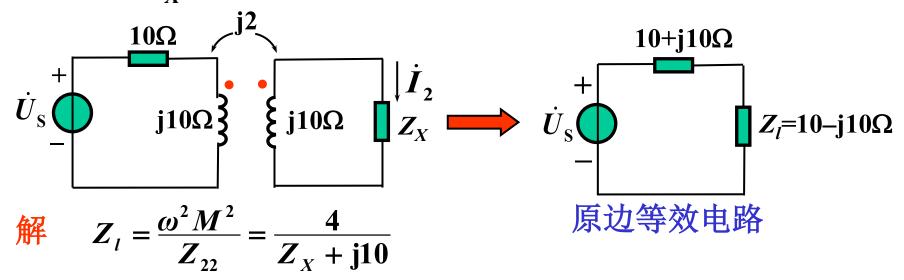
$$\frac{\dot{I}_{1}}{\dot{I}_{2}} = -\frac{N_{2}}{N_{1}} \longrightarrow \frac{\dot{I}_{1}}{\dot{I}_{3}} = \frac{\dot{I}_{1}}{\dot{I}_{1} - \dot{I}_{2}} = \frac{N_{2}}{N_{1} + N_{2}}$$

推导要点:能量守恒或者安培环路定理。



例1 已知 U_S =20 V,原边引入阻抗 Z_l =10-j10Ω。

求: Z_X ,并求负载获得的有功功率。



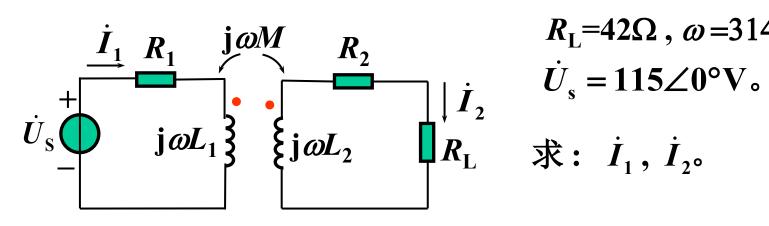
$$\therefore Z_X = 0.2 + j9.8\Omega$$

此时负载获得的功率 $P = P_{R_{\parallel}} = (\frac{20}{10+10})^2 R_l = 10 \text{ W}$ 本例实际是最佳匹配状态

$$Z_{l} = Z_{11}^{*}, \qquad P = \frac{U_{S}^{2}}{4R} = 10 \text{ W}$$

变压器是否消耗功率?

例2 已知 L_1 =3.6H, L_2 =0.06H, M=0.465H, R_1 =20 Ω , R_2 =0.08 Ω ,



$$R_{\rm L}$$
=42 Ω , ω =314rad/s, $\dot{U}_{\rm s}$ = 115 \angle 0°V.

原边等效电路

$$Z_{11} = R_1 + j\omega L_1 = 20 + j1131\Omega$$

$$Z_{22} = R_2 + R_L + j\omega L_2 = 42.08 + j18.85\Omega$$

$$Z_{11} = R_1 + j\omega L_1 = 20 + j1131\Omega$$

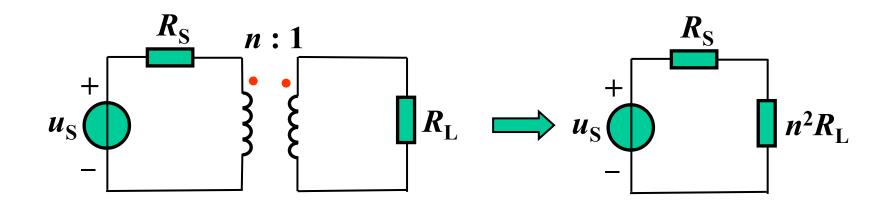
$$Z_{22} = R_2 + R_L + j\omega L_2 = 42.08 + j18.85\Omega$$

$$Z_{11} = \frac{X_M^2}{Z_{22}} = 464\angle - 24.1^{\circ} \Omega$$

$$\dot{I}_1 = \frac{U_S}{Z_{11} + Z_I} = 0.111 \angle - 64.9^{\circ} \text{ A} \qquad \dot{I}_2 = \frac{j\omega M \dot{I}_1}{Z_{22}} = 0.351 \angle 1^{\circ} \text{ A}$$

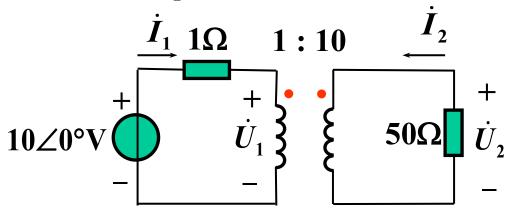
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例3 已知电源内阻 $R_S=1k\Omega$,负载电阻 $R_L=10\Omega$ 。为使 R_L 上获得最大功率,求理想变压器的变比n。



解 当 $n^2R_{
m L}$ = $R_{
m S}$ 时匹配,即 $10n^2$ =1000 $\therefore n^2$ =100, n=10.

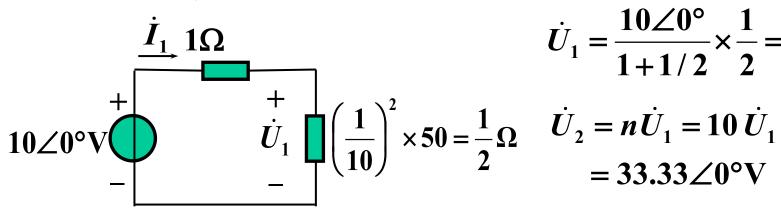




方法1 列方程

$$\begin{cases}
1 \times \dot{I}_{1} + \dot{U}_{1} = 10 \angle 0^{\circ} \\
50 \dot{I}_{2} + \dot{U}_{2} = 0 \\
\dot{U}_{1} = \frac{1}{10} \dot{U}_{2} \\
\dot{I}_{1} = -10 \dot{I}_{2}
\end{cases}$$
解得

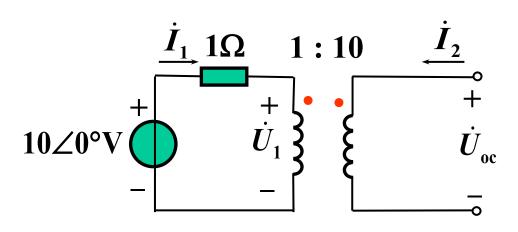
方法2 阻抗变换



$$\dot{U}_1 = \frac{10 \angle 0^{\circ}}{1 + 1/2} \times \frac{1}{2} = \frac{10}{3} \angle 0^{\circ} V$$

$$\dot{U}_2 = n\dot{U}_1 = 10\dot{U}_1$$

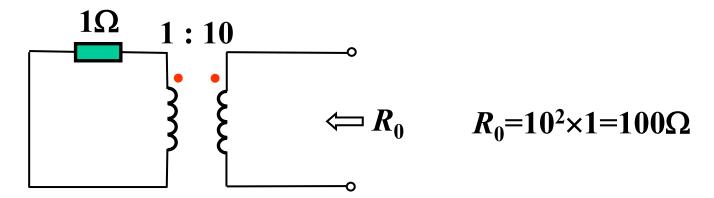
方法3 戴维南等效



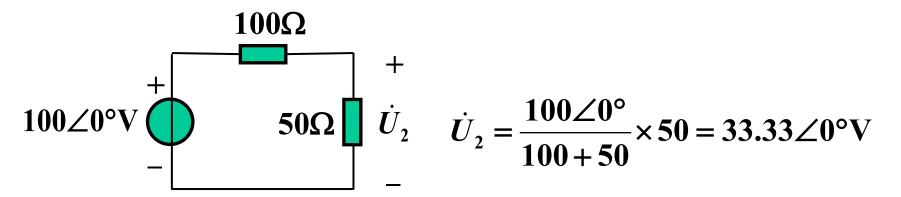
(1) 求 $\dot{U}_{\rm oc}$

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(2) 求 R_0



戴维南等效电路



作业

• 13.2节: 13-6

• 13.3节: 13-9

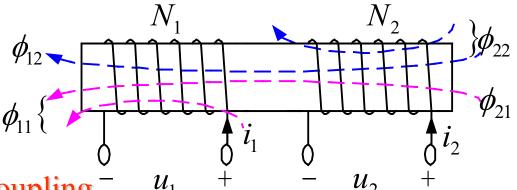
• 13.4节: 13-15

• 13.5节: 13-20

Self-inductance and mutual inductance 3. 自感和互感

$$L_1$$
, L_2 ——Self-inductance

——Mutual inductance



Coefficient of coupling 4. 耦合系数

$$k = \frac{M}{\sqrt{L_1 L_2}} \quad (0 \le k \le 1)$$

$$k = \frac{1}{\sqrt{L_1 L_2}} \quad (0 \le k \le 1)$$

$$k = \frac{M}{\sqrt{L_1 L_2}} = \sqrt{\frac{M_{12} M_{21}}{L_1 L_2}} = \sqrt{\frac{\frac{\psi_{12} \cdot \psi_{21}}{i_2}}{\frac{i_2}{i_1} \cdot \frac{\psi_{22}}{i_2}}}$$

$$= \sqrt{\frac{N_1 \phi_{12} \cdot N_2 \phi_{21}}{N_1 \phi_{11} \cdot N_2 \phi_{22}}} = \sqrt{\frac{\phi_{12} \cdot \phi_{21}}{\phi_{11} \cdot \phi_{22}}} \le 1$$
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$$\begin{cases} \psi_{1} = \psi_{11} + \psi_{12} \\ \psi_{2} = \psi_{21} + \psi_{22} \end{cases}$$

$$= L_{1}i_{1} + M_{12}i_{2}$$

$$= M_{21}i_{1} + L_{2}i_{2}$$

$$\begin{cases} \psi_{1} = N_{1}\phi_{11} + N_{1}\phi_{12} \\ \psi_{2} = N_{2}\phi_{21} + N_{2}\phi_{22} \\ 35 \end{cases}$$