

Chapter 1

TD1

1.1 Eulerian/Lagrangian cinematics.

We consider the following velocity field: $\mathbf{v} = (\alpha x, -\alpha y, 0)$.

1.1.1

To check whether it is compressible we compute:

$$\nabla \cdot \mathbf{v} = (\alpha, -\alpha, 0) \cdot \vec{0}$$

To check whether it is irrotational we compute:

$$\boldsymbol{\omega} = \nabla \times \mathbf{v} = 0$$

1.1.2

The streamlines follow the following:

$$d\mathbf{l} \times \mathbf{v} = 0$$

1.1.3

1.1.4

1.1.5

We now consider the following flow:

$$\mathbf{v} = \begin{pmatrix} v_0 e^{kz} \sin(\omega t - kx) \\ 0 \\ v_0 e^{kz} \cos(\omega t - kx) \end{pmatrix}$$

a)

We have that:

$$\nabla \cdot \mathbf{u} = v_0 e^{kz} (-k \cos(\omega t - kx) + k \cos(\omega t - kx)) = 0$$

And:

$$\nabla \times \mathbf{u} = \mathbf{e}_y (v_0 e^{kz} (k \sin(\omega t - kx) - (-1)(-k) \sin(\omega t - kx))) = 0$$

The streamlines then respect:

$$d\mathbf{l} \times \mathbf{v} = 0 \Leftrightarrow dz v_0 e^{kz} \sin(\omega t - kx) - dx v_0 e^{kz} \cos(\omega t - kx) = 0$$

Which simplifies:

$$dz \sin(\omega t - kx) - dx \cos(\omega t - kx) = 0 \Leftrightarrow z = \int \tan^{-1}(\omega t - kx) dx = -\frac{\log(|\sin(kx - t\omega)|)}{k} + c$$

b)

We have the following: $v_0 \ll \frac{\omega}{k}$.

1.1.6

Streaklines follow the following PDE:

$$\begin{cases} \frac{\partial x_p}{\partial t} = v_0 e^{kz} \sin(\omega t - kx) \\ \frac{\partial z_p}{\partial t} = v_0 e^{kz} \cos(\omega t - kx) \end{cases}$$

Hence at the first order we can write:

$$x_p(t) = x_0 + \varepsilon X_1 + \varepsilon^2 X_2 + \dots \quad \& \quad z_p(t) = z_0 + \varepsilon Z_1 + \varepsilon^2 Z_2 + \dots$$

Then the velocity field can be written as:

$$\mathbf{v}(x_p(t), z_p(t), t) = \underbrace{\mathbf{v}(x_0, z_0, t)}_{\sim \varepsilon} + \underbrace{\frac{\partial \mathbf{v}}{\partial x} (x - x_0) + \frac{\partial \mathbf{v}}{\partial z} (z - z_0)}_{\sim \varepsilon^2}$$

Then at the first order we get:

$$\begin{cases} \varepsilon \dot{X}_1 = v_0 e^{kz_0} \sin(\omega t - kx_0) \\ \varepsilon \dot{Z}_1 = v_0 e^{kz_0} \cos(\omega t - kx_0) \end{cases} \Leftrightarrow \begin{cases} \dot{x}_1 = -\frac{v_0}{\omega} e^{kz_0} \cos(\omega t - kx_0) \\ \dot{z}_1 = \frac{v_0}{\omega} e^{kz_0} \sin(\omega t - kx_0) \end{cases}$$

So we observe a circular trajectory. Now at second order we get:

$$\begin{cases} \dot{x}_2 = v_0 e^{kz_0} k (-x_1 \cos(\omega t - kx_0) + z_1 \sin(\omega t - kx_0)) \\ \dot{z}_2 = v_0 e^{kz_0} k (x_1 \sin(\omega t - kx_0) + z_1 \cos(\omega t - kx_0)) \end{cases} \Leftrightarrow \begin{cases} \dot{x}_2 = v_0^2 e^{2kz_0} \frac{k}{\omega} \\ \dot{z}_2 = 0 \end{cases}$$

We therefore obtain Stokes' drift.

1.2 Dimensional Analysis.

1.2.1

a)

The parameters of our problem are: $\omega [s^{-1}]$, $k [m^{-1}]$, $g [m.s^{-2}]$, $h [m]$

b)

By dimensional analysis we guess:

$$\omega(k) \propto \sqrt{gk}$$

c)

We can use the above formula only if the height is negligible. Otherwise we would have to add a corrective term:

$$\omega(k) \propto \sqrt{gk} f(k \cdot h)$$

Now making asymptotic analysis we know that:

$$\lim_{h \rightarrow +\infty} f(kh) = 1 \quad \& \quad \lim_{h \rightarrow 0} f(kh) = 0$$

From physical intuition we also expect the system to respond linearly with kh close to 0 hence a good candidate for our general dispersion relation would be something of the form:

$$\omega(k) \propto \sqrt{gk} \tanh(\alpha kh)$$

d)

Similarly when the only force we are considering is surface tension we then have the following parameters:

$$\omega [s^{-1}], k [m^{-1}], \gamma [N.m^{-1}], h [m], \rho [kg.m^{-3}]$$

We then can guess something of the form:

$$\Pi_1 = kh, \quad \Pi_2 = \frac{\rho \omega^2 k^3}{\gamma}$$

Pi's theorem then gives:

$$\Pi_2 = f(\Pi_1) \Leftrightarrow \omega^2 = \frac{\gamma}{\rho k^3} f(kh)$$

So in deep water we guess:

$$\omega^2 = \frac{\gamma}{\rho k^3}$$

1.2.2

The parameters of the problem are:

$$R [m], t [s], E[m.s^{-2}]$$