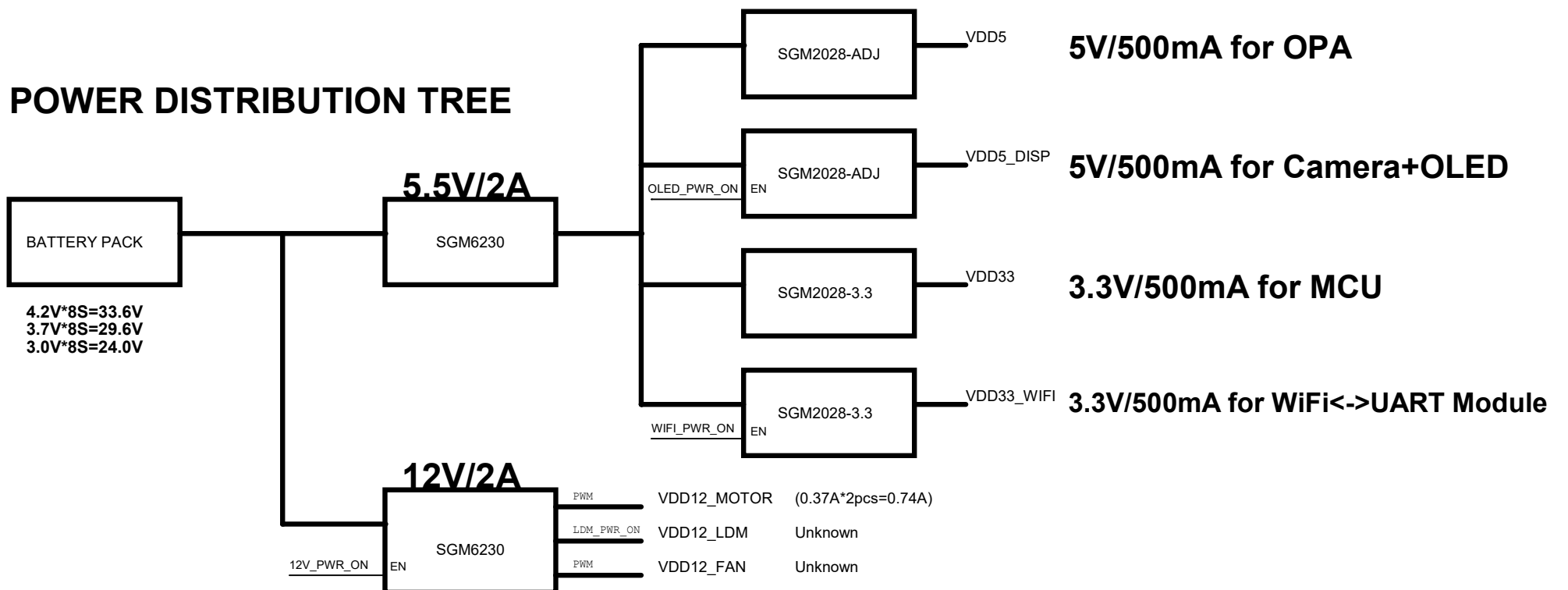


PAGE-0: OVERVIEW
PAGE-1: POWER SUPPLY
PAGE-2: MCU + KEYS
PAGE-3: CONSTANT CURRENT ADC
PAGE-4: MOTOR + FAN DRIVER
PAGE-5: PHYSICAL CONNECTORS



Title		
0-OVERVIEW		
Size	Document Number	Rev
A	FLASH LIGHT	A2
Date:	Thursday, June 02, 2022	Sheet 0 of 6

18650 Battery Pack (3.7V~4.2V)*8S=29.6V~33.6V

The charging cut-off voltage of the 3.7V battery is 4.2V and the discharge cut-off voltage is 3.0V.
4.2V*8S=33.6V, 3.7V*8S=29.6V, 3.0V*8S=24.0V

The minimum current of zener is 1mA,
but we use 1.5mA in calculations to ensure its in Zener mode completely.

Pre-Power Supply 4.7V@10mA

I_{zk}=I_{load} (Suppose I_{zk}=1.5mA, Predict Load=10.5mA)
[U_{min}-4.7V]/12mA < R < [U_{max}-4.7V]/12mA
[24.0-4.7]/12mA < R < [33.6-4.7]/12mA
1608 < R < 2408
Here choose E96,1%,2K-OHMS

OVC>1A

I_{zk}=1mA
[U_{min}-4.7V]/1mA < R < [U_{max}-4.7V]/1mA
[24.0-4.7]/1mA < R < [33.6-4.7]/1mA
19.3K < R < 28.9K
Mid-Point: (29.6-4.7)/1mA=24.9K
Waster current I=29.6V/24.9K=1.2mA

Disable in low-power-consumption requirements.

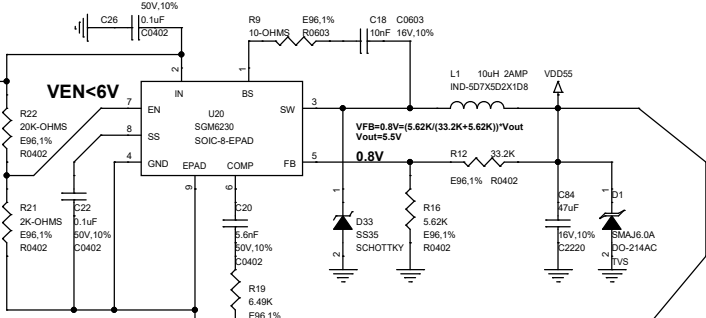
UVP<24V

I_{zk}=1mA
[U_{min}-24V]/1mA < R < [U_{max}-24V]/1mA
[24.0-24]/1mA < R < [33.6-24]/1mA
100 < R < 9600
Mid-Point: (29.6-24)/1mA=5600

OVP>36V
Action Voltage: 38V

I_{zk}=1mA
[U_{min}-38V]/1mA < R < [U_{max}-38V]/1mA
[24.0-38]/1mA < R < [33.6-38]/1mA
100 < R < 9600
Mid-Point: (29.6-38)/1mA=5600

VEN=2K/(20K+2K)*Vin=2.69V~3.0545V

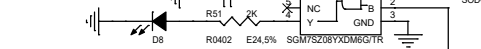


I=1mA
[U_{min}-24V]/10mA < R < [U_{max}-24V]/10mA
U_{min}=24.0V U_{max}=33.6V
[24.0-24.0]/10mA < R < [33.6-24.0]/10mA
0 < R < 960

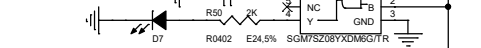
Here choose E96,1%,825-ohms
Verification:
(33.6-24)/825=11.6mA
(29.6-24)/825=6.8mA
(25-24)/825=1.2mA
(24.0-24)/825=0.12mA

Equation: R1=R2*(Vout/1.206V-1)
Choose R2=47.5K-ohms
So R1=47.5K*(5V/1.206V-1)=149.432K
We choose 150K from EIA E96 resistor codes,
So verification below
Vout=1.206*(R1/R2+1)=5.01442V

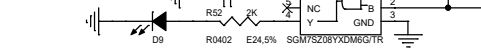
Over Current Indicator



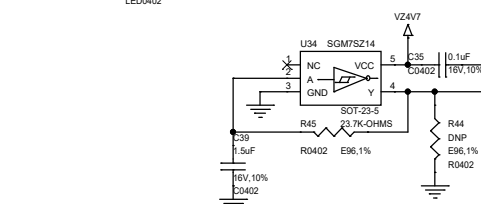
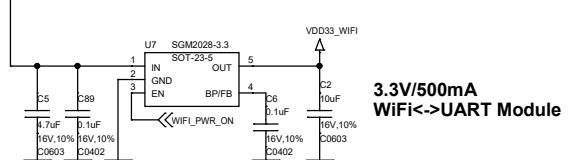
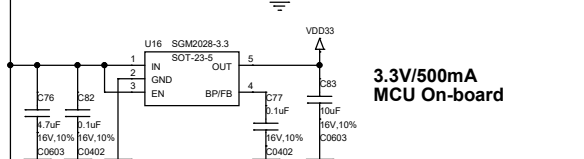
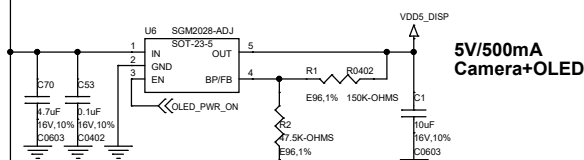
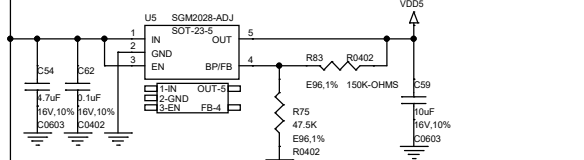
Under Voltage Indicator



Over Voltage Indicator

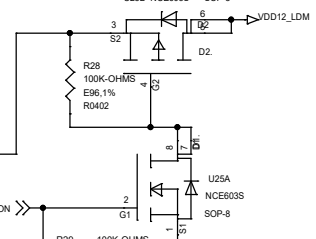
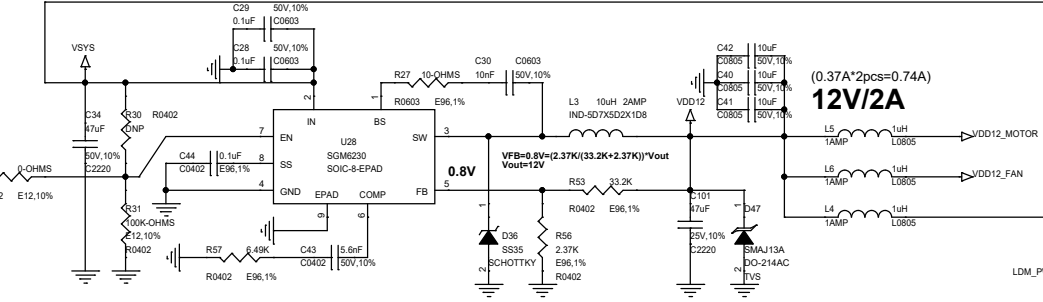


VIH=0.75Vcc(MIN)=3.525V
VIL=0.25Vcc(MAX)=1.175V



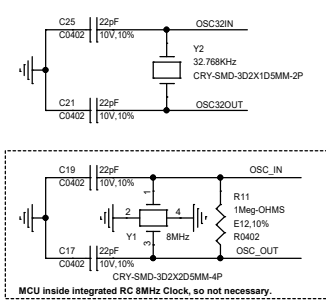
f=0.8RC
we expect 5Hz frequency, so choose R=100K-OHMS, then
5Hz=0.8/(100K*10uF)
C=0.000016F=1.6uF
choose 1.5uF from EIA E96,1%
verification below:
f=0.8/(100K*1.5uF)=0.8/150=5.33Hz

(0.37A*2pcs=0.74A)
12V/2A



500mA, Ultra-Low Dropout, Low Power, RF Linear Regulator
Input Voltage: 2.5V(Min)-5.5V(Max)
Dropout Voltage
54-90mV(Max)@I_{out}=100mA
162-270mV(Max)@I_{out}=300mA
270-420mV(Max)@I_{out}=500mA

Title			1-POWER-SUPPLY
Size	A3	Document Number	FLASH LIGHT
Date:	Thursday, June 02, 2022	Sheet	1 of 6



MCU inside integrated RC 8MHz Clock, so not necessary.

Selected boot source	BOOT1	BOOT0
Main Flash Memory	X	0
Boot loader	0	1
On-chip SDRAM	1	1

Motor#1 Position Min&Max Limit Switch

Motor#2 Position Min&Max Limit Switch

DEBUG LEDx2

UART0: For Debug TTL-USB.

UART1: To communicate with Laser Distance Module.

UART2: To communicate with Display module.

UART3: To communicate with WiFi-UART module.

UART4: To communicate with Laser Module.

UART0 For Debug TTL-USB

UART2 For Display Module

UART3 For WiFi-UART Module

UART4 For Laser Module

KEY ADC1

KEY ADC1	KEY ADC2	VOLTAGE
IO CON Flash	IO SHOT SW1	387.7mV±100mV
IO Day Night	IO SHOT SW2	1.047V±100mV
IO FL ADD	IO SET	1.641V±100mV
IO FL SUB	IO RESERVE2	2.306V±100mV
IO RESERVE1		
NO KEYS	NO KEYS	3.3V±100mV

VOLTAGE AXIS

ARM Cortex-M4 32-bit MCU

ADC01_IN14

ADC01_IN15

ADC01_IN14

ADC01_IN15

ADC01_IN14

ADC01_IN15

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ADC01_IN14

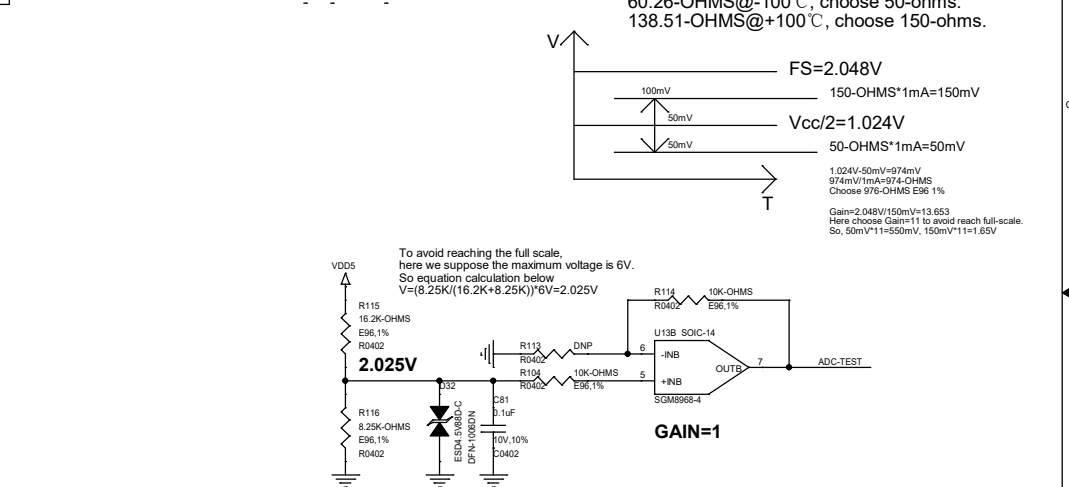
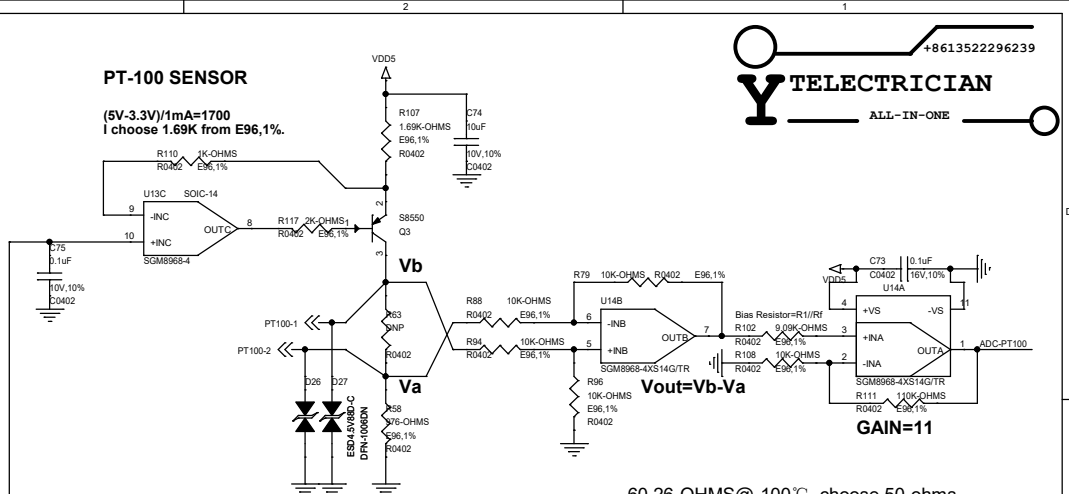
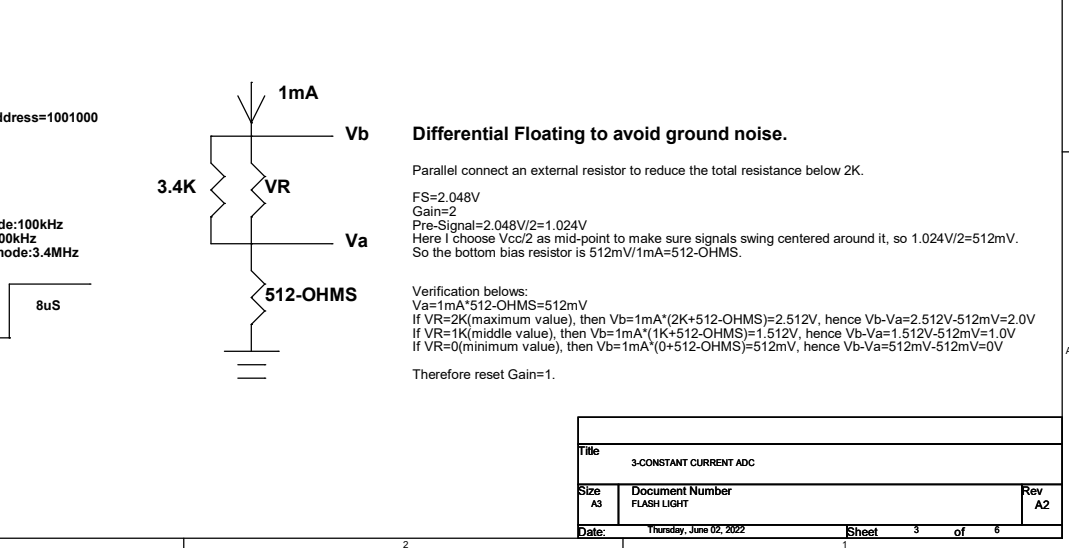
ADC01_IN15

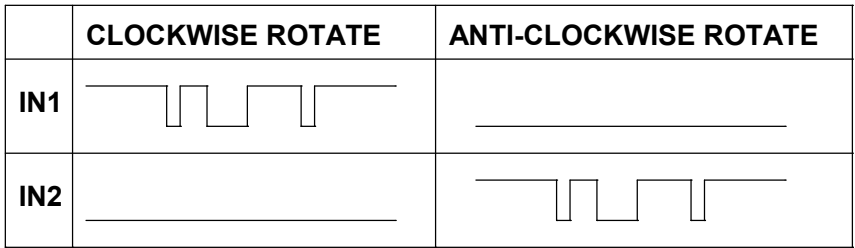
ADC01_IN14

ADC01_IN15

ADC01_IN14

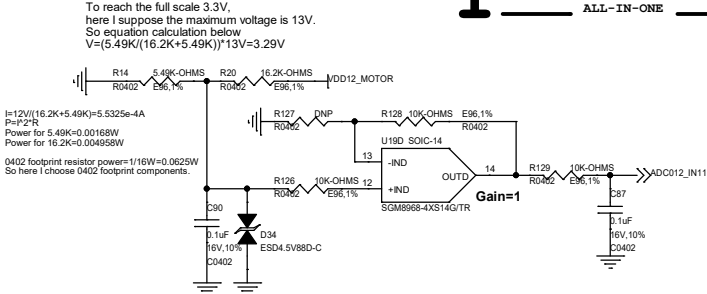
ADC01_IN15

[illegible]

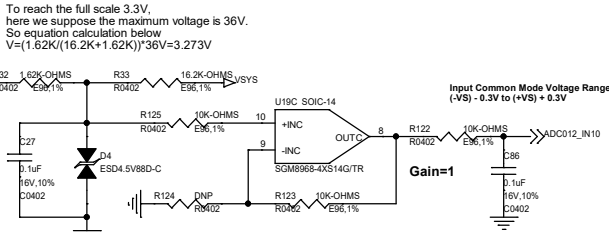


Rotate speed depends on frequency.
Torque depends on duty cycle.

DCU10025P12
Rated Voltage: 12V
No-Load Current: 4.6mA
Maximum continous current: 0.188A
Locked rotor current: 0.37A
Coil resistance: 32.4-OHMS



SGM8968-4 (-40°C to +125°C)
10MHz, High Precision, Low Noise,Rail-to-Rail I/O, CMOS Operational Amplifiers



NON-INVERTING AMPLIFIER
Gain=1+Rf/Rin
Input Impedance=Rf//Rin

Here I choose 0.68-OHMS shunt resistor, analysis below:
No-load condition, 0.68R*4.6mA=3.128mV (After Gain, 3.128mV*9=28.152mV)
Continuous condition, 0.68R*0.188A=127.84mV (After Gain, 127.84mV*9=1.15V)
Lock rotor condition, 0.68R*0.37A=251.6mV (After Gain, 251.6mV*9=2.264V)
Because Full-scale of ADC is 2.048V, Gain=2.048V/251.6mV=8.1399

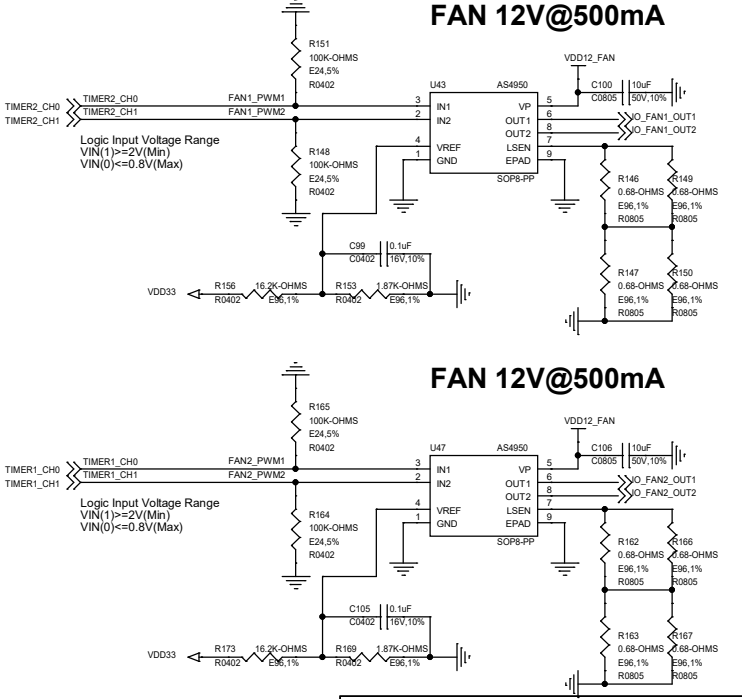
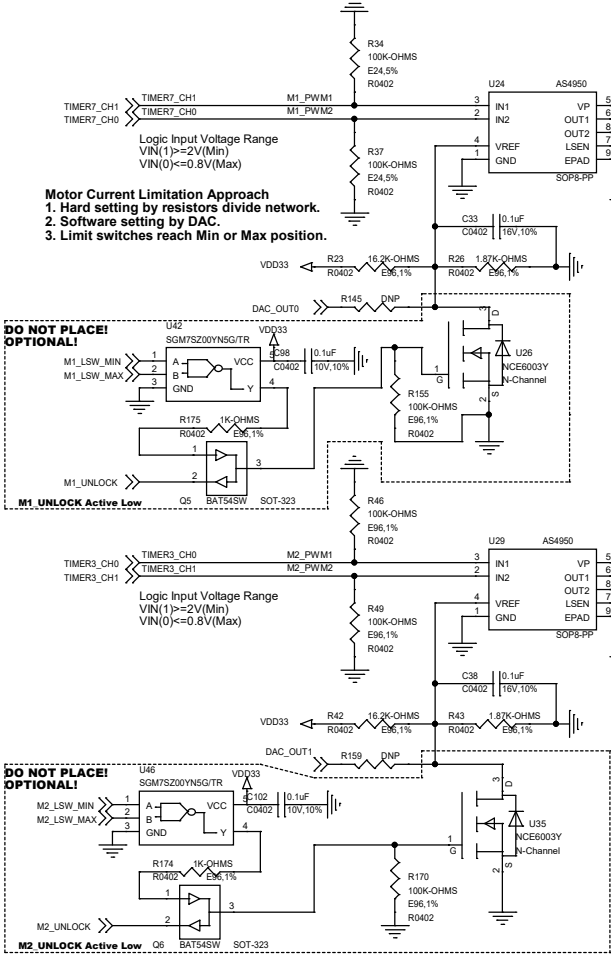
Current Limit Condition: (Visen*10) > VREF
Locked rotor current is 370mA
Here I choose 500mA
 $500mA * 0.68R = 0.34V$
 $0.34V = (R2 / (R1 + R2)) * 3.3V$
Fetch R1=16.2K from E96 tables, then R2=1.87K.
Verification below
 $(1.87K / (16.2K + 1.87K)) * 3.3V = 0.3415V$

Pin-Pin Compatible
SGM8967-4XTS14G/TR
27MHz

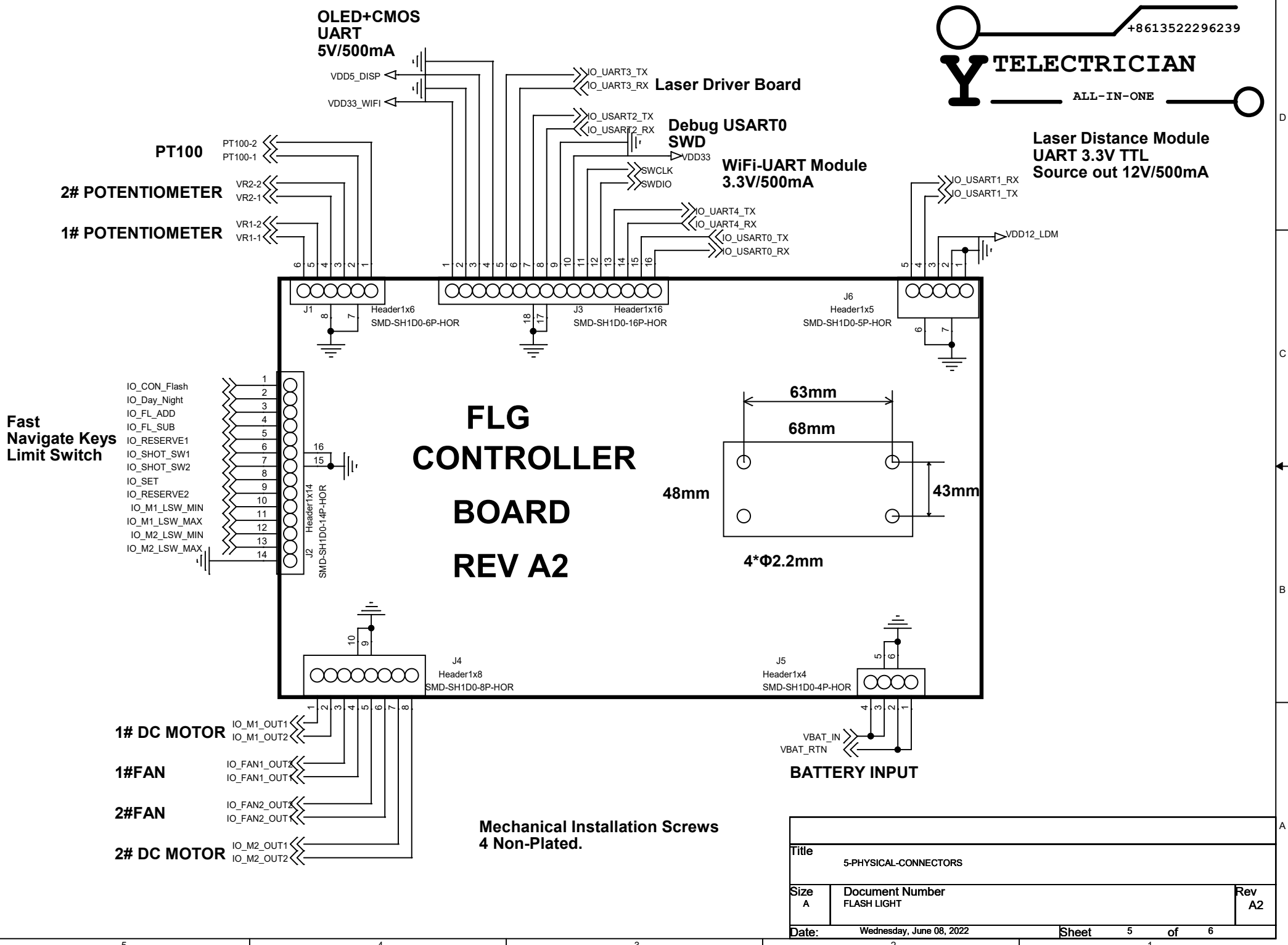
FAN 12V@500mA

FAN 12V@500mA

Title			4-MOTOR+FAN DRIVER
Size			Document Number
A3	FLASH LIGHT		Rev A2
Date:	Wednesday, June 08, 2022	Sheet	4 of 6

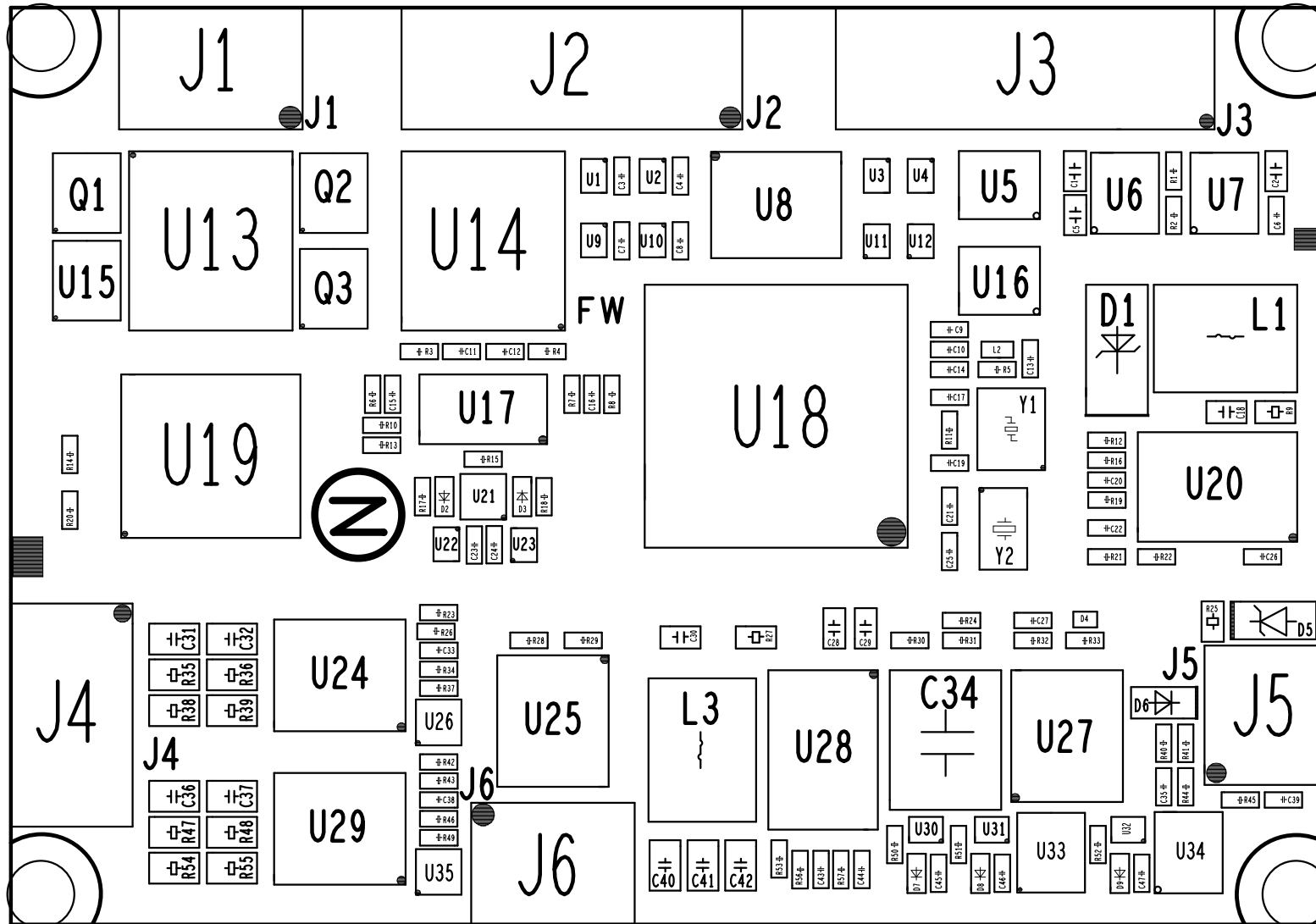


IN1	IN2	Visen*10 > VREF	OUT1	OUT2	Function
0	1	FALSE	L	H	Reverse
1	0	FALSE	H	L	Forward
0	1	TRUE	H/L	L	Chop (mixed decay), reverse
1	0	TRUE	L	H/L	Chop (mixed decay), forward
1	1	FALSE	L	L	Brake (slow decay)
0	0	FALSE	Z	Z	Coast, enters Low Power Standby mode after 1 ms

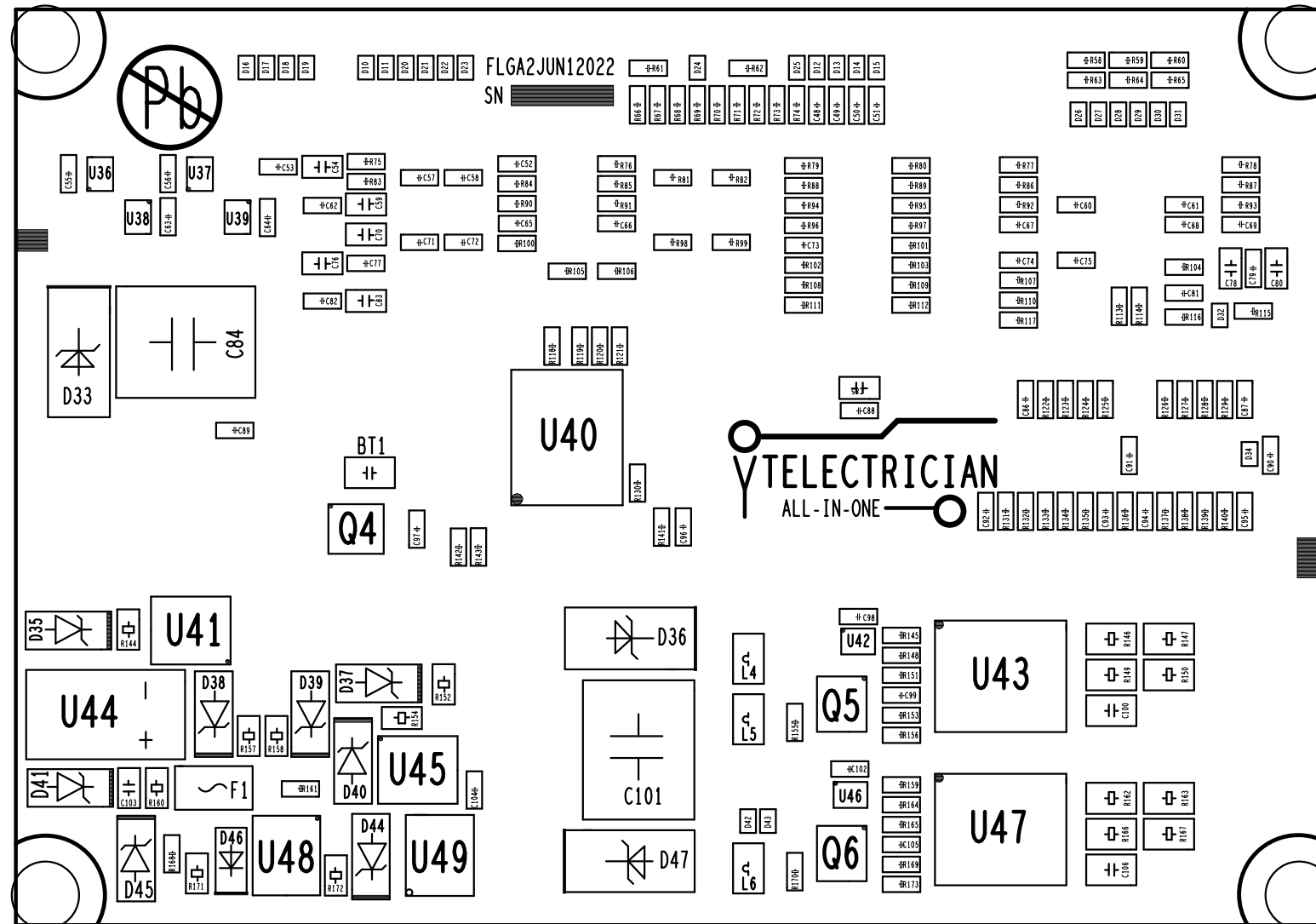


Title		
5-PHYSICAL-CONNECTORS		
Size	Document Number	Rev
A	FLASH LIGHT	A2
Date:	Wednesday, June 08, 2022	Sheet 5 of 6

SILKSCREEN_TOP REFERENCE DESCRIPTION



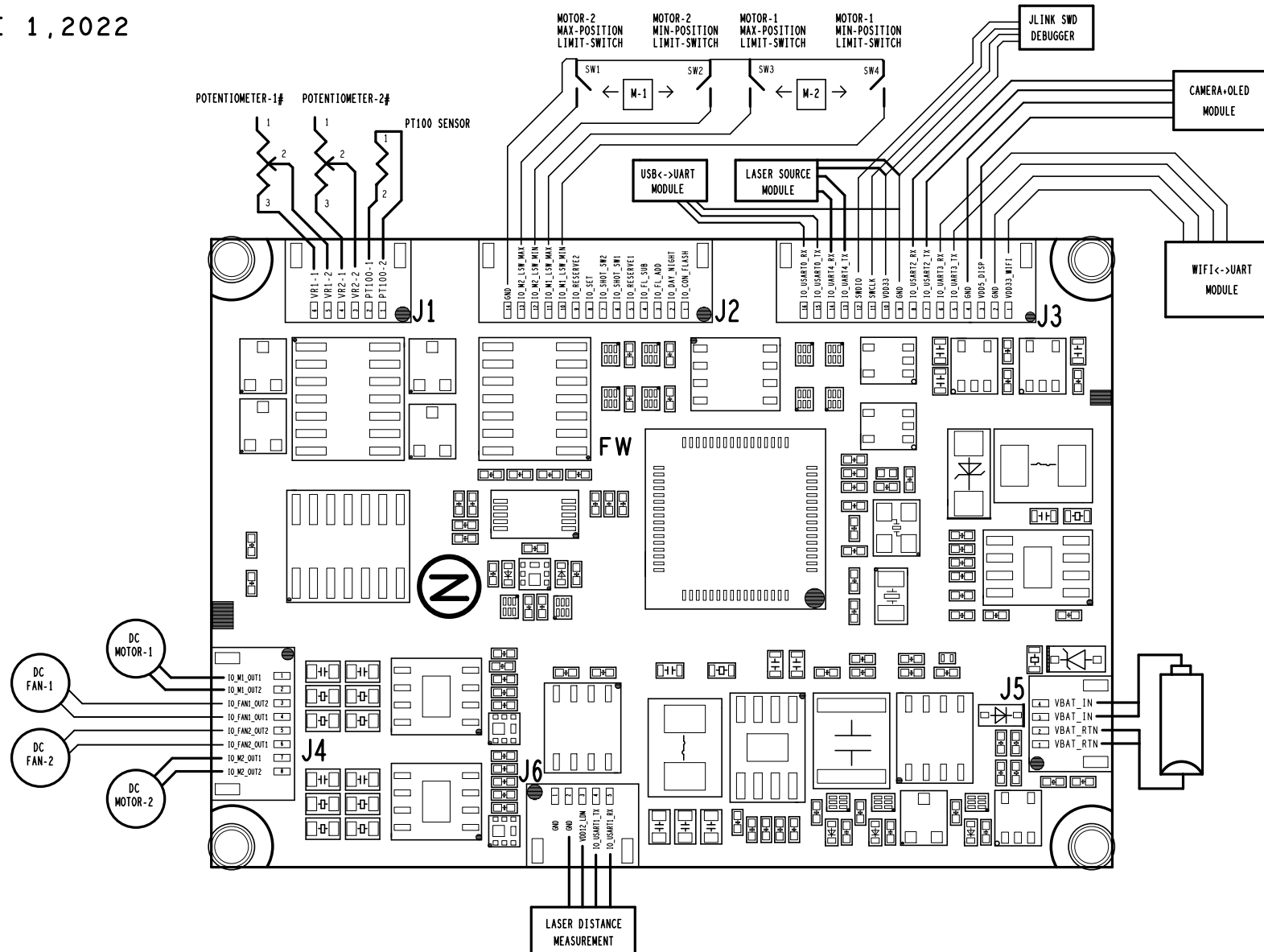
SILKSCREEN_BOTTOM REFERENCE DESCRIPTION



ASSEMBLY REFERENCE DIAGRAM

PROJECT: FLASH-LIGHT-GUN-REV-A2

JUNE 1, 2022



Bill of Materials (DNP removed)

Item	Quantity	Reference	Part	PCBFootprint	Detail
2	8	C1, C2, C59, C78, C80, C83, C85, C103	10uF	C0603	CAPACITOR SMD 0603 16V ±10%
3	66	C3, C4, C6, C7, C8, C10, C11, C12, C13, C14, C15, C16, C22, C23, C24, C27, C33, C35, C38, C44, C45, C46, C47, C48, C49, C50, C51, C52, C53, C55, C56, C57, C58, C60, C61, C62, C63, C64, C65, C66, C68, C71, C72, C73, C75, C77, C79, C81, C82, C86, C87, C88, C89, C90, C91, C92, C93, C94, C95, C96, C97, C98, C99, C102, C104, C105	0. 1uF	C0402	CAPACITOR SMD 0402 16V ±10%
4	4	C5, C54, C70, C76	4. 7uF	C0603	CAPACITOR SMD 0603 16V ±10%
5	4	C9, C67, C69, C74	10uF	C0402	CAPACITOR SMD 0402 16V ±10%
6	4	C17, C19, C21, C25	22pF	C0402	CAPACITOR SMD 0402 16V ±10%
7	2	C18, C30	10nF	C0603	CAPACITOR SMD 0603 16V ±10%
8	2	C20, C43	5. 6nF	C0402	CAPACITOR SMD 0402 16V ±10%
9	1	C26	0. 1uF	C0402	CAPACITOR SMD 0402 50V ±10%
10	2	C28, C29	0. 1uF	C0603	CAPACITOR SMD 0603 50V ±10%
11	9	C31, C32, C36, C37, C40, C41, C42, C100, C106	10uF	C0805	CAPACITOR SMD 0805 50V ±10%
12	3	C34, C84, C101	47uF	C2220	Multilayer Ceramic Capacitors MLCC - SMD/SMT 2220-INCH(5750-MM) 50VDC 47uF 20% X7R
13	1	C39	1. 5uF	C0402	CAPACITOR SMD 0402 16V ±10%
14	1	D1	SMAJ6. 0A	DO-214AC	TVS Diode Surface Mount DO-214AC (SMA) from Littelfuse Inc.
15	3	D2, D3, D7	BLUE	LED0402	LED SMD 0402 BLUE COLOR
16	27	D4, D10, D11, D12, D13, D14, D15, D16, D17, D18, D19, D20, D21, D22, D23, D24, D25, D26, D27, D28, D29, D30, D31, D32, D34, D42, D43	ESD4. 5V88D-C (PESDHC2FD4V5BH)	DFN-1006DN	Transient Voltage Suppressors for ESD Protection -40°C to +125°C
17	1	D5	BZT52C6V8	SOD-123	SURFACE MOUNT SILICON ZENER DIODES -55°C to +150°C
18	2	D6, D46	MBRX0560	SOD-323	0.5 Amp Schottky Rectifier
19	1	D8	RED	LED0402	LED SMD 0402 BLUE COLOR
20	1	D9	YELLOW	LED0402	LED SMD 0402 BLUE COLOR
21	2	D33, D36	SS35	DO-214AC	DOWOSEMI SURFACE MOUNT SCHOTTKY BARRIER RECTIFIER -65°C to +125°C
22	5	D35, D37, D41, D44, D45	BZT52C4V7	SOD-123	SURFACE MOUNT SILICON ZENER DIODES -55°C to +150°C
23	1	D38	BZT52C36V	SOD-123	SURFACE MOUNT SILICON ZENER DIODES -55°C to +150°C
24	2	D39, D40	BZT52C24	SOD-123	SURFACE MOUNT SILICON ZENER DIODES -55°C to +150°C
25	1	D47	SMAJ13A	DO-214AC	TVS Diode Surface Mount DO-214AC (SMA) from Littelfuse Inc.
26	1	F1	1AMP	FUSE1206	
27	1	J1	Header1x6	SMD-SH1D0-6P-HOR	SH1.0mm 6-PINS CONNECTOR SINGLE ROW HORIZONTAL SMD/SMT
28	1	J2	Header1x14	SMD-SH1D0-14P-HOR	SH1.0mm 14-PINS CONNECTOR SINGLE ROW HORIZONTAL SMD/SMT
29	1	J3	Header1x16	SMD-SH1D0-16P-HOR	SH1.0mm 16-PINS CONNECTOR SINGLE ROW HORIZONTAL SMD/SMT
30	1	J4	Header1x8	SMD-SH1D0-8P-HOR	SH1.0mm 8-PINS CONNECTOR SINGLE ROW HORIZONTAL SMD/SMT
31	1	J5	Header1x4	SMD-SH1D0-4P-HOR	SH1.0mm 4-PINS CONNECTOR SINGLE ROW HORIZONTAL SMD/SMT
32	1	J6	Header1x5	SMD-SH1D0-5P-HOR	SH1.0mm 5-PINS CONNECTOR SINGLE ROW HORIZONTAL SMD/SMT
33	2	L1, L3	10uH	IND-5D7X5D2X1D8	SRP5020TA-2R2M Fixed Inductors 10uH 20% 2.5A -40°C to +125°C
34	1	L2	BLM15BD182SN1D	FB0402	Ferrite Chip Beads SMD/SMT 0402 100mA 25% 1.8 kOhms@100MHz
35	3	L4, L5, L6	1uH	L0805	Fixed Inductors 1uH 20% 1.2A SMD/SMT 1206-INCH -40°C to +85°C
36	3	Q1, Q2, Q3	S8550	SOT-23-3	JCST SOT-23 Plastic-Encapsulate Transistors (PNP)
37	1	Q4	BAT54CW	SOT-323	SWITCHING DIODE Low forward voltage
39	2	R1, R83	150K-OHMS	R0402	RESISTOR SMD 0402 ±1% 1/16W
40	2	R2, R75	47. 5K-OHMS	R0402	RESISTOR SMD 0402 ±1% 1/16W

41	42	R3, R4, R5, R6, R7, R8, R10, R13, R40, R41, R76, R79, R80, R88, R89, R90, R94, R95, R96, R97, R101, R103, R104, R108, R109, R112, R114, R118, R122, R123, R125, R126, R128, R129, R130, R131, R133, R134, R136, R138, R140, R141	10K-OHMS	R0402	RESISTOR SMD 0402 ±1% 1/16W
42	2	R9, R27	10-OHMS	R0603	RESISTOR SMD 0603 ±1% 1/10W
43	1	R11	1Meg-OHMS	R0402	RESISTOR SMD 0402 ±1% 1/16W
44	2	R12, R53	33. 2K-OHMS	R0402	RESISTOR SMD 0402 ±1% 1/16W
45	1	R14	5. 49K-OHMS	R0402	RESISTOR SMD 0402 ±1% 1/16W
46	9	R15, R34, R37, R46, R49, R148, R151, R164, R165	100K-OHMS	R0402	RESISTOR SMD 0402 ±1% 1/16W
47	1	R16	5. 62K-OHMS	R0402	RESISTOR SMD 0402 ±1% 1/16W
48	2	R17, R18	2. 2K-OHMS	R0402	RESISTOR SMD 0402 ±1% 1/16W
49	2	R19, R57	6. 49K-OHMS	R0402	RESISTOR SMD 0402 ±1% 1/16W
50	7	R20, R23, R33, R42, R115, R156, R173	16. 2K-OHMS	R0402	RESISTOR SMD 0402 ±1% 1/16W
51	1	R21	2K-OHMS	R0402	RESISTOR SMD 0603 ±1% 1/10W
52	1	R22	20K-OHMS	R0402	RESISTOR SMD 0603 ±1% 1/10W
53	1	R24	0-OHMS	R0402	RESISTOR SMD 0603 ±1% 1/10W
54	2	R25, R154	5. 62K-OHMS	R0603	RESISTOR SMD 0603 ±1% 1/10W
55	4	R26, R43, R153, R169	1. 87K-OHMS	R0402	RESISTOR SMD 0402 ±1% 1/16W
56	5	R28, R29, R31, R161, R168	100K-OHMS	R0402	RESISTOR SMD 0402 ±1% 1/10W
58	1	R32	1. 62K-OHMS	R0402	RESISTOR SMD 0603 ±% 1/10W
59	16	R35, R36, R38, R39, R47, R48, R54, R55, R146, R147, R149, R150, R162, R163, R166, R167	0. 68-OHMS	R0805	Current Sense Resistors - SMD 0.2 OHM 3/4W
60	1	R45	23. 7K-OHMS	R0402	RESISTOR SMD 0402 ±1% 1/16W
61	6	R50, R51, R52, R77, R78, R117	2K-OHMS	R0402	RESISTOR SMD 0402 ±1% 1/16W
62	1	R56	2. 37K-OHMS	R0402	RESISTOR SMD 0402 ±1% 1/16W
63	1	R58	976-OHMS	R0402	RESISTOR SMD 0402 ±1% 1/16
64	2	R59, R60	511-OHMS	R0402	RESISTOR SMD 0402 ±1% 1/16
65	2	R61, R62	3. 32K-OHMS	R0402	RESISTOR SMD 0402 ±% 1/16W
66	2	R63, R127	DNP	R0402	DNP (DO NOT PLACE, RESERVED)
67	2	R64, R65	3. 4K-OHMS	R0402	RESISTOR SMD 0402 ±1% 1/16
68	2	R66, R71	442-OHMS	R0402	RESISTOR SMD 0402 ±% 1/16W
69	2	R67, R72	1. 1K-OHMS	R0402	RESISTOR SMD 0402 ±% 1/16W
70	2	R68, R73	1. 74K-OHMS	R0402	RESISTOR SMD 0402 ±% 1/16W
71	2	R69, R74	4. 42K-OHMS	R0402	RESISTOR SMD 0402 ±% 1/16W
72	1	R70	22. 1K-OHMS	R0402	RESISTOR SMD 0402 ±% 1/16W
73	6	R81, R82, R91, R98, R99, R100	10K-OHMS	R0402	RESISTOR SMD 0402 ±% 1/16W
75	3	R86, R87, R110	1K-OHMS	R0402	RESISTOR SMD 0402 ±1% 1/16W
76	3	R92, R93, R107	1. 69K-OHMS	R0402	RESISTOR SMD 0402 ±1% 1/16W
77	1	R102	9. 09K-OHMS	R0402	RESISTOR SMD 0402 ±1% 1/16W
78	2	R105, R143	0-OHMS	R0402	RESISTOR SMD 0402 ±1% 1/16W
79	1	R111	110K-OHMS	R0402	RESISTOR SMD 0402 ±1% 1/16W
80	1	R116	8. 25K-OHMS	R0402	RESISTOR SMD 0402 ±1% 1/16W
81	3	R119, R120, R121	33-OHMS	R0402	RESISTOR SMD 0402 ±1% 1/16W
82	2	R132, R139	71. 5K-OHMS	R0402	RESISTOR SMD 0402 ±1% 1/16W
83	2	R135, R137	8. 66K-OHMS	R0402	RESISTOR SMD 0402 ±1% 1/16W
84	1	R144	1. 4K-OHMS	R0603	RESISTOR SMD 0603 ±1% 1/10W
85	2	R152, R171	24. 9K-OHMS	R0603	RESISTOR SMD 0603 ±1% 1/10W
87	2	R157, R160	2K-OHMS	R0603	RESISTOR SMD 0603 ±1% 1/10W
88	1	R158	825-OHMS	R0603	RESISTOR SMD 0603 ±1% 1/10W
89	1	R172	33. 2K-OHMS	R0603	RESISTOR SMD 0603 ±1% 1/10W

90	17	U1, U2, U3, U4, U9, U10, U11, U12, U22, U23, U30, U31, U32, U36, U37, U38, U39	SGM7SZ08YXDM6G/TR	XTDFN-1X1-6L	SGM7SZ14, Small Logic Inverter with Schmitt Trigger Input -40℃ to +125℃
91	2	U5, U6	SGM2028-ADJ	SOT-23-5	SGM2028, 500mA, Ultra-Low Dropout, Low Power, RF Linear Regulator -40℃ to +85℃
92	2	U7, U16	SGM2028-3. 3	SOT-23-5	SGM2028, 500mA, Ultra-Low Dropout, Low Power, RF Linear Regulator -40℃ to +85℃
93	1	U8	SGM8968-2XS8G/TR (SGM8967-4XS8G/TR , SOIC-8)	SOIC-8	SGM8968-2, 1.6mA, 10MHz, High Precision, Low Noise, Rail-to-Rail I/O, CMOS Operational Amplifiers -40℃ to +125℃
94	3	U13, U14, U19	SGM8968-4XS14G/TR (SGM8967-4XS14G/TR, SOIC-14)	SOIC-14	SGM8968-4, 1.6mA, 10MHz, High Precision, Low Noise, Rail-to-Rail I/O, CMOS Operational Amplifiers -40℃ to +125℃
95	1	U15	TPR3333-S3TR	SOT-23-3	3PEAK 3.3V Voltage Reference
96	1	U17	SGM58031XMS10G/TR	MSOP-10	SGM58031, Ultra-Small, Low-Power, 16-Bit Analog-to-Digital Converter with Internal Reference -40℃ to +125℃
97	1	U18	GD32F303RGT6	LQFP64	GigaDevice ARM Cortex-M4 32-bit MCU Green Industrial -40° C to +85° C
98	2	U20, U28	SGM6230	SOIC-8-EPAD	SGM6230, 2A, 38V, 385kHz Buck Converter -40℃ to +85℃
99	1	U21	NCE3013J	DFN2X2-6L	N-Channel Enhancement Mode Power MOSFET
100	4	U24, U29, U43, U47	AS4950	SOP8-PP	Full-Bridge DMOS PWM Motor Driver -40° C to +85° C
101	2	U25, U27	NCE603S	SOP-8	MOSFET N & P Trench 60V 6.3A,6A 2.5V @ 250uA,3.5V @ 250uA 30 m?? @ 6A,10V;80 m?? @ 5A,10V SOP-8 150mil RoHS
103	1	U33	NCE6003Y	SOT-23-3L	N-Channel Enhancement Mode Power MOSFET
104	2	U34, U49	SGM7SZ14	SOT-23-5	SGM7SZ14, Small Logic Inverter with Schmitt Trigger Input -40℃ to +125℃
105	1	U40	GD25Q40ETIG	SOP8-150MIL	GigaDevice SERIAL NOR FLASH 4Mbit SOP8 150mil -40℃ to +85℃
106	3	U41, U45, U48	NCE60P04Y	SOT-23-3L	60V 4A 120mΩ@10V,4A 1.5W 3V@250μA P Channel SOT-23-3L MOSFETs ROHS
107	1	U44	KMB26S (MB10F)	TO-269AA	Bridge Rectifier Single Phase Schottky 60 V Surface Mount MBS from SMC Diode Solutions
108	1	Y1	8MHz	CRY-SMD-3D2X2D5MM-4P	SMD CRYSTAL 3.2mmx2.5mm 4-PINS
109	1	Y2	32.768KHz	CRY-SMD-3D2X1D5MM-2P	SMD CRYSTAL 3.2mmx1.5mm 2-PINS

SCHEMATIC BRIEF DESCRIPTION

Page 1 – POWER SUPPLY

The board is feed by a 18650 battery pack. We need 8 batteries in serial connection to get a higher voltage for something particular reason. It seems the laser source module needs a high voltage, it was been done by other teammates we don't know. To avoid reverse connection damage, I add a bridge rectifier(U44) at the entrance, so the power source polarity isn't significant. There is a re-settable fuse 1AMP used to cut off power supply when a over current situation occurs. I also considered appropriate working voltage range, so a under voltage protection and a over voltage protection are necessary. According to the features of a 18650 battery, I know the charging cut-off voltage is 3.7V and discharging cut-off voltage is 3.0V. So, the threshold for under voltage I chose $3.0V \times 8S = 24V$, the threshold for over voltage I chose 36V, a little bit higher than $4.2V \times 8S = 33.6V$.

The main switcher to deliver power to backward stage is a P-MOSFET(U27). The VSYS network name is a key point after protection, once it gets power, all system gets power.

The following, I'd wanna describe protective theory in detail.

First, I need a auxiliary power to keep LED warning indication working in case of emergencies. R160 and D41 are used to generate a 4.7V voltage, it's always valid unless components crash.

If the fuse(F1) breaks, VBAT network lost power. Zener(D45) is ON, the voltage between Gate and Source of P-MOSFET(U41) now equals -4.7V enough to turn on it. So Zener(D5) starts to work to generate a 6.8V voltage and then Zener(D35) is on. Attention 2-INPUT AND Gate(U31), Pin-2(B) is feed by a 5Hz oscillator, Pin-1(A) keeps 4.7V, so Pin-4(Y) outputs to drive a RED LED(D8) frequently to indicate a over current error occurs.

All 12V power rails are controlled by MCU. As a portable device, to reduce power consumption is critical. The EN pins of step down converter is driven by network 12V_PWR_ON. Drive it to low to turn off in different software requirements. And power for Laser Distance Measurement is also controllable. I call it two-stage switcher.

Page 2 – MCU + KEYS

I add two LEDs on board to debug firmware conveniently. But the driving approach is a little difference than usual. Lacks of GPIO, so only one Pin can be used.

When LED outputs 0, D3 turns ON and D2 turns off.

When LED outputs 1, D3 turns OFF, but N-MOSFET(U21) turns ON, so D2 turns on.

If you wanna both turn ON, drive LED pin with a wave of higher frequency, 50% duty cycle is better.
Set LED GPIO pin to floating input to turn both off.

I'm sorry about this unfriendly and stupid design, but all GPIO had been gone.

There's a serial Flash IC with 4Mbits capacity on board. It's optional, parameters also can be stored inside MCU integrated Flash.

It's really, really, really difficult to expand many peripherals with a 48-Pins MCU. Please forgive me, this MCU was ideal at the beginning of project, but the requirements was changed later. And it's a challenge, unwise to change to another one. The purchase is also harder. So the software engineer must recognize keys input using a ADC. Don't worry, all inputs were processed with impedance match. See equations to learn how to recognize each key easily.

And you must notice that all UARTS interfaces are isolated by a AND gate. This is intend to protect MCU I/O to reduce repair fees.

Page 3 – CONSTANT CURRENT ADC

In this design, we use two potentiometers to measure the accurate position of motors. In order to get a high accuracy and to avoid influence of voltage ripple, we built a 1mA constant current source to excite the sensor. There's a question here, the resistor is 5K-OHMS maximum value, if excite it with 1mA, then we get 5V voltage. It exceeds the power supply voltage, we might lost resolution. So I connect an external 3.4K-OHMS resistor in parallels to reduce the total resistance. Here it is $5K//3.4K=2.02381K$. I use a 511-OHMS resistor to level up the voltage and convert the single-ended signals to a differential signal. Now assume the value of potentiometer is 0-OHMS, so the voltage of $V_b=V_a=1mA*511-OHMS=511mV$, $V_b-V_a=0V$. If the value is 5K-OHMS, then $V_b=1mA*(5K//3.4K+511)=2.02381V$, $V_a=1mA*511=0.511V$, so $V_b-V_a=1.51281V$. It's within the range of full scale of ADC 2.048V.

There's also a exciting source for PT100 temperature sensor. I read its data sheet and know it's 60.26-OHMS@-100, 138.51-OHMS@+100. So if the environment temperature below -100, the value is about 50-OHMS, then $V_b-V_a=1mA*50-OHMS=0.05V$, amplify with a Gain=11, we get $0.05V*11=0.55V$. As the same, when it below +100, $V_b-V_a=1mA*150-OHMS=0.15V$, the real voltage applied to ADC is $0.15V*11=1.65V$.

I also apply a fixed voltage value 5V to the spare channel, then the software can check if the ADC chip works well.

Page 4 – MOTOR+FAN DRIVER

Here I will give out a brief example about how to drive DC motor. AS4950 is a H-bridge integrated chip, so we feed it with PWM. The Motor-1 connects to TIMER7_CH0/TIMER7_CH1. The Motor-2 connects to TIMER3_CH0/TIMER3_CH1. AS4950 has a built-in current limitation. The Pin-4(VREF) is used to apply a appropriate voltage outside. I offer two ways to do that. We can set up a fixed resistor network divider. Or feed it with a DAC output accurately. But may I have your attention please? In order to protect motors to avoid physical damage, there's a fast cut

off mechanism active. For Motor-1, attention with U42,Q5 and U26 components. When motor-1 reaches minimum position, M1_LSW_MIN gets 0. When motor-1 reaches maximum position, M1_LSW_MAX gets 0.

To accelerate cut-off driving source, here I limit the maximum current to a lower value nearly to zero. It's all hardware driven without software attention. When M1_LSW_MIN or M1_LSW_MAX gets 0, NAND gate outputs 1 to turn on NMOS to drop VREF to GND. At this time, M1_UNLOCK must stay HIGH. So motor-1 stops without driving. In other words, right now, motor-1 reaches physical minimum or maximum position. Under this situation, if we want motor-1 to rotate toward opposite direction, we drive M1_UNLOCK to LOW to bypass limitation of switches. We must handle it carefully to avoid mechanism damage.

The working current of the motor is sampled by a shunt resistor. To get more flexibility and stability, I use four 0.68-OHMS resistors, combine them to one to replace a big one, to reduce PCB space taken up. According to the motor data sheet, we get to know current consumption under different situation. 4.6mA with no load condition, 0.188A with continuous working condition and 0.37A with lock rotor condition. So the calculating equations are below, and in order to reach the full scale of ADC input to optimize performance, a non-inverting amplifier with gain x 9 approximately is followed. Gain=8.15 in real.

$$\begin{aligned} 0.68R * 4.6mA &= 3.128mV & (*8.15 = 25.4932mV) \\ 0.68R * 0.188A &= 127.84mV & (*8.15 = 1.042V) \\ 0.68R * 0.37A &= 251.6mV & (*8.15 = 2.05V) \end{aligned}$$

We also need to monitor the power rails of 12V for motor and the whole system power. VDD12_MOTOR is divided by a resistor network connection in serial to drop down the voltage to adapt the ADC input range.

The real voltage apply into ADC pin is $V=(5.49K/(5.49K+16.2K))*12V=3.037V$,
meanwhile the VSYS voltage apply into ADC pin is $V=(1.62K/(1.62K+16.2K))*33.6V=3.0545V$

Here I still use AS4950 H-bridge Chips to drive two FANs, although a small footprint NMOSFET is enough. I consider more, once the requirement change, no need to re-layout the PCB. It's a reserved solution. No perfect solution to adapt all requirements. With a H-bridge, we can drive a FAN to rotate in two directions, clockwise and anti-clockwise. Unfortunately, there's no current monitoring due to the lack of GPIO pins.

Page 5 – PHYSICAL CONNECTORS

Nothing to be noticed. Each connector has different amount numbers of pins to allow operators to assemble easily and rapidly.

That's all. No bugs permanently! God Bless Us!

June 8,2022
Yanai Electrician