



LHCb Vertex Locator

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## Documentation

# TECHNICAL DESCRIPTION OF THE VELO THERMAL CONTROL SYSTEM

LHCb VELO group

**Abstract:** This document describes the design and construction of the VELO Thermal Control System.

**Keywords:** CO<sub>2</sub>, Cooling, 2PACL, VTCS,

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# 1 Introduction

## 1.1 Introduction to the *VELO* detector

The Vertex Locator (LHCb-VELO) is the central detector of the LHCb experiment (1). LHCb is one of the four experiments of the newly constructed LHC proton collider at CERN in Geneva. The VELO detector is designed to make precise measurements of vertex positions from high energy particle decays like B-mesons. The B-mesons are made by the proton-proton collisions of the LHC collider. The requirements for precise detection of the B-meson vertices are the highest of all 4 LHC experiments. Therefore the silicon sensors have to be placed very close to the collision point. To achieve this the VELO detector is situated inside the LHC vacuum only 8 mm away from the proton beams.

The active detection surface is a disc shaped silicon strip sensor with an outer diameter of 80mm and an inner diameter of 16mm. The inner diameter hole is for the proton beam to pass through. The detector is split in two halves. Both halves can be moved 30mm away from the beam. The increased beam space is necessary as the beam trajectory can vary during beam injection.

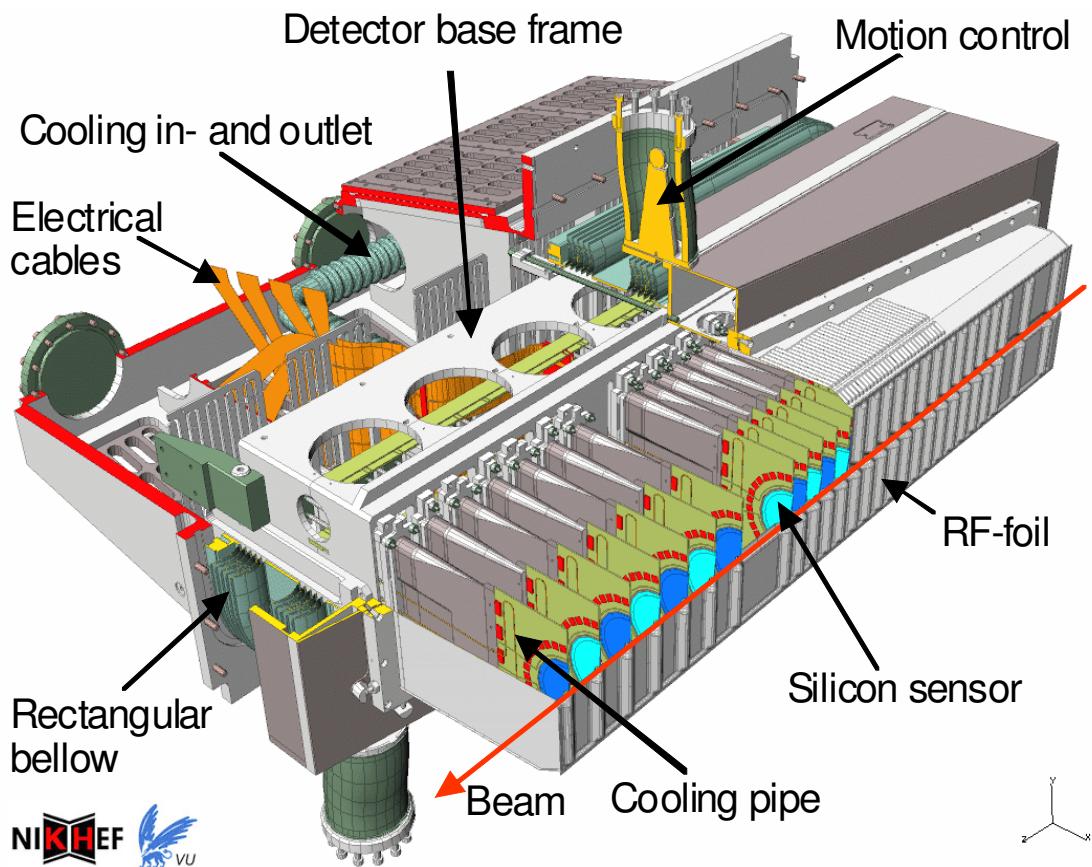


Figure 1.1-1: Inside look of 1 VELO detector half

Figure 1.1-1 shows an inside look of 1 detector half. The blue half circles are the detection silicon sensors. In total there are 21 VELO modules and 2 Pile-Up modules per half. The VELO modules are used to measure the particle tracks, the pile-up modules are used for triggering. All modules are assembled on an electronic substrate

(green plate) housing the Beetle read-out chips (red dots around silicon periphery) (2). The modules are mounted via stand-off paddles on a precise machined aluminum base frame. Each detector half is situated inside a 300 micron thick aluminum foil box. The foil acts as a Faraday cage to protect the sensitive silicon from the beam interference. It is also a gas barrier to protect the ultra high accelerator vacuum from the out gassing of the silicon modules. A maximum pressure difference of 5 mbar may occur between the detector and the accelerator volumes. A complex vacuum system is designed to maintain a lower pressure difference at all times (3).

The silicon sensors are exposed to radiation. Cooling of the sensors to sub zero temperatures is needed to minimize the effect of radiation damage. The Beetle chips on the modules are also dissipating heat inside the vacuum, so an active cooling system is needed to remove the heat and keep the silicon sensors cold. The base frame is the positional reference of the modules, this frame must therefore stay at room temperature. The stand-off paddles have therefore a low thermal conductance. Additional heaters control the base frame to maintain at room temperature.

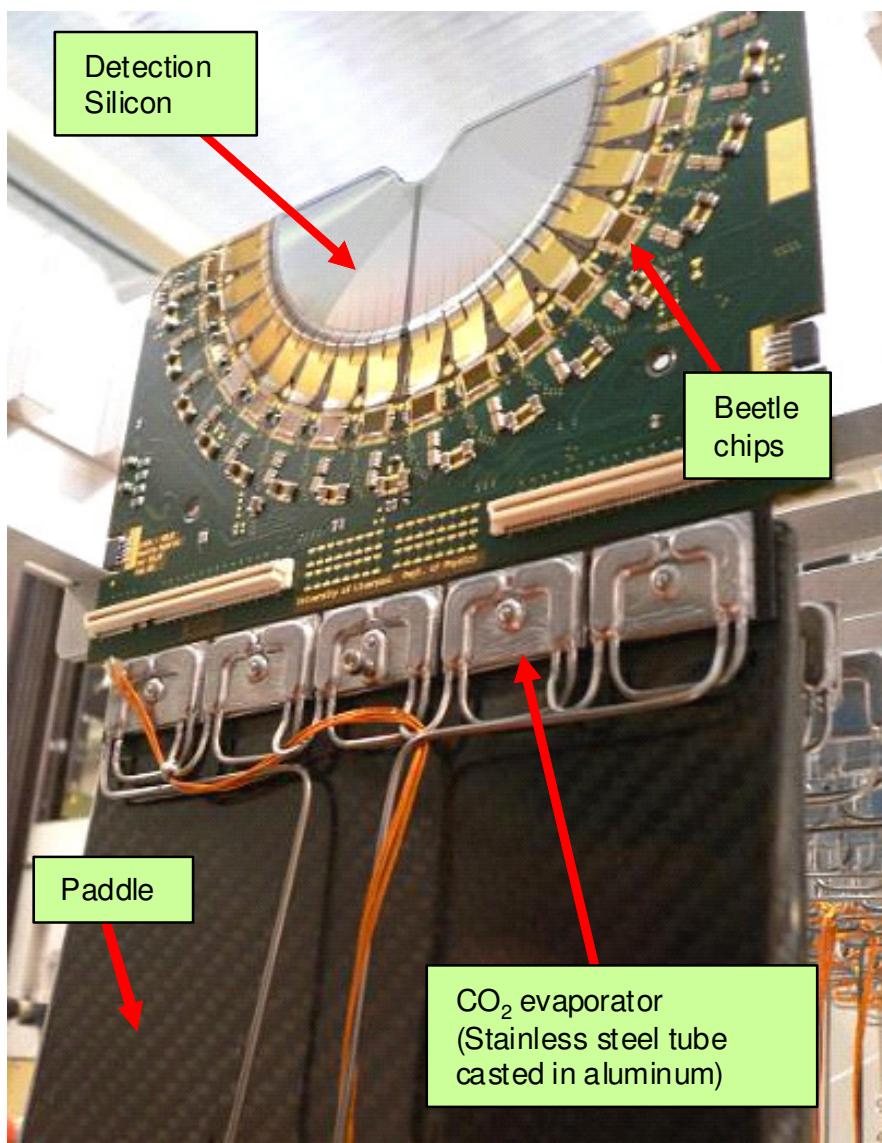


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## 3 Velo Thermal requirements and specifications.

### 3.1 Temperature requirements

Table 3.1-1 shows the main thermal requirements of the key-components, Table 3.2-1 shows the dissipated power in the detector which must be absorbed by the thermal control system. The thermal control system has been designed to meet these requirements. Interlocks have been integrated to prevent overheating or overcooling, if in extreme cases the thermal control system fails to do so.

Table 3.1-1: Operational and survival temperature limits of Velo key components.

	Operational temperatures:	Survival temperatures:	
		Before irradiation:	After irradiation:
Silicon Wafers	-12°C / -5°C (Nominal tip = -7°C )	-30°C / 100°	Long-term: -30°C / 0°C Short term: 0°C / 24°C (100 hours)
Hybrid	-20°C / 80°C	-30°C / 150°C	
Beetle chips	-20°C / 80°C	-30°C / 100°C	
Cables	-20°C / 100°C	-30°C / 200°C	
RF-Foil	<20°C	NA	
Module base frame	18°C to 22°C (Stable)	NA	

### 3.2 Dissipation specifications

Table 3.2-1: Power dissipation of Velo hardware inside the detector vacuum.

	Per Velo module	Per PU module	RF-Foil	Total for Velo
Nominal power	21.8 W	13.3 W	8 W	978 W
Maximum power	27.5 W	16.2 W	8 W	1255 W
Absolute maximum power*	30.2 W	17.5 W	8 W	1617 W

\*Absolute maximum power is the highest possible dissipated power when software settings are made accidentally wrong. A power limiter will prevent higher dissipation.

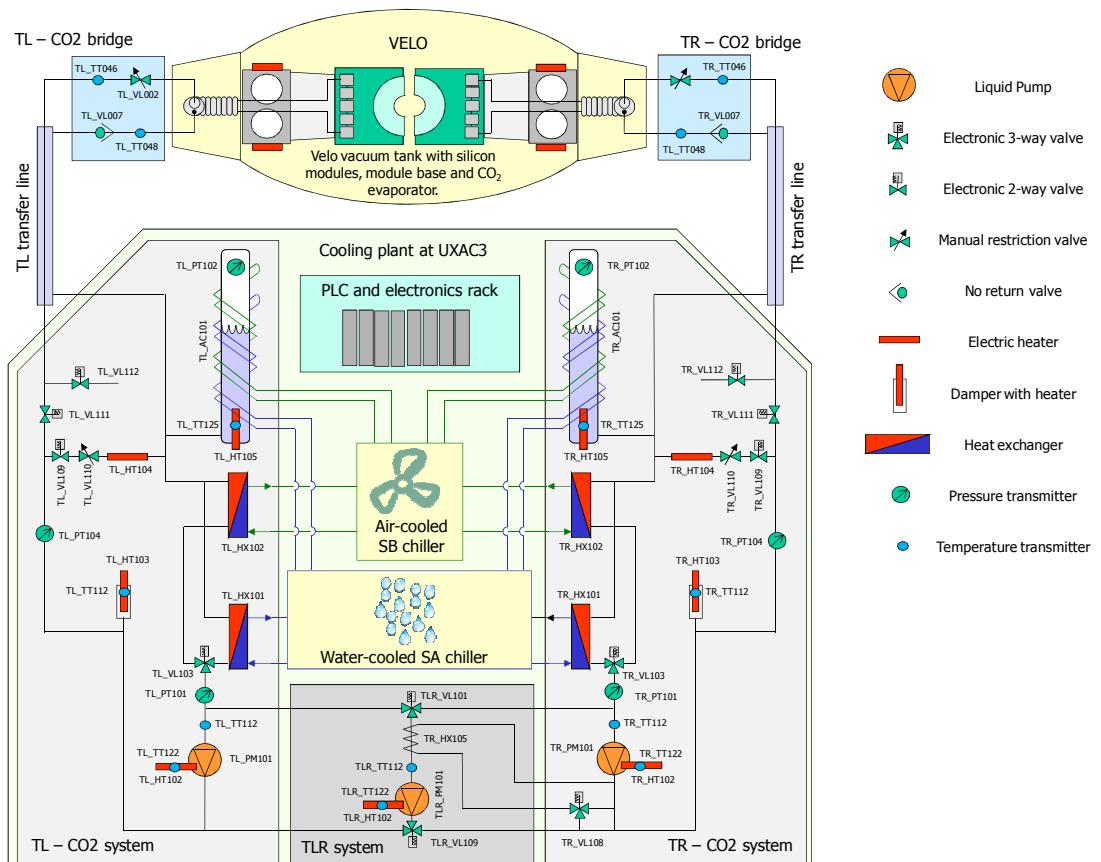
After irradiation it is essential that the silicon sensor temperature stays below 0°C at all time. Exposure to higher temperatures causes the radiation damage to reveal. The revealed damaged is a function of temperature times the “warm” time. It was considered that a room temperature is reasonable to encounter in the silicon lifetime, so the amount of hours spent at room temperature is the driving requirement for integration or maintenance matter, when the cooling system cannot keep the sensors below 0°C.

## 4 VELO Thermal Control System (VTCS)

The full thermal control of the detector (module cooling and base frame heating) is done by the VTCS (VELO Thermal Control System). The cooling part inside the VELO is an evaporative system using CO<sub>2</sub> as coolant. The heating part is with normal electrical heating. The cooling system uses the 2PACL method (2-Phase Accumulator Controlled Loop) for circulating and conditioning the CO<sub>2</sub> (4). The 2PACL method condenses and sub cools the CO<sub>2</sub> with an external chiller.

### 4.1 VTCS layout

The VELO cooling system is a cascade of 3 hydraulic systems. Liquid CO<sub>2</sub> is pumped from the cooling plant on the service platform UXAC3 in the safe area to the detector in the experimental cavern. Figure 4.1-1 shows a schematic layout of the VTCS with the main components involved. The CO<sub>2</sub> system consists of 2 parallel systems each connected to one VELO detector half (Visible on both sides of the schematic layout). Both CO<sub>2</sub> systems are cooled by individual evaporator branches of the same hydrofluorocarbon (HFC) chiller. The heat in the detector is removed by evaporating part of the supplied CO<sub>2</sub>. The CO<sub>2</sub> liquid-vapor mixture floats back to the cooling plant via the so called transfer lines. The returned CO<sub>2</sub> is condensed and sub-cooled by the HFC chiller which rejects its waste heat to the cold water system of CERN. In the VTCS the CERN cold water system is called the primary cooling system, the HFC-chiller the secondary and the CO<sub>2</sub> system the tertiary cooling system.



There are 2 HFC chillers in the VTCS. The main chiller is a large capacity water cooled chiller ( $2.5\text{ kW}@-40^\circ\text{C}$ ). A smaller capacity air cooled chiller ( $1.5\text{ kW}@-25^\circ\text{C}$ ) is available for back-up operations. The heat load of the VTCS exists of 2 main sources. The detector heat load due to the low voltage dissipation ( $\sim 1\text{ kW}$ ) and the heat leak from the environment ( $\sim 1\text{ kW}$ ), which is mainly picked up by the 55m CO<sub>2</sub> transfer line.

The air-cooled back-up chiller has a smaller capacity compared to the water cooled main chiller. It is designed for keeping the detector cold only. The back-up chiller is used only when there is a problem with the main chiller. The back-up system is air-cooled so problems with the CERN cooling water are also abolished. In case the back-up chiller is operational, it is not possible to power the VELO detector. It is designed only for maintaining the detectors cold enough to avoid the outcome of the radiation damage of the silicon sensors. Figure 4.1-2 shows a block diagram of the several cooling stages of the VTCS.

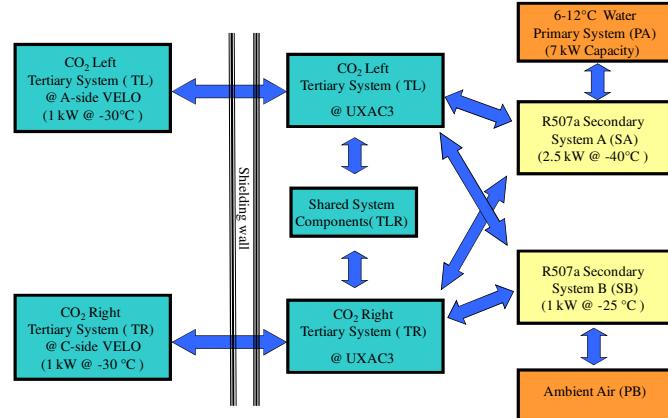


Figure 4.1-2: Schematic layout of the 3 VTCS stages

The tertiary CO<sub>2</sub> system is a concept which was originally designed for a satellite cooling application (5). It is a mechanically pumped loop system where the system pressure is controlled using an two-phase accumulator. The accumulator's pressure is kept constant by controlling its two-phase content. The principle is called 2-Phase Accumulator Controlled Loop (2PACL) (4). The pressure of the 2PACL directly controls the evaporative temperature in the detector. In this way it is possible to control the detector temperature accurately from a remote plant in the safe area. The evaporator and condenser of the tertiary 2PACL operate at the same pressure and hence at the same saturation temperature. For the liquid pumps it is needed to sub cool the CO<sub>2</sub> liquid. An external chiller which is colder than the CO<sub>2</sub> loop will take care of this and reject the waste heat to the cold water system of CERN. (6) Figure 4.1-3 shows the temperature profile and heat balance of the 3 VTCS stages. Seen from the detector the temperature is decreasing in the CO<sub>2</sub> loop from detector to the chiller. In the chiller the temperature is increased by the compression of the gas. The hot gas in the chiller is cooled and condensed by the coldwater system of LHCb. The final heat rejection Q<sub>p1</sub> (primary heat load) to the water system is the sum of all the collected heat along the different systems shown.

The VTCS is not only a cooling system it is -as the name is indicating- a thermal control system. This means that it is designed to maintain the detector on the design temperature. In the requirement table (Table 3.1-1) it is stated that the module base must be kept at room temperature. Although the module base is not connected directly to the cooling system hardware a heating system on the module base is needed to

prevent it from cooling down. The base plate heating is described together with the evaporator system in paragraph 7.2.

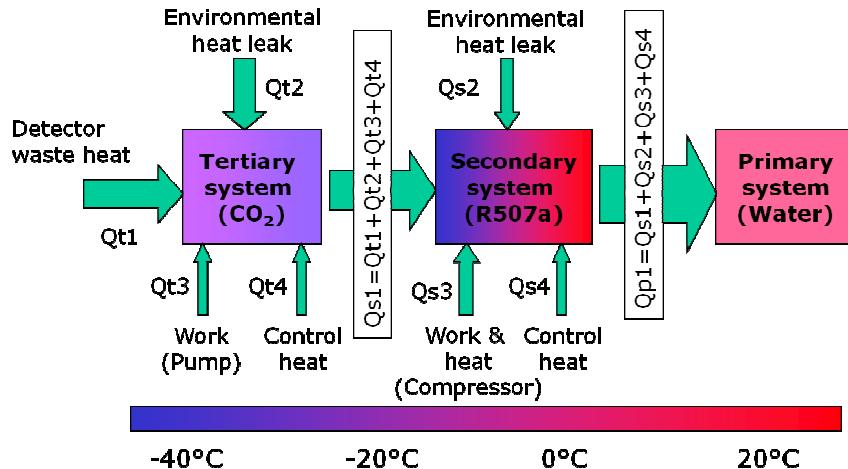


Figure 4.1-3: The thermal balance of the VTCS

All cooling stages and base plate heating are controlled by a Siemens S7-400 series Programmable Logic Controller (PLC). The PLC handles the PID controls, the alarm handling and the monitoring. A PVSS interface is used to monitor and archive all the system variables.

## 4.2 VTCS hardware location.

The majority of the cooling system hardware is located in the safe zone of the LHCb cavern. On the UXAC3 platform the cooling plants are located as well as the PLC control rack. This is all the hardware inside the light green field of Figure 4.1-1. Figure 4.2-1 shows a artistic interpretation of the cooling system hardware locations.

The  $\text{CO}_2$  of both tertiary systems is transferred by two 50m long transfer lines to the two VELO detector halves. The transfer lines pass the thick concrete shielding wall via the piping and cable chicane. The transfer lines are connected to the  $\text{CO}_2$  distribution box on top of the VELO (also called cooling bridge). From this box the 2 evaporators inside the VELO secondary vacuums are fed with saturated liquid. Figure 4.2-2 shows the cooling system hardware and its location in the LHCb cavern. Figure 4.2-3 shows detailed views of the platform and detector area.

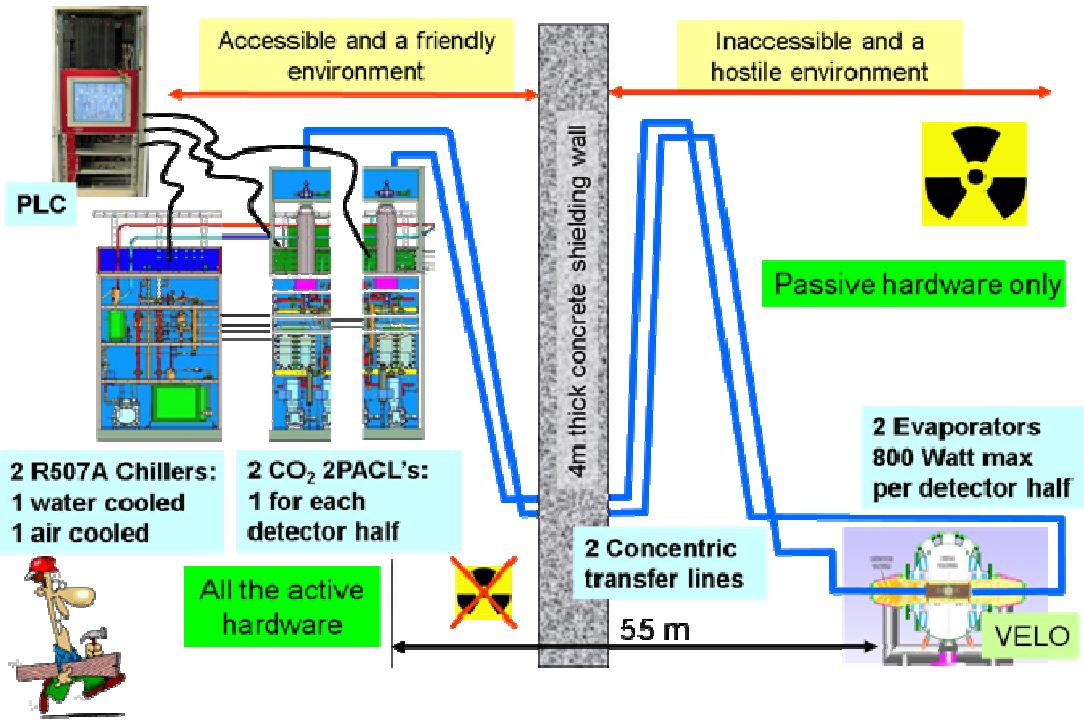


Figure 4.2-1: Interpretation of VTCS in LHCb

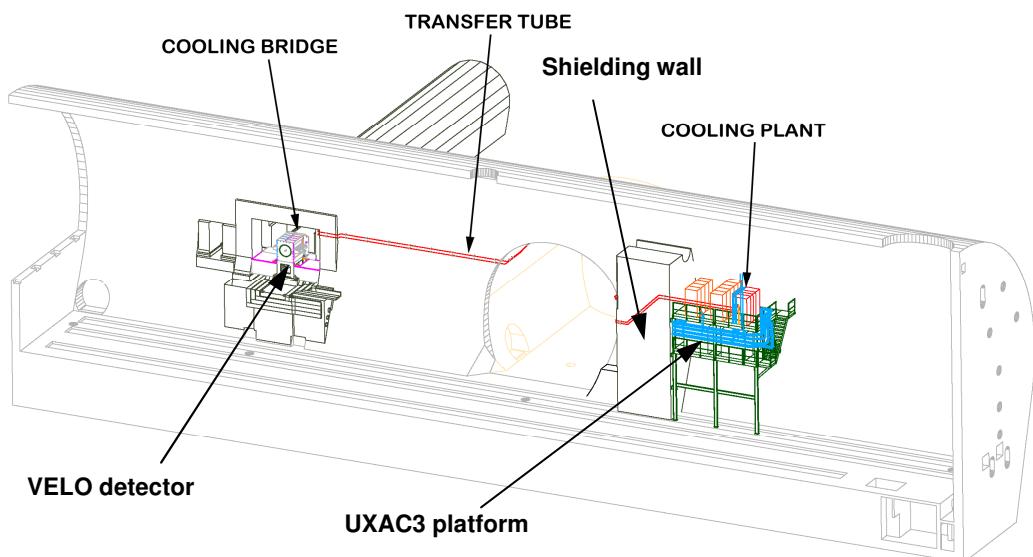


Figure 4.2-2: The VTCS cooling system hardware location in the LHCb cavern.

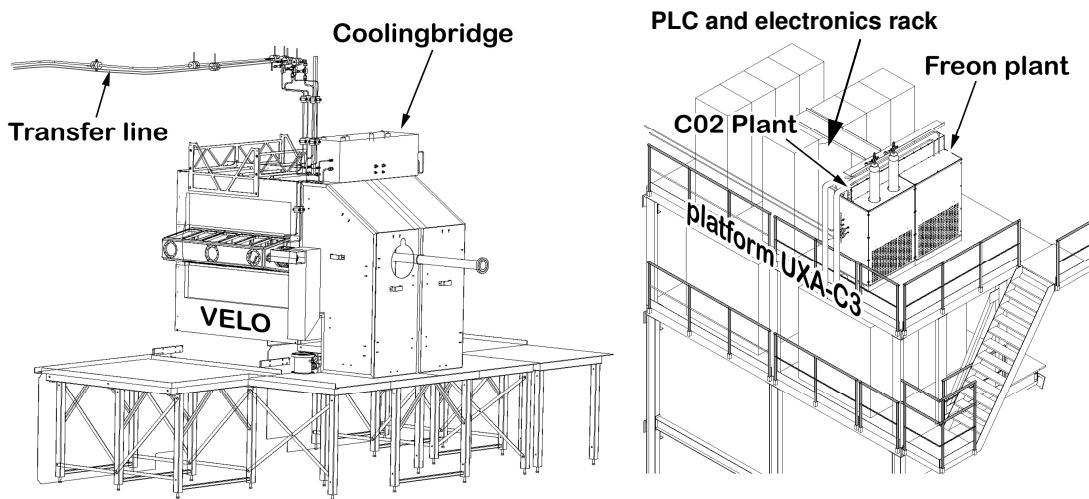


Figure 4.2-3: Detailed view of the VTCS cooling system locations

### 4.3 VTCS nomenclature

The various systems and components have a dedicated nomenclature to recognize the location and function of the labeled element. All labeling is of the format XY\_ZZ999. Where X is the sub system (P=primary, S=secondary, T=tertiary), Y is the system identification (A for main, B for back-up or L and R for the left and right CO<sub>2</sub> system).

After the underscore the ZZ is the component identifier. For example PT stands for Pressure Transmitter, TT for Temperature Transmitter and VL for Valve. A complete list of the nomenclature is shown in Table 4.3-1. After the component identifier a 3 digit number (shown as “999” in the example) is shown giving a unique label to the component. Numbers starting with a “1” are located in the plant zone of UXA-C3, all numbers starting with “0” are located in the Velo zone.

For the PVSS readout the same labeling sequence is used to label other non-hardware items like PLC variables or non-cooling system sensors like the temperature sensors on the modules. These sensors are of importance for the cooling system monitoring and are therefore relabeled to the same labeling concept. This is done to make the PVSS monitoring, data export and data analysis to be done in a homogeneous way. A list of these nomenclatures is shown in Table 4.3-2.

In some circumstances the labeling may diverge from the above presented method. If a label shares more systems then the dedicated label is shown as an “x”.

Table 4.3-1: Nomenclature of cooling hardware

PA_*****	Primary A system (Water cooling)
PB_*****	Primary B system (Air cooling)
SA_*****	Secondary A system (Main Freon chiller)
SB_*****	Secondary B system (Back-up Freon chiller)
TL_*****	Tertiary Left system (Left CO <sub>2</sub> system for the A-side VELO)
TR_*****	Tertiary Right system (Right CO <sub>2</sub> system for the C-side VELO)
TLR_*****	Tertiary Left and Right system (Labeling for combined used components for Left and Right) (Sometimes label TM_***** is used)
VL_*****	Left VELO detector (A-side)
VR_*****	Right VELO detector (C-side)
**_TT***	Temperature transmitter
**_PT***	Pressure transmitter
**_LT***	Level transmitter
**_VL***	Valve
**_HT***	Heater
**_PM***	Pump (or compressor)
**_AC***	Accumulator
**_BD***	Relieve device (Burst disc)
**_FL***	Filter
**_HX***	Heat exchanger
**_SG***	Sight glass

Table 4.3-2: Nomenclature of PLC and PVSS variables

**_IL***	Interlock signal
**_PV***	PVSS FSM state
**_BA***	Base plate alarm
**_BW***	Base plate warning
**_HA***	Heater alarm
**_HW***	Heater warning
**_PA***	Pressure alarm
**_PW***	Pressure warning
**_MA***	Miscellaneous alarm
**_MW***	Miscellaneous warning
**_BL***	Base plate limit
**_HL***	Heater limit
**_PL***	Pressure limit
**_ML***	Miscellaneous limit
**_PC***	Pressure clock timer
**_MC***	Miscellaneous clock timer
**_VC***	Valve clock timer
**_HC***	Heater clock timer
**_SC***	Clock timer setting

Components have often more than 1 reference to for example an output variable. A pressure sensor gives out a pressure, but as well a saturation temperature and a status. In PVSS these variables are handled with an extra 4 digit code after a dot. For example the pressure variable from pressure transmitter TL\_PT101 is labeled as

TL\_PT101.pres, the saturation temperature TL\_PT101.tsat. Table 4.3-3 shows an overview of the mostly used sub labels.

Table 4.3-3: Nomenclature of the PVSS sub labels

.stat	Status
.temp	Temperature
.tsat	Saturation temperature
.powr	Power (in % of maximum heater power, actually the heater duty cycle)
.watt	Power in Watts
.curr	Current
.volt	Voltage
.PWon	Power switched on (in case of on-off heaters)
.levl	Calibrated level
.rawl	Raw level signal
.posi	Position
.SWon	Switched on
.TRon	Thermal relay on
.TRok	Thermal relay okay
.VLoc	Valve okay
.FRac	Actual frequency
.FRtr	Target frequency
.MPok	Motor protection okay
.alarm	Alarm
.CLtm	Clock timer value
.CLsp	Clock timer set point
.SPac	Actual set-point
.SPtr	Target set-point
.Rthm	Thermal resistance
.lmit	Limit

## 5 Primary cooling system

### 5.1 Overview of the primary systems

The primary cooling for the SA-chiller is the chilled water system of CERN, the primary cooling for the SB-back-up chiller is the air of the cavern. The primary systems are coded with PA (water) and PB (air).

### 5.2 The PA-chilled water system of LHCb

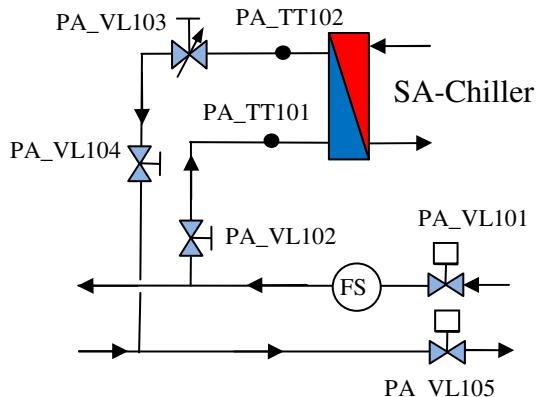


Figure 5.2-2: Simplified scheme of the primary chilled water system.

VTCS is in the same group of the TT and OT cooling stations on the lower platform UXAC2. This group is controlled and monitored by the DSS system of LHCb (7). Figure 5.2-2 shows a schematic of the cold water group of the UXAC platforms. The UXAC group can be shut-off from the main cold water supply using the electrical valves PA\_VL101 and PA\_VL105. The flow is monitored using a flow switch in the supply line. The branch to the VTCS can be shut-off manually for maintenance reasons. In Figure 5.2-1 a photo is shown of the VTCS cooling plant with the coldwater lines in front. The valves on top of the metal shielded part are the manual valves PA\_VL102 and PA\_VL104. These valves are the interface between the LHCb provided piping and the VTCS provided piping.

#### 5.2.1 PA-construction

The inlet piping is a DN20 pipe with a maximum flow rate of  $1.3 \text{ m}^3/\text{h}$ . The flow must be reduced to a maximum water return temperature of  $12^\circ\text{C}$  at the maximum heat load. This reduction is necessary to supply enough cooling water to all the other connected systems. The maximum design heat load is 2.5

The chilled water system of LHCb (6) is for the VTCS the final location for the heat disposal. Although the cold water is cooled by a chilling system as well, from the VTCS point of view it remains to be called the primary system, as it was the final heat dump. The chilled water system is a general supply of chilled water with a temperature of about  $6^\circ\text{C}$ . It is provided from the main LHCb cooling station. The chilled water supply for the

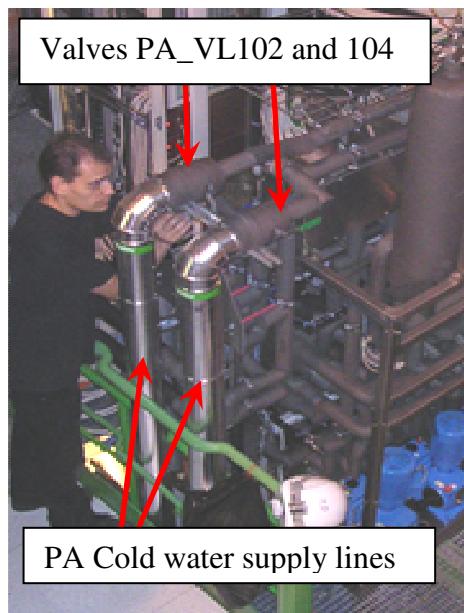


Figure 5.2-1: Cold water supply lines from the CERN cold water system

kW which means that the flow needs to be reduced to 0.36 m<sup>3</sup>/h. Reduction valve PA\_VL103 is set to achieve this flow setting. The in and outlet temperature can be monitored using PA\_TT101 and PA\_TT102.

### **5.2.2 PA- monitoring and control**

The flow of the cold water is monitored with a flow switch. If the flow switch detects insufficient flow a DSS interlock signal will be send to the PLC and the main chiller will be stopped. The detector may not become warm, so the air-cooled back-up chiller is automatically switched on. An air cooled chiller is chosen as back-up to be independent of cooling water failures. Both VTCS plant units have floater switches in the capture bottom to detect a possible leak of the water system. A leak signal will automatically close the 2 in- and outlet valves (PA\_VL101 and PA\_VL105). During maintenance one has to be very careful with the flow switches or the corresponding connectors, a triggering of the VTCS floater switches also stops the OT and TT cooling and hence the OT and TT detectors. As these cooling station are on the same closed off group.

### **5.3 PB air cooling**

The PB air cooling of the SB back-up chiller is not more than a ventilator which cools the condenser of the SB back-up chiller. The airflow inside the plant unit is provided by multiple holes in the unit covers. The ventilator is speed controlled depending on the heat load it must reject. See paragraph 6.2.1.2 for more details about the air cooling of the SB condenser.

# 6 Secondary cooling system

## 6.1 Overview of the secondary systems

The secondary systems are relative ordinary chillers using the HFC refrigerant R507a. The secondary stage cools the two CO<sub>2</sub> condensers of the tertiary CO<sub>2</sub> systems and controls the pressure in the two accumulators. The secondary stages consist of two independent operating chillers. One is a water cooled system for high power and low temperatures (~2.5kW@-40°C) and is referred to as main chiller. The second one is a low power system for warmer temperatures (~1kW@-25°C) and is cooled by ambient air. The air cooled system is a back-up system for the water cooled main chiller. Figure 6.1-1 shows the chiller hardware in the secondary system rack. This rack contains all of the chillers hardware except from the evaporators. The 4 evaporators are placed outside the rack in the tertiary CO<sub>2</sub> rack. The green blocks are the main HFC evaporators cooling the CO<sub>2</sub> condensers, the spirals on top are inside the CO<sub>2</sub> accumulators and control the pressure of the CO<sub>2</sub> in combination with a heater.

In Figure 6.1-2 a simplified scheme of the secondary chillers is shown. The low pressure gas is compressed by the compressor (A) to a pressure with a saturation temperature above the temperature of the primary cold source. In this case the discharge gas (1) will be condensed to liquid in the condenser (B). The condensed liquid is stored in the reservoir (2). The high pressure liquid from the reservoir (2) is sub-cooled in the sub-cooler (D) by exchanging heat with the evaporator exhaust. The cold liquid (3) is expanded by a restriction valve (E) and injected into the evaporator (F). The low pressure liquid starts to evaporate by extracting heat from the tertiary system. The cold gas (5) is fed through the sub cooler (D), where the residual cold is used for the sub-cooling of the inlet liquid. The warmer gas (6) is fed

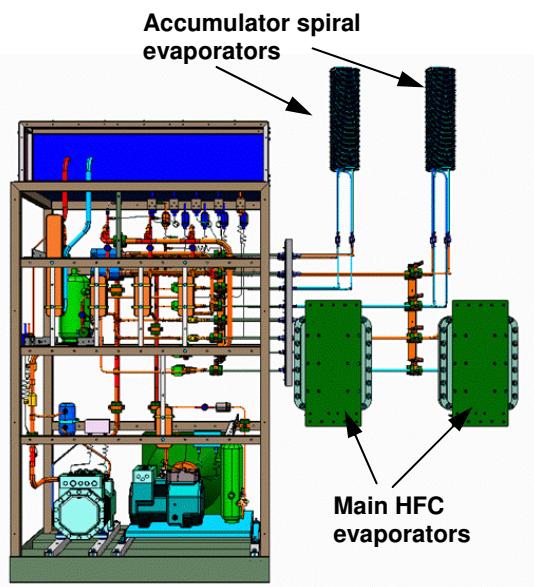


Figure 6.1-1: Both HFC chillers in the chiller rack with the external evaporators.

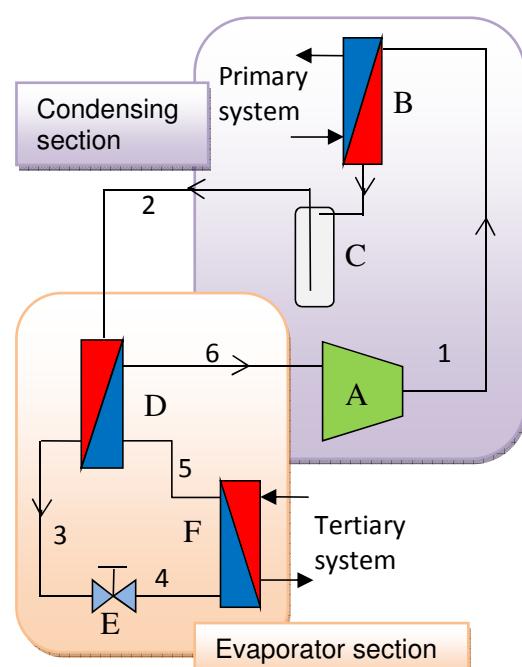


Figure 6.1-2: Simplified scheme of the secondary chillers.

in the sub-cooler (D), where the residual cold is used for the sub-cooling of the inlet liquid. The warmer gas (6) is fed

back to the compressor (A) and the cycle starts over again. Figure 6.1-3 shows the fluid state points 1 to 6 in the Pressure–Enthalpy diagram of the refrigerant R507a. Two cycles are shown. The state points of the SA-main chiller are indicated with A, the state points of the SB-back-up chiller with B. The SA-main chiller is the lower cycle where the evaporator is operating around -40°C and the condenser around 15°C with the cold water source at 6-12°C. The SB back-up chiller operates with an evaporator temperature around -20°C and a condenser temperature of about 35°C to condense against the ambient air temperature.

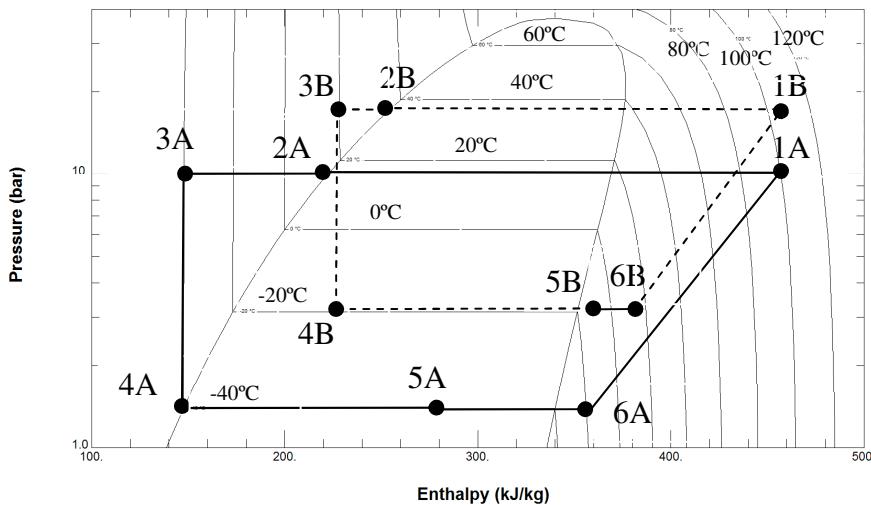


Figure 6.1-3: The SA main and SB back-up chiller in the PH diagram of R507a.

The section from 6 to 2 is called the condensing section (compressor and condenser); from 2 to 6 is the evaporator section (expansion valve, evaporator and sub cooler).



Figure 6.1-4: Secondary SA and SB chillers in the chiller rack

The simplified scheme in Figure 6.1-2 shows only 1 evaporator branch, in reality each system has 4 parallel evaporator branches (2 main HFC evaporators and 2 accumulator spirals). Figure 6.1-3 shows a picture of the HFC chiller rack with most of the hardware visible. Picture was taken before the insulation was applied.

## 6.2 Chiller descriptions.

The next two figures show the full schematic of the SA-Main and SB-Back-up chillers. Larger prints can be found in the appendix at paragraph 11.1. On the left the 4 evaporator sections are shown, on the right the condensing section. In the schematics all parts have unique labeling. A full list of the components with a reference to the unique labeling is

given in the parts lists in the appendix. Paragraph 11.2 shows a list of all the sensors, 11.3 shows a list of actuators and 11.4 shows all the passive line components.

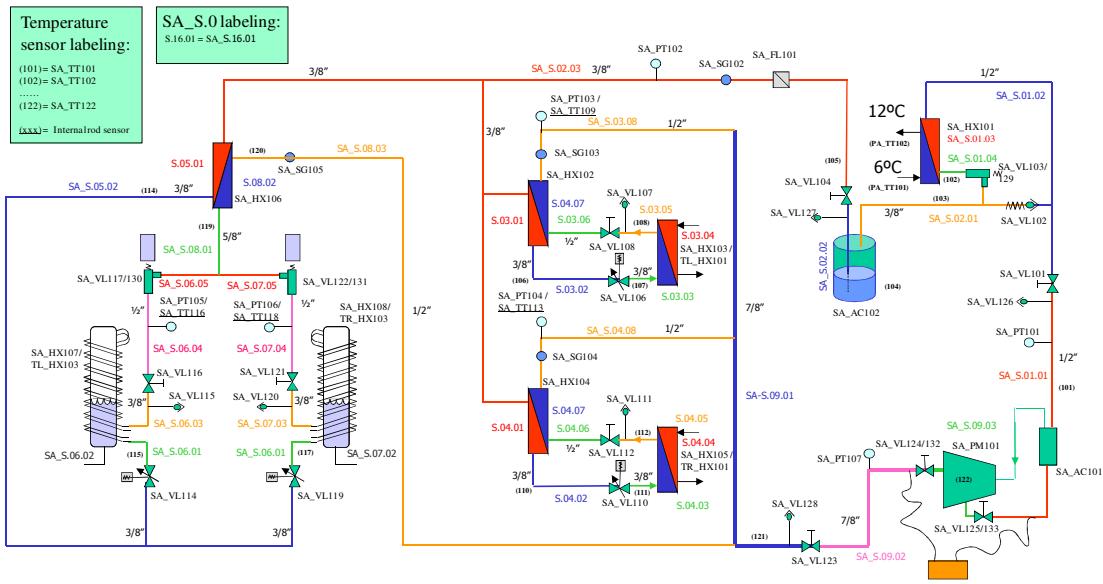


Figure 6.2-1: SA-Main schematic layout.

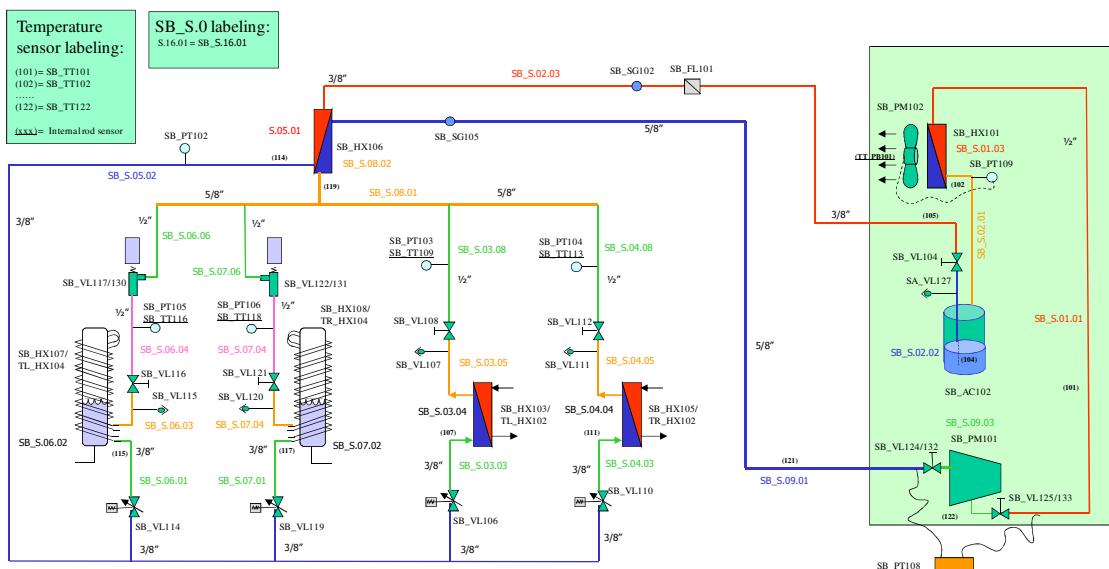


Figure 6.2-2: SB-Back-up chiller schematic layout.

The chillers are divided in several sub-volumes indicated with Sx\_S.yy.yy (where yy.yy is the sub-volume number). The color of the section label corresponds to the near hardware volume with the same color (Blue code belongs to the volume of the blue line). The evaporators sections are sub-volume Sx\_S.03, Sx\_S.04, Sx\_S.05, Sx\_S.06, Sx\_S.07 and Sx\_S.08. The condensing section consists of the sub-volumes Sx\_S.09, Sx\_S.01 and Sx\_S.02. The section volumes are used for charge calculation (paragraph 6.3) and system modeling (chapter 7.7.5).

## 6.2.1 HFC Condensing section

The condensing section of the secondary chillers compresses the low pressure gas and condenses it back to high pressure liquid. Both chillers use different condensing techniques.

### 6.2.1.1 SA Condensing section

Figure 6.2-3 shows the condensing section of the SA-main chiller. The low pressure gas in SA\_S.09.02 is compressed by the compressor SA\_PM101 into the discharge tubes (SA\_S.01.01). The compressor is a frequency controlled Bitzer 2CC-3.2Y compressor with a capacity of about 2.5kW@-40°C. Specifications can be found in the documentation directory on the same EDMS entry. The frequency can be adjusted between 40 and 70 Hz. The compressor is protected against over and under pressure by pressostat SA\_PT108. The high pressure discharge gas is led through oil separator SA\_AC101. This separates most of the oil from the refrigerant and feeds it back to the compressors carter. After the oil separator the discharge gas is cooled, condensed and sub-cooled by the condenser SA\_HX101. The condenser pressure is controlled by pressure regulating valve SA\_VL103. This valve assures that the condenser saturation temperature is above the temperature of the primary chilled water circuit. In this case the R507a can be condensed and sub cooled.

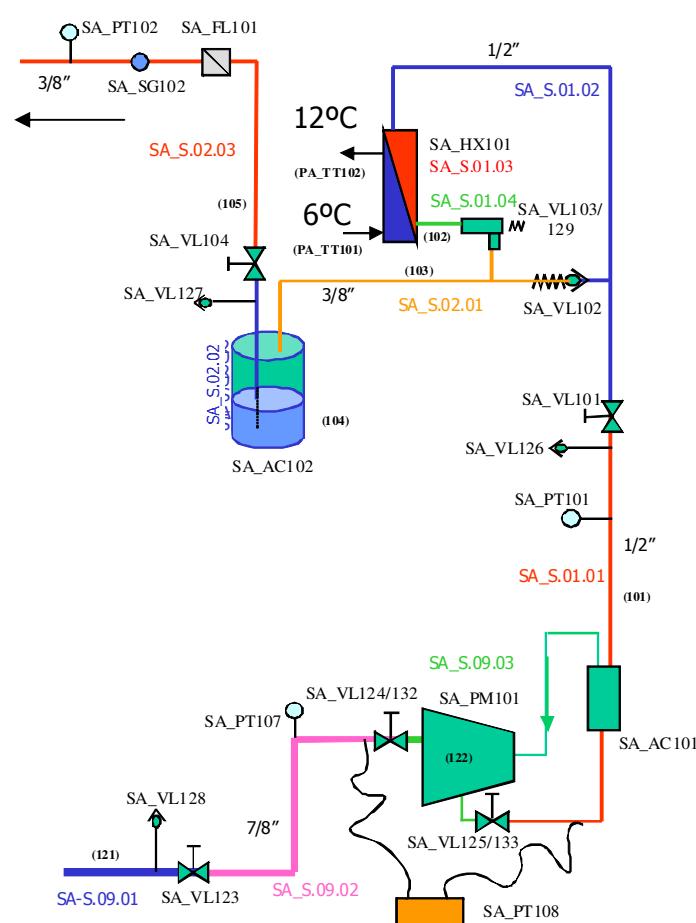


Figure 6.2-3: Detailed schematics of the SA-main condensing section

The liquid is now fed into the reservoir SA\_AC102 which has a volume of 5.6 liter. This reservoir is compensating the varying content of liquid and vapor in the system and will always contain both phases in it. The condenser supplies the liquid to the reservoir; by-pass valve SA\_VL102 supplies the necessary vapor content by directly inject the discharge gas.

The by-pass valve SA\_VL102 is a Danfoss NRD differential pressure valve which starts to open at 1.4 bar and is fully open at 3 bar pressure difference. In this way the pressure of the reservoir is maintained between 1.4 to 3 bar below the condenser pressure setting. The condenser pressure setting of the SA-main chiller is around 10.5 bar, which correspond to a

saturation temperature of about 18 °C. The primary cold water supply is 6°C the outlet varies between 8 and 10 °C depending on the absorbed heat load.

The evaporators are fed with saturated liquid of about 12 °C and 9 bar from the bottom of the reservoir. The liquid supply line contains components such as a filter/dryer (SA\_FL101) and a sight glass (SA\_SG102). The sight glass is used to check whether or not there is indeed liquid in the liquid lines. Passing vapor bubbles indicate an insufficient refrigerant charge.

In Figure 6.2-3 more components are shown than discussed. The system contains extra shut-off valves for maintenance (such as SA\_VL123) and Schrader valves for filling, emptying or extra sensing (such as SA\_VL128). Some line components come with an integrated Schrader valve, if the Schrader valve is not shown the label and existence is indicated by an additional valve number after the original component number like SA\_VL103/129; here 103 is the label for the condenser pressure valve and 129 is the label for the integrated Schrader valve. A full list of the components in the condensing section is given in the parts lists in the appendix. Paragraph 11.2 shows a list of all the sensors, 11.3 shows a list of actuators and 11.4 shows all the passive line components.

### 6.2.1.2 SB Condensing section.

The SB condensing section is a standard air cooled condensing unit from Bitzer. The LH32/2KC-05.2y condensing unit contains all the hardware inside the green box of Figure 6.2-2 (Detailed view in Figure 6.2-4). It consists of an air cooled condenser with a variable speed fan, a 2KC-05.2y Bitzer compressor and a 3 liter reservoir. The capacity of the condensing unit is around 1kW @ -25°C. The condensing pressure is regulated by the fan speed and is controlled around 15.5 bar which corresponds to a condensing temperature of about 32 °C. The exit air temperature is around 28 °C.

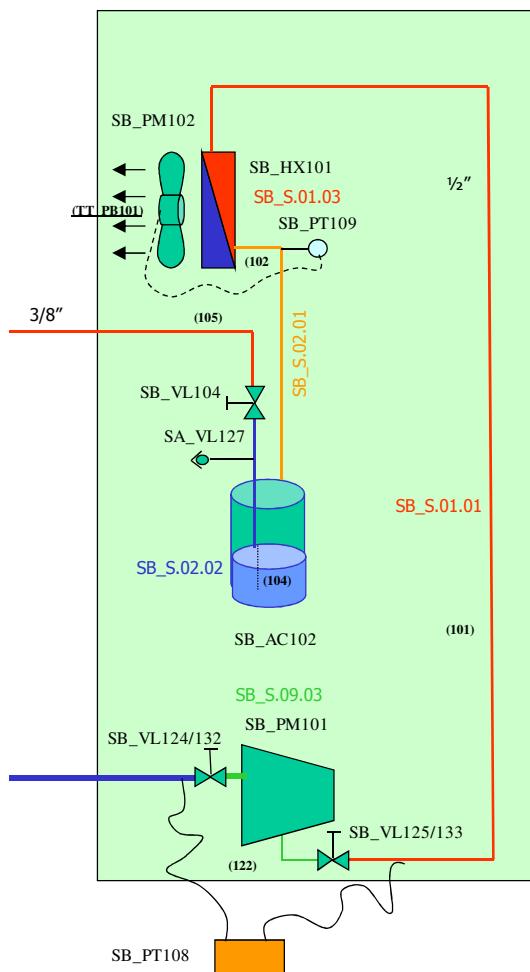


Figure 6.2-4: Detailed schematics of the SB-Back-up condensing section

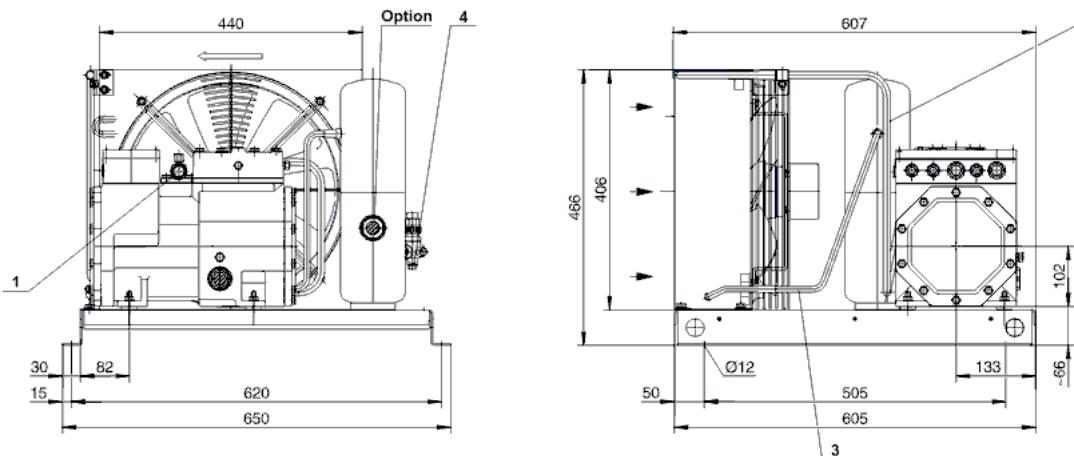


Figure 6.2-5: The Bitzer LH32/2KC-05.2y condensing unit

### 6.2.1.3 Condensing section components

Figure 6.2-6 and Figure 6.2-7 show pictures of several condensing section components. A full list of these components is given in the parts lists in the appendix. Paragraph 11.2 shows a list of all the sensors, 11.3 shows a list of actuators and 11.4 shows all the passive line components.

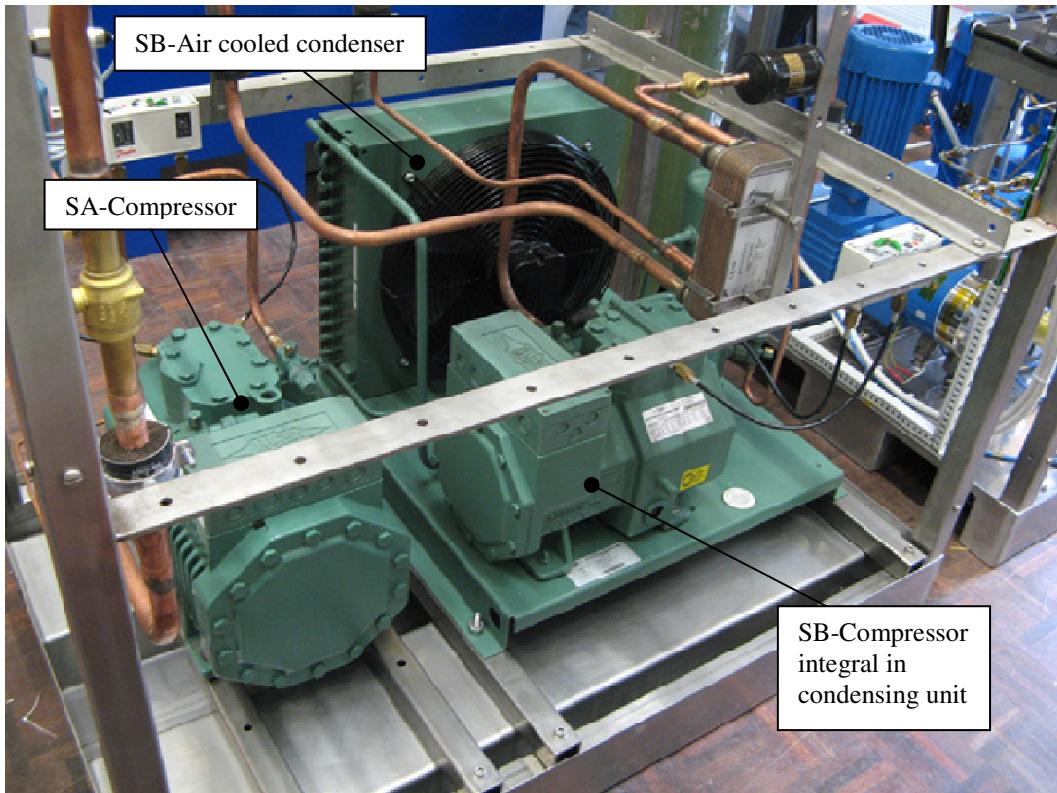


Figure 6.2-6: The SA compressor and SB condensing unit in the chiller rack.

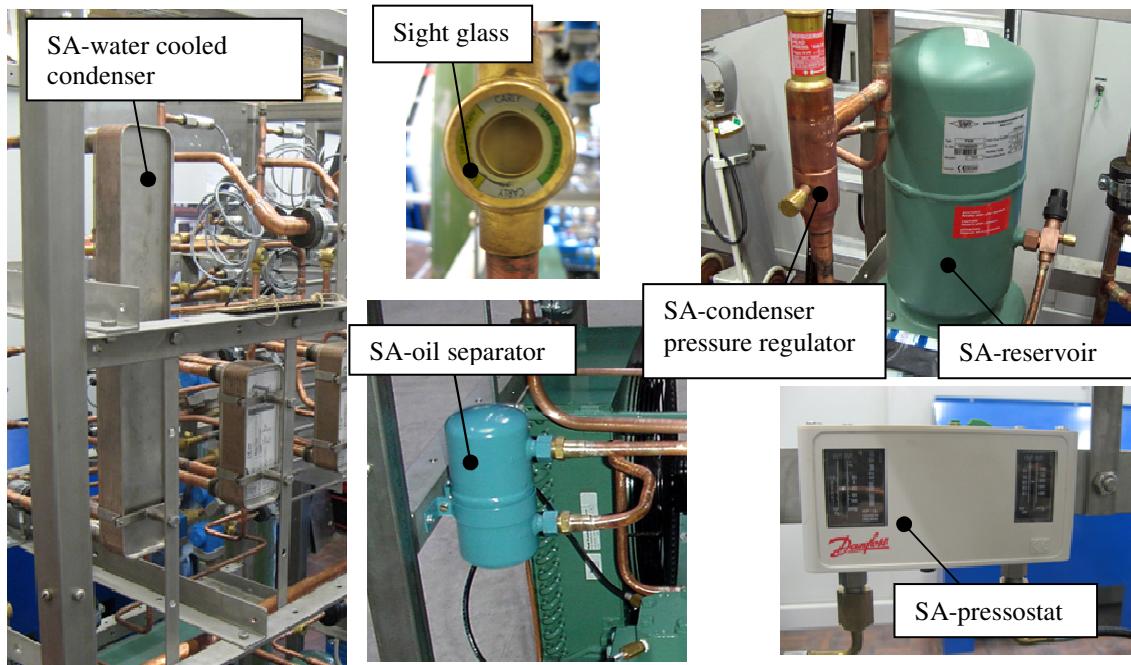


Figure 6.2-7: SA condensing section components

### 6.2.2 HFC Evaporator sections.

Both the SA-main and SB-back-up chillers have 4 parallel HFC evaporator branches. These branches are all fed with high pressure warm R507a liquid from the reservoir of the condensing section. After expansion in the controlled injection valve the low pressure cold liquid is evaporated and the low pressure gas is fed back to the compressor.

There are 2 different type of HFC evaporators in the chillers. The 2 main HFC evaporators are cooling the CO<sub>2</sub> condensers, the other 2 HFC evaporators are the accumulator spirals evaporators, these are cooling the CO<sub>2</sub> accumulators. See Figure 6.1-1 for the evaporator locations. The main HFC evaporators are commercially brazed plate heat exchangers from SWEP. These plate heat exchangers are reinforced with steel plates for the high CO<sub>2</sub> pressure. The accumulator spiral evaporators are 3/8" x 0.035" coiled tubes constructed inside the CO<sub>2</sub> accumulator. Figure 6.2-8 shows the principle of the evaporator spiral inside the accumulator vessel.

Both tertiary CO<sub>2</sub> systems are connected to the SA-main and SB-back-up chillers. Each tertiary CO<sub>2</sub> system is connected to four HFC evaporators. Two of these HFC evaporators are connected to the SA and two connected to the SB chiller. Figure 4.1-2 shows schematically the cross linked configuration.

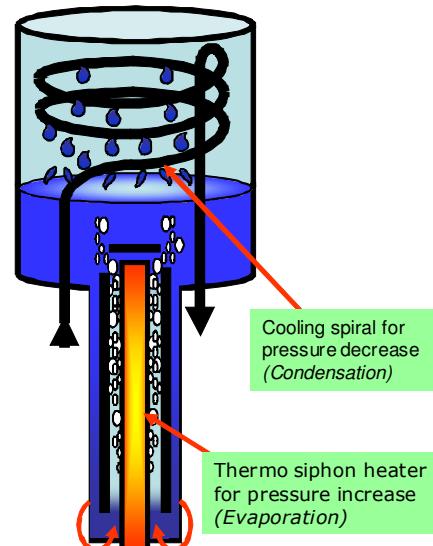


Figure 6.2-8: Principle of the CO<sub>2</sub> accumulator

All the evaporator branches are mass flow controlled using binary electronic restriction valves. The flow is controlled using the PWM (Pulse Width Modulation) method. Regulation of the refrigerant flow in the evaporator branches is achieved by controlling the outlet super heated gas temperature. The evaporator inlet liquid is sub cooled in sub-cooler (Sx\_HX106) which uses the excess cold of evaporator cold gas from the outlet. In this way the vapor quality in the inlet of the evaporator is lower and the heat transfer is more efficient.

The inlet temperature of the CO<sub>2</sub> condensing side connected the HFC evaporator must be higher as the requested super heating temperature of the HFC refrigerant. In this way the CO<sub>2</sub> temperature is able to generate the requested super heating. In case of the CO<sub>2</sub> condensers of the SA main chiller this not always the case. At low CO<sub>2</sub> set-points the CO<sub>2</sub> inlet temperature can be too low not to generate sufficient superheating. Therefore the super heated vapor is controlled after the sub-cooler (SA\_HX102 and SA\_HX104). The main function of this heat exchanger is not any more to obtain sub-cooling of the inlet liquid, its main function has now become super heating of the outlet flow. Therefore these heat exchangers are called super heaters rather than sub-coolers. A consequence of this is that the two main evaporator branches have a dedicated heat exchanger in their evaporator branch. The other evaporator branches (2 accumulator branches in SA and all 4 evaporators in SB) share 1 sub-cooler. In both cases this is Sx\_HX106. The effect on the evaporator of the displaced superheat control is clearly visible in the enthalpy-pressure cycles in Figure 6.1-3. State point 5 is the evaporator outlet; for the SA cycle this is in the 2-phase area, for the SB cycle this is in the superheated vapor area.

The AKV10 expansion valve is used for all 4 evaporator branches. The AKV10 is an electrically operated expansion valve using a solenoid operated armature for closing and opening a small orifice restriction. A drawing cut of the valve is shown in Figure 6.2-9. The restriction is #3 and the armature #6. The binary solenoid valve is made proportional using pulse width modulation with a modulation time of 6 seconds. The maximum capacity of the valve can be adjusted using a different orifice. The SA main evaporator branches have a 2kW orifice, the accumulator spiral evaporators and SB main evaporators branches a 1.2 kW orifice.

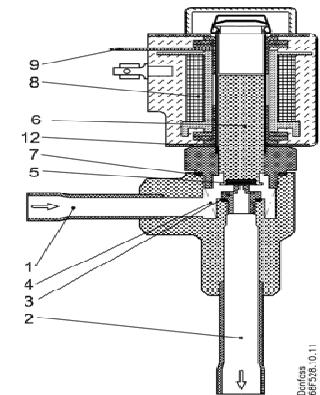


Figure 6.2-9: The AKV10 expansion valve

A full list of the other components in the evaporator section is given in the parts lists in the appendix. Paragraph 11.2 shows a list of all the sensors, 11.3 shows a list of actuators and 11.4 shows all the passive line components.

### 6.2.2.1 SA main HFC evaporator branches for cooling the CO<sub>2</sub> condensers.

Figure 6.2-10 and Figure 6.2-11 show the schematic layout of the two main HFC evaporator branches that cool the two CO<sub>2</sub> condensers. They both have their own dedicated super heater as discussed in the previous chapter. The refrigerant flow is regulated using the overheating after the super heater. The evaporator itself stays completely two-phase which induces a better heat transfer in the evaporator itself.

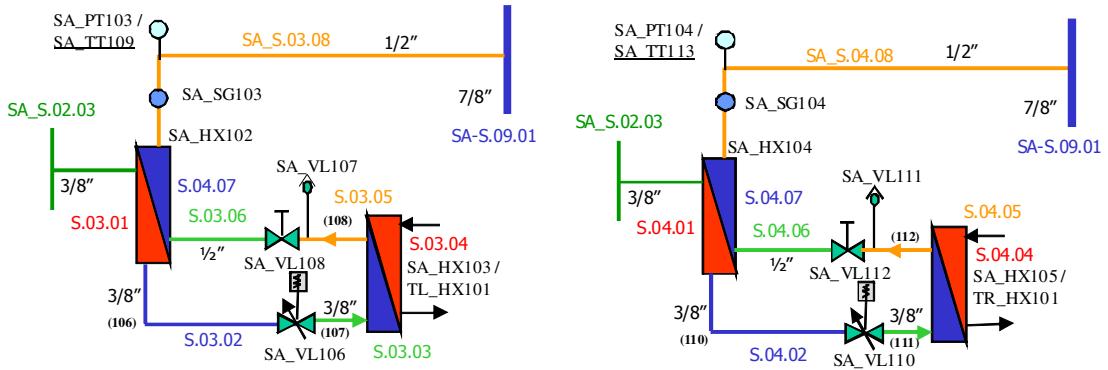


Figure 6.2-10: Main HFC Evaporator (branch 1) for the TL CO<sub>2</sub> condenser      Figure 6.2-11: Main HFC Evaporator (branch 2) for the TR CO<sub>2</sub> condenser

The warm high pressure inlet liquid from the reservoir is cooled by the outlet super heater. (SA\_HX102 & 104). The cold liquid approaches the same temperature of the evaporator (See Figure 6.1-3). The cold liquid is expanded from the high reservoir pressure to the low evaporator pressure by the electronic expansion valve (SA\_VL106 & 110). The inlet liquid is saturated so evaporation is present in the main HFC evaporator (SA\_HX103 & 105). The remaining liquid and vapor is fed through the super heater where the excess liquid is evaporated and superheated. The super heated vapor temperature (A combination of SA\_PT103 with SA\_TT109 and SA\_PT104 with SA\_TT113) is used to control the expansion valve (See paragraph 6.4.1. for details on the expansion valve control).

The main HFC evaporators are reinforced brazed plate heat exchangers from SWEP. They are reinforced because of the high pressures in the CO<sub>2</sub> side. The reinforcing metallic plates protect the heat exchangers from bursting. The CO<sub>2</sub> operates with pressures up to 100 bar (170 bar proof pressure), while R507a has low pressures. The internal structure of this heat exchanger must withstand this pressure difference as well. A special double wall heat-exchanger from SWEP was used. This B16DW series has double plates and a small wave pattern. This combination makes the plate heat exchanger suitable for withstanding these high pressure differences. The VTCS safety document (8) gives a detailed design and testing overview of this custom made heat exchanger.

### 6.2.2.2 SA accumulator spiral evaporators.

Figure 6.2-12 shows the schematic layout of the SA accumulator spiral evaporators branches 3 and 4. The CO<sub>2</sub> pressure in the accumulator is controlled by heating and cooling of the two-phase content. A CO<sub>2</sub> pressure decrease is achieved by condensing of the vapor in the upper region using the HFC spiral evaporator. Pressure increase of the CO<sub>2</sub> is achieved by evaporating the liquid using an electrical heater in the bottom part of the accumulator (See Figure 6.2-8). The expansion valves (SA\_VL114 & SA\_VL119) are not controlled by the evaporator outlet superheating, but by the accumulators PID pressure control. The capacity of the cooling spiral is of the same order as the heating capacity of the liquid heater. The accumulator's PID control combines both actuators in 1 algorithm, where the cooling effect of the expansion valve control is treated as a negative heating element. More about this combined accumulator control can be found in paragraph 7.7.1.

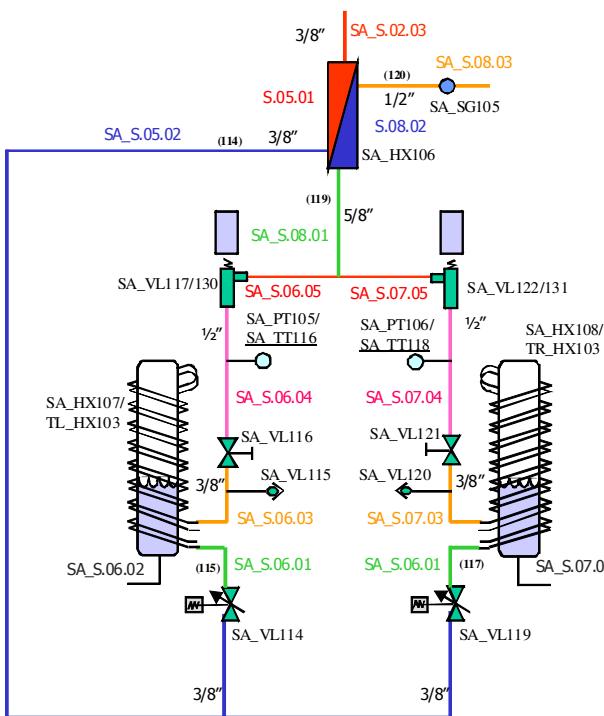


Figure 6.2-12: Evaporator section 6&7 cooling the CO<sub>2</sub> accumulators

top of the vessel and have feed-throughs at the bottom flange. Figure 6.2-13 shows the accumulator during assembly. The evaporator spirals are clearly visible. The spirals are rolled up 3/8" x 0.035" stainless steel tubes with a length of 10.1 m. There are 2 coils in the accumulator, one connected to the SA-Main chiller, the other connected to the SB-back-up chiller.

### 6.2.2.3 SB Evaporator branches.

Contrary to the SA evaporator branches, all SB evaporator branches use one common sub cooler. The main evaporator branches (SB\_HX103 & 105) connected to the CO<sub>2</sub> condensers have the super heating control directly at the outlet of the evaporator. The superheating (a combination of SB\_PT103 with SB\_TT109) controls the refrigerant flow of the main evaporator SB\_HX103 (cooling the TL condenser) by adjusting the injection valve SB\_VL106. The SB\_PT104 with SB\_TT113 superheating controls the injection valve SB\_VL110 for main evaporator SB\_HX105 (cooling the TR condenser). The accumulator evaporator branches of SB are identical to the branches of the SA main chiller.

Both SA evaporator branches for the accumulator control use one combined sub cooler (SA\_HX106). Each evaporator branch has a manual back-pressure regulator which limits the evaporator pressure, so a minimum temperature of the CO<sub>2</sub> accumulators can be set. Both branches have super heating sensing by pressure and temperature sensors combinations SA\_PT105/SA\_TT116 and SA\_PT106/SA\_TT118. The superheating sensing is not used to control the refrigerant flow they are only present for monitoring.

Inside the accumulators two-coiled spirals are installed for condensing the CO<sub>2</sub> vapor in the vessel. The coils are located in the



Figure 6.2-13: Cooling spirals in the accumulator

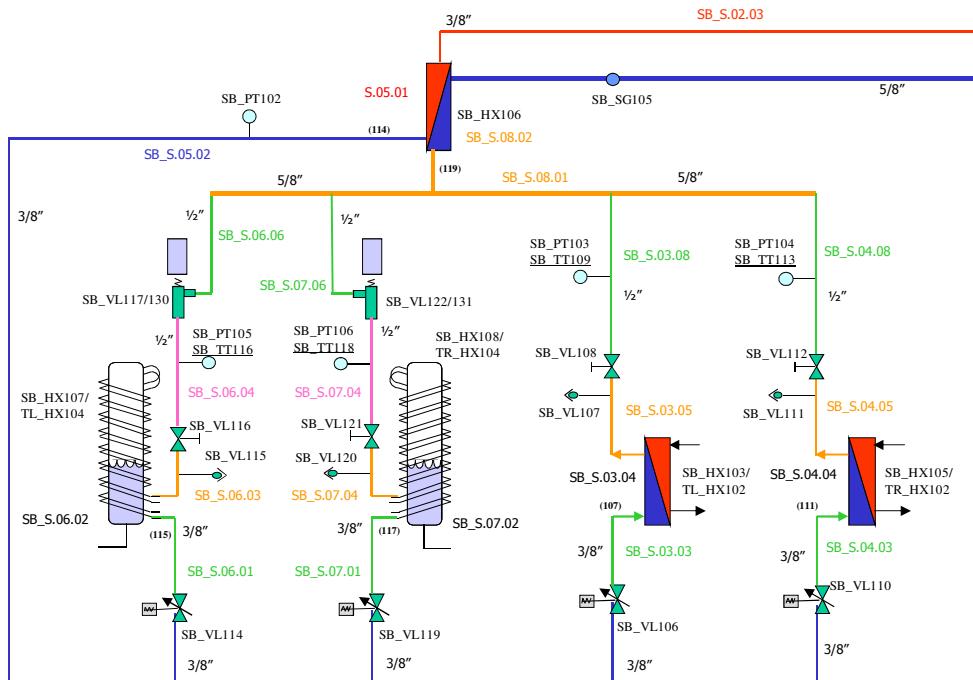


Figure 6.2-14: All four SB evaporator branches.

#### 6.2.2.4 Evaporator section components

A full list of the components in the evaporator section is given in the parts lists in the appendix. Paragraph 11.2 shows a list of all the sensors, 11.3 shows a list of actuators and 11.4 shows all the passive line components.

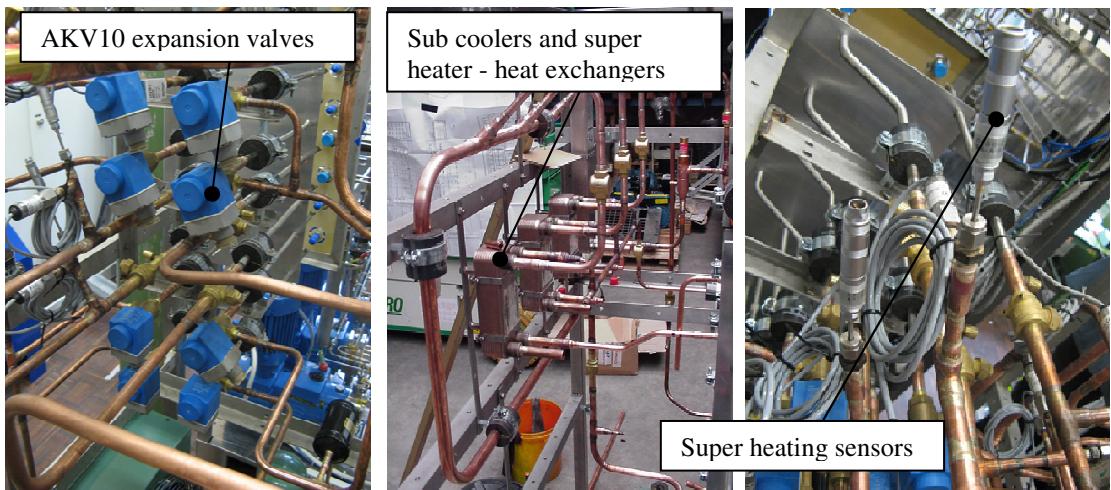


Figure 6.2-15: Evaporator section components

### 6.3 Chiller volumes and charges

A chiller must have sufficient refrigerant charge to have liquid in the supply lines, sufficient liquid in the evaporators and gas in the suction lines. The evaporators and condenser have a varying refrigerant content depending on the cooling temperature and absorbed heat load. This varying liquid/vapor content must be accumulated in the reservoir. This reservoir must have always liquid and vapor present.

The submerged suction tube in the reservoir must always be below the liquid level. In this case the evaporators are fed with liquid of the right enthalpy. At a too low charge,

the submerged tube will suck vapor bubbles and the total inlet enthalpy of the evaporators will increase. With higher inlet enthalpy less cooling power for the evaporators is available. The first signs of a too low charge can be seen by vapor bubbles in the sight glass SA\_SG102. The needed refrigerant charge is determined by calculating the fillings under nominal conditions and the two extremes. The extreme for the lowest reservoir level is a total flooding of all the evaporators and the condensers. This is a worst case situation for a too low heat input. A total flooding however will never appear, since a zero heat input is never taking place due to environmental heat loads, and alarms like the compressor low pressure will be triggered far before. The worst case for the highest level in the reservoir takes place during maintenance. In this case the liquid lines, the evaporators and cold gas lines are emptied by the compressor. The fluid is stored this way in the reservoir after being condensed in the condenser.

Table 11.5-1 and Table 11.5-3 show volumes of the several sections of the two chillers as indicated in the schematic of Figure 6.2-1 and Figure 6.2-2 . For each volume the refrigerant state is calculated for a nominal operation. When the state of the fluid in each section is known, the density per volume can be calculated and so the needed refrigerant mass.

Table 6.3-1 and

Table 6.3-2 show summaries of the combined volumes of the several sections. At the bottom off the table the corresponding reservoir levels are given for the nominal level, the minimum level (All external heat-exchangers flooded) and the maximum level (All the liquid stored in the reservoir). With a refrigerant charge of 4.5 kg in SA and 2.7 kg in SB there is in all cases sufficient liquid remaining in the reservoir.

A state point model of the chillers is made using the sections as marked in the schematic drawings (Figure 6.2-1 and Figure 6.2-2). In this state point model the pressure and enthalpy at each section is calculated in an iterative calculation process. A detailed description of the state point model is explained in chapter 9. From the enthalpy-pressure state points the temperature and density of the section volumes can be derived using the integrated Refprop database (9). The mass filling at each section is known this way. The state point results of the SA and SB chiller for a nominal situation including the derived mass filling is shown in the appendix in Table 11.5-1 and Table 11.5-3.

Table 6.3-1: Overview of the SA volumes, charge and reservoir levels

Discharge and condensing section	1.25	Liter
Liquid and buffer section	5.78	Liter
Evaporator section	4.04	Liter
Cold gas section	1.28	Liter
System volume w.o. reservoir	6.74	Liter
Total system volume	12.34	Liter
Max flooded volume	2.85	Liter
Reservoir volume	5.60	Liter
Filling	4.5	kg
Homogeneous filling	0.36	kg/L
Maximum buffer level	74.10%	
Nominal buffer level	48.98%	
Minimum buffer level	14.25%	

Table 6.3-2: Overview of the SB volumes, charge and reservoir levels

Discharge and condensing section	0.82	Liter
Liquid and buffer section	3.32	Liter
Evaporator section	2.23	Liter
Cold gas section	0.52	Liter
System volume w.o. buffer	3.90	Liter
Total system volume	6.90	Liter
Max flooded volume	1.90	Liter
Reservoir	3.00	Liter
Filling	2.7	kg
Homogeneous filling	0.39	kg/L
Maximum buffer level	83.75%	
Nominal buffer level	70.26%	
Minimum buffer level	14.00%	

## 6.4 Chiller operation and control

The SA-Main chiller is operated by 9 controlled actuators. 4 of these actuators are mechanically controlled with a onetime adjustment. These are the condenser control valves SA\_VL102 and SA\_VL103 (see paragraph 6.2.1.1) and the evaporator control valves SA\_VL117 and SA\_VL122 of the accumulator evaporators (see paragraph 6.2.2.2). The other 5 actuators are electrically controlled by the PLC. Four are electronic expansion valves SA\_VL106, SA\_VL110, SA\_VL114 and SA\_VL119 (see paragraph 6.2.2) the other one the frequency controlled compressor SA\_PM101 (see paragraph 6.2.1.1). The SB Back-up chiller has a different condenser pressure control. No valves are present but a frequency control of the ventilator speed maintains the condensing pressure. A local electronic control (SB\_PT109) controls independent from the PLC the fan speed. The SB evaporator branches are controlled in a similar way as the SA evaporator branches. The expansion valves SB\_VL106, SB\_VL110, SB\_VL114 and SB\_VL119 are controlled electronically by the PLC while the evaporator control valves SB\_VL117 and SB\_VL122 are set manually. The SB compressor has no frequency control. It is operated at 50 Hz at all time. Detailed explanation about the control algorithms is discussed in the PLC code documentation (10).

### 6.4.1 Control of the SA evaporator branches cooling the CO<sub>2</sub> condensers

The expansion valves SA\_VL106 and SA\_VL110 regulate the amount of needed refrigerant to condense and sub cool the CO<sub>2</sub> in the heat exchangers SA\_HX103 and SA\_HX105. The flow is regulated by measuring the overheating of the exhaust of heat exchanger SA\_HX102 and SA\_HX104. The overheating is the measured temperature of SA\_TT109 minus the translated saturation temperature of pressure sensor SA\_PT103 for the branch 1 evaporator and SA\_PT113 and SA\_PT104 for branch 2 evaporator. Figure 6.4-1 shows

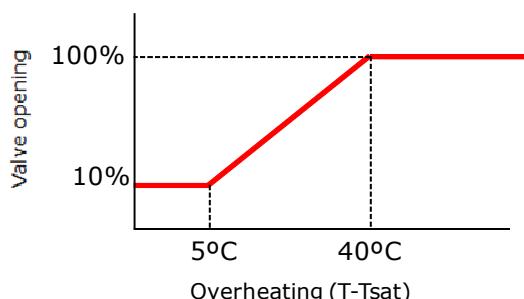


Figure 6.4-1: Expansion valve control

the control relation between the measured overheating and the expansion valve set-

point. A direct control was applied as a PID control was too hard to implement due to the difficult dynamics of the sub cooling cycle. The super heater has a direct influence of the inlet condition, which together with the delay between inlet and outlet condition makes it hard to regulate. The present control makes the evaporator flow to vary a lot but is never exceeding the alarm limits as a previous PID control did. The variations however are not a problem for the system behavior. The CO<sub>2</sub> temperature in the detector is very stable as the 2PACL principle is damping out any variations at the condenser side. This is exactly where it was designed for in the AMS-TTCS; damping out the orbital variations. This good feature of the 2PACL behavior did make further tuning of the chiller unnecessary. An example of the measured dynamic behavior of the SA evaporators is shown in Figure 6.4-2.

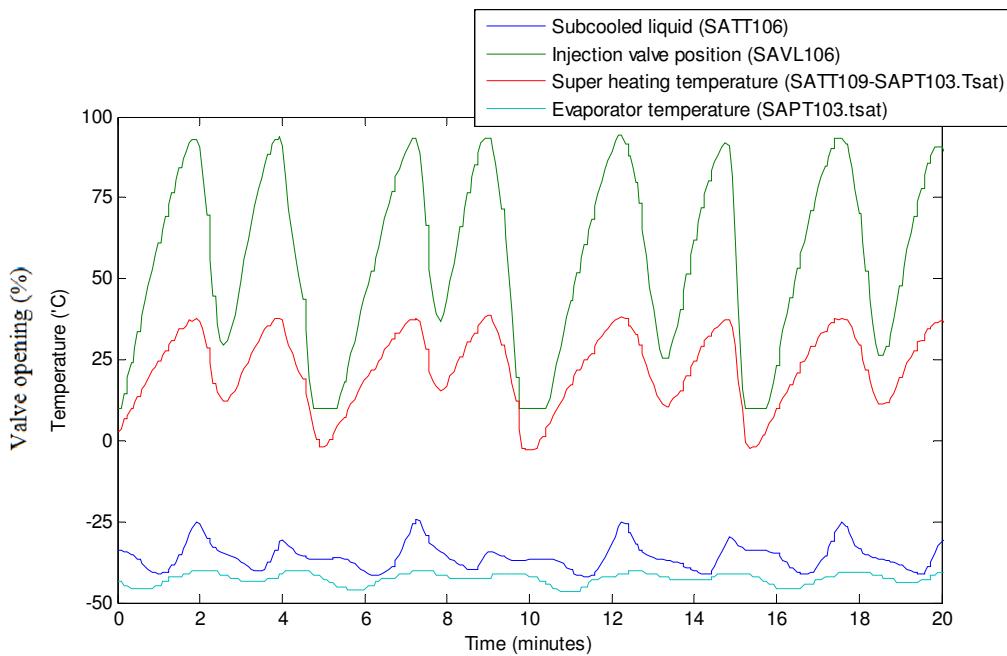


Figure 6.4-2: Dynamic behavior of the SA main HFC evaporator control.

#### 6.4.2 Control of the SB evaporator branches cooling the CO<sub>2</sub> condensers

The expansion valves SB\_VL106 and SB\_VL110 regulate the amount of needed refrigerant to condense and sub cool the CO<sub>2</sub> in the heat exchangers SB\_HX103 and SB\_HX105. The flow is regulated by measuring the super heating of the exhaust of the evaporators. The super heating is the measured temperature of SB\_TT109 minus the translated saturation temperature of pressure sensor SB\_PT103 for the evaporator branch 1 and SB\_TT113 and SB\_PT104 for evaporator branch 2. A PID algorithm in the PLC maintains the super heating around 10°C.

#### 6.4.3 Control of the SA and SB accumulator spirals evaporators.

The control of the expansion valves for the accumulator spirals is integrated in the PID control of the accumulator pressure control. The capacity of the cooling spiral is of the same order as the heating capacity of the liquid heater. The accumulator's PID control combines both actuators in 1 algorithm, where the expansion valve control is treated as a negative heating element. More about this combined accumulator control can be found in paragraph 7.1.1. The control of SA and SB is identical.

#### 6.4.4 Control of the SA compressor suction pressure.

The varying refrigerant flow caused by the 4 different expansion valve settings causes a varying suction pressure in the compressor. The compressor is a fixed volume flow pump, meaning a smaller mass flow needs a smaller density. The smaller density results in a lower pressure in front of the compressor. The suction pressure has a direct influence on the evaporation pressure in the two CO<sub>2</sub> condensers. The pressure of these two branches are not controlled by an additional pressure regulator as it is the case for the accumulator branches. The varying suction pressure therefore causes a varying evaporation temperature and hence a varying CO<sub>2</sub> liquid temperature.

For the VTCS it is not important to have stable chiller temperatures as the 2PACL principle in the CO<sub>2</sub> system will dampen all the temperature fluctuations of the cold CO<sub>2</sub> liquid. The fluctuations in the CO<sub>2</sub> liquid flow are not influencing the CO<sub>2</sub> evaporator temperatures in the VELO detector. The fluctuations in the chiller temperatures are directly caused by the fluctuations in the suction pressure of the compressor. The suction pressure of the compressor need to stay within reasonable limits for several reasons. A too low suction pressure has a low massflow as a result. This will give insufficient cooling of the compressor itself. The low suction pressure in the chiller will give a low evaporation pressure and hence a low evaporation temperature, this low temperature may cause the CO<sub>2</sub> to freeze which freezes around -56°C . A too high suction pressure will limit the ability of the VTCS to run cold as the evaporation temperature increases.

To stay within a good range a frequency control of the compressor was implemented. For high heat loads a large speed is needed to maintain the pressure low enough, for low heat loads a low speed is required not to go too low in suction pressure. A too low suction pressure will trigger the low pressure alarm of pressure switch SA\_PT108, which needs to be avoided at any time. Figure 6.4-3 shows the relation between the frequency set point as a function of the measured suction pressure.

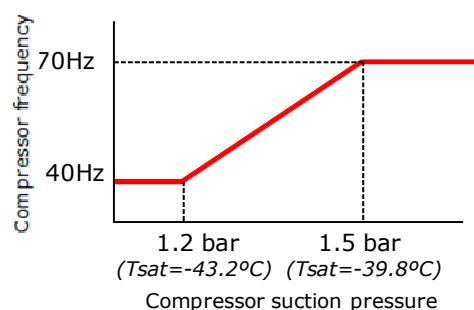


Figure 6.4-3: Compressor speed control

#### 6.4.5 Chiller alarm handling.

A proper operation of the chillers is monitored by the PLC. If the system is out of its design working range alarms are generated and proper actions are taken. The alarm handling procedure is in detail described in the user manual (11). A table with the alarms properties can be found in the appendix at paragraph 11.6.

## 7 Tertiary cooling system

### 7.1 Overview of the Tertiary CO<sub>2</sub> 2PACL systems

Each detector half is cooled by an individual CO<sub>2</sub> circulation loop. The 2 CO<sub>2</sub> loops are cooled by a common HFC chiller (see Figure 4.1-2). The two CO<sub>2</sub> loops are running independently from each other, but have some interconnects and share the same back-up pump. The interconnections are only used in emergency cases and can connect both detector halves or transfer lines to a single loop. The tertiary CO<sub>2</sub> loops connect the detector in the experimental cavern via the so-called transfer lines to the cooling plant in the safe zone on the UXAC3 platform. (See Figure 4.2-2). Figure 7.1-1 shows a schematic interpretation of the CO<sub>2</sub> loops as they are implemented in the LHCb cavern. The CO<sub>2</sub> plant with all the control hardware is located in the safe zone next to the secondary chillers and are shielded from radiation by the thick concrete shielding wall. The plant part is always accessible for maintenance or troubleshooting. The evaporators in the detector and large part of the transfer lines located in the experimental zone are hard to access. This hardware is only passive so the risk of an unreachable failure is limited.

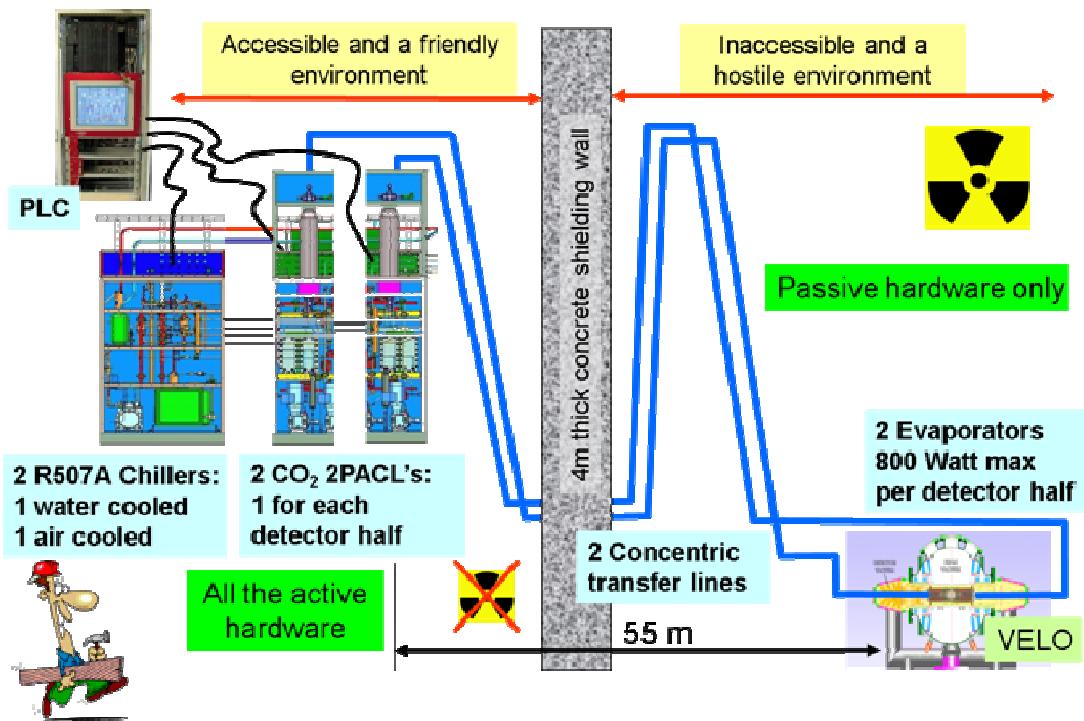


Figure 7.1-1: Artistic view of the tertiary CO<sub>2</sub> loops in LHCb

#### 7.1.1 2PACL principle

The tertiary CO<sub>2</sub> loops use a novel technology of controlling the evaporator pressure and enthalpy. The principle is called 2-Phase Accumulator Controlled Loop (2PACL) (4) and is originating from satellite cooling systems. It was developed for the AMS-TTCS (5) by Nikhef and NLR. The 2PACL principle controls the evaporator pressure and inlet enthalpy remotely and is therefore ideal for cooling and temperature control of an inaccessible detector. In the case of the VTCS, all the control is located in the plant in the safe area, the evaporator and transfer lines are only passive tubing. Figure

7.1-2 shows a simplified scheme of the 2PACL as it is implemented for the VELO in LHCb.

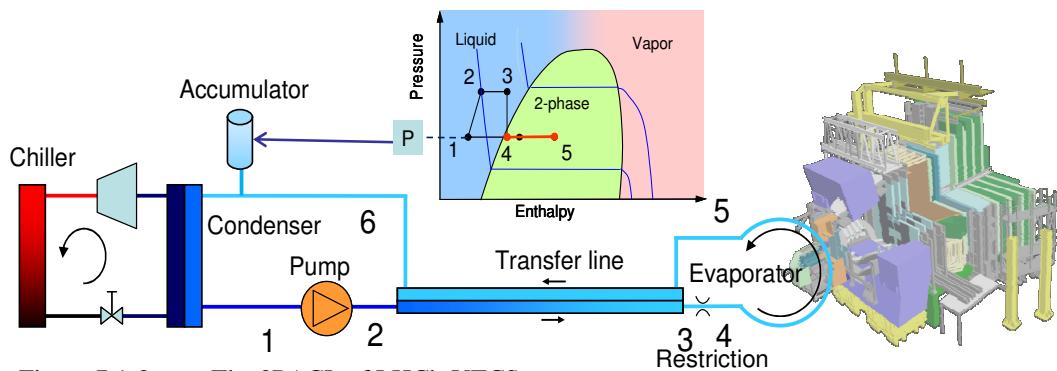


Figure 7.1-2: The 2PACL of LHCb-VTCS

A 2PACL is a liquid circulation loop where the sub cooled liquid is heated to saturation by an internal heat exchanger. The evaporator, the return tube and the condenser are connected without a significant pressure drop and thus work at the same pressure. An accumulator vessel is side mounted in front of the condenser, controlling this pressure. The accumulator is designed to have always a liquid and vapor content. Evaporating the accumulator's liquid or condensing the accumulators vapor directly influences the pressure of the accumulator, condenser, return tube and the evaporator.

The regulation of the system work as follows (see Figure 7.1-2 for node locations); the accumulator vessel needs to be maintained at a fixed temperature and hence pressure set-point. This is achieved with a cooling and heating combination. The pressure drop between the outlet of the evaporator (5) and the accumulator connection (6) is low, therefore the accumulator directly controls the pressure of the evaporator. The transfer line / internal heat exchanger (2-3) heats up the pumped sub-cooled liquid to saturation, causing the inlet of the evaporator always to be saturated (point 4 within green 2-phase zone of the pressure-enthalpy diagram). The system works with an overflow of liquid. The fluid state in the evaporator is per definition 2-phase, and independent from the absorbed heat. The independence of heat absorption is ideal for detector cooling as they need to be kept cold all the time, even if there is no dissipated power in the detector. The returning vapor is condensed in the condenser (6-1) which is cooled by a standard chiller. The sub cooled liquid (1) is pumped back into the system by a liquid pump (1-2). The chiller of the VTCS remains always cold (around  $-40^{\circ}\text{C}$ , depending on heat load) and the accumulator can be set between  $-5^{\circ}\text{C}$  and  $-35^{\circ}\text{C}$ .

The key items in the system are the accumulator and the transfer line. They are responsible for the condition of the evaporator. More details about the working of the accumulator and transfer line are given in paragraph 7.4.1 and 7.3.

### 7.1.2 Tertiary schematics

Figure 7.1-3 shows a simplified scheme of the CO<sub>2</sub> systems. The A side of the VELO detector is cooled by the TL (Tertiary Left) system, the C-side is cooled by the TR (Tertiary Right) system. A shared back-up pump is available. Related system hardware is referred to as TLR (Tertiary Left-Right) system. Both TL and TR are connected to the SA-Main chiller and the SB-Back-up chiller. The TL and TR are

identical, except from the TLR pump cooling. This extra heat exchanger is only in the TR system and is used to maintain the “not-used” TLR pump cold, so a cold start-up is possible.

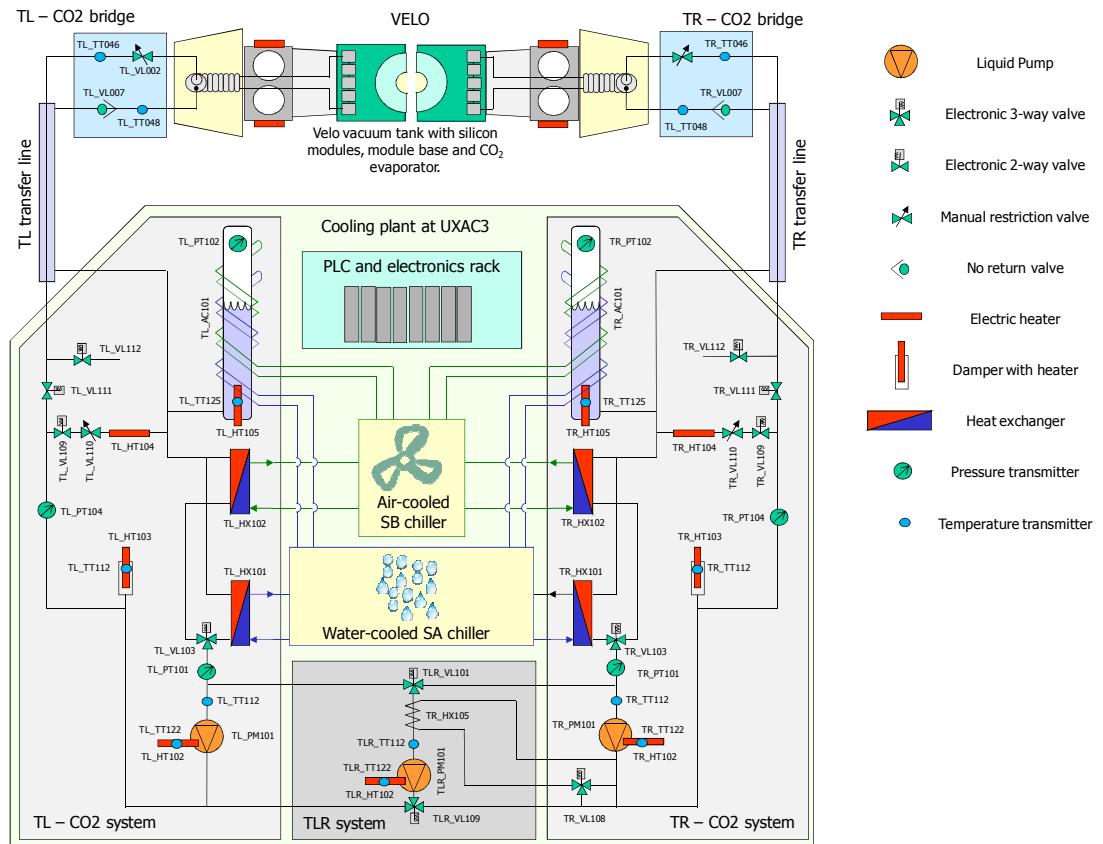


Figure 7.1-3: Simplified schematics of the tertiary  $\text{CO}_2$  systems

In the above scheme only the important hardware is shown and labeled. Detailed schematics can be found in the appendix in paragraph 11.1. A full list of the components in the tertiary systems is given in the parts lists in the appendix. Paragraph 11.2 shows a list of all the sensors, 11.3 shows a list of actuators and 11.4 shows all the passive line components.

## 7.2 VTCS hardware at VELO

The hardware of the VTCS located inside the VELO cave is the evaporator, the base-plate heating and the cooling distribution bridge. Figure 7.2-1 shows the labeling of all the VTCS hardware near the VELO. The evaporator has a fluid connection on the outside of the vacuum. The cooling bridge is mounted on top of the VELO tank. The electrical signals from within the VELO vacuum vessel (temperature sensors and base plate heaters) are fed to the outside via 2 extra VELO kapton cables and vacuum feed-through. A dummy electronic board on the outside is used to group these electrical signals from the VELO and the cooling bridge for a connection to the distant cooling PLC. Figure 7.2-2 shows the VELO internal hardware and the interconnects.

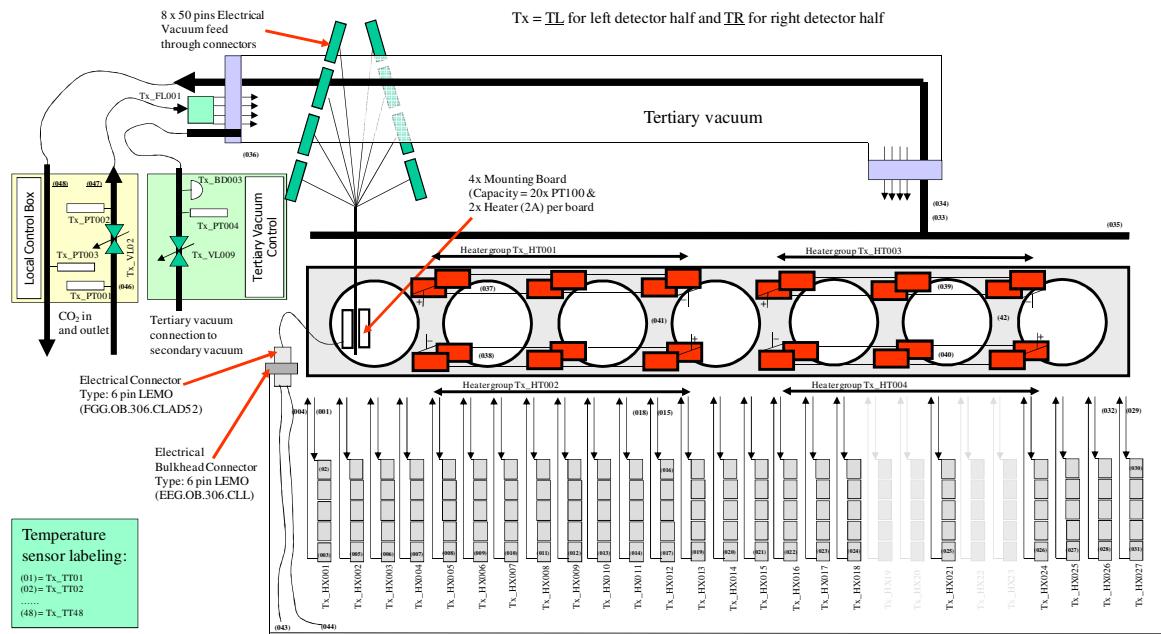


Figure 7.2-1: VTCS hardware labeling inside the VELO detector

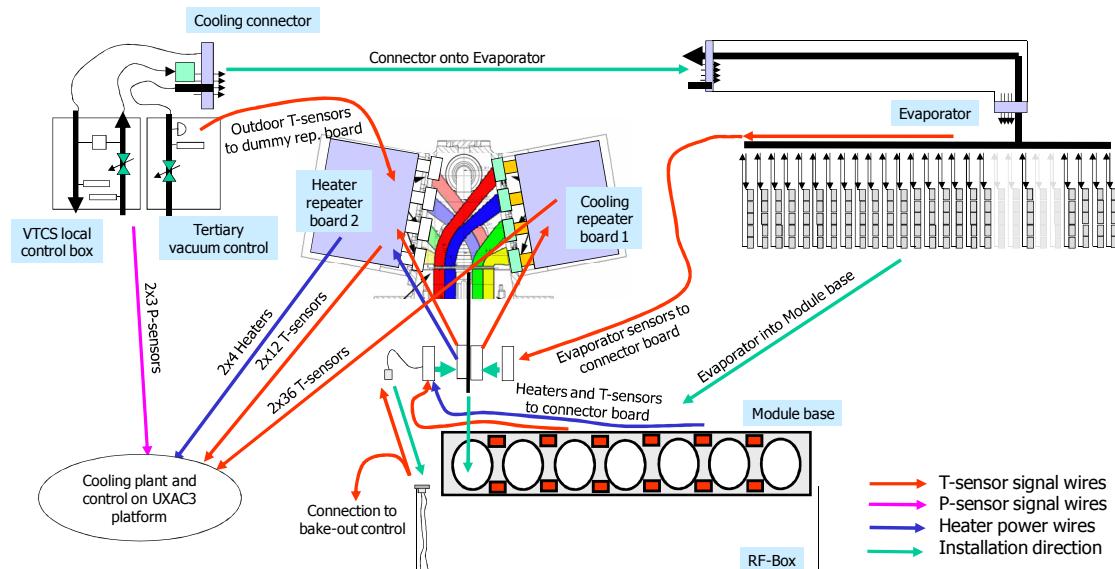


Figure 7.2-2: VELO internal hardware and interconnects

### 7.2.1 Module base plate heating

The module base plate is the positional reference of the modules. The precision interfaces are machined at room temperature. The base plate must therefore stay around 20°C all time (see requirements in chapter 3). The base plate is indirectly connected to the cooling system via some supports and via the module support paddles which causes the base plate to be cooled down eventually. The base plate is maintained at room temperature by kapton foil heaters glued on the inside of the frame. Figure

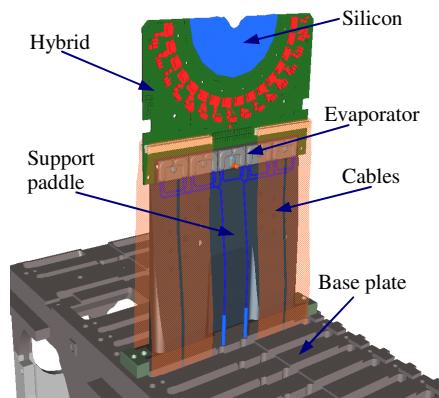


Figure 7.2-3: Overview of a VELO module on the base plate

7.2-4 shows an inside view with the heaters. In total 24 heater pads are present per detector half. 6 heaters are combined in a group and are controlled together by 1 temperature sensor. The group layout is shown in Figure 7.2-1. Additional information about the base plate heating can be found in the appendix in paragraph 11.8.

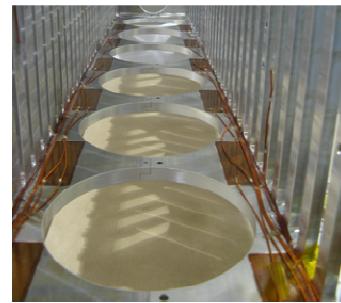


Figure 7.2-4: Base plate heaters

### 7.2.2 Evaporator

The evaporator absorbs the heat from the modules by evaporating the injected liquid CO<sub>2</sub>. The CO<sub>2</sub> evaporation pressure is controlled by the 2PACL principle, resulting in a stable evaporation temperature of the evaporator. The evaporator temperature indirectly controls the temperature of the silicon which according to the requirements (Chapter 3) must stay below -7°C. At full power the gradients in the modules are in the order of 20-25°C resulting in a required evaporator temperature of about -25 to -30°C (12).

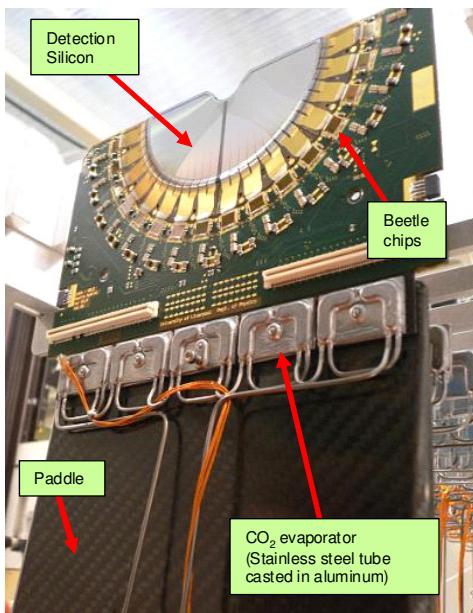


Figure 7.2-5: Velo module with CO<sub>2</sub> cooling connection evaporator

The CO<sub>2</sub> evaporator consist of 23 parallel branches of 1.5x0.25mm 1115mm long CRES321 stainless steel tubes. Each tube is coiled to prevent thermal expansion. A 457mm long section of the tube is embedded in casted aluminum cooling blocks for heat exchange. The cooling blocks are nicknamed cooling cookies as the production method of casting showed similarities with baking cookies in an oven. The thermal interface of the cookies to the modules is achieved with THERMFLOW® T710 phase-change Thermal Interface Material (TIM). This TIM was chosen because of its low melting temperature and low clamping force. Figure 7.2-5 shows a picture of a cooling cookie assembly mounted to a module. Each VELO module consists of a double sided hybrid (printed circuit board) with two silicon sensors. The core of the hybrid is a

thermally conductive Carbon fiber-TPG laminate supporting the module and conducting the heat to the cooling cookies. The cooling cookies are mounted with M2.5 screws to the module using the stiff paddle structure on the opposite side as contra clamp. Each evaporator branch has one PT100 sensor glued to the last cookie in the flow direction to monitor possible dry-out phenomena of the tube.

Figure 7.2-6 shows the layout of the evaporator assembly. The whole assembly is situated inside the VELO vacuum vessel. The requirements for leak tightness are extremely high. All the wetted parts are made of stainless steel and only reliable joining techniques as orbital welding and vacuum brazing (Nicrobraz EL-36) are applied. The 1.5x0.25mm cooling tubes from the aluminum cooling cookies are connected via 4x0.7mm tubes to the support manifold. The support manifold connects

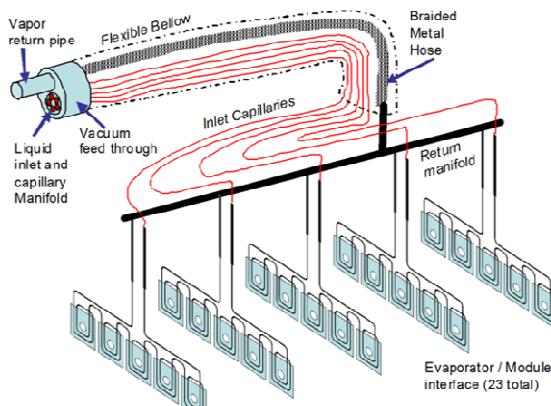


Figure 7.2-6: Concept of the VTCS evaporator

feature which was used during the installation and commissioning of the VELO modules, where individual modules needed to be cooled. The capillaries are routed into a small channel on the outside of the support manifold. This channel also houses the PT100 cables. Detailed pictures about cabling of this are shown in Figure 7.2-9.

For LHC proton beam injection the detector halves need to be retracted away from the beam by 30mm. The evaporator connection to the outside needs to be flexible to allow for this movement. The flexible return hose together with the inlet capillaries are inside a sealed vacuum bellow. The bellow is indicated as dotted line in Figure 7.2-6. Figure 7.2-8 shows a photo of the evaporator assembly, and Figure 7.2-7 shows the CAD design with cut-out views to show internal structures.

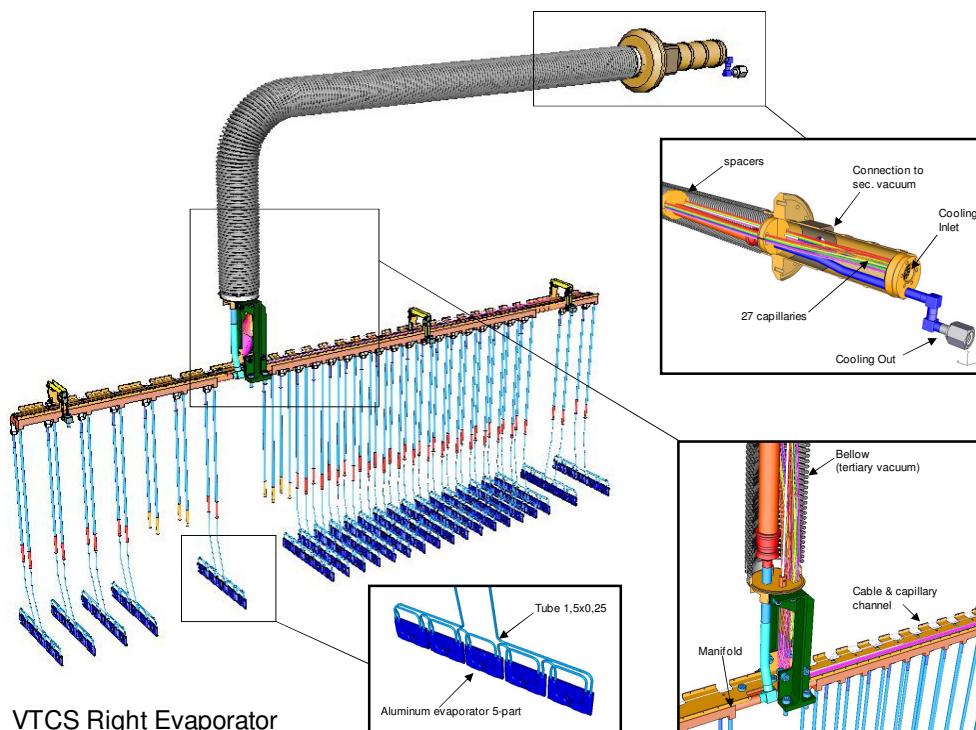


Figure 7.2-7: The VTCS evaporator design

the outlets of all the branches together. A flexible braided metal hose connects the manifold to the vacuum feed through.

The inlet of the branches are connected via 2038mm long 1x0.25mm capillaries directly to the vacuum feed through flange. The capillaries all have the same length so the flow impedance is the same for all. This ensures a good flow distribution for all the parallel channels. The capillaries are accessible from the outside, a

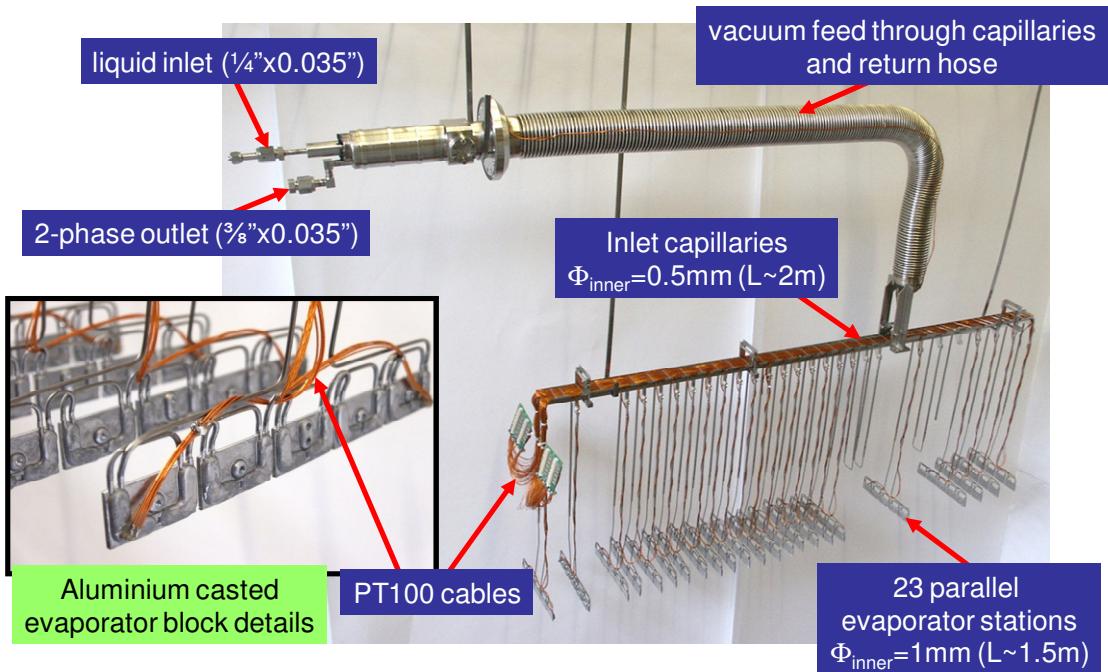


Figure 7.2-8: The VTCS evaporator construction



Figure 7.2-9: Evaporator PT100 cabling

### 7.2.2.1 Evaporator cooling cookies

The aluminum cooling blocks are casted around the cooling tube with a specially developed procedure (13), (12). The evaporator must have a low mass near the modules, to minimize distortion of the particle tracks. Aluminum has a low density and good conductive properties. Casting gives the freedom of applying material only at the place where it is needed. The thermal connection to the cooling pipe is achieved by the crimping of aluminum around it. The CTE differences between steel and

aluminum clamps the aluminum around the pipe during cooling down. The shape of the cooling cookies is achieved by the stainless steel mould. The flat interface to the module is made by milling.

The melting of the aluminum is done in a vacuum oven. The aluminum flows perfectly in the mould under vacuum conditions ( $<10^{-3}$  mbar) creating a smooth finish. The view of the cookies in Figure 7.2-5 is the result of the mould print. The best results were obtained with ACP 5080 (AlMg4,5Mn).

The vacuum however causes the magnesium content to vaporize during the melting, which creates bubbles in the liquid aluminum. Solidification of the aluminum is done under a 1 bar argon atmosphere to suppress the created magnesium vapor. The vacuum oven was heated in 1½ hour to 700°C, 10 minutes later the argon was applied, and another ten minutes later the oven was switched off. Figure 7.2-10 shows the fresh backed cooling cookie prior to machining.



Figure 7.2-10: Aluminum cookie still in the casting mould

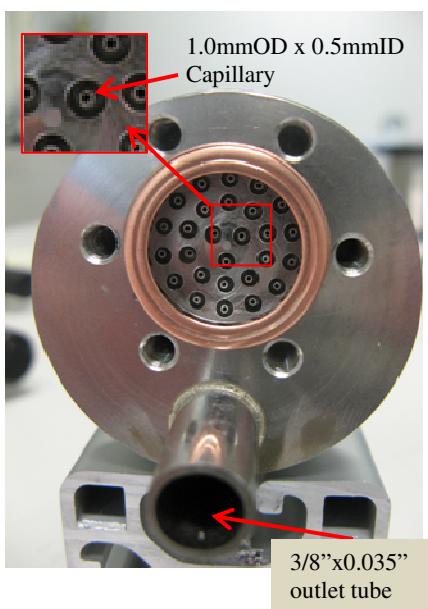


Figure 7.2-11: Evaporator inlet manifold and outlet connection.

### 7.2.2.2 Evaporator capillaries

The VTCS evaporator has 23 parallel branches. The flow resistance of each branch depends on the amount of created vapor. The more vapor, the more flow resistance, the less fluid is floating through the branch. This is an instable situation since an increased heat load causes a decreased flow while an increased flow is needed.

In the VELO all the modules can be individually powered up. This means that the evaporator branches can be loaded as well on an individual basis. The vapor increase only has effect on the outlet of the evaporator branches. The fluid condition at the inlet is for all the branches the same and not dependent on the heat load of the specific branch. The flow resistance of the inlet must therefore be dominant over the outlet flow resistance.

In the VTCS this is achieved by an inlet capillary of 2038mm x 0.5mmID at each evaporator branch. The capillaries are routed inside the vacuum bellow to an interface on the outside of the VELO vacuum vessel. In this way all the branches can be reached from the outside for individual cooling or additional flow tuning (See Figure 7.2-11). The individual tuning is not done in the

VELO but one has the opportunity to do so when needed. All the capillaries have the same length. The extra length is stored in the U-channel on top of the manifold underneath the PT-100 cables. The branch stand-offs are mounted to the support bar underneath the cable channel (See Figure 7.2-12).

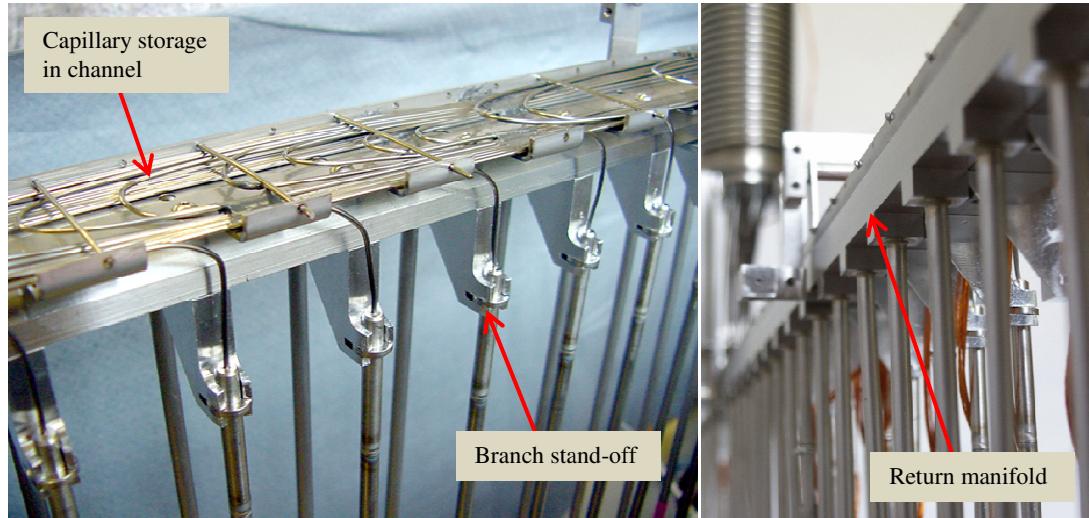


Figure 7.2-12: Capillary routing (Left) and return manifold (Right)

### 7.2.2.3 Evaporator Manifold.

The resistance of the outlet of the evaporator branches must be as small as possible not to disturb the flow distribution. Therefore the branches must be manifolded as close to the outlet as possible. The return manifold of the VTCS evaporator is the main support bar supporting all the parallel branches and is located underneath the cable channel. The manifold is a machined tube where the branch connections (4mmODx2.6IDmm) are brazed into (See Figure 7.2-12 right picture). The manifold sections are orbital welded to each other and to the outlet return hose.

### 7.2.2.4 Evaporator terminal and evaporator vacuum bellow

The evaporator is flexible to allow the detector to move inside the vacuum. This movement is necessary if the particle beam is injected and tuned. The inlet capillaries and the return hose are the flexible parts of the evaporator. These flexing parts were considered to be a possible leak risk of the pressurized volumes. To minimize the risk of a CO<sub>2</sub> leak into the vacuum system an extra vacuum volume was created around the flexible hose and capillaries. The evaporator terminal (See Figure 7.2-13) is sticking out of the vacuum volume and consists of the connection to the CO<sub>2</sub> in- and outlet and the connection to the evaporator vacuum. The evaporator vacuum is a volume that is evacuated once. It has a vacuum pressure sensor

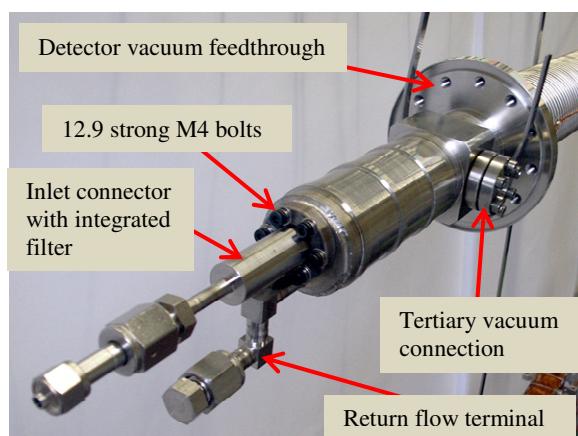


Figure 7.2-13: Evaporator terminal and vacuum connection.

(Tx\_PT004) and a burst disc in case of a pressure increase due to a CO<sub>2</sub> leak. The schematic of the vacuum lines is shown in the schematic of Figure 7.2-14.

The inlet of the evaporator is a conflat-16 connector with an integrated filter and is mounted with 6 M4 screws to the inlet capillary manifold using a copper gasket (See Figure 7.2-11). The conflat is from origin a vacuum connector. It must be installed with strong grade 12.9 bolts and torqued to 4.5Nm. The calculation is given in Figure 11.9-1 in the appendix.

### 7.2.3 Cooling bridge

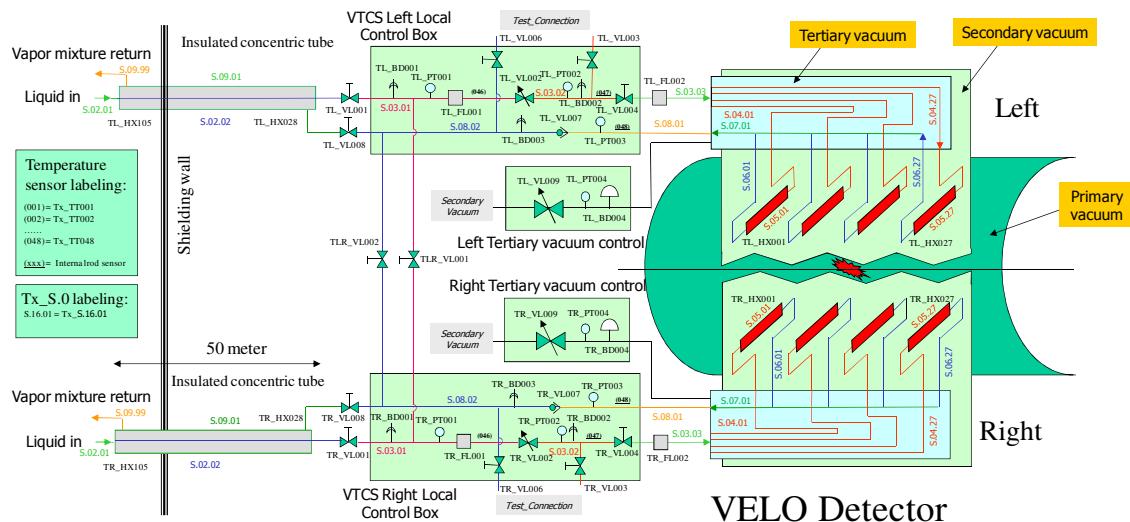


Figure 7.2-14: VTCS schematics and hardware labeling in the VELO cavern.

The cooling bridge is the link between the transfer lines and the evaporator. All the components are housed in a box located above the VELO. The schematics of the bridge is shown in Figure 7.2-14. The transfer lines are fed into the alcove on the ceiling and enter the box from the left side. The TL and TR system have interconnects so both detectors can be connected to 1 tertiary system in case of problems with 1 system. The valves can only be operated manually.

On the cooling bridge test heaters can be mounted to simulate a heat load. This is used for testing the VTCS without cooling the detector. The heaters are visible in the picture of Figure 7.2-15. During LHC operations, the heaters and their control are removed from the system as they are not radiation tolerant.

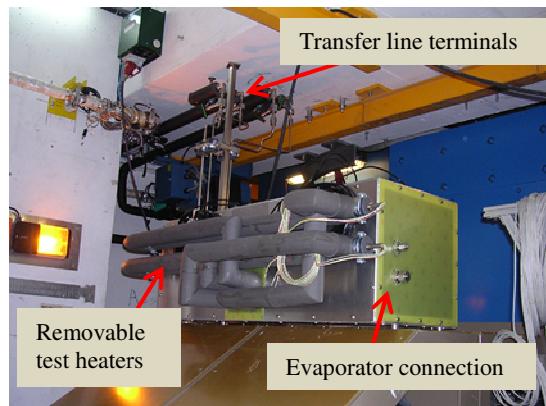


Figure 7.2-15: Cooling bridge above VELO

### 7.3 CO<sub>2</sub> system Transfer lines

The transfer lines are concentric tubes where the liquid feed line is located inside the vapor return line. Figure 7.3-1 shows a cross section of a transfer line with the insulation layer. The inner tube is laying loose inside the return tube and is not centered by spacers or so. It is bend a bit so it is jammed inside the return tube. The purpose of the transfer line is multiple. Besides from transferring the cooling fluid from the cooling plant to the evaporator and back, it has also an integrated functionality of conditioning the right liquid enthalpy of the evaporator inlet.

The transfer tube is a simple device, however its working is rather important and complicated. It serves a few purposes at the same time which also all rely on each other. An important feature is the heating of the inlet liquid line. The concentric layout functions as an internal heat exchanger where the cold liquid in the central feed line is heated to the right temperature by exchanging heat with the return flow in the outer annulus.

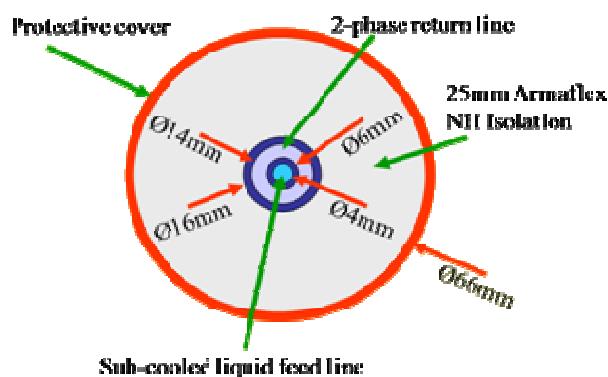


Figure 7.3-1: Transfer line crosssection

The energy which is exchanged between the two lines can be more than there is absorbed by the system (detector heat load and environmental losses). One can say that the efficiency of heating is very high, but in fact the large temperature difference involved makes the system a very inefficient system from the point of heat transfer. The heat sink of the 2PACL is the chiller temperature. This is always around -40 °C to -50°C. The evaporator temperature can be set to higher temperatures. The transfer line has to cope with the difference between them. The limit of the highest possible evaporation temperature is determined by the conduction of the heat exchange surface of the concentric tube. The transfer tube can only exchange heat if there is some heat absorbed by either evaporator heat load or by transfer line environmental losses. This absorbed heat creates the necessary temperature gradient needed to exchange heat between the feed and return line. The temperature of the evaporator can never be higher than the environment in case of no evaporator power, as there is no heat absorbed to create a temperature gradient for a heat exchange. The environmental heat leak on the transfer tube is the driving factor for the permanent heat exchange, the detector power can be off while the detector still needs to be temperature controlled by the evaporator. This is why the heat exchanger is included in the full return line rather than a local heat exchanger in the detectors vicinity.

The maximum range of the 2PACL is the temperature of the evaporator under full liquid condition. From this point onwards the accumulator can let the evaporator boil until the sub cooled liquid temperature of the pump is approached. In practice the lowest accumulator temperature is a few degrees above the liquid temperature of the pump inlet. The working of the transfer line can be explained by Figure 7.3-2. Here

one sees the temperature distribution over the tube length of the feed and return tube under 3 different accumulator set-point temperatures. Plot A shows the temperature distribution of the transfer line at a high set point of about 22°C. The evaporator (at the right) is full with liquid of about 18°C. The set point temperature is the dotted horizontal line. Lowering the set point will not change much in the temperatures until it passes the evaporator temperature. From this point on it starts to evaporate in the evaporator and the beginning of the return transfer line. Heat is removed from the

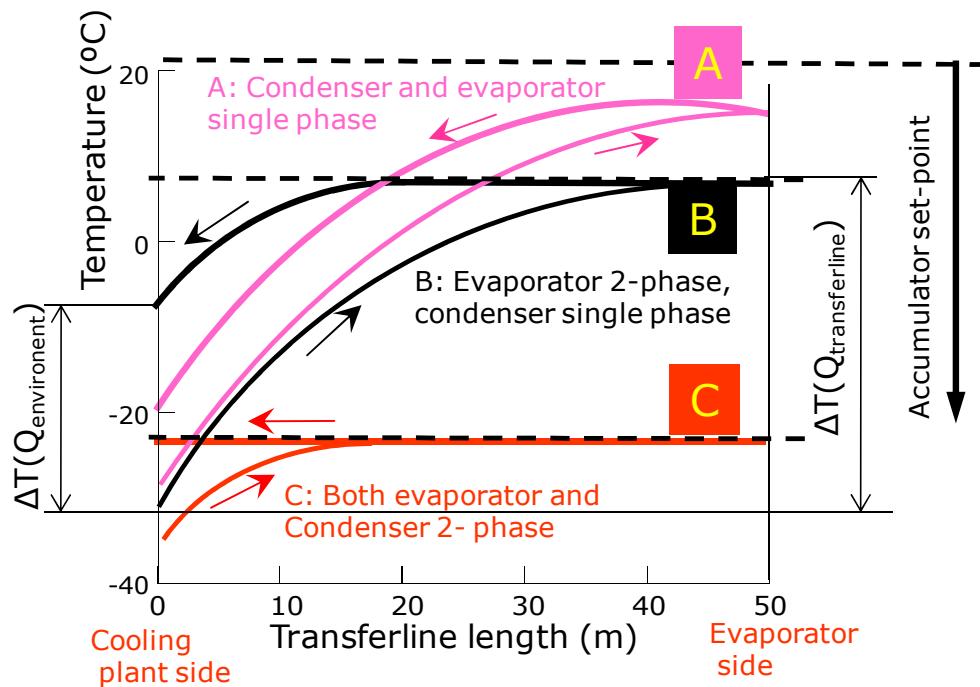


Figure 7.3-2: Transfer line temperatures at different operational states

return line to heat up the inlet flow so at a certain moment the return tube will become single phase again. This is illustrated in the plot B lines. Here the evaporator is 2-phase while the condenser is single phase and is in fact not a condenser but a liquid cooler. Lowering the set point even more will decrease the amount of internally exchanged heat, so the outlet of the transfer tube becomes 2-phase as well. This is illustrated by the lines of plot C. The transfer tube picks up a relatively large amount of heat from the environment. This is needed for a good transfer line operation. The amount of pick-up heat increases with a lower set point. As long as the outlet of the return tube is single phase the difference between the inlet of the feed line and the outlet of the return line temperature is a measure of the amount of picked up heat from the environment. ( $Q = \dot{m} * C * \Delta T$ ). This  $\Delta T$  is shown as an example for the plot B situation. This environmental heat is less than what is exchanged in the transfer line. The  $\Delta T$  of the exchanged heat in the transfer line is illustrated on the right of the plot B example. The transferred heat increases with setpoint, the environmental heat decreases due to a higher average transferline temperature. The above example shows the independence of the sub cooled liquid heating and the amount of absorbed environmental heat.

The plots in Figure 7.3-2 show just an example of principle. The temperatures do not match with the VTCS. In paragraph 9.4 a detailed simulation of this behavior is shown. Simulations show that the maximum possible set point temperature is at  $-10^{\circ}\text{C}$ . Measurements have shown that for the VTCS it is around  $-5^{\circ}\text{C}$ .

## 7.4 CO<sub>2</sub> system circulation plant

### 7.4.1 CO<sub>2</sub> plant schematics

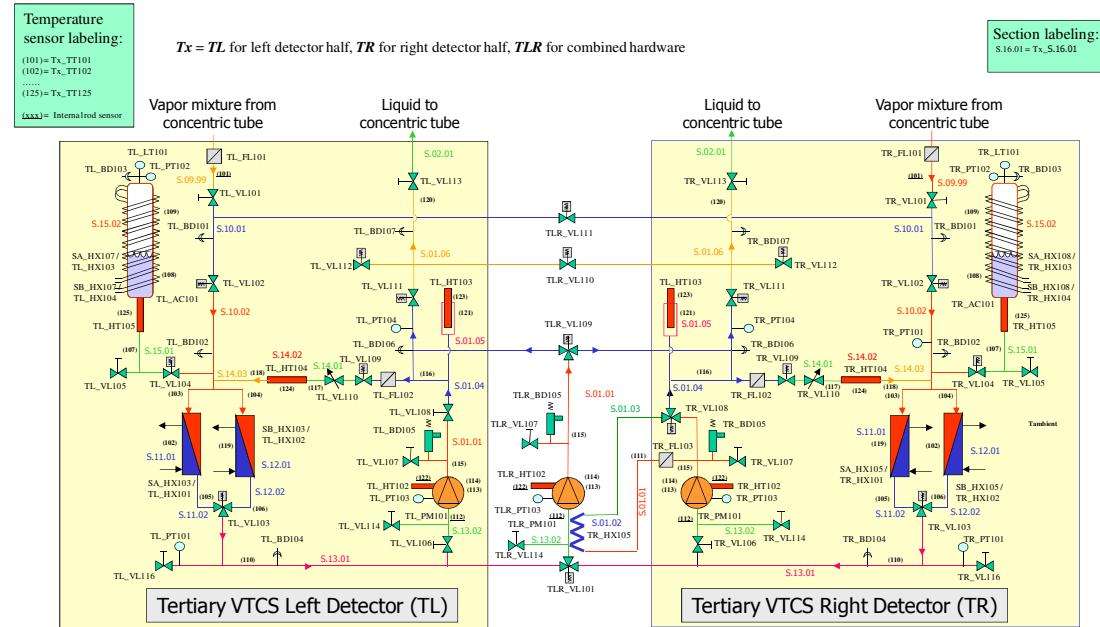


Figure 7.4-1: CO<sub>2</sub> plant schematics.

Figure 7.4.1 shows the schematics of the CO<sub>2</sub> plants. A large scale copy of the layout can be found in the appendix at paragraph 11.1. A full list of the components in the tertiary systems is given in the parts lists in the appendix. Paragraph 11.2 shows a list of all the sensors, 11.3 shows a list of actuators and 11.4 shows all the passive line components. The TL and TR are identical except from the TLR pump cooling heat exchanger. This TLR cooling is only present in the TR system. For the rest the 2 systems are identical and are more or less mirror oriented to each other.

Each system has 1 pump with oil bath heating and a pulse damper. Each pump can be shut-off from the system in case of pump maintenance. These are the valves Tx\_VL106 and Tx\_VL108. Valves Tx\_VL114 and Tx\_VL107 are used to flush the pump with CO<sub>2</sub> after the maintenance. The pump may never be evacuated as it damages the Teflon membrane. A by-pass is present to circulate the fluid internally via a liquid heater. The liquid heater can be used to supply heat for testing. The by-pass has a restriction valve (Tx\_VL110) which is set to the same pressure drop as the transfer line and evaporator resistance.

Two condensers are present. One is connected to the SA chiller one to the SB chiller. The condenser flow can be selected by 3-way valve Tx\_VL103. The accumulator is connected above the condensers and can be shut-off from the system with valve Tx\_VL104. An external valve Tx\_VL105 is connected to the accumulator and is used for filling. A second external valve (Tx\_VL116) is present on the outlet of the condensers.

Both systems are interconnected with valves TLR\_VL110 and TLR\_VL111. These can be used in case of a serious problem with one of the systems. They are not used in the current back-up procedures. The valves can be used to evacuate both systems

together prior to filling. Opening the valves during normal operation mixes up the fluid content resulting in unknown fillings of both system.

The plant can be shut-off from the transfer line with the manual valves Tx\_VL101 and Tx\_VL113 . Manual valves must always be in the original position as the PLC cannot identify the status.

Each section which can be closed off from the rest of the system has a burst disc to minimize the damage of a cold liquid trap expansion. Only the pump discharge has a spring relieve as the fast pulses can break the burst disc at lower pressures. Both relieve types open at around 130 bar.

#### 7.4.2 Accumulator

The main control of the system is the accumulator. It regulates the pressure in the system and hence the temperature in the evaporator. The accumulator size, together with the fluid filling of the system is designed such that there is in all cases a liquid and vapor mixture present. With the 2-phases present the pressure can be increased by evaporating part of the liquid, the pressure can be decreased by condensing part of the vapor. The heater must always be submerged to prevent dry-out of the heating surface. The cooling spiral must have a significant portion in the vapor volume. A partly submerged cooling spiral is not a problem. The heater is located in a thermosyphon underneath the accumulator, the thermosyphon allows the heater to remain in full contact with a small remaining volume of liquid. Figure 7.4-2 shows the principle of the accumulator with the thermosyphon heater and the cooling spiral. Figure 7.4-3 and Figure 7.4-4 show pictures of the accumulator hardware.

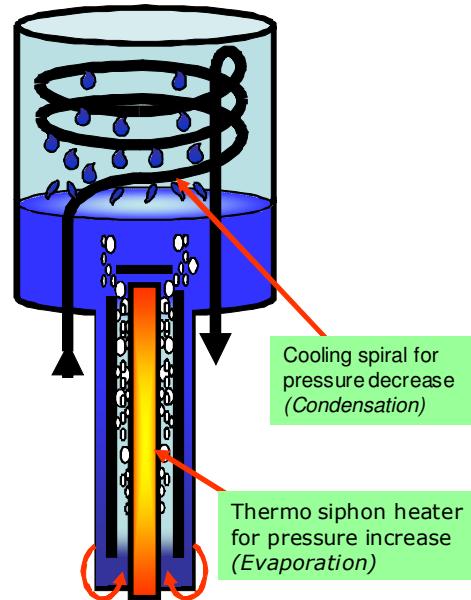


Figure 7.4-2: Principle of the CO<sub>2</sub> accumulator



Figure 7.4-3: Accumulator cooling spiral (left) and thermosyphon heater (right)

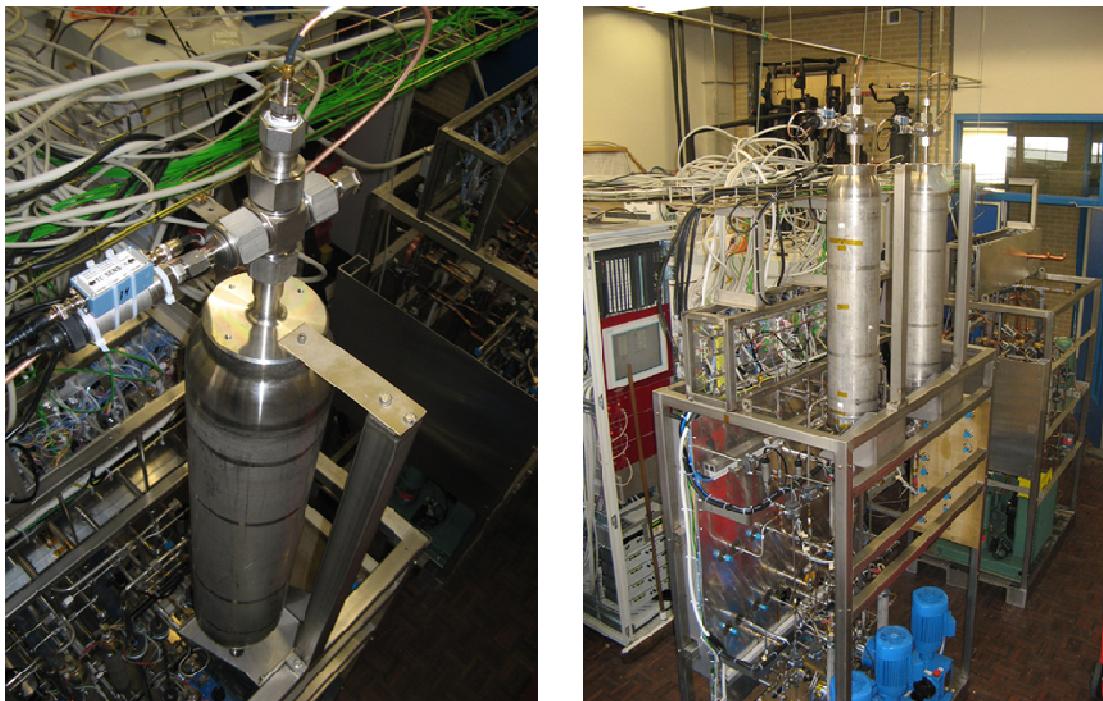


Figure 7.4-4: Accumulator in the cooling plant.

The thermosyphon heater is a 1kW heater. The convective cooling flow around the heater is a function of the density difference between the liquid and the vapor. CO<sub>2</sub> has its critical point at 31°C. Near the critical point the liquid/vapor density ratio is decreasing resulting in a reduced convective flow around the heater. Around 50 bar (14°C) the convective flow is insufficient for the 1kW of the heater, so the maximum heater power must be reduced with increasing accumulator temperature. Figure 7.4-5 shows the measured dependence of the maximum heater power as a function of the accumulator saturation temperature.

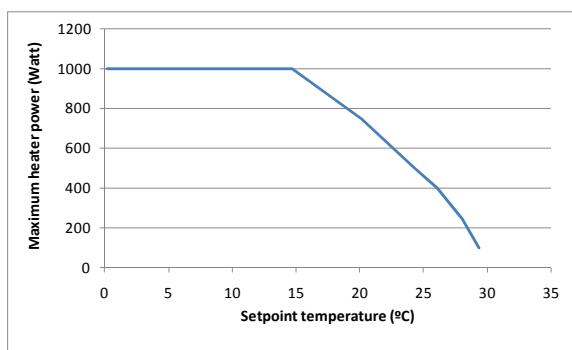


Figure 7.4-5: Maximum accumulator heater power

grades decreases with increasing saturation temperature, while at higher fill grades it increases with saturation temperature. The dependence of the level to the saturation temperature is important to realize, as the level decreases without exchanging fluid with the system.

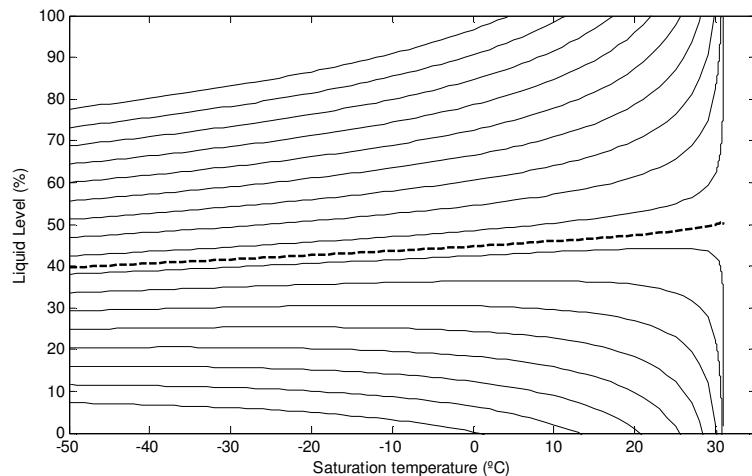


Figure 7.4-6: Accumulator liquid level as function of temperature and filling

At low fill grades the level decreases with increasing temperature, this phenomena must be taken into account when sizing an accumulator. It shows that the minimum level occurs at start-up. At start-up the loop is fully filled with liquid and the accumulator saturation temperature is high. These conditions determine the minimum filling of the system.

The accumulator is an in-house fabricated vessel. It has a volume of 14.2 liter and is the most important component with respect to pressure safety. The VTCS safety document (8) gives a detailed design and testing overview of this custom made pressure vessel.

The densities of the liquid and vapor near the critical point change rapidly. The liquid level is not only a function of the fluid mass it also depend a lot on the density ratio of the liquid and vapor. Figure 7.4-6 shows a plot of the liquid level of a CO<sub>2</sub> filled accumulator as function of saturation temperature for several fill grades. The dashed line is the level when filled with 468 g/l, which is the density in the critical point. The liquid level of lower fill

### 7.4.3 LEWA LDC-1 liquid pump

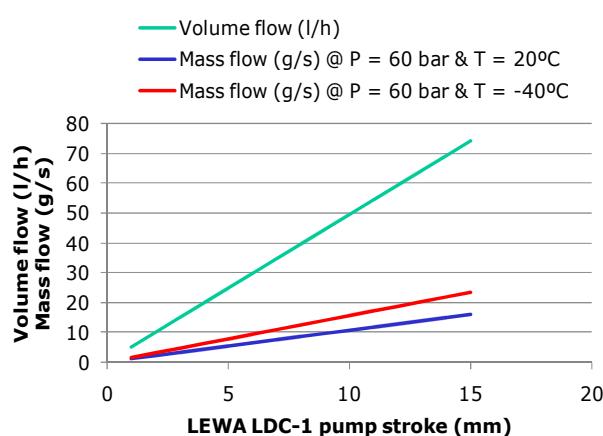


Figure 7.4-8: Pump flow as a function of the stroke setting

Each CO<sub>2</sub> system has one liquid pump (TL\_PM101 and TR\_PM101). One spare pump (TLR\_PM101) is available for both halves and can be connected to any of the 2 systems by the 3 way valves TLR\_VL101 and TLR\_VL109. The two 3-way valves always operate together in a procedure so that the fluid content of TL cannot be mixed up with the content of TR. The pumps are LEWA LDC-1 membrane metering pumps and provide a constant volume flow. The pump head can be as high as 100 bar. The volume flow of the pump is constant and can be set manually with the black-knob on the side of the crankshaft (see black knob in picture of Figure 7.4-8). The adjustment is achieved by changing the stroke of the membrane. Figure 7.4-9 shows the obtained volume flow as a function of the stroke setting. The resulting mass flow is also a function of the pumped density. The green and red lines are the pumped mass flow at two temperature extremes of 20°C and -40°C. The default stroke setting is 7mm, resulting in a 10 g/s mass flow under cold operation.

The Teflon membrane is displaced hydraulically with



Figure 7.4-7: The LEWA LDC-1 metering pump

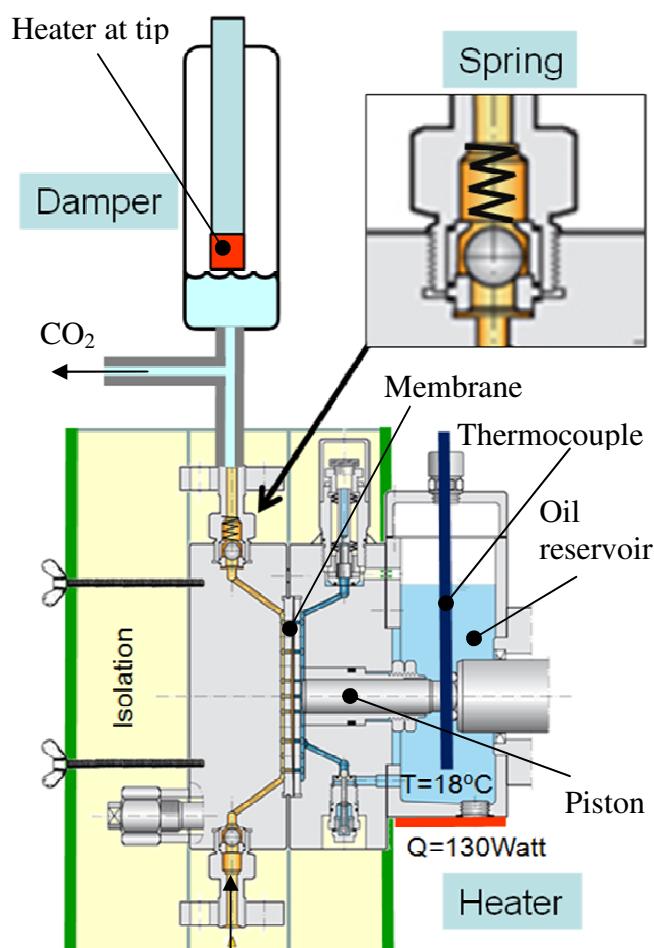


Figure 7.4-9: Cross section of the LEWA metering pump

oil. In this way the membrane is homogeneously stressed by the constant back-pressure. Figure 7.4-7 shows a cross section of the hydraulic part of the LEWA pump. The oil is displaced by a piston which is connected to the crankshaft and electric motor. The membrane has two Teflon layers so that a leak in one membrane is not polluting the CO<sub>2</sub> with oil. A pressure switch is connected to the volume in between the membrane layers, which is filled with alcohol of 1 bar. A pressure increase of the alcohol volume is a direct consequence of a leak to the high pressure volumes of either the oil or CO<sub>2</sub> side. The pressure switches act at a measured pressure of 10 bar, resulting in an immediate pump shut-down. The TLR pump will be automatically switched on as a replacement.

The LEWA pump is used to pump cold liquid, therefore the pump head is insulated. The oil in the pump head is becoming cold too. There is a small flow of oil from the pump head to the reservoir. The oil in the reservoir may not become cold as moisture will get in the open oil bath. A heater (Tx-HT102) is placed underneath the oil reservoir to maintain the oil at 18°C. The oil temperature is measured using Tx\_TT122 and is a rod thermocouple dipped in the oil bath. The heater control is done by the PLC PID control. Figure 7.4-7 shows the heater and thermocouple location with respect to the oil bath.

The pump flow is directed by 2 no-return valves. A ball is laying on a seat at the in- and outlet of the pump head. The balls are put in their seats by gravity. The pump is modified with an extra spring loading on the exhaust to prevent bouncing. The pump provides a pulsed flow. A damper is placed in the discharge liquid line to dampen the pressure pulses by creating a compressible gas volume in the damper. Figure 7.4-7 shows the damper and ball valves. Details about the dampers are given in Paragraph 7.4.5.

#### 7.4.4 Valves

6 valve types are used in the CO<sub>2</sub> systems. Below the valve types are discussed. A detailed list of all the valves used is given in the appendix in paragraph 11.3.1.

##### 7.4.4.1 2-Way valves

In the cooling plant all the 2-way valves are Swagelok 43G series valves. (SS-43GHLVCR4). The valves have been modified with an extension so they can be mounted to a warm panel. All the valves are mounted on the front panel of the CO<sub>2</sub> plant unit. The valves can be equipped with a manual knob or an electrical motor. The flow path of the ball valves is a T-shape. With a T-shape the valve can be closed but liquid can never be trapped. Trapped cold liquid can give very high pressures when warmed up and so the valve will be damaged.

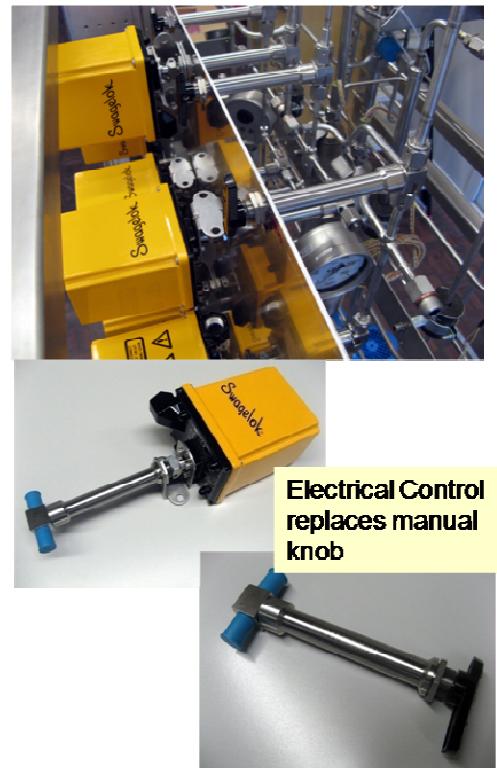


Figure 7.4-10: Swalok 43G 2-way valves with extensions.

The ball valve seats are made of Teflon. Teflon is not radiation resistant. Therefore other 2-way valves are used in the cooling bridge on top of the VELO these are SS-4UW-TW and are full metal shut-off valves. All of them are manual.

#### 7.4.4.2 3-Way valves

The 3-way valves have the same handle interface as the 2-way ones (SS-43GXVCR4). The same extension concept is used. All the 3-way valves are panel mounted and equipped with an electrical motor.



Figure 7.4-11: Valve mounting panel of the CO<sub>2</sub> plant.

#### 7.4.4.3 Restrictor valves

Restrictor valves are present in the cooling bridge (Tx\_VL002) and the by-pass in the plant itself (Tx\_VL110). They throttle the flow such that the pumps have a pressure head of about 10 to 20 bar. Low pressure heads cause the pump to malfunction. A high pressure in the supply lines also suppresses the risk of vapor in the supply lines. The used valves are SS31RS4 valves and have a onetime adjustment. The Teflon shaft seal of the valve in the cooling bridge (Tx\_VL002) is replaced by Viton O-rings.

#### 7.4.4.4 No return valves.

A no return valve is present in the cooling bridge in the return line. The valve must prevent back flow in case of a leak of the evaporator in the vacuum tank. See details about this in paragraph 7.7.5. The valve is a modified Swagelok Swagelok SS-58SW8T. The full metal poppet is replaced by an o-ring sealed poppet.

#### 7.4.4.5 Relieve valves.

Relieve valves are present in the pump discharge lines. The relieve valves are Swagelok SS-4R3A-EP and have the label Tx\_BD105. Originally these were burst discs as present in each closed section. The pump pulses caused the burst discs to

burst sometimes when pumping against a closed valve due to the short time pressure peaks. A relieve valve acts more as a slow fuse and is therefore not delicate for short time pressure peaks. The relieve valves have the same pressure setting as the burst discs which is 130 bar.

#### 7.4.5 Vibration dampers

The damper is a 500cc reservoir with a heater inside to generate vapor. The heater is a rod heater with a heating element only at the tip. The liquid from the liquid line is vaporized and rises into the reservoir. The gas damps the pulsed flow which is directly fed into the damper. The ongoing flow is perpendicular to the damper and not floating through the damper. The heat generation does not reach the flowing liquid.

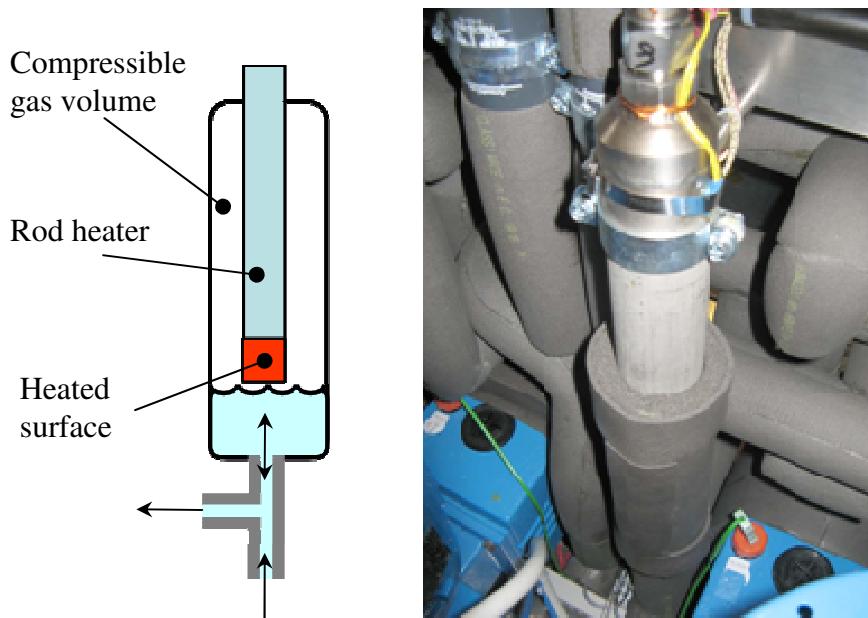


Figure 7.4-12: VTCS Pulse damper

#### 7.5 CO<sub>2</sub> condensers

The condensers are reinforced brazed plate heat exchangers from SWEP. They are reinforced because of the high pressure of the CO<sub>2</sub>. The reinforcing metallic plates protect the heat exchangers from bursting. The CO<sub>2</sub> operates with pressures up to 100 bar (170 bar proof pressure), while R507a on the other side has low pressures. The internal structure of this heat exchanger must withstand this pressure difference as well. A special double wall heat-exchanger from SWEP was used. This B16DW series has double plates and a small wave pattern. This combination makes the plate heat exchanger suitable for withstanding these high differential pressure. The VTCS safety document (8) gives a detailed design and testing overview of this custom made heat exchanger. Figure 7.5-1 shows the reinforced condensers installed in the CO<sub>2</sub> rack.

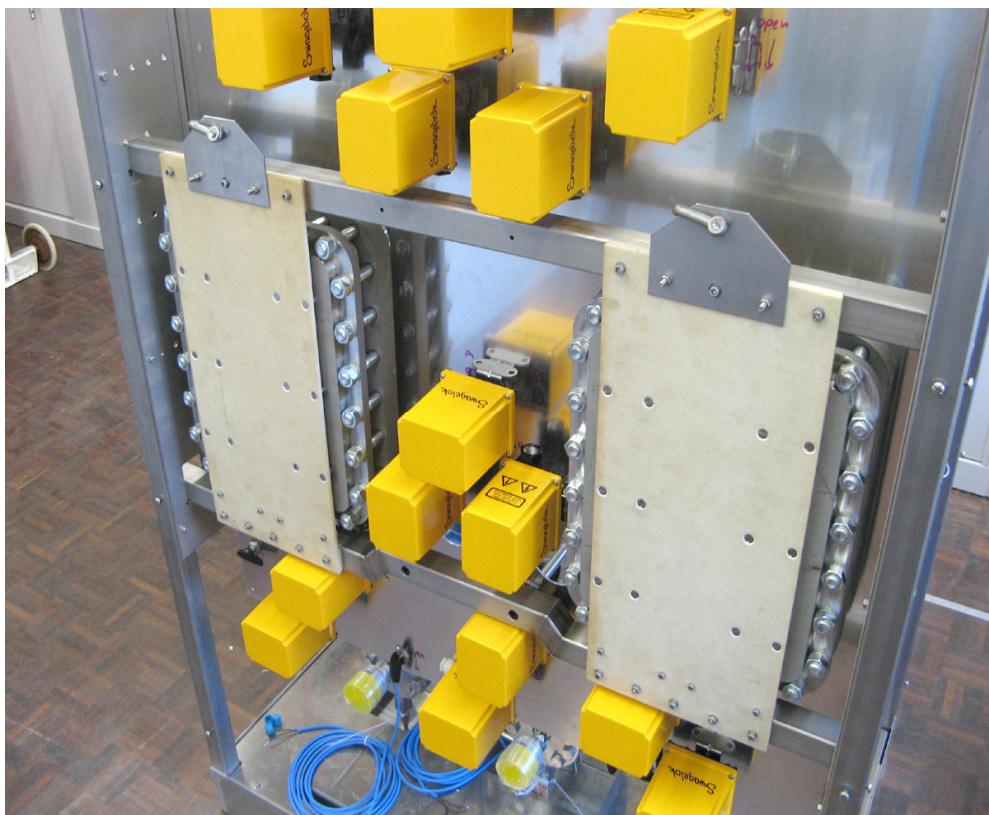


Figure 7.5-1: Reinforced CO<sub>2</sub> condensers.

## 7.6 CO<sub>2</sub> system volume and charge

The accumulators must always have a liquid/vapor mixture to maintain the set-point pressure in the loop. The heater must stay submerged which determines the minimum level, while the cooling spiral must have a significant fraction in the vapor volume. The accumulator volume can be determined by analyzing the total loop mass and verify at a certain filling or a 2-phase mixture is still present in the accumulators. Table 7.6-1 shows the volumes of the main sections of the CO<sub>2</sub> systems.

Table 7.6-1 Summary of the Tertiary volume.

Subsystem	TL volume (ml)	TR Volume (ml)
Evaporator	220.0	220.0
Liquid feed	944.4	957.8
Vapor return	6213.7	6062.4
SA-Condenser	311.4	310.8
SB-Condenser	128.4	127.8
Liquid suction	59.1	59.1
By-pass	260.7	260.7
Dampers	605.0	605.0
Accumulator	14203.0	14203.0
Total system volume	22969.0	22822.6
Loop volume	8766.0	8619.6
Plant volume	15728.6	15748.5
Transfer volume	7240.4	7074.2

The loop filling is calculated in the state point model. See chapter 9 for details of the state point model. A detailed overview of the results is given in the appendix in Table 11.5-5 for the TL system and Table 11.5-6 for the TR system. The tables show the nominal powered case.

The liquid level in the accumulator changes as a function of the set-point temperature and the applied load. Figure 7.6-1 shows the simulation results of the TL liquid level as a function of set point. The worst case low level occurs at high set point and an unpowered loop. The worst case high level at low set points and maximum heat load. Both systems need to be filled with 12kg CO<sub>2</sub> in order to have a liquid level in range at any time during any operation.

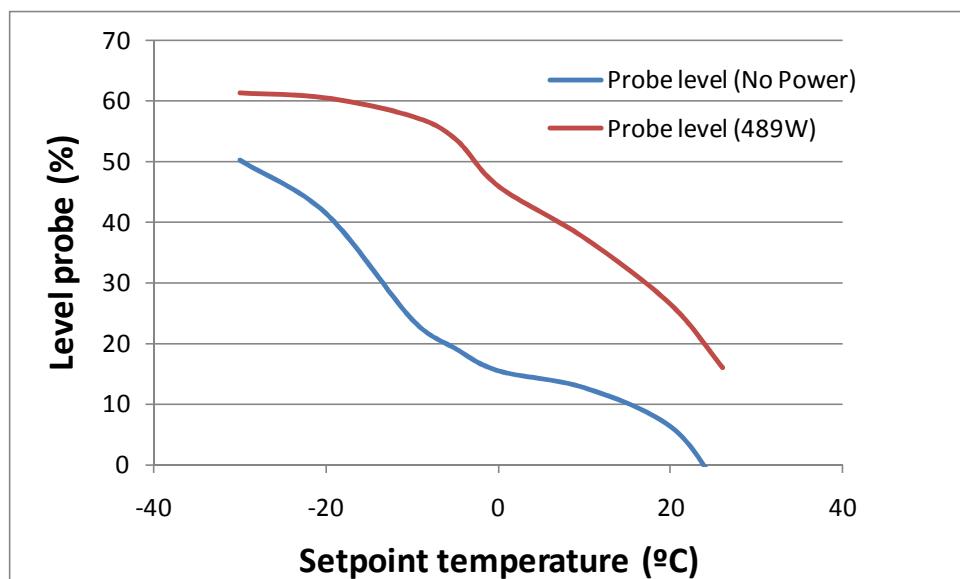


Figure 7.6-1: TL accumulator liquid levels

## 7.7 CO<sub>2</sub> system operation and control

### 7.7.1 Accumulator control

The main control of the VTCS is the accumulator pressure control. The accumulator pressure is a direct measure of the evaporator temperature. By heating and cooling the liquid content in the accumulator is varying by evaporation or condensation. As the accumulator is able to variate the fluid content in the system, it can also empty it or fill it with liquid. The filling option is used at start-up, the emptying procedure is used for maintenance. Figure 7.7-1 shows the principle of the accumulator control.

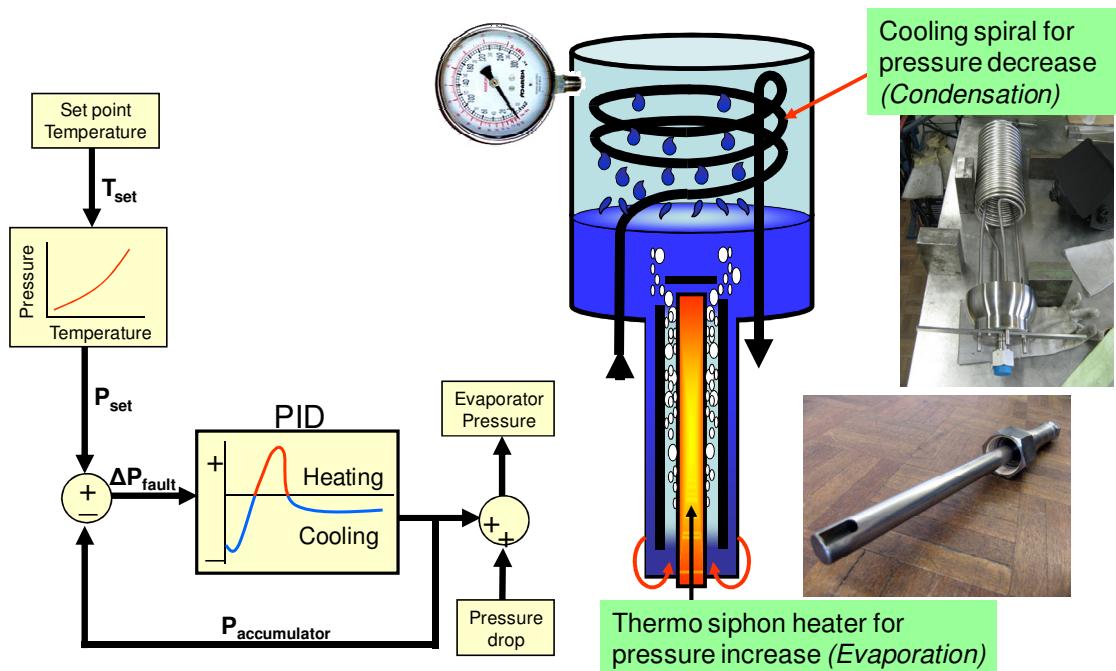


Figure 7.7-1: Accumulator control principle

The LHCb-VTCS accumulator pressure control is a bipolar PID-process, it regulates both the heater element (Tx-HT105) and the expansion valve to the cooling spiral (Sx\_VL114/Sx\_VL119). Which of the two expansion valves is controlled depends on whether the main (SA) or backup chiller (SB) is used. The cycle time of the PID process is 100 ms. A detailed description of the accumulator control is written in the PLC technical description (10).

Input to the PID-controller are the actual pressure in the accumulator (Tx\_PT102) and the saturation pressure of the set-point temperature (see Figure 7.7-2). The PID controller only uses the P-action with a gain-factor of 100. The PID process has upper and lower limiters which limit the output to guarantee a good system operation. The upper limiter limits the heater in case of a dry-out of the heater, the lower limiter limits the cooling in case the accumulator saturation temperature is approaching the pumped liquid temperature, as a too low sub cooling causes cavitation in the pumps.

### 7.7.1.1 Accumulator control at start-up

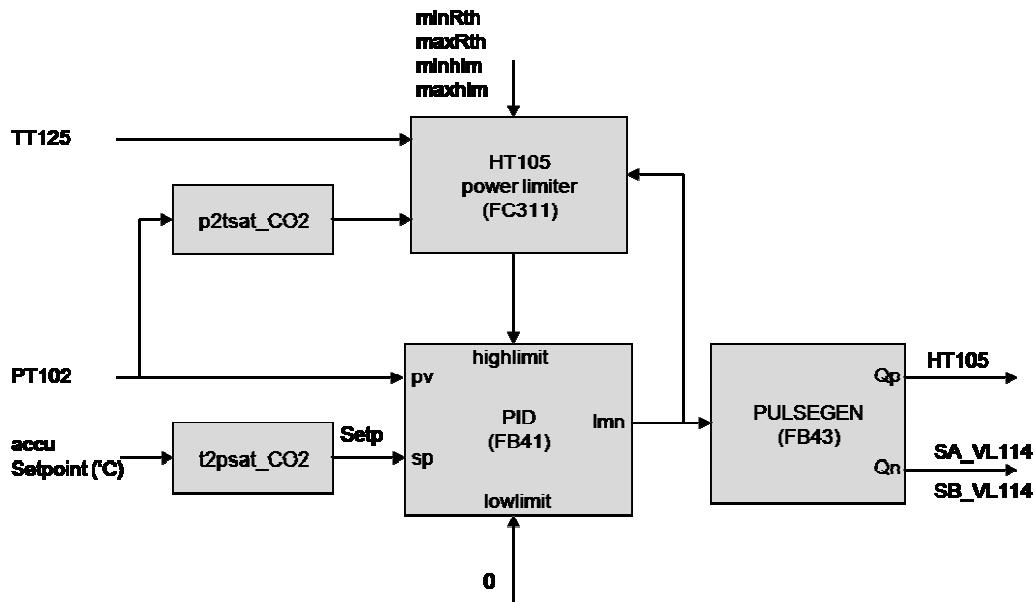


Figure 7.7-2: Start-up accumulator control of the VTCS

During startup the accumulator is heated for a long time. The heater is evaporating liquid and generates vapor in the accumulator. The increasing pressure pushes liquid from the accumulator into the loop. The existing vapor in the loop is condensing to liquid when the saturation temperature is getting above the ambient temperature. At start-up a set-point temperature of 6°C above the temperature of the pump inlet ( $T_x\_TT112$ ) is taken. The maximum start-up set-point is cut-off at 26°C. A start-up of a cold system can go fast without heating. If the sub cooled temperature of  $T_x\_TT112$  is already lower than the required  $\Delta T$  of 6°C, the threshold is reached immediately and the system starts directly without an accumulator heating action.

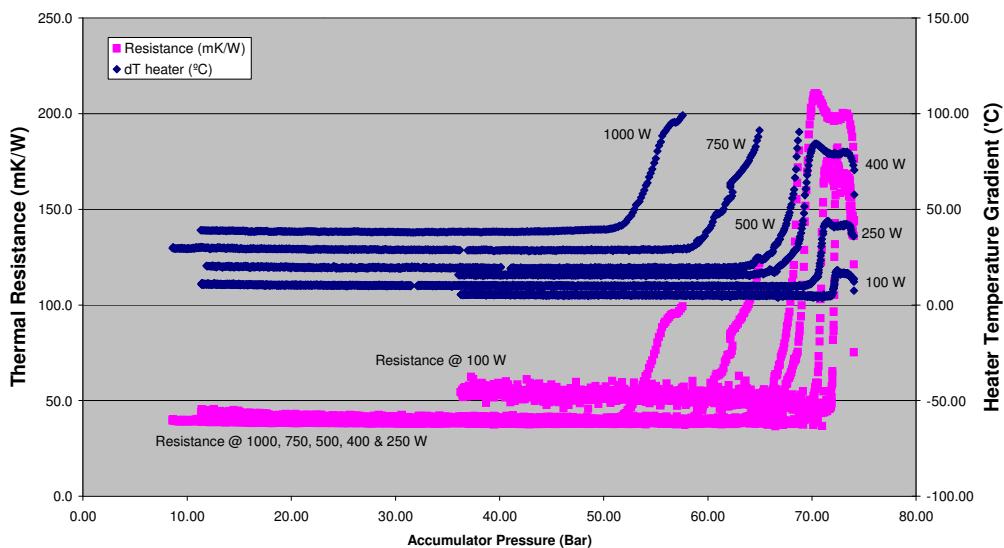


Figure 7.7-3: Accumulator heater performance

At higher pressures (temperatures) not all power of the heater can be transferred to the liquid CO<sub>2</sub> and the risk of overheating exists. The CO<sub>2</sub> is supplied to the heater by a thermosyphon configuration. At increasing pressures the density ratio between the

liquid and vapor is decreasing resulting in a less convective fluid flow. To compensate for the reduced flow the upper power limiter in the PID control limits the heater power to avoid dry-out. Figure 7.7-3 shows the measured temperature difference of the heater with respect to the saturation temperature (blue lines). For each applied power it is constant until dry-out occurs. The pink lines show the calculated heater resistance which is denoted as:

$$R_{th} = \frac{T_{heater} - T_{saturation\_accu}}{Power}, \quad \text{Equation 7.1}$$

Where  $T_{heater}$  and  $T_{saturation\_accu}$  in °C and Power in Watts which is derived from the output ( $lmn$ ) of the PID-controller.

The resistance of the heater is not depending on the heater power, only at low powers (100 Watt) it shows a dependency. The heater limiter is limiting the output power with the relation as shown in Figure 7.7-4.

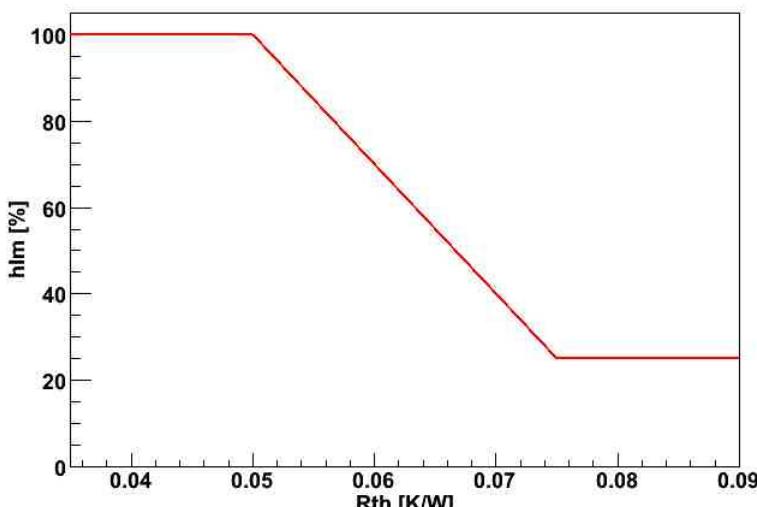


Figure 7.7-4: High limit as function heater resistance

In order to avoid jumps in the PID process, the high-limit used by the PID process is the moving average of the last 10 calculations. During the accumulator heating stage and subsequent stages up to the cooling of the accumulator, the low-limit of the PID process is kept a 0.

### 7.7.1.2 Accumulator control during operation

When the cooling system reaches the stage where the cooling of the accumulator starts, the above mentioned control of the high-limit based on thermal resistance is replaced by a joint high- and low-limit control based on the sub cooling conditions of the pump as shown in Figure 7.7-5. Sub cooling is defined as the difference of the saturation temperature of the accumulator (from pressure) minus the temperature at the inlet of the pump (Tx\_TT112).

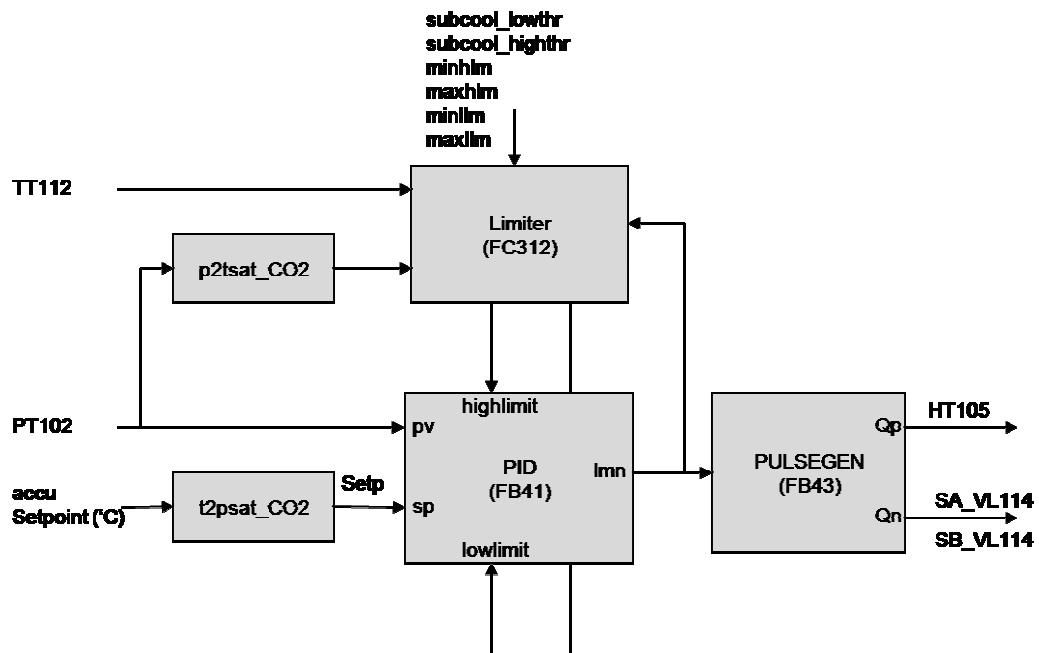


Figure 7.7-5: Operational control of the VTCS accumulator

During normal operations the accumulator saturation temperature must be maintained at least a few degrees above the pump sub cooled temperature (Tx\_TT112). If the sub cooling is insufficient the pump can cavitate resulting in a stop of the liquid flow. If the accumulator saturation temperature is getting to close to the sub-cooled temperature, the accumulator cooling power must be reduced. The lower limiter of the PID process is limiting this cooling output with the relation as shown in Figure 7.7-6.

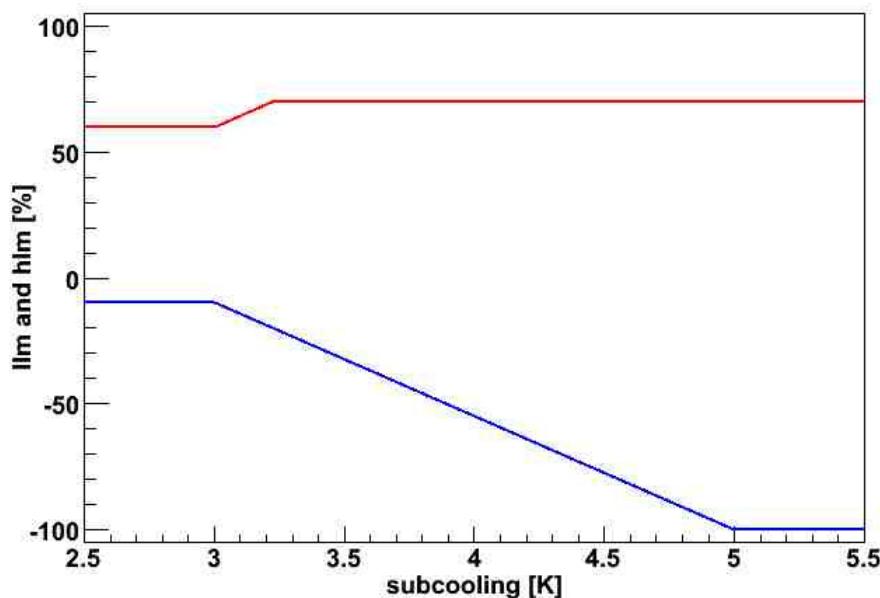


Figure 7.7-6: VTCS low and high limit settings as a function of the sub cooling

The upper limiter based on heater thermal resistance used at start-up is replaced by limiter based on sub cooling too. A heating action in the accumulator pushes saturated

liquid into the system which can have a sub cooling increase as a result. Here the heating power is also limited based on sub cooling conditions.

### 7.7.2 Heater control and safety.

The CO<sub>2</sub> system has 4 heaters per system. One heater to maintain the pump oil at room temperature (see paragraph 7.4.3). One heater in the vibration damper (see paragraph 7.4.5) one heater in the bypass circuit to test the system under load conditions and the accumulator heater (See paragraph 7.4.1).

Heaters are the most dangerous elements in a cooling system. Liquid heaters have in general a very high heat density. If a liquid heater is switched on without a provided coolant flow it can dry-out with high temperatures as a result. The heaters are within the insulation and have therefore no convective cooling as emergency. Often a heater failure will result in a fire of the insulation material, which is a very serious issue.

In the VTCS a triple redundant fail safe approach is used concerning heaters. The first level is a warning threshold of the heater internal temperature sensor. The PLC will turn-off the heater involved. The second protection is a higher threshold of the same sensors. The PLC will shut-off all heaters. This is done to avoid the possible mistake of a temperature sensor swap. The third level of protection is an independent thermal switch (clixon) on the outside of the tubing. All clixons are mounted in series and are normally closed. Opening up 1 clixon will break the circuit and will directly open the main heater relay independent of the PLC.

Table 7.7-1 Heater alarms and warnings

Heater label	Function	Temperature sensor label	Warning level (°C)	Alarm level (°C)	Clixon level (°C)
TL_HT102	TL pump oil heater	TL_TT122	40	50	70
TL_HT103	TL press damper heater	TL_TT123	120	160	90
TL_HT104	TL by-pass heater	TL_TT124	80	120	90
TL_HT105	TL accumulator heater	TL_TT125	120	160	90
TR_HT102	TR pump oil heater	TR_TT122	40	50	70
TR_HT103	TR press damper heater	TR_TT123	120	160	90
TR_HT104	TR by-pass heater	TR_TT124	80	120	90
TR_HT105	TR accumulator heater	TR_TT125	120	160	90
TLR_HT102	TLR pump oil heater	TLR_TT122	40	50	70

### 7.7.3 Tertiary system alarm handling.

The PLC controls and monitors the CO<sub>2</sub> systems. If the system is out of its design working range alarms are generated and proper actions are taken by the PLC. The alarm handling procedure is in detail described in the user manual (11). A table with the alarms properties can be found in the appendix in section 11.6. In some cases an alarm requires an automatic switch over to a back-up component. In this case the system is automatically restarted with a changed configuration. See paragraph 8.3 for details on the restart procedure and the selection of default components.

## 7.7.4 VTCS 2PACL operation

### 7.7.4.1 Start-up

The system is started-up under full liquid condition. First the system is filled with liquid by heating the accumulator to a saturation temperature above ambient. See paragraph 7.7.1 for details on the accumulator start-up heating. Figure 7.7-7 shows the start-up from the system from an ambient condition. Around 13:30 the system is started with a heating of the accumulator. The red line is the accumulator heater power. As a consequence the accumulator pressure increases (light green line). The liquid level in the accumulator is decreasing as the loop is filled with liquid from the accumulator (dark blue line). The heater power is limited by the accumulator control as the heater is subject to dry-out. This is visible by a the decreasing trend of the varying heater power. The variation is an oscillation of the limiter control. Around 13:40 the start-up set point of the accumulator is reached. The liquid pump starts pumping liquid which is visible by the occurring pressure increase of the pump outlet (dark green line). When a liquid flow is present the chiller is started and the liquid in the condenser is cooled down (purple line). The system is now pumping around cold liquid for a while and cools down the system in full liquid mode.

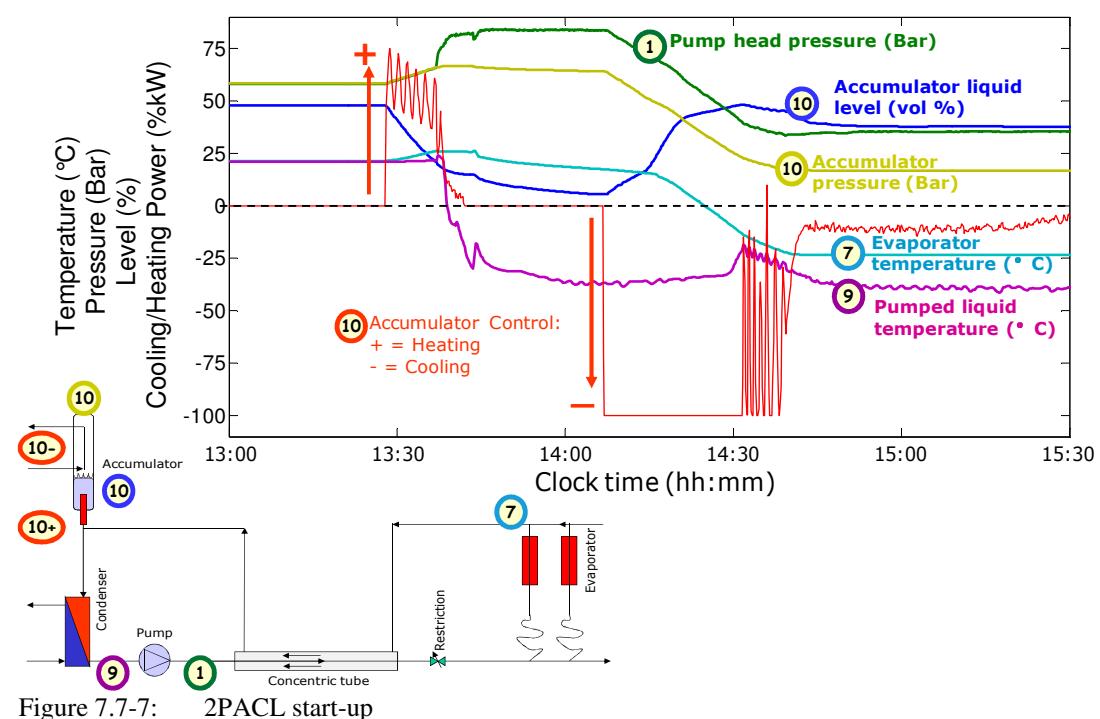


Figure 7.7-7: 2PACL start-up

The evaporator (also in liquid mode) is cooling down in a much slower rate. The heat exchange in the transfer line is heating up the liquid before it enters the evaporator (Details about the working of the transfer line is explained in paragraph 7.3). If the evaporator is around 18°C the accumulator set-point is changed to the requested temperature, which is in this example -25°C. This occurs around 14:06. The temperature sensor which triggers the set-point change is Tx\_TT046. The -25°C set-point request causes the accumulator control to cool the accumulator with 100%. This is visible by the red line which shows a -100% heating. As a consequence to the cooling, the pressures (dark and light green lines) are decreasing and the liquid level in the accumulator (dark blue line) is increasing, due to the condensation of the vapor in the accumulator.

At first the temperature of the evaporator is not affected by the pressure decrease. Evaporation in the evaporator starts when the saturation temperature is equal to the liquid (~14:15). The evaporator temperature is now following the accumulator saturation temperature and full temperature control of the evaporator by the accumulator is present. Due to the evaporation in the system the liquid level in the accumulator is rising more rapidly than before.

Around 14:30 the sub cooling is getting too small as the pump liquid temperature is approaching the saturation temperature (purple line is approaching light blue line). To avoid pump cavitation the accumulator PID control is limiting the accumulator cooling power (See paragraph 7.7.1 for details about the limiter). The limiting action is visible by oscillations in the red line.

Around 14:45 the -25°C set-point is reached and the cooling of the accumulator is decreased to a steady level of about -10%. This continuous cooling is due to the environmental heat leak on the accumulator itself. The VTCS system is now ready, the detector can be powered-up.

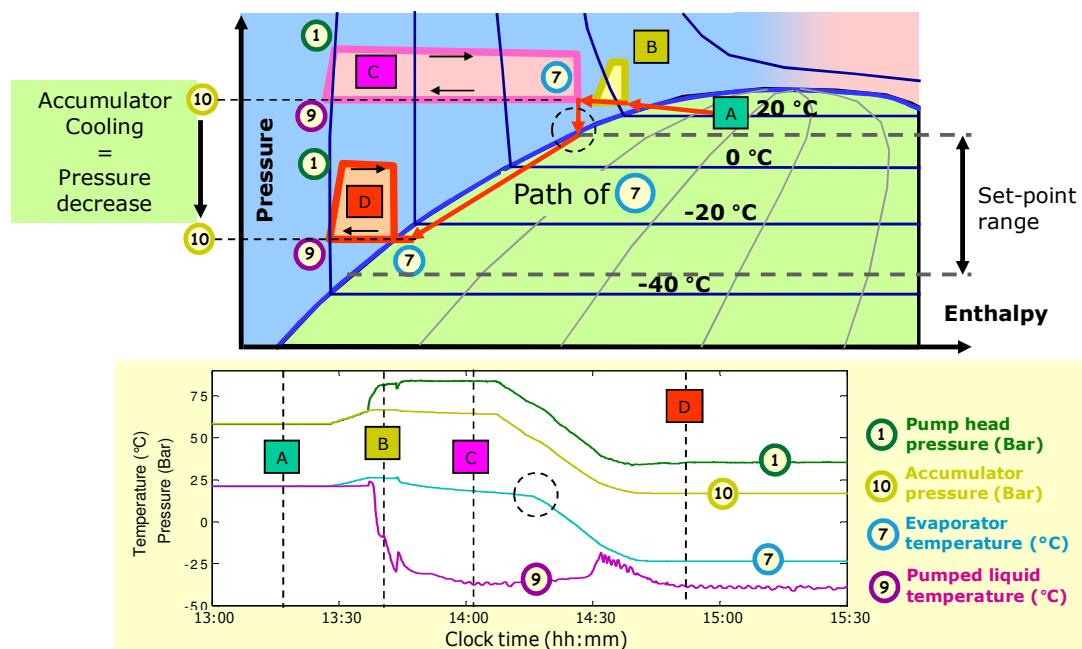


Figure 7.7-8: 2PACL start-up in the PH-diagram

Figure 7.7-8 shows the same start-up but now with the state-points plotted in the PH-diagram. In the PH-diagram it is better visible which part is operating in single- or two- phase. Prior to start-up the condition of the system is unknown. Liquid and vapor are present anywhere (Situation A). Heating the accumulator brings the system to situation B where everything is liquid. Cooling down brings the loop in situation C, where the pumped liquid temperature is cold, while the evaporator remains relatively warm. The stretched horizontal line length is mainly due to the heat exchanged internally by the transfer line. After C the accumulator is cooled and the pressure is decreased which is visible by a lowering of the cycle along the vertical axis. At the moment that state point 7 of the cycle hits the saturation line (dashed circle), the evaporator starts boiling and the accumulator has the full control over the evaporator

temperature. Lowering the pressure brings state point 7 closer to the sub cooling which is state point 9. When they become too close the accumulator control limits the accumulator cooling power and the lowest possible set-point is reached. The full operational range is the range shown by the diagonal red arrow.

The situation above shows a start-up from an ambient condition. A start-up from a cold condition can be much different. If the system is shut-down and immediately restarted, it goes rather fast as most of the state requests are already fulfilled.

#### 7.7.4.2 Detector powering.

If the accumulator saturation temperature is within  $0.5^{\circ}\text{C}$  of the required set-point, the cooling ready state is released by the PLC. The interlock to the detector low-voltage is cleared. The detector can now be powered-up. There is no specific power-up sequence, any module can be powered-up individually or together with the rest. A power-up will create more vapor in the system which must be compensated for by the accumulator. Figure 7.7-9 shows a full power-up of a VELO half at a set-point of  $-25^{\circ}\text{C}$ . The power-up around 0:18 causes the pressure in the loop to increase, which causes a cooling action of the accumulators PID control. The PID cooling action is visible by the decreasing trend of PID output which is the light blue line.

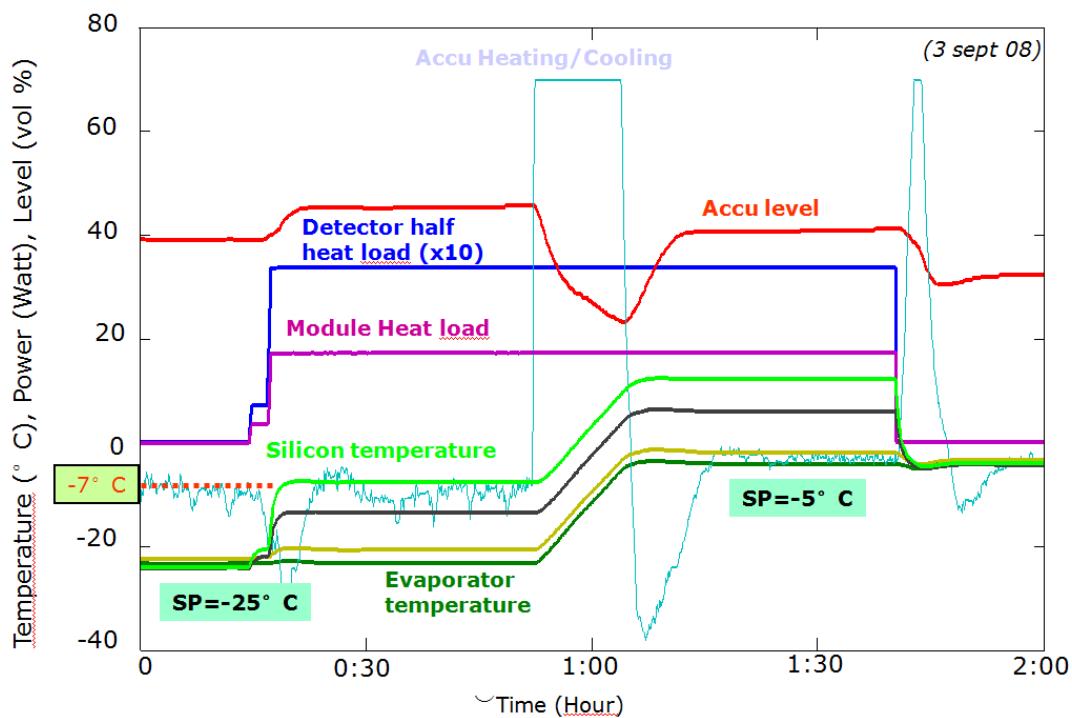


Figure 7.7-9: Set-point change and powering

The extra vapor generation in the loop causes the liquid level in the accumulator to rise. The red line shows the accumulator liquid level. After a power-up the system is behaving as before, with the accumulator cooling power being the same as before.

A power down of the detector works similar but reversed to a power-up. In Figure 7.7-9 a set-point change to  $-5^{\circ}\text{C}$  is shown. A set point change explanation is given in paragraph 7.7.4.3. After the set point change the detector is powered down around 1:40. The loss of heat causes the vapor volume in the loop to decrease which has a pressure decrease as a result. The accumulator PID control reacts with heating the

accumulator to restore the pressure. The liquid level in the accumulator is lowered as more liquid is present in the loop now.

#### 7.7.4.3 Change of accumulator set-point

Figure 7.7-9 shows as well the response of the system to a set-point change. Around 0:50 the set point is changed from -25°C to -5°C. The accumulator PID control reacts by heating the accumulator to bring the pressure to the requested saturation pressure of -5°C. The evaporator and the detector temperatures are following the changing accumulator saturation temperature. During the heating the accumulator liquid level is decreasing. Around 1:10 the -5°C is reached and the accumulator heating is lowered and finally cooled to compensate for the environmental heat leak. The heat leak compensation is lower than at -25°C as the heat loss is less due to the smaller temperature difference to ambient. The accumulator is stable again around 1:20.

#### 7.7.5 Evaporator venting

The VTCS has an automatic venting procedure of the volumes which are connected to the pressurized parts of the VTCS inside the VELO vacuum tank. In case of a leak of the CO<sub>2</sub> system into the tank volume a maximum of 12kg of CO<sub>2</sub> can float into the vessel which will make severe damage to the VELO detector. A pressure switch is mounted on the VELO vacuum system which switches around 1150 mbar. A pressure in the tank above atmospheric pressure is most likely caused by a CO<sub>2</sub> leak. When the PLC gets the 1150 mbar switch signal it stops the VTCS and closes valve Tx\_VL111 and opens valve Tx\_VL112 to vent the content of the feed line and evaporator to the atmosphere. The no-return valve in the cooling bridge must make sure that the rest of the system is not floating back to the leaking evaporator. The rest of the CO<sub>2</sub> remains in the system, only the content of the evaporator and feed line is vented. In this way the pressure can be relieved quickly from the pressurized part inside the vacuum.

## 8 VTCS Control System

### 8.1 PLC

The VTCS is controlled by a Siemens S7-400 series Programmable Logic Controller (PLC). The PLC contains the individual control loops, the sensor read-outs, the alarm handling and the procedural steps. The PLC is mounted with the electronics in a 19-inch rack next to the cooling plant on the UXAC3 platform. The PLC controls all of the VTCS, no user interference is needed other than switching it on and setting the desired evaporation temperature in the detector. The PLC also switches automatically to back-up configurations if a malfunction of a part is occurring. A detailed description of the PLC control is written in the PLC technical description (10).

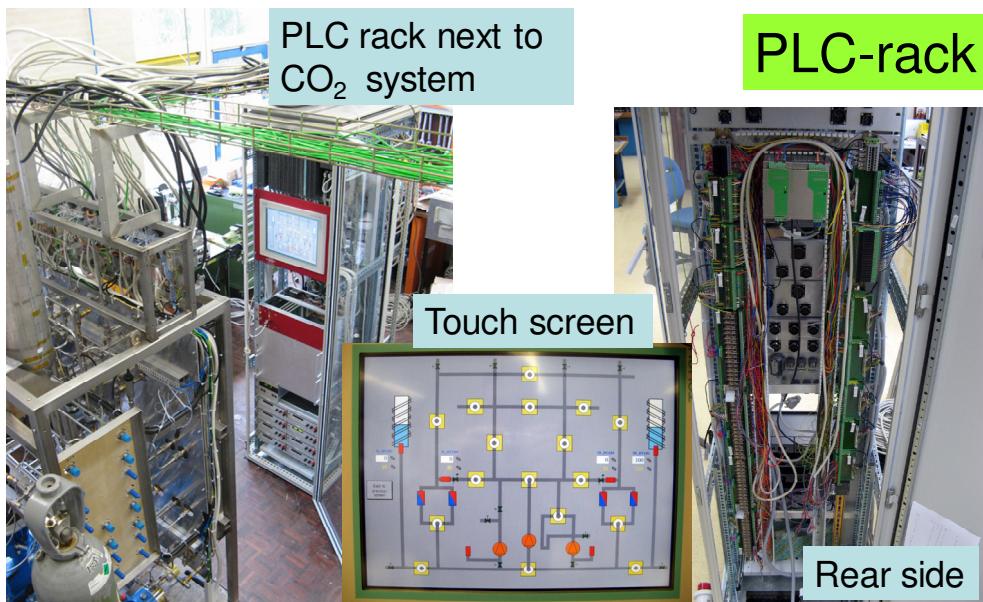


Figure 8.1-1: VTCS PLC and electronics rack and user interface.

The PLC can be operated via the touch-screen. The touch screen has several panels from where a user can control things. It also displays all the variables for system monitoring. A detailed description of all the user screens is given in the user manual (11).

## 8.2 *VTCS electronics.*

The electronics are all mounted in the same rack as the PLC. Detailed descriptions of the electronics can be found in EDMS (14).

## 8.3 *VTCS configuration and start-up*

The VTCS can be configured to operate in several ways. The configuration is in detail described in the user manual (11). In short the system can run with the following configurations:

1. TR on/auto / manual
2. TL on/ auto/manual
3. TLR auto/forced left/forced right/manual
4. SA auto/manual
5. SB auto/manual

The configurations can be set on the touch screen of the PLC. See Figure 8.3-1 for a screen shot of the configuration panel.

Both TL and TR can be switched on individually. If the TL or TR configuration is automatic it will start the corresponding CO<sub>2</sub> system with the default pump. If the configuration is on manual it will claim the TLR pump on a “who is first” bases. If the TLR pump is unavailable the corresponding system will stop. When the procedure is starting the chiller it will first look to the SA chiller configuration. If the SA is configured on auto it will start on SA. If the SA is set to manual it will automatically start SB. If SB is also on manual the system will stop.

The configurations can be set manually or by the PLC itself. In case of an alarm in the pump group or chiller group it will put the corresponding group on manual. A restart of the system automatically switches to the back-up solution.

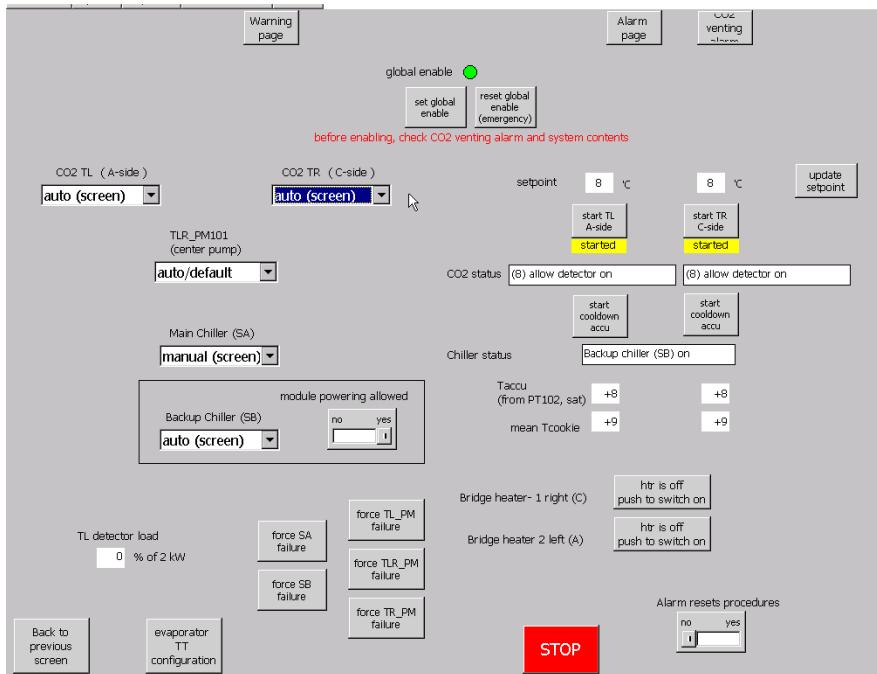


Figure 8.3-1: PLC configuration touch screen

At start-up first the accumulator will be heated up to prime the loop with liquid. Secondly the pump will start pumping over the by-pass (see paragraph 7.4.1) and later the chiller will be switched on. When the pump is sufficiently cooled the flow is diverted from the by-pass to the transfer line. After pumping liquid for a while the accumulator pressure is lowered to the desired set-point. When the set point in the accumulator is reached the cooling is ready for the detector to be powered. If one system is switched on the other system will also be switched on and follows the steps towards cold liquid pumping over the by-pass. This partially switched on mode has no effect for the temperature of the evaporator. A later start of the second system is much faster this way as part of the time consuming start-up has already passed. A start-up of only 1 half has the consequence that the heat load for the chiller is less. In case that the SA main chiller this low heat load can be a problem. Therefore the test heater in the by-pass line is switched on to 500W when one tertiary system is running in the stand-by mode

## 8.4 PVSS interface

The PLC user interfaces have a copy in the overall LHCb PVSS monitoring and control software. In this way the cooling system can be monitored by the experimental control team in the LHCb control room. Operation from PVSS is for the VTCS not possible as the system may never be switched off. Operation can only be done at the cooling station itself via the PLC touch screen. All of the VTCS variables (sensors values and PLC variables) are visible in PVSS and logged to an oracle database. A detailed list of all the PVSS variables can be found in the appendix at paragraph 11.7.

## 9 System simulation.

For the static analyses a state point model was generated of the SA, SB and TL and TR system. In a state point model the pressure and enthalpy is calculated iteratively at defined points starting from known boundaries. The state point model has an integrated physical property database of Refprop (9). With this Refprop database the right properties are used at any iteration round. The pressure drop and applied power between each points is calculated and added to the pressure and enthalpy of the next state point. In this way a complete overview is generated for each location in one of the VTCS systems.

For the VTCS models a state point is in a section as indicated on the schematic layouts of paragraph 11.1. The pressure drop is calculated by mass flow through the local pipe length and diameter or restrictor. The applied heat is calculated by the environmental heat leak on the same pipe configuration with the present insulation applied. An extra applied load like the detector heat is added in the same way between the state points if present. Knowing all the states of the sections (pressure and enthalpy), the density and temperatures can be derived. Together with the section volume and the derived density the fillings at each section can be calculated. The fluid charge in the R507a reservoirs and CO<sub>2</sub> accumulators can be calculated when knowing the fluid content in each section and the total charge applied.

### 9.1 SA system simulation

Figure 9.1-2 shows the simulation result of the SA state-point model in the pressure enthalpy diagram. The plotted state-point locations can be found in the drawing of Figure 9.1-1. The calculation is done with each section being a state-point, but only the important points are plotted. The different operation of the main evaporators and the accumulator spirals is visible. The superheating control after the internal heat exchangers makes the entire evaporators to be in the 2-phase region (Point 6ab). The accumulator evaporator operates at a higher pressure due to the manual back pressure valve. The shown simulation is a nominal heat load situation of 900 Watt (detector power + environment heat) on each main evaporator and 400 Watt on each accumulator evaporator. The state point values can be found in the table below. All the section state values can be found in Table 11.5-1 in the appendix.

Table 9.1-1: SA simulation state-points

	Enthalpy (kJ/kg)	Pressure (bar)	Enthalpy (kJ/kg)	Pressure (bar)	Enthalpy (kJ/kg)	Pressure (bar)
State point			ab	ab	cd	cd
1	428.0	10.5				
2	206.7	10.5				
3	216.0	9.1	216.0	9.1	216.0	9.1
4			134.7	9.1	184.4	9.1
5			134.7	0.9	184.4	1.2
6			275.1	0.9	351.0	1.2
7					351.0	0.9
8			356.5	0.9	382.6	0.9
9	363.6	0.9				

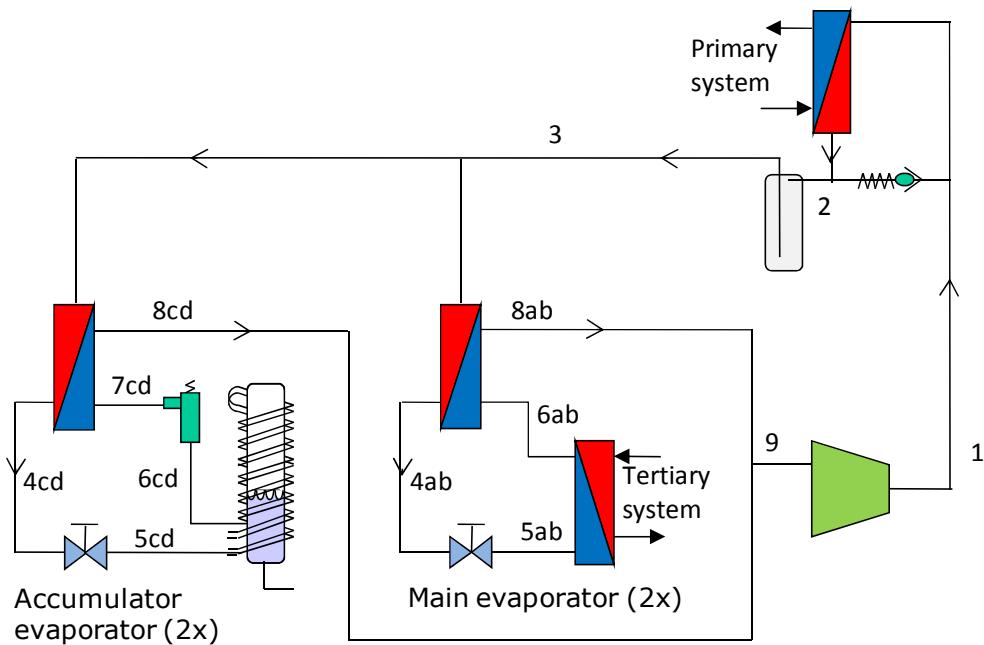


Figure 9.1-1: State-points of the SA main chiller.

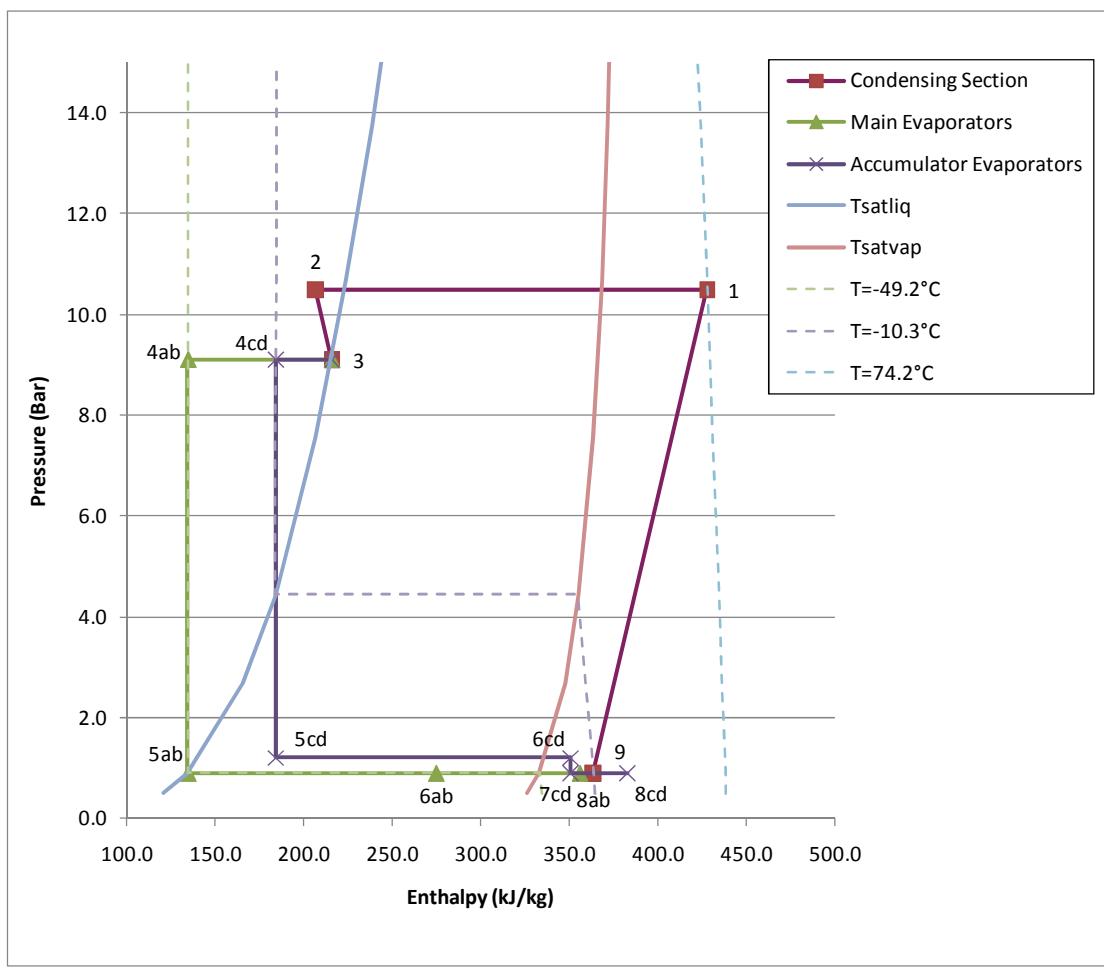


Figure 9.1-2: State point model result of the SA-chiller in the pressure enthalpy diagram of R507a.

## 9.2 SB system simulation

The SB chiller simulation is similar to the SA chiller simulation. The SB chiller has 1 common internal heat exchanger and therefore all the evaporator branches (accumulator and main) start with the same fluid condition. The only difference is the higher evaporator pressure in the accumulator evaporator. This is due to the manual back-pressure valve. Figure 9.2-1 shows the state-point locations and Figure 9.2-2 shows the results in the pressure-enthalpy diagram. The shown simulation is a nominal heat load situation of 300 Watt (detector power + environment heat) on each main evaporator and 400 Watt on each accumulator evaporator. The state point values can be found in the table below. All the section state values can be found in Table 11.5-3 and Table 11.5-1 in the appendix.

Table 9.2-1: SB simulation state-points

	Enthalpy (kJ/kg)	Pressure (bar)	Enthalpy (kJ/kg)	Pressure (bar)	Enthalpy (kJ/kg)	Pressure (bar)
State point			ab	ab	cd	cd
1	447.6	15.0				
2	242.2	15.0				
3	243.9	15.0				
4	204.5	15.0	204.5	15.0	204.5	15.0
5			204.5	2.5	204.5	3.0
6			355.1	2.5	359.1	3.0
7					359.1	2.5
8	357.0	2.5				
9	396.4	2.5				

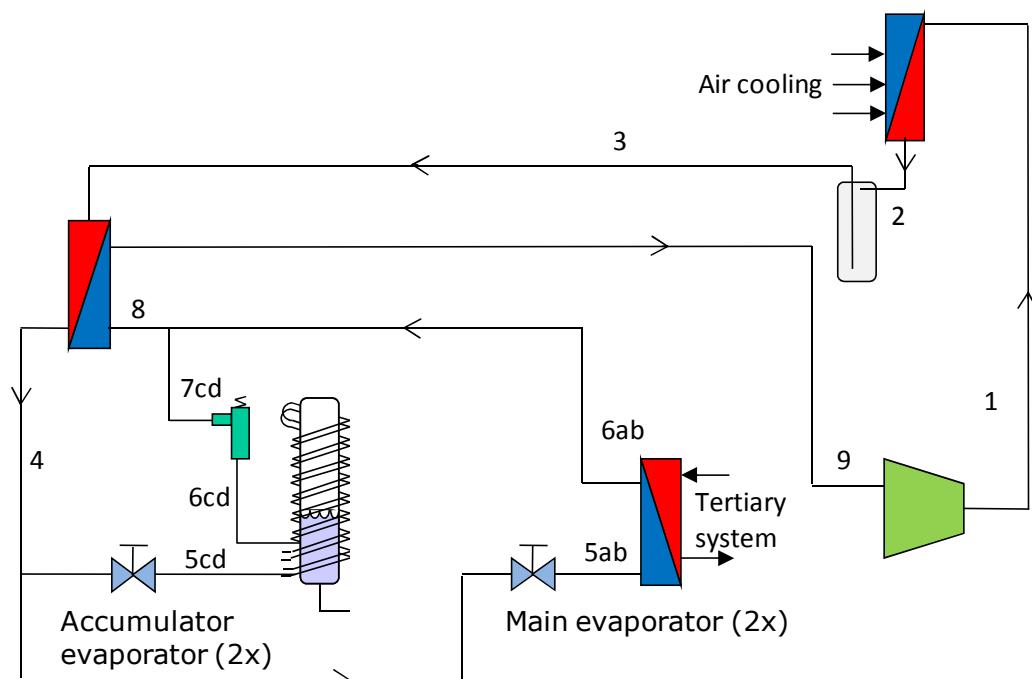


Figure 9.2-1: State-points of the SB main chiller.

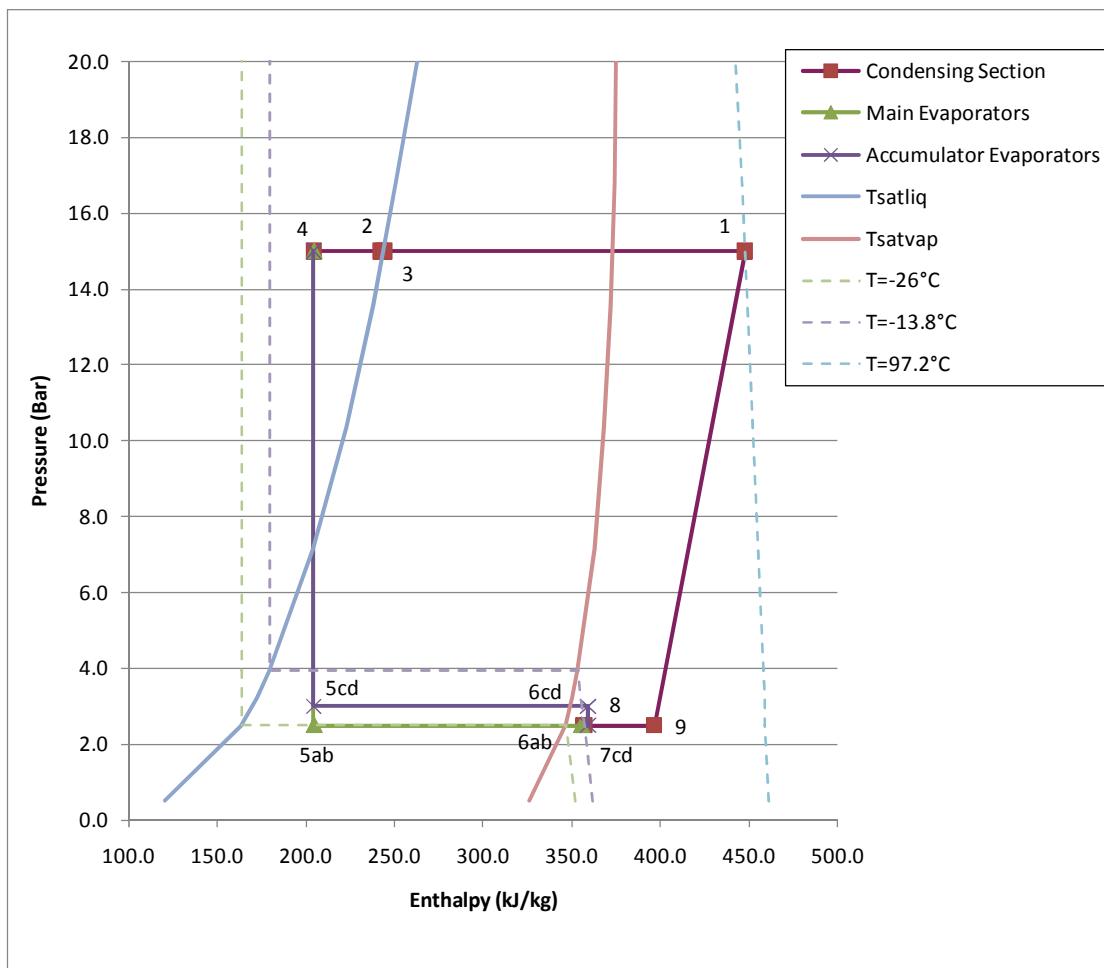


Figure 9.2-2: State point model result of the SB-chiller in the pressure enthalpy diagram of R507a.

### 9.3 Tertiary system simulation

A state point model has been build to simulate the tertiary CO<sub>2</sub> 2PACL systems. Figure 9.3-1 shows a schematic diagram of the cycle with the main state points numbered. The model is calculated with each section being a state-point.

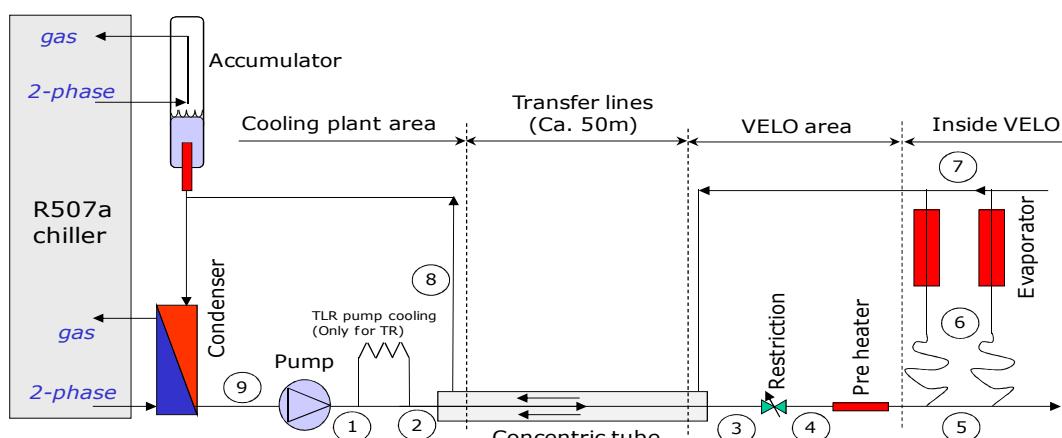


Figure 9.3-1: State point locations of the TL- and TR-CO<sub>2</sub> systems.

The 2PACL state models are much more detailed than the chiller models. The 2PACL state models are used to investigate the behavior of the CO<sub>2</sub> systems under the various conditions in which it is used. The 2PACL's are started with a pressurization to turn the system into a single phase liquid loop. The model shows in detail what happens if the single phase operation turns into a 2-phase operation, so the start-up and the application range can be explained.

The models of the TL and TR are a bit different from each other. The main difference is that TR has an extra heat exchanger after the pump to maintain the TLR pump cold for start-up. This is shown in the schematic between state-point 1 and 2. For the rest there are no big differences, other than some small volume differences. The real volumes are used for both the TL and TR models. In the model a pre-heater between state point 4 and 5 is present. In the current VTCS this heater does not exist. It is in the model to study a possible modification in the system. This is not discussed in this document. This power is set to zero.

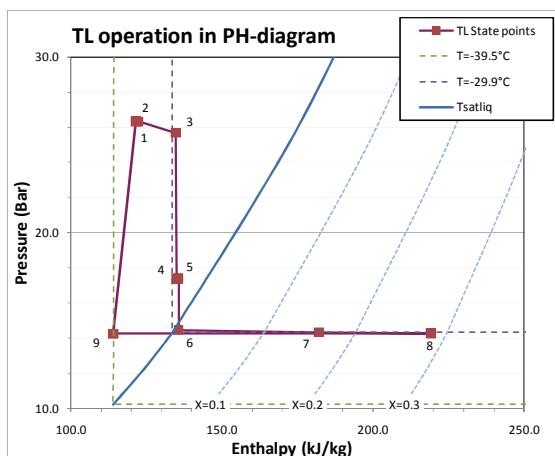


Table 9.3-1: TL state-points

TL State points	Enthalpy (kJ/kg)	Pressure (Bar)	Temperature (°C)	Vapor Quality
1	121.6	26.3	-35.8	Sub cooled
2	122.4	26.3	-35.4	Sub cooled
3	134.7	25.7	-29.3	Sub cooled
4	135.0	17.4	-29.2	Sub cooled
5	135.6	17.4	-28.9	Sub cooled
6	135.6	14.5	-29.6	0.00
7	182.1	14.3	-29.9	0.16
8	219.2	14.3	-30.0	0.28
9	114.0	14.3	-39.5	Sub cooled

Figure 9.3-2: TL state-points in the PH diagram (Tsat = -30, Q=489W)

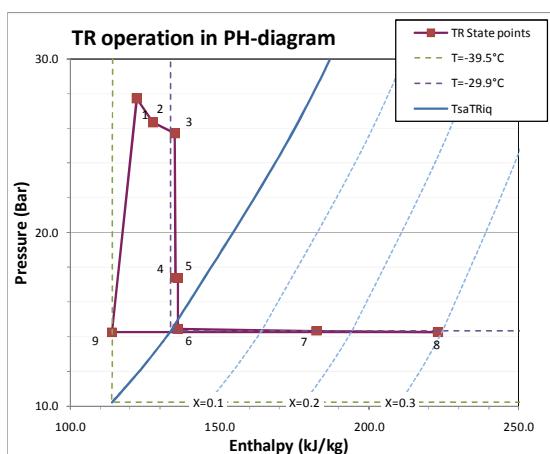


Table 9.3-2: TR state-points

TR State points	Enthalpy (kJ/kg)	Pressure (Bar)	Temperature (°C)	Vapor Quality
1	122.3	27.7	-35.4	Sub cooled
2	127.7	26.3	-32.8	Sub cooled
3	135.1	25.7	-29.2	Sub cooled
4	135.3	17.4	-29.0	Sub cooled
5	135.9	17.4	-28.7	Sub cooled
6	135.9	14.5	-29.6	0.01
7	182.4	14.3	-29.9	0.16
8	223.1	14.3	-30.0	0.30
9	114.0	14.3	-39.5	Sub cooled

Figure 9.3-3: TR state-points in the PH diagram (Tsat = -30, Q=489W)

The influence of the TLR pump cooling is clearly visible, at the TR results node 2 is below node 1, at TL they are overlapping. The detector load which is applied is 489 Watt, this is the section between node 6 and 7.

## 9.4 Transfer line simulation

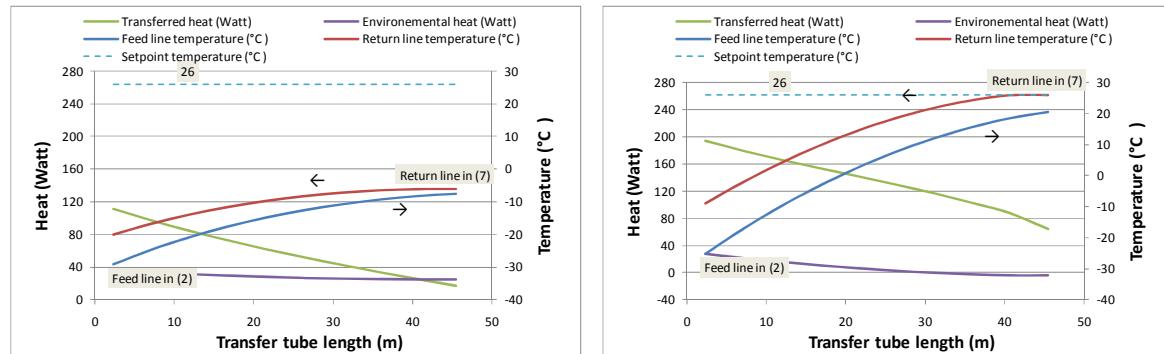


Figure 9.4-1: Set point 26°C (left Unpowered, right powered with 489W)

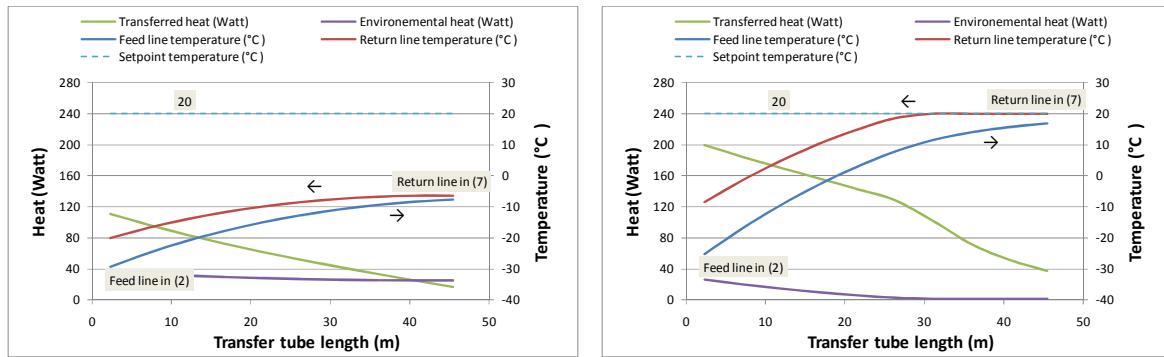


Figure 9.4-2: Set point 20°C (left Unpowered, right powered with 489W)

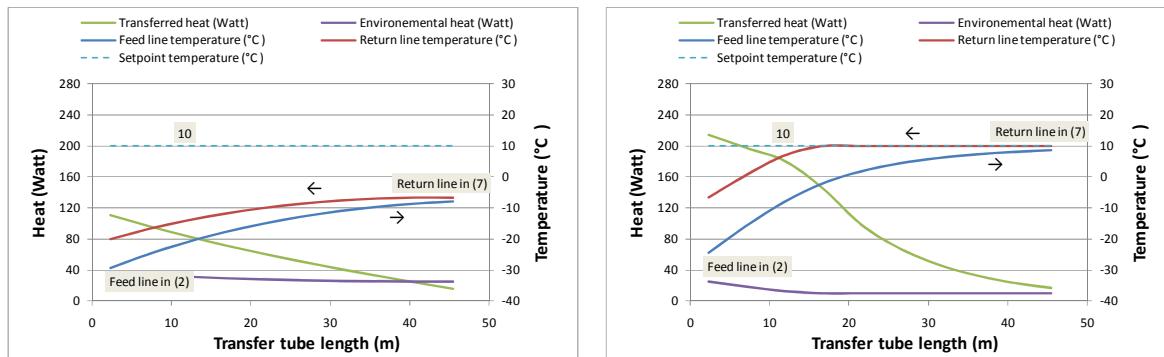


Figure 9.4-3: Set point 10°C (left Unpowered, right powered with 489W)

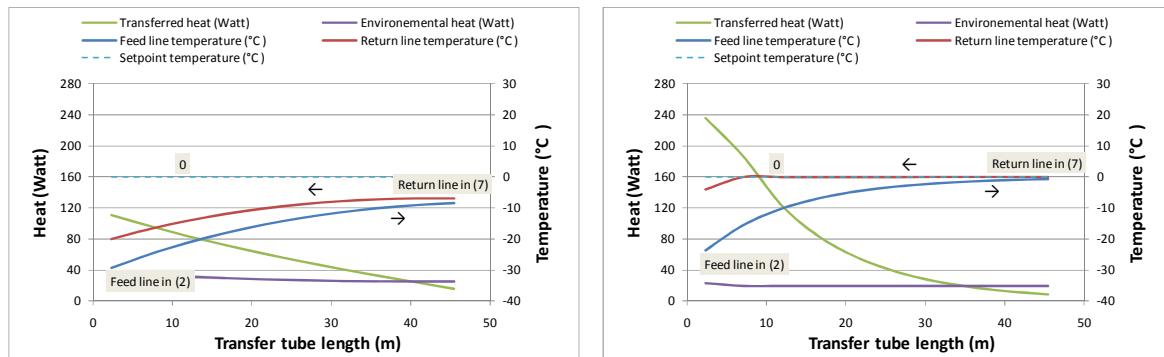
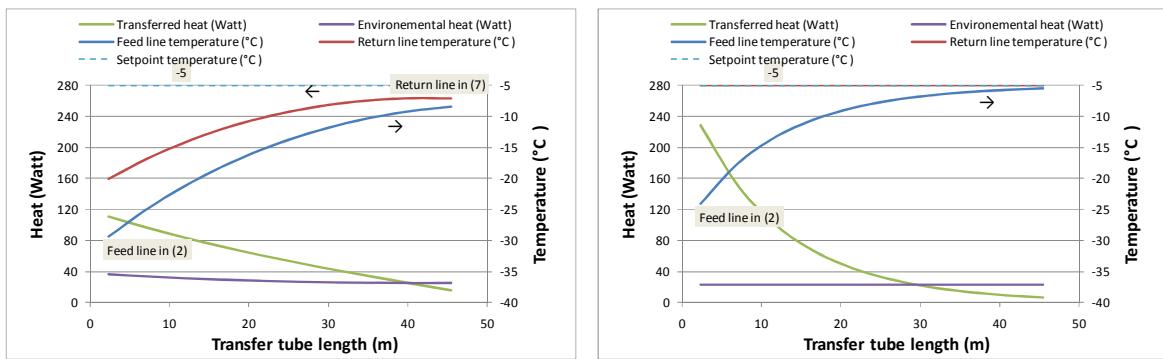
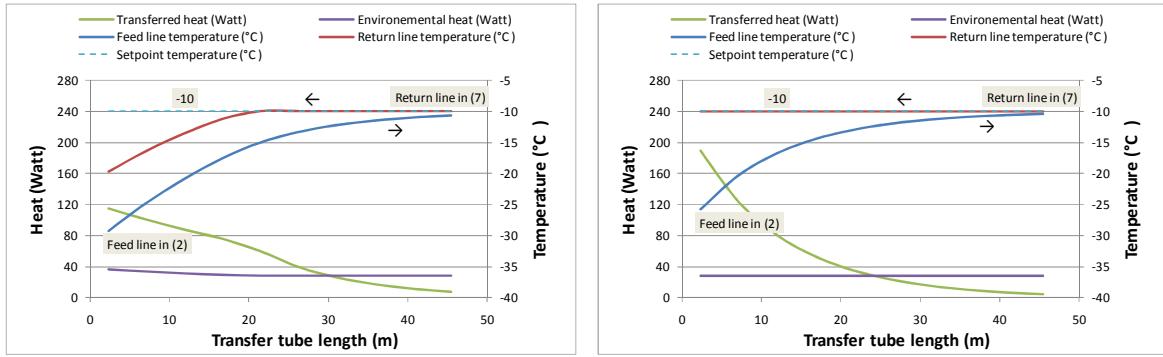
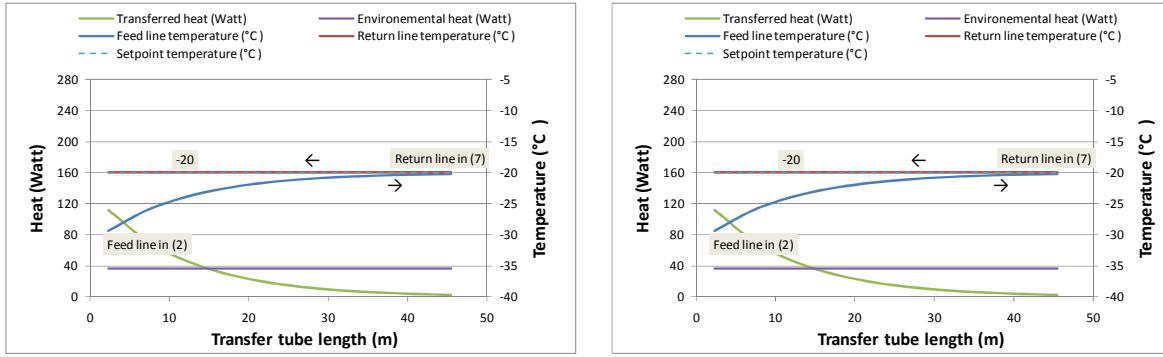
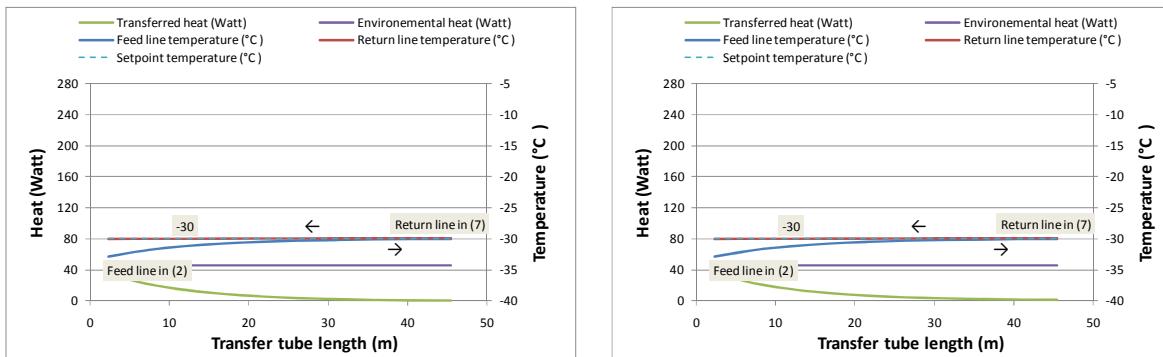


Figure 9.4-4: Set point 0°C (left Unpowered, right powered with 489W)

Figure 9.4-5: Set point  $-5^{\circ}\text{C}$  (left Unpowered, right powered with 489W)Figure 9.4-6: Set point  $-10^{\circ}\text{C}$  (left Unpowered, right powered with 489W)Figure 9.4-7: Set point  $-20^{\circ}\text{C}$  (left Unpowered, right powered with 489W)Figure 9.4-8: Set point  $-30^{\circ}\text{C}$  (left Unpowered, right powered with 489W)

The transfer line has a special role in the 2PACL principle. Besides from transferring the liquid from and to the evaporator, it must heat-up the inlet liquid of the evaporator towards saturation. The transfer line does this with virtual energy as it does not cost any additional applied heat. It is often believed that the maximum exchanged heat is the heat which is absorbed in the system and will so be reused. This is not the case, it is really virtual and as the simulations show, more heat can be exchanged than there is applied by heat loads or the environment. Figure 9.4-1 to Figure 9.4-8 show the results of the transfer line for simulations under different set point temperatures. The left figure indicates the unpowered situation, the right figure the powered situation. The nominal applied power is in all cases 489 Watt. The environmental load changes as the temperature changes.

## 9.5 *CO<sub>2</sub>* 2PACL start-up simulation

The 2PACL is started up by priming the complete loop with liquid. In the VTCS the loop is “pumped-up” to a saturation temperature 6 degrees above the measured temperature on Tx\_TT112. The start-up set point is limited to 26°C, otherwise the accumulator will have no liquid anymore. The simulations show that the loop is completely operated in single phase at this time. The figures starting from Figure 9.5-1 show the steady state results of the different start-up stages. The left row of plots show the unpowered situation of the start-up stage the right row of plots show the powered situation.

The trapezium sized cycles in the PH diagram are lowered by lowering the accumulator set-point. At the moment that point 6 (the evaporator inlet) hits the saturation line it starts to evaporate in the evaporator. From that moment on a further lowering of this point follows the saturation line. It shows that the accumulator has full control over the evaporator temperature in the range between -10°C to -30°C. In this range the VTCS is operated. The shown simulation results are from the same simulation as shown for the transfer line (paragraph 9.4). State point temperatures 2,3,7 and 8 in the PH diagram can be compared to the temperatures in the transfer line in and outlets.

The simulation results will be compared with measurements of the VTCS in future publications. First measurements show a good comparison of the simulation with real measurement data.

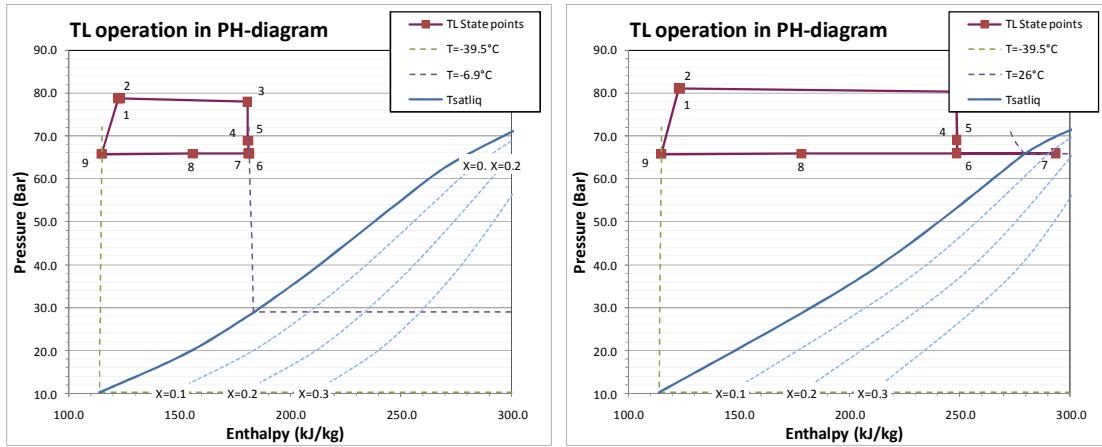


Figure 9.5-1: Set point 26°C (left Unpowered, right powered with 489W)

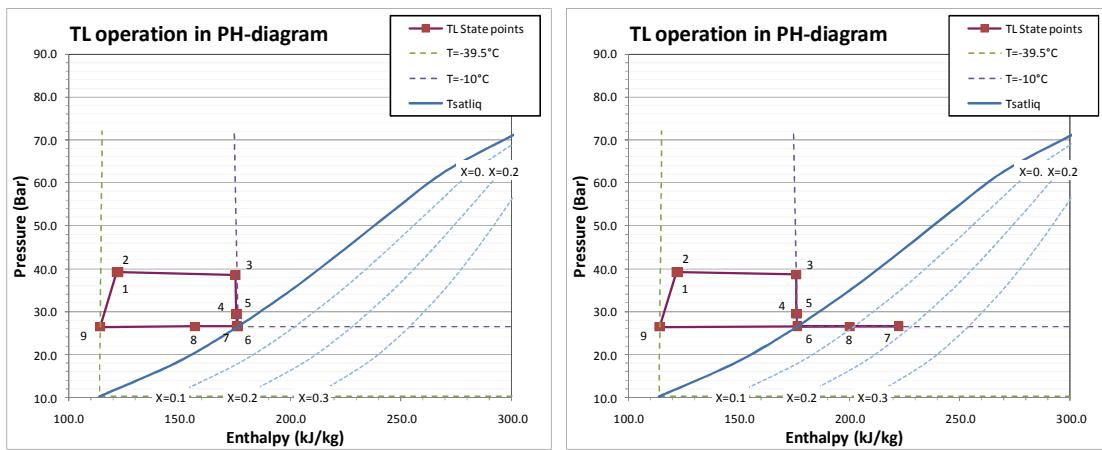


Figure 9.5-2: Set point -10°C (left Unpowered, right powered with 489W)

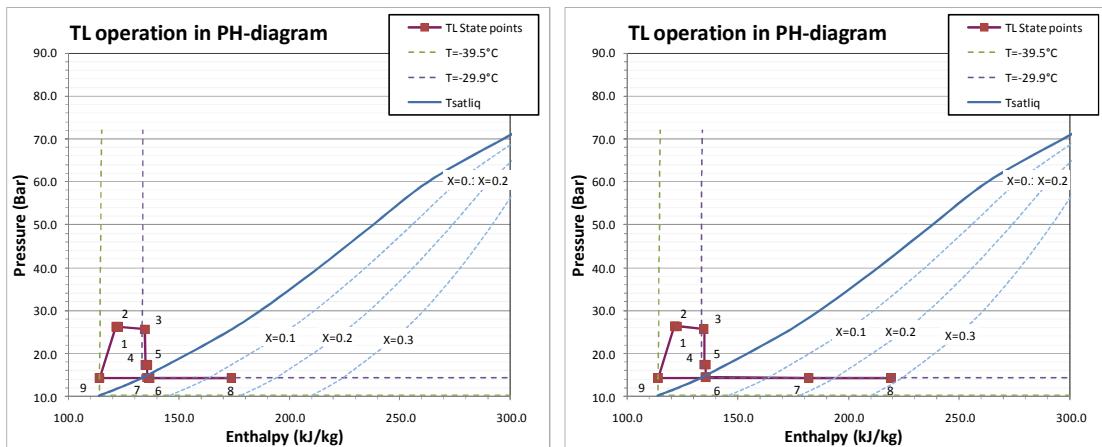


Figure 9.5-3: Set point -30°C (left Unpowered, right powered with 489W)

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[http://www.nikhef.nl/pub/departments/mt/projects/lhcb-vertex/production/Coolingsystem/Evaporator\\_casting\\_process.pdf](http://www.nikhef.nl/pub/departments/mt/projects/lhcb-vertex/production/Coolingsystem/Evaporator_casting_process.pdf).
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# 11 Appendix

## 11.1 Schematics

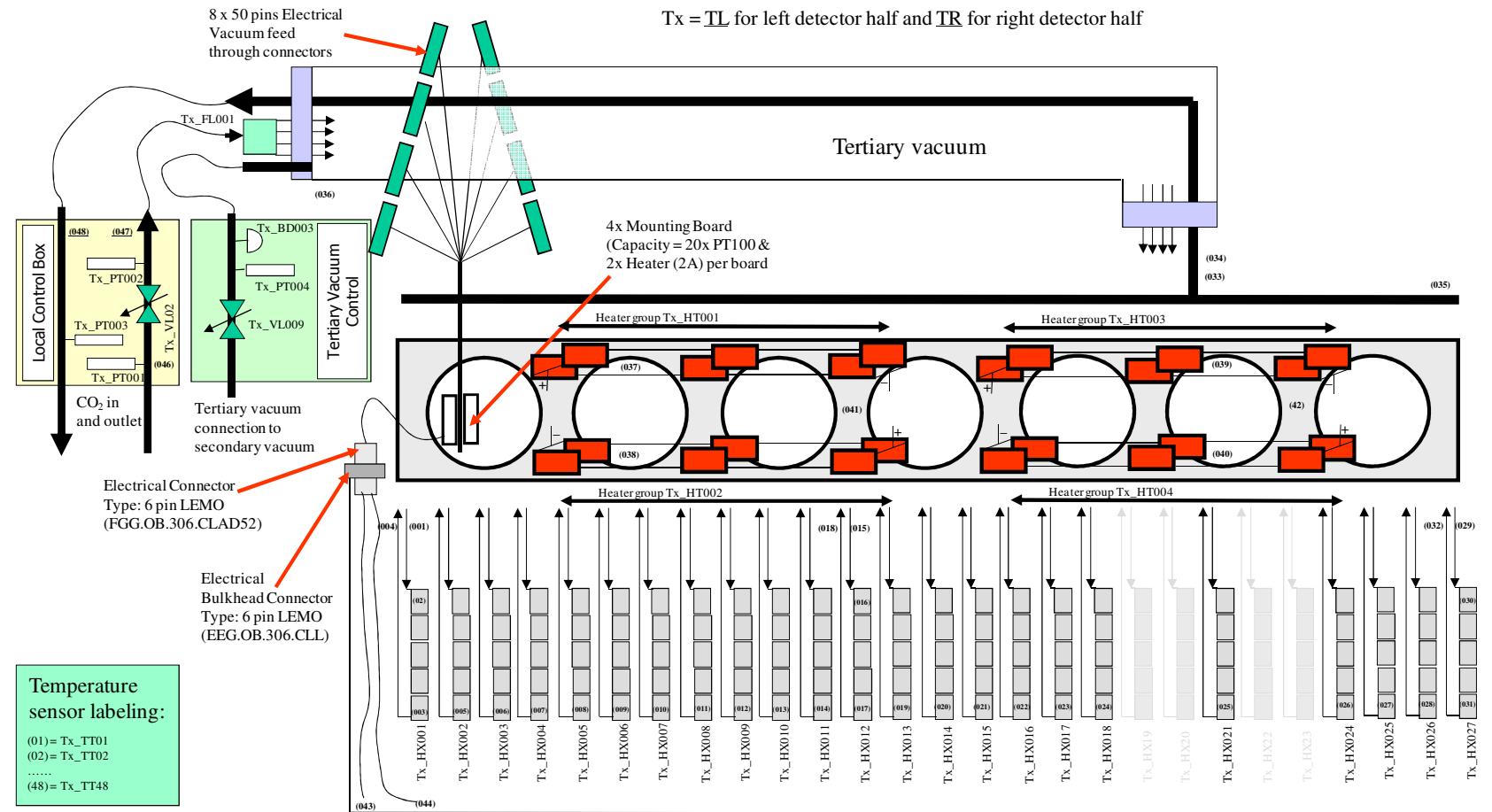
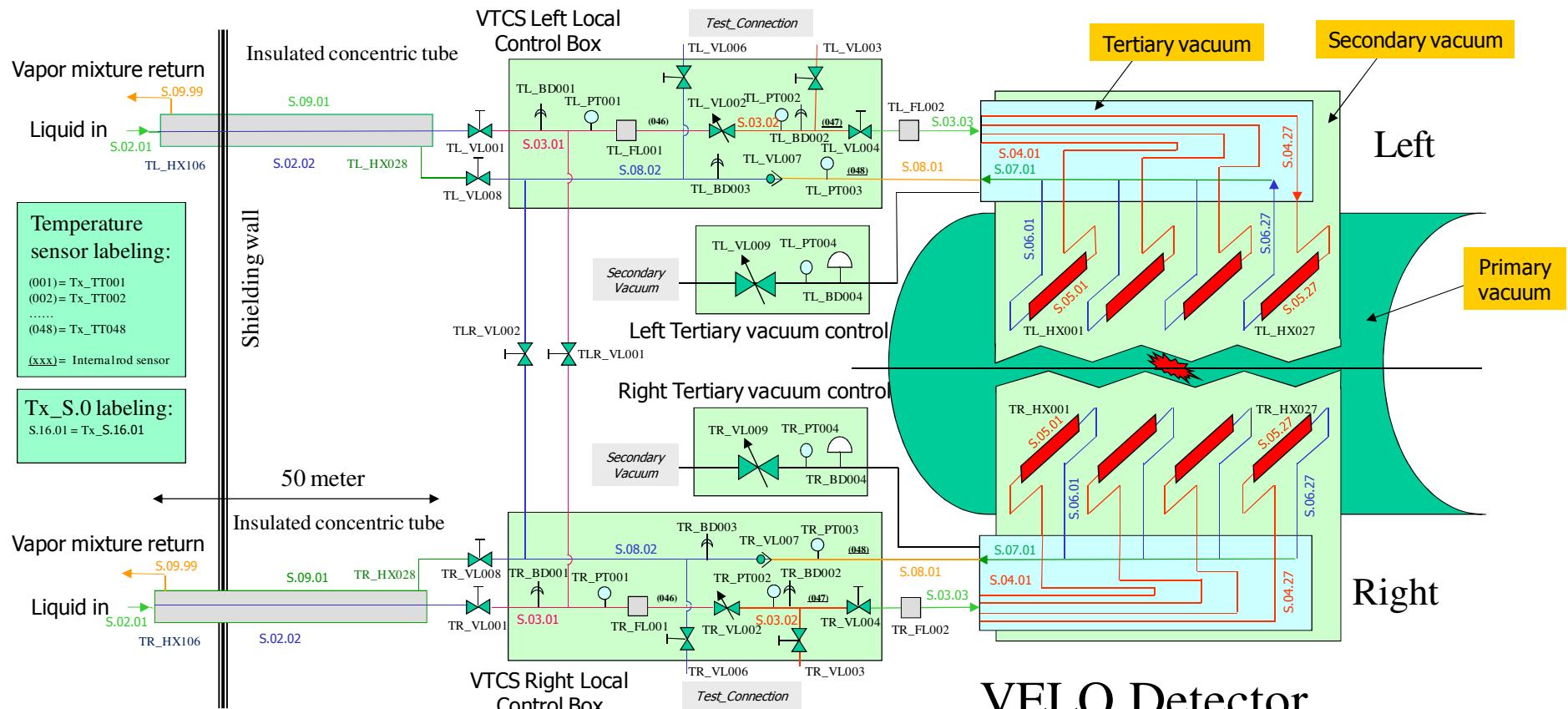
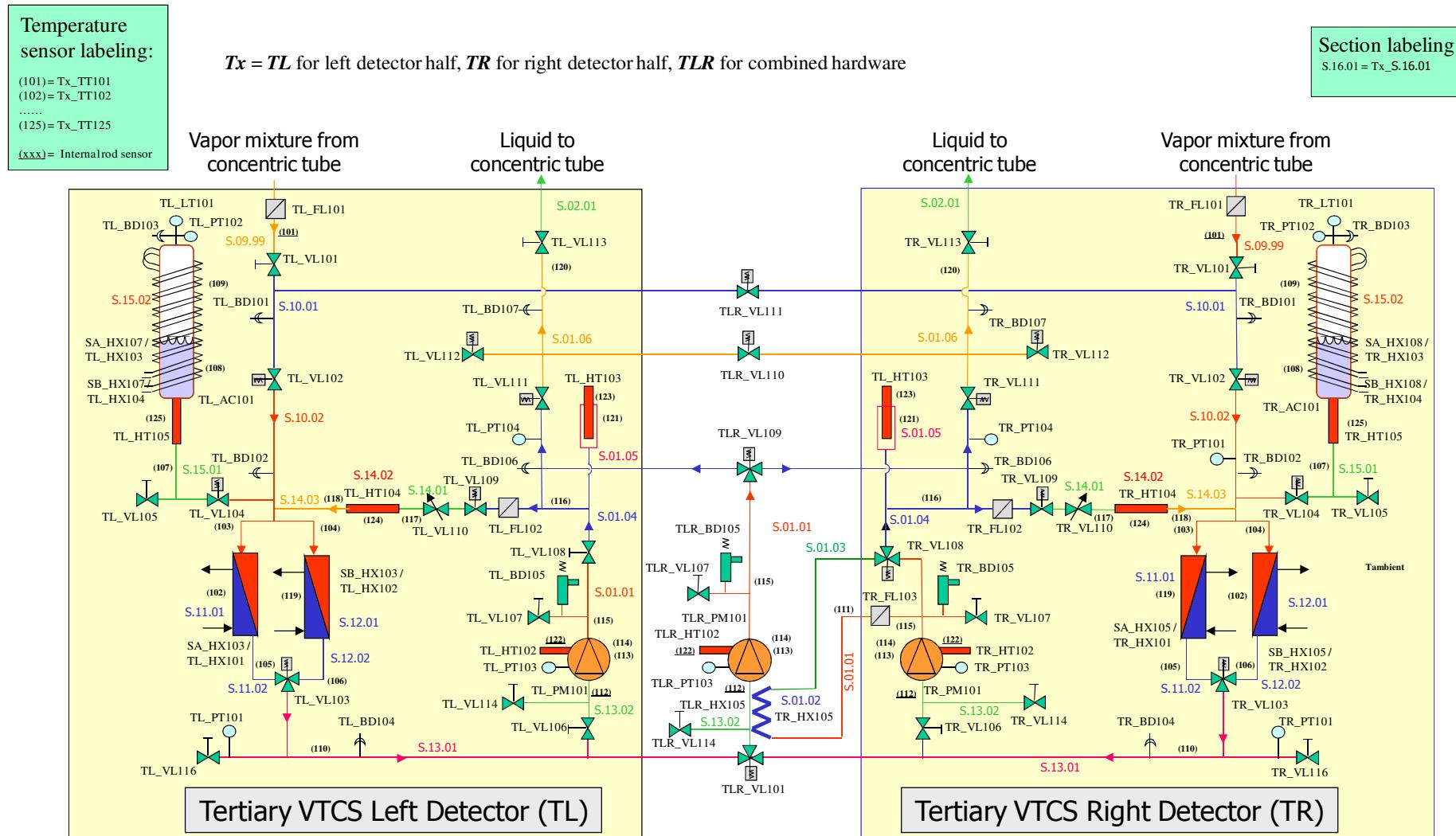


Figure 11.1-1: VTCS hardware labeling inside the VELO detector



**Tx** = **TL** for left detector half, **TR** for right detector half, **TLR** for combined hardware

Figure 11.1-2: VTCS schematics and hardware labeling outside the VELO detector in the VELO cavern

Figure 11.1-3: VTCS Tertiary CO<sub>2</sub> plant schematics and labeling

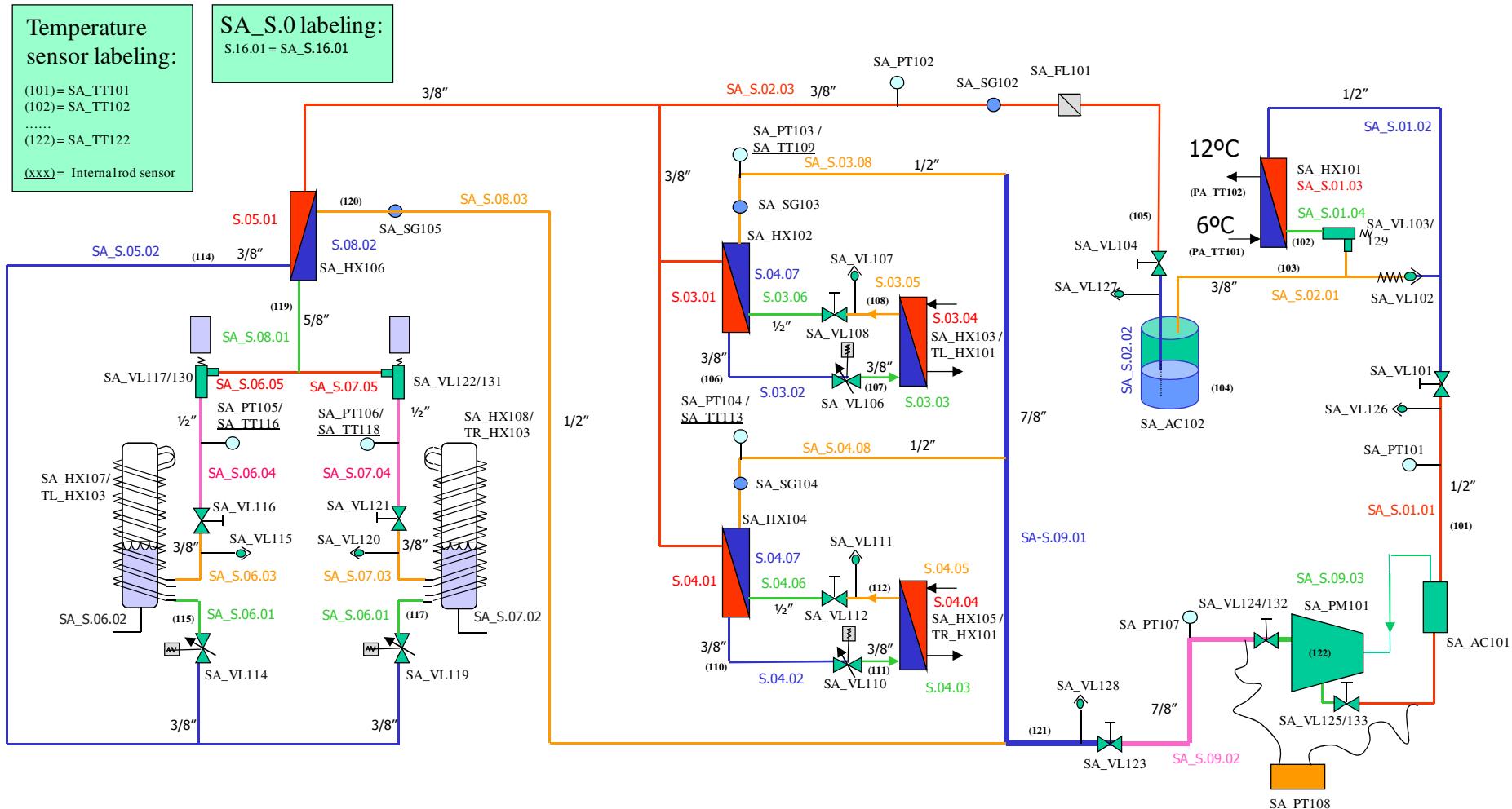


Figure 11.1-4: Secondary main chiller schematics and labeling

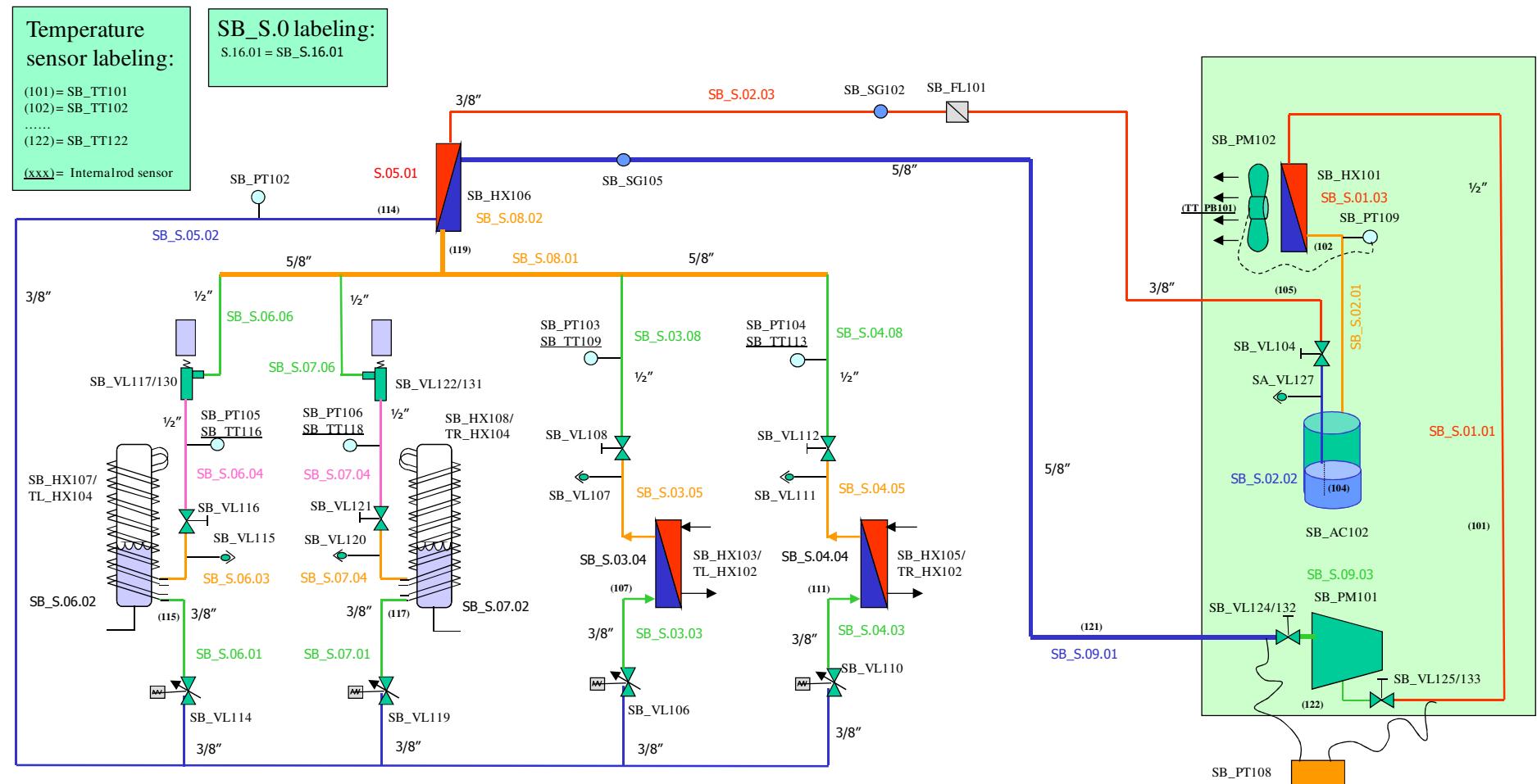


Figure 11.1-5:

Secondary Back-up chiller schematics and labeling

## 11.2 Sensors

### 11.2.1 Temperature Transmitters

<b>Code</b>	<b>low</b>	<b>high</b>	<b>Part number</b>	<b>Function</b>
TL_TT001	-35	10	PT100	TL_HX001 Liquid inlet
TL_TT002	-35	10	PT100	TL_HX001 block 1
TL_TT003	-35	10	PT100	TL_HX001Dry-out monitoring
TL_TT004	-35	10	PT100	TL_HX001 Vapor outlet
TL_TT005	-35	10	PT100	TL_HX002 Dry-out monitoring
TL_TT006	-35	10	PT100	TL_HX003 Dry-out monitoring
TL_TT007	-35	10	PT100	TL_HX004 Dry-out monitoring
TL_TT008	-35	10	PT100	TL_HX005 Dry-out monitoring
TL_TT009	-35	10	PT100	TL_HX006 Dry-out monitoring
TL_TT010	-35	10	PT100	TL_HX007 Dry-out monitoring
TL_TT011	-35	10	PT100	TL_HX008 Dry-out monitoring
TL_TT012	-35	10	PT100	TL_HX009 Dry-out monitoring
TL_TT013	-35	10	PT100	TL_HX010 Dry-out monitoring
TL_TT014	-35	10	PT100	TL_HX011 Dry-out monitoring
TL_TT015	-35	10	PT100	TL_HX012 Liquid inlet
TL_TT016	-35	10	PT100	TL_HX012 block 1
TL_TT017	-35	10	PT100	TL_HX012 Dry-out monitoring
TL_TT018	-35	10	PT100	TL_HX012 Vapor outlet
TL_TT019	-35	10	PT100	TL_HX013 Dry-out monitoring
TL_TT020	-35	10	PT100	TL_HX014 Dry-out monitoring
TL_TT021	-35	10	PT100	TL_HX015 Dry-out monitoring
TL_TT022	-35	10	PT100	TL_HX016 Dry-out monitoring
TL_TT023	-35	10	PT100	TL_HX017 Dry-out monitoring
TL_TT024	-35	10	PT100	TL_HX018 Dry-out monitoring
TL_TT025	-35	10	PT100	TL_HX021Dry-out monitoring

TL_TT026	-35	10	PT100	TL_HX024 Dry-out monitoring
TL_TT027	-35	10	PT100	TL_HX025 Dry-out monitoring
TL_TT028	-35	10	PT100	TL_HX026 Dry-out monitoring
TL_TT029	-35	10	PT100	TL_HX027 Liquid inlet
TL_TT030	-35	10	PT100	TL_HX027 block 1
TL_TT031	-35	10	PT100	TL_HX027 Dry-out monitoring
TL_TT032	-35	10	PT100	TL_HX027 Vapor outlet
TL_TT033	-35	10	PT100	Vapor return
TL_TT034	-35	10	PT100	Vapor return
TL_TT035	-35	20	PT100	Manifold
TL_TT036	12	30	PT100	Bellow flange
TL_TT037	15	27	PT100	TL_HT001 Heater Control
TL_TT038	15	27	PT100	TL_HT002 Heater Control
TL_TT039	15	27	PT100	TL_HT003 Heater Control
TL_TT040	15	27	PT100	TL_HT004 Heater Control
TL_TT041	15	27	PT100	Module base
TL_TT042	15	27	PT100	Module base
TL_TT043	15	27	PT100	RF-Foil
TL_TT044	15	27	PT100	RF-Foil
TL_TT045	-35	30	PT100	Transfer tube liquid outlet
TL_TT046	-35	10	PT100	Local control box liquid inlet
TL_TT047	-35	10	PT100	Capillaries inlet
TL_TT048	-35	10	PT100	Local control box vapor outlet
TL_TT101	-45	5	Internal PT100 Rodax: PPA_PT100_SO_S_A1_D3_W4_130_6D	Transfer tube vapor outlet
TL_TT102	-48	30	PT100	Main condenser Front plate
TL_TT103	-48	5	PT100	Main condenser inlet
TL_TT104	-48	5	PT100	Back-up condenser inlet
TL_TT105	-48	5	PT100	Main condenser outlet
TL_TT106	-48	5	PT100	Back-up condenser outlet
TL_TT107	-45	5	PT100	Accumulator line

TL_TT108	-20	5	PT100	Accumulator Liquid
TL_TT109	-5	20	PT100	Accumulator Vapor
TL_TT110	-48	-2	PT100	Condenser outlet
xx_TTamb	15	25		
TL_TT112	-48	-2	Internal PT100 Rodax: PPA_PT100_SO_S_A1_D3_W4_130_6D	TL-PM101 pump.state inlet
TL_TT113	-40	30	PT100	TL-PM101 pump.state head oil side
TL_TT114	-40	30	PT100	TL-PM101 pump.state head CO <sub>2</sub> side
TL_TT115	-45	-2	PT100	TL-PM101 pump.state outlet
TL_TT116	-45	-2	PT100	liquid line
TL_TT117	-45	30	PT100	By-pass liquid
TL_TT118	-45	30	PT100	By-pass vapor
TL_TT119	-48	30	PT100	Condenser Back plate
TL_TT120	-48	30	PT100	Transfer tube liquid inlet
TL_TT121	0	100	Thermocouple K	Press damper temperature
TL_TT122	12	25	Thermocouple K	TL-HT102 Control (pump.state oil heater)
TL_TT123	0	100	Thermocouple K	TL-HT103 Control
TL_TT124	-45	50	Thermocouple K	TL-HT104 Control
TL_TT125	-45	100	Thermocouple K	TL-HT105 Control (Accu heater)
TR_TT001	-35	10	PT100	TR_HX001 Liquid inlet
TR_TT002	-35	10	PT100	TR_HX001 block 1
TR_TT003	-35	10	PT100	TR_HX001Dry-out monitoring
TR_TT004	-35	10	PT100	TR_HX001 Vapor outlet
TR_TT005	-35	10	PT100	TR_HX002 Dry-out monitoring
TR_TT006	-35	10	PT100	TR_HX003 Dry-out monitoring
TR_TT007	-35	10	PT100	TR_HX004 Dry-out monitoring
TR_TT008	-35	10	PT100	TR_HX005 Dry-out monitoring
TR_TT009	-35	10	PT100	TR_HX006 Dry-out monitoring
TR_TT010	-35	10	PT100	TR_HX007 Dry-out monitoring
TR_TT011	-35	10	PT100	TR_HX008 Dry-out monitoring
TR_TT012	-35	10	PT100	TR_HX009 Dry-out monitoring

TR_TT013	-35	10	PT100	TR_HX010 Dry-out monitoring
TR_TT014	-35	10	PT100	TR_HX011 Dry-out monitoring
TR_TT015	-35	10	PT100	TR_HX012 Liquid inlet
TR_TT016	-35	10	PT100	TR_HX012 block 1
TR_TT017	-35	10	PT100	TR_HX012 Dry-out monitoring
TR_TT018	-35	10	PT100	TR_HX012 Vapor ouTRet
TR_TT019	-35	10	PT100	TR_HX013 Dry-out monitoring
TR_TT020	-35	10	PT100	TR_HX014 Dry-out monitoring
TR_TT021	-35	10	PT100	TR_HX015 Dry-out monitoring
TR_TT022	-35	10	PT100	TR_HX016 Dry-out monitoring
TR_TT023	-35	10	PT100	TR_HX017 Dry-out monitoring
TR_TT024	-35	10	PT100	TR_HX018 Dry-out monitoring
TR_TT025	-35	10	PT100	TR_HX021Dry-out monitoring
TR_TT026	-35	10	PT100	TR_HX024 Dry-out monitoring
TR_TT027	-35	10	PT100	TR_HX025 Dry-out monitoring
TR_TT028	-35	10	PT100	TR_HX026 Dry-out monitoring
TR_TT029	-35	10	PT100	TR_HX027 Liquid inlet
TR_TT030	-35	10	PT100	TR_HX027 block 1
TR_TT031	-35	10	PT100	TR_HX027 Dry-out monitoring
TR_TT032	-35	10	PT100	TR_HX027 Vapor ouTRet
TR_TT033	-35	10	PT100	Vapor return
TR_TT034	-35	10	PT100	Vapor return
TR_TT035	-35	20	PT100	Manifold
TR_TT036	12	30	PT100	Bellow flange
TR_TT037	15	27	PT100	TR_HT001 Heater Control
TR_TT038	15	27	PT100	TR_HT002 Heater Control
TR_TT039	15	27	PT100	TR_HT003 Heater Control
TR_TT040	15	27	PT100	TR_HT004 Heater Control
TR_TT041	15	27	PT100	Module base
TR_TT042	15	27	PT100	Module base
TR_TT043	15	27	PT100	RF-Foil
TR_TT044	15	27	PT100	RF-Foil

TR_TT045	-35	30	PT100	Transfer tube liquid outlet
TR_TT046	-35	10	PT100	Local control box liquid inlet
TR_TT047	-35	10	PT100	Capillaries inlet
TR_TT048	-35	10	PT100	Local control box vapor outlet
TR_TT101	-45	5	Internal PT100 Rodax: PPA_PT100_SO_S_A1_D3_W4_130_6D	Transfer tube vapor outlet
TR_TT102	-48	30	PT100	Main condenser Front plate
TR_TT103	-48	5	PT100	Main condenser inlet
TR_TT104	-48	5	PT100	Back-up condenser inlet
TR_TT105	-48	5	PT100	Main condenser outlet
TR_TT106	-48	5	PT100	Back-up condenser outlet
TR_TT107	-45	5	PT100	Accumulator line
TR_TT108	-20	5	PT100	Accumulator Liquid
TR_TT109	-5	20	PT100	Accumulator Vapor
TR_TT110	-48	-2	PT100	Condenser outlet
TR_TT111	-5	10	PT100	TLR-PM101 pump.state head cooling
TR_TT112	-48	-2	Internal PT100 Rodax: PPA_PT100_SO_S_A1_D3_W4_130_6D	TR-PM101 pump.state inlet
TR_TT113	-40	30	PT100	TR-PM101 pump.state head oil side
TR_TT114	-40	30	PT100	TR-PM101 pump.state head CO <sub>2</sub> side
TR_TT115	-45	-2	PT100	TR-PM101 pump.state outlet
TR_TT116	-45	-2	PT100	liquid line
TR_TT117	-45	30	PT100	By-pass liquid
TR_TT118	-45	30	PT100	By-pass vapor
TR_TT119	-48	30	PT100	Condenser Back plate
TR_TT120	-48	30	PT100	Transfer tube liquid inlet
TR_TT121	0	100	Thermocouple K	Press damper temperature
TR_TT122	12	25	Thermocouple K	TR-HT102 Control (pump.state oil heater)
TR_TT123	0	100	Thermocouple K	TR-HT103 Control
TR_TT124	-45	50	Thermocouple K	TR-HT104 Control
TR_TT125	-45	100	Thermocouple K	TR-HT105 Control (Accu heater)

TLR_TT112	-35	10	Internal PT100 Rodax: PPA_PT100_SO_S_A1_D3_W4_130_6D	TLR-PM101 pump.state inlet
TLR_TT113	-35	10	PT100	TLR-PM101 pump.state head oil side
TLR_TT114	-35	10	PT100	TLR-PM101 pump.state head CO <sub>2</sub> side
TLR_TT115	-35	10	PT100	TLR-PM101 pump.state outlet
TLR_TT122	-45	80	Thermocouple K	TLR-HT102 Control (pump.state oil heater)
SA_TT101	15	25	PT100	Discharge
SA_TT102	4	25	PT100	Condensor outlet
SA_TT103	12	25	PT100	Liquid vessel inlet
SA_TT104	12	25	PT100	Liquid vessel
SA_TT105	12	25	PT100	Liquid
SA_TT106	-45	25	PT100	SA-HX103 subcooled liquid
SA_TT107	-45	25	PT100	SA-HX103 evaporator inlet
SA_TT108	-45	25	PT100	SA-HX103 evaporator outlet
SA_TT109	-45	25	Internal PT100 Rodax: PPA_PT100_SO_S_A1_D3_W4_130_6D	SA-HX103 superheat
SA_TT110	-45	25	PT100	SA-HX105 subcooled liquid
SA_TT111	-45	25	PT100	SA-HX105 evaporator inlet
SA_TT112	-45	25	PT100	SA-HX105 evaporator outlet
SA_TT113	-45	25	Internal PT100 Rodax: PPA_PT100_SO_S_A1_D3_W4_130_6D	SA-HX105 superheat
SA_TT114	-35	25	PT100	SA-HX107/108 subcooled liquid
SA_TT115	-35	25	PT100	SA-HX107 evaporator inlet
SA_TT116	-35	25	Internal PT100 Rodax: PPA_PT100_SO_S_A1_D3_W4_130_6D	SA-HX107 superheat
SA_TT117	-35	25	PT100	SA-HX108 evaporator inlet
SA_TT118	-35	25	Internal PT100 Rodax: PPA_PT100_SO_S_A1_D3_W4_130_6D	SA-HX108 superheat
SA_TT119	-35	25	PT100	SA-HX107/108 cold gas
SA_TT120	-35	25	PT100	SA-HX107/108 Suction
SA_TT121	-35	25	PT100	Suction

SA_TT122	12	60	PT100	Compressor
SB_TT101	15	100	PT100	Discharge
SB_TT102	4	35	PT100	Condensor outlet
SB_TT104	12	35	PT100	Liquid vessel
SB_TT105	12	35	PT100	Liquid
SB_TT107	-35	25	PT100	SB-HX103 evaporator inlet
SB_TT109	-35	25	Internal PT100 Rodax: PPA_PT100_SO_S_A1_D3_W4_130_6D	SB-HX103 superheat
SB_TT111	-35	25	PT100	SB-HX105 evaporator inlet
SB_TT113	-35	25	Internal PT100 Rodax: PPA_PT100_SO_S_A1_D3_W4_130_6D	SB-HX105 superheat
SB_TT114	-25	25	PT100	subcooled liquid
SB_TT115	-25	25	PT100	SB-HX107 evaporator inlet
SB_TT116	-25	25	Internal PT100 Rodax: PPA_PT100_SO_S_A1_D3_W4_130_6D	SB-HX107 superheat
SB_TT117	-25	25	PT100	SB-HX108 evaporator inlet
SB_TT118	-25	25	Internal PT100 Rodax: PPA_PT100_SO_S_A1_D3_W4_130_6D	SB-HX108 superheat
SB_TT119	-25	25	PT100	Cold gas
SB_TT121	-25	25	PT100	Suction
SB_TT122	12	25	PT100	Compressor
PA_TT101	4	15	PT100	Cooling water inlet
PA_TT102	4	15	PT100	Cooling water outlet
PB_TT101	12	35	PT100	Air inlet

**rodax**  
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Rodax N.V. K.Van Overmeirelaan 21-23 B-2100 Antwerpen, Belgium Tel +32 3 360 90 00 Fax +32 3 326 44 74 <a href="http://www.rodax-europe.com">www.rodax-europe.com</a> BTW nr : BE 425.216.722 HRA nr : 239.013	<b>ISO 9001 certified</b>	<b>Fax nr</b>	<b>pietdg@nikhef.nl</b>
	<b>FAX</b>	Date: 28-Jun-10	Ref : RD NIKHEF D41118 D0 TS

**To : NIKHEF**  
**From : Tom Smets**  
E-mail address: [tsmets@rodax.be](mailto:tsmets@rodax.be)

**Attn : Dhr. P.J.M. de Groen**  
**Page : 1**

In case you did not receive all pages, please contact +32 3 360 90 00

Geachte heer de Groen,

Betreft : Uw prijsaanvraag d.d. 13/11/2004

Hiermede hebben wij het genoegen U volgende aanbieding te maken :

PZA PT100 NW S A1 D3 W4 750

PZA	: RTD model
PT100 NW	: RTD type
S	: Single element
A1	: Nauwkeurigheidsklasse
D3	: Diameter 3 mm
W4	: 4-draads uitvoering
750	: Lengte element 750 mm

Prijs voor 1-9 stuks : 55,70 Euro/stuk  
prijs vanaf 10 stuks : 45,50 Euro/stuk  
Levertarief : - 4-6 weken (eventueel nadere besprekken)

#### **VERKOOPSOORWAARDEN:**

Onze algemene verkoopsvoorwaarden zijn van toepassing.

Wanneer U deze niet in uw bezit heeft sturen wij U deze toe op uw eerste verzoek.  
Ze staan ook beschikbaar op onze website : [www.rodax-europe.com](http://www.rodax-europe.com)

De hiermogelijkde bijzondere voorwaarden zijn eveneens geldig:

Prijs	: excl. BTW
Betaling	: 30 nat
Levering	: DDP Benelux > 125 € - Voor een orderbedrag minder dan 125,00 €, zal 17,00 € vachtkosten aangerekend worden - minimum orderbedrag: 75,00 € - voor een orderbedrag minder dan 75,00 €, zal 17,00 € administratiekosten aangerekend worden

Leverijd	: Zie hierboven
Waborg	: 1 jaar bij juist gebruik met goed vakmanschap, onder normale werkingsomstandigheden en binnen de limieten van het product.
Geldigheidsduur	van de offerte : 30 dagen

Als u nog eventuele vragen heeft hoor ik het graag.

Met vriendelijke groeten,

**Tom Smets**  
Inside Sales Engineer  
RODAX NV

Figure 11.2-1: Submerged PT100's

## 11.2.2 Pressure Transmitters

Table 11.2-1: VTCS Pressure sensors

Code	Part number	Function	Connection	Operating Pressure (Bar)	Maximum Pressure (Bar)	Minimum design temperature (°C)	Maximum design temperature (°C)	Minimum measuring range (Bar)	Maximum measuring range(Bar)	Supply (V)	Output signal
TL_PT001	Kulite HKM-375M-100BAR-A	Transfer tune outlet pressure	M10x1 Male	100	200			0	100	10Vdc	100mV
TL_PT002	Kulite HKM-375M-100BAR-A	Evaporator inlet pressure	M10x1 Male	100	200			0	100	10Vdc	100mV
TL_PT003	Kulite HKM-375M-100BAR-A	Evaporator (outlet) pressure	M10x1 Male	100	200			0	100	10Vdc	100mV
TL_PT004	Balzers Pirani TPR0118 (DN 16 CF-F) BGG15011	Tertiary vacuum monitoring	CF16	2				1.00E-06	1		
TL_PT101	Druck PTX7511-100bar	Condenser pressure	G1/4"Female	100	200	-40	80	0	100	9-30Vdc	4-20mA
TL_PT102	Druck PTX7511-100bar	Accumulator pressure	G1/4"Female	100	200	-40	80	0	100	9-30Vdc	4-20mA
TL_PT103	Lewa pump integral	TL-PM101 Membrane Pressure		100							Open/close
TL_PT104	Druck PTX7511-100bar	Pump outlet	G1/4"Female	100	200	-40	80	0	100	9-30Vdc	4-20mA
TR_PT001	Kulite HKM-375M-100BAR-A	Transfer tune outlet pressure	M10x1 Male	100	200			0	100	10Vdc	100mV
TR_PT002	Kulite HKM-375M-100BAR-A	Evaporator inlet pressure	M10x1 Male	100	200			0	100	10Vdc	100mV
TR_PT003	Kulite HKM-375M-100BAR-A	Evaporator (outlet) pressure	M10x1 Male	100	200			0	100	10Vdc	100mV
TR_PT004	Balzers Pirani TPR0118 (DN 16 CF-F) BGG15011	Tertiary vacuum monitoring	CF16	2				1.00E-06	1		
TR_PT101	Druck PTX7511-100bar	Accumulator pressure	G1/4"Female	100	200	-40	80	0	100	9-30Vdc	4-20mA
TR_PT102	Druck PTX7511-100bar	Accumulator pressure	G1/4"Female	100	200	-40	80	0	100	9-30Vdc	4-20mA
TR_PT103	Lewa pump integral	TR-PM101 Membrane Pressure		100							Open/close
TR_PT104	Druck PTX7511-100bar	Pump outlet	G1/4"Female	100	200	-40	80	0	100	9-30Vdc	4-20mA
TLR_PT103	Lewa pump integral	TLR-PM101 Membrane Pressure		100							Open/close
SA_PT101	Danfoss AKS 33 60G2051	Discharge pressure	1/4" Male Flare	33	55	0	80	0	35		4-20mA



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# PTX 7500 Specifications

## Pressure Measurement

### Operating Pressure Ranges

Any zero based full scale (FS) from 1.5 to 1000 psi (100 mbar to 70 bar) gauge or absolute  
Any zero based FS above 1000 psi (70 bar) up to 10000 psi (700 bar) sealed gauge or absolute  
Barometric 11.5 to 17.4 psi (800 to 1200 mbar) absolute

For other barometric, elevated zero (e.g. 15 to 60 psi (1 to 4 bar)) and compound ranges (e.g. -15 to +15 psi (-1 to +1 bar)) Refer to GE Druck for further information

### Pressure Units

psi, mbar, bar, hPa, kPa, MPa, mmH<sub>2</sub>O, torr, kgf/cm<sup>2</sup>  
cmH<sub>2</sub>O, mmH<sub>2</sub>O, inH<sub>2</sub>O, ftH<sub>2</sub>O, mmHg, inHg, kg/cm<sup>2</sup>

### Over Pressure

The operating FS pressure range can be exceeded by the following multiples with negligible effect on calibration:

- 8 x for ranges up to 2.5 psi (160 mbar)
- 6 x for ranges above 2.5 to 7.5 psi (160 up to 500 mbar)
- 4 x for ranges above 7.5 to 30 psi (500 mbar up to 2 bar)
- 3 x for ranges above 30 up to 2030 psi (2 up to 140 bar) (2900 psi (200 bar) max)
- 2 x for ranges above 2030 up to 10000 psi (140 up to 700 bar) (14500 psi (1000 bar) max)

### Pressure Containment

The operating FS pressure range may be exceeded by the following multiples without a loss of mechanical containment:-

### Gauge ranges:

- 12 x for ranges up to 2.5 psi (160 mbar)
- 8 x for ranges above 2.5 to 7.5 psi (160 up to 500 mbar)
- 6 x for ranges above 7.5 to 30 psi (500 mbar up to 2 bar)
- 4 x for ranges above 30 to 1015 psi (2 up to 70 bar) (2900 psi (200 bar) max)

### Sealed gauge and absolute ranges:

- 3625 psi (250 bar) for ranges 1.5 to 2030 psi (100 mbar to 140 bar)
- 14500 psi (1000 bar) for ranges above 2030 up to 10155 psi (140 up to 700 bar)

Pressure Equipment Directive (PED) 97/23/EC approved (Category 1 - Pressure Accessory)

### Pressure Media

Fluids compatible with 316L stainless steel and Hastelloy C276 (NACE compatible grades)

### Supply Voltage

9 to 30 V at PTX terminals (28 V maximum for Intrinsically Safe option)

### Start -Up Time

Recommended minimum power on time before output sample is taken is 500 msec

### Output Signal

4 to 20 mA (2 wire) proportional to the zero to FS pressure range

## Performance

### Accuracy

Combined effects of non-linearity, hysteresis and repeatability  
±0.1% FS Best Straight Line (BSL) typical (±0.2% FS BSL max)  
0.15% Terminal Straight Line (TSL) typical (0.3% TSL max)

### Zero Offset and Span Setting

Supplied with ±5% zero and span noninteractive site adjustable potentiometers (excludes 7533 model)

### Long Term Stability

±0.1% FS per year

### Operating Temperature Range

-40 to 212°F (-40 to 100°C) ambient (176°F (80°C) max for 7511/7533/7534 models)  
-40 to 248°F (-40 to 120°C) process media

### Temperature Effects

Output will not deviate from room temperature (RTET) by more than:  

- 0.7% FS typical (1% FS max) over 14 to 122°F (-10 to 50°C)
- 1.5% FS typical (2% FS max) over -40 to 176°F (-20 to 80°C)

 For ranges below 500 bar, these values will multiply on a pro rata basis.

### Shock

- 100g, half sine pulse, duration 1 msec
  - 100g, peak half sine wave duration 11 msec
  - 2000g, half sine pulse, duration 0.5 msec
- All in each of 3 mutually respendicular axis will not effect calibration.

### Vibration

Conforms to MIL-STD 810C method 514.2 figure 514.2-2 curve L

### Pressure Response

1kHz band width (63% response to step change in pressure).

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### Certification

Certificate of Calibration supplied as standard.

### CE marking

Marked for use in potentially explosive atmosphere, electromagnetic compatibility and the pressure equipment directive.

### Hazardous Area Approval

EEX ia IIC T4 (-40 < T amb < 80°C)  
Certificate BAS01 ATEX1254  
300 metres max integral cable (models PTX 7511/7533)

## Physical

### Pressure Connection

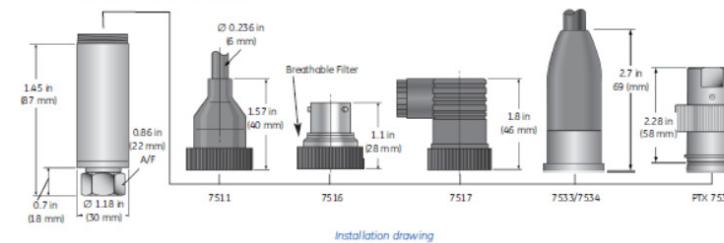
G1/4 female with Option B screw-in adaptors

### Electrical Connection

- IP65 Integral 5.7mm polyurethane cable
- IP65 6-pin bayonet plug
- IP65 DIN 43650A plug/socket
- IP68 Integral 8mm polyurethane or hytrel cable
- IP65 M20 female conduit (PTX 7500)

## Options

- (A) ATEX Intrinsically Safe Approval
- (B) Screw in adaptors with bonded seals
- (C) Separate vented cable (7517)  
5.7mm vented cable provided as a separate line item (supplied unfitted)
- (D) Pressure snubber adaptor  
Refer to GE for further information



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## Ordering Information

Please state the following:

(1) Select model number

Code Output

PTX75

mA output

Code Electrical Connections

- |    |                                   |
|----|-----------------------------------|
| 11 | 5.7 MM INTEGRAL CABLE Core (IP65) |
| 16 | 6-pin bayonet plug (IP65)         |
| 17 | DIN 43650 plug/socket (IP 65)     |
| 33 | 8 mm integral cable (IP 68)       |
| 34 | 8 mm integral Hytrel cable (IP68) |
| 35 | M20 female conduit (IP65)         |

PTX 75 11 Typical model number

(2) Pressure range

(3) Pressure units e.g. psi, bar, etc..

(4) Specify gauge or absolute

(5) Cable lengths (7511, 7533, 7534)

(6) Required options

[www.gesensing.com](http://www.gesensing.com)

Figure 11.2-2: CO<sub>2</sub> pressure sensors in the cooling plant



## MINIATURE HIGH PRESSURE IS® PRESSURE TRANSDUCER

## HKL-375 (M) SERIES

- Excellent Stability
- All Welded Construction
- Robust Construction
- High Natural Frequencies
- 3/8-24 UNJF or M10 X 1 Thread
- Patented Leadless Technology (HKL Series)

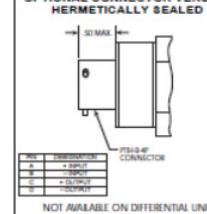
The HKM-375 is a miniature threaded pressure transducer. The hexagonal head and o-ring seal make it easy to mount and simple to apply.

The HKM-375 utilizes a flush metal diaphragm as a force collector. A solid state piezoresistive sensing element is located immediately behind this metal diaphragm which is protected by a metal screen. Force transfer is accomplished via an intervening film of non-compressible silicone oil. This sensing sub assembly is welded to a stainless steel body. The HKL-375 Series utilizes Kulite's Patented Leadless Technology.

This advanced construction results in a highly stable, reliable and rugged instrument with all the advantages of microcircuitry: significant miniaturization, excellent repeatability, low power consumption, etc. The miniaturization process also yields a marked increase in the natural frequencies of the transducers, making them suitable for use even in shock pressure measurements.



## OPTIONAL CONNECTOR VERSION HERMETICALLY SEALED



NOT AVAILABLE ON DIFFERENTIAL UNIT

## INPUT

## Pressure Range

## Operational Mode

## Over Pressure

## Burst Pressure

## Pressure Media

## Rated Electrical Excitation

## Maximum Electrical Excitation

## Input Impedance

## OUTPUT

## Output Impedance

## Full Scale Output (FSO)

## Residual Unbalance

## Combined Non-Linearity, Hysteresis and Repeatability

## Resolution

## Natural Frequency (kHz) (Typ.)

## Acceleration Sensitivity % F/Sig

## Perpendicular

## Transverse

## Insulation Resistance

## ENVIRONMENTAL

## Operating Temperature Range

## Compensated Temperature Range

## Thermal Zero Shift

## Thermal Sensitivity Shift

## Linear Vibration

## Humidity

## Mechanical Shock

## PHYSICAL

## Electrical Connection

## Weight

## Sensing Principle

## Mounting Torque

Note: Custom pressure ranges, accuracies and mechanical configurations available.  
Continuous development and refinement of our products may result in specification changes without notice - all dimensions nominal (0)

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Figure 11.2-3: CO<sub>2</sub> pressure sensors in cooling bridge

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[info@stekon.nl](mailto:info@stekon.nl)

Datum/Date : 13 april 2007  
Aan/To : Nikhef  
T.a.v./Attn. : Dhr. B. Verlaat  
Betr./Re. : offerte Kulite drucksensoren / AW980 versterkers  
Onze/Our ref. : S-K-02587-EL  
Email : [bverlaat@nikhef.nl](mailto:bverlaat@nikhef.nl)

Aantal pagina's/Number of pages: 1 (incl. voorpagina/frontpage)

Geachte heer Verlaat,

Naar aanleiding van ons telefonisch onderhoud van hedenmiddag bieden wij u hierbij als volgt aan:

**6 x Kulite drucksensor, model HKM-375M-100BAR-A.**

Drukbereik: 100 BAR (Absoluut): \$ 777,00  
De sensor wordt voorzien van een connector en 'mating'-connector: \$ 138,00  
Gecompenseerde temperatuur range: -30°C tot +20°C: \$ 57,00  
Overige technische gegevens volgens bijlage.  
Prijs per stuk: \$ 972,00

Totaalprijs 6 stuks: \$ 5.832,00

**3 x Meetversterker, 2-kanaals, model AW980-2K.**

Output 4-20mA / 0-10V  
De Kulite sensoren worden afgeregeld op deze meetversterkers.  
Technische gegevens reeds in uw bezit.  
Prijs per stuk: € 525,00

Totaalprijs 3 stuks: € 1.575,00

Wij wijzen u erop dat de prijzen voor de Kulite sensoren zijn vermeld in US-dollars.  
Uiteraard is betaling in Euro's mogelijk tegen de ten tijde van facturatie geldende koers.

**Introduction**

AKS 32 and AKS 33 are pressure transmitters that measure a pressure and convert the measured value to a standard signal:

- 1 → 5 V d.c. or 0 → 10 V d.c. for AKS 32
- 4 → 20 mA for AKS 33

A robust design makes the AKS very suitable for application within a number of fields e.g.

- Air conditioning systems
- Refrigeration plant
- Process control
- Laboratories

**Features**

Highly developed sensor technology means high pressure regulation accuracy, a very important factor in the precise and energy-economic capacity regulation of refrigeration plant.

- Temperature compensation for LP and HP pressure transmitters, developed specially for refrigeration plant:  
LP: -30 → +40°C (≤16 bar)  
HP: 0 → +80°C (>16 bar)
- Compatibility with all refrigerants incl. ammonia means less stock and greater application flexibility.
- Built-in voltage stabiliser, i.e. the AKS pressure transmitters can be powered from an unregulated voltage supply of any output within given limits.
- Effective protection against moisture means that the sensor can be mounted in very harsh environments, e.g. in the suction line encapsulated in an ice block.

- Robust construction gives protection against mechanical influences such as shock, vibration and pressure surge. AKS sensors can be mounted direct on to the plant.
- No adjustment necessary. With the highly developed sensor technology and sealed gauge principle, the accuracy of the factory setting is maintained independent of variations in ambient temperature and atmospheric pressure. This is very important when ensuring evaporating pressure control in air conditioning and refrigeration applications.
- EMC protection according to EU EMC-directive (CE-marked)
- UL approved
- Polarity protected inputs.

AKS 33, version 4 → 20 mA

Operating range bar	Max. working pressure PB bar	Compensated temperature range °C	Code no.					
			DIN 43650 plug			Cable		
			1/8 NPT 1)	G 1/8 A 2)	1/4 flare 3)	1/8 NPT 1)	G 1/8 A 2)	1/4 flare 3)
LP	-1 → 5	33	-30 → +40	060G2112	060G2108	060G2047		
	-1 → 6	33	-30 → +40	060G2100	060G2104	060G2048	060G2116	060G2120
	-1 → 9	33	-30 → +40	060G2113	060G2111	060G2044		060G2062
	-1 → 12	33	-30 → +40	060G2101	060G2105	060G2049	060G2117	
	-1 → 20	40	0 → +80	060G2102	060G2106	060G2050	060G2118	
HP	-1 → 34	55	0 → +80	060G2103	060G2107	060G2051	060G2119	060G2065
	0 → 16	40	0 → +80	060G2114	060G2109			
	0 → 25	40	0 → +80	060G2115	060G2110		060G2127	060G2067

1) 1/8-18 NPT

2) Thread ISO 228/1 - G 1/8 A (BSP)

3) 1/8-20 UNF

Figure 11.2-4: HFC pressure sensors

**Technical data****Performance**

Accuracy (3 σ)	±0.3% FS (typ.)/±0.8% FS (max.)
Non-linearity (Best fit straight line)	< ±0.2% FS
Hysteresis and repeatability	≤ ±0.1% FS
Thermal zero point shift	≤ ±0.1% FS/10K (typ.) ≤ ±0.2% FS/10K (max.)
Thermal sensitivity (span) shift	≤ ±0.1% FS/10K (typ.) ≤ ±0.2% FS/10K (max.)
Response time	< 4 ms
Max. operating pressure	See ordering, overleaf
Burst pressure	min. 300 bar

*Electrical specifications for AKS 33, 4 - 20 mA output signal*

Rated output signal	4 to 20 mA
Supply voltage, $V_{\text{supply}}$ (polarity protected)	10 to 30 V d.c.
Voltage dependency	< 0.05% FS/10V
Current limitation (linear output signal up to 1.5 × rated range)	28 mA
Max. load, $R_L$	$R_L \leq \frac{V_{\text{supply}} - 10 \text{ V}}{0.02 \text{ A}} [\Omega]$

*Electrical specifications for AKS 32, 0 - 10 V d.c. output signal*

Rated output signal (short-circuit protected)	0 to 10 V d.c.
Supply voltage, $V_{\text{supply}}$ (polarity protected)	15 to 30 V d.c.
Supply current consumption	< 8 mA
Supply voltage dependency	< 0.05% FS/10V
Output impedance	< 25 Ω
Load resistance, $R_L$	$R_L \geq 10 \text{ kΩ}$

*Electrical specifications for AKS 32, 1-5 V d.c. output signal*

Rated output signal (short-circuit protected)	1 to 5 V d.c.
Supply voltage, $V_{\text{supply}}$ (polarity protected)	9 to 30 V d.c.
Supply current consumption	< 5 mA
Supply voltage dependency	< 0.05% FS/10V
Output impedance	< 25 Ω
Load resistance, $R_L$	$R_L \geq 10 \text{ kΩ}$

**Environmental conditions**

Operating temperature range	-40 to 85°C	
Compensated temperature range	LP: -30 to +40°C / HP: 0 to +80°C	
Transport temperature range	-50 to 85°C	
EMC - Emission		
Electrostatic discharge	Air	8 kV
	Contact	4 kV
RF conducted	10 V/m, 26 MHz - 1 GHz	EN 50082-2 (IEC 801-2)
	3 V/m, 150 kHz - 30 MHz	EN 50082-2 (IEC 801-3)
Transient	burst	4 kV (CM)
	surge	1 kV (CM,DM)
Insulation resistance		
Mains frequency test	500 V, 50 Hz	> 100 MΩ at 500 V d.c.
Vibration stability	Sinusoidal	20 g, 25 Hz - 2 kHz
	Random	7.5 g <sub>ms</sub> , 5 Hz - 1 kHz
Shock resistance	Shock	500 g / 1 ms
	Free fall	IEC 68-2-27
Enclosure		
Plug version	IP 65 - IEC 529	
Cable version	IP 67 - IEC 529	



## 11.3 Actuators

### 11.3.1 Valves

Table 11.3-1: VTCS Valves

Code	Part number	Function	Connection	Operating Pressure (Bar)	Maximum Pressure (Bar)	Minimum temperature (°C)	Maximum design temperature (°C)	Pressure setting range (Bar)	Cv (-)	Orifice (mm)	Supply (V)	Power (W)	Electrical Control	Manual Control	Output signal
TL_VL102	Swagelok SS-43GHLVCR4-42dc	Left VTCS shut-off	1/4"VCR male	100	172	-53	37	NA	2.4	4.8	24Vdc	22	motor/end switch		Position switch
TL_VL103	Swagelok SS-43GXVCR4-42dcx	3-way Condenser selection	1/4"VCR male	100	172	-53	37	NA	0.9	4.8	24Vdc	22	motor/end switch		Position switch
TL_VL104	Swagelok SS-43GHLVCR4-42dc	Accumulator shut-off	1/4"VCR male	100	172	-53	37	NA	2.4	4.8	24Vdc	22	motor/end switch		Position switch
TL_VL109	Swagelok SS-43GHLVCR4-42dc	By-pass	1/4"VCR male	100	172	-53	37	NA	2.4	4.8	24Vdc	22	motor/end switch		Position switch
TL_VL111	Swagelok SS-43GHLVCR4-42dc	Left VTCS shut-off	1/4"VCR male	100	172	-53	37	NA	2.4	4.8	24Vdc	22	motor/end switch		Position switch
TL_VL112	Swagelok SS-43GHLVCR4-42dc	Liquid vent	1/4"VCR male	100	172	-53	37	NA	2.4	4.8	24Vdc	22	motor/end switch		Position switch
TR_VL102	Swagelok SS-43GHLVCR4-42dc	Left VTCS shut-off	1/4"VCR male	100	172	-53	37	NA	2.4	4.8	24Vdc	22	motor/end switch		Position switch
TR_VL103	Swagelok SS-43GXVCR4-42dcx	3-way Condenser selection	1/4"VCR male	100	172	-53	37	NA	0.9	4.8	24Vdc	22	motor/end switch		Position switch
TR_VL104	Swagelok SS-43GHLVCR4-42dc	Accumulator shut-off	1/4"VCR male	100	172	-53	37	NA	2.4	4.8	24Vdc	22	motor/end switch		Position switch
TR_VL108	Swagelok SS-43GXVCR4-42dcx	Pump shut-off/TLR pump cooling	1/4"VCR male	100	172	-53	37	NA	0.9	4.8	24Vdc	22	motor/end switch		Position switch
TR_VL109	Swagelok SS-43GHLVCR4-42dc	By-pass	1/4"VCR male	100	172	-53	37	NA	2.4	4.8	24Vdc	22	motor/end switch		Position switch
TR_VL111	Swagelok SS-43GHLVCR4-42dc	Left VTCS shut-off	1/4"VCR male	100	172	-53	37	NA	2.4	4.8	24Vdc	22	motor/end switch		Position switch
TR_VL112	Swagelok SS-43GHLVCR4-42dc	Liquid vent	1/4"VCR male	100	172	-53	37	NA	2.4	4.8	24Vdc	22	motor/end switch		Position switch

TLR_VL101	Swagelok SS-43GXVCR4-42dcx	Spare pump	1/4"VCR male	100	172	-53	37	NA	0.9	4.8	24Vdc	22	motor/end switch		Position switch
TLR_VL109	Swagelok SS-43GXVCR4-42dcx	3-way Condenser selection	1/4"VCR male	100	172	-53	37	NA	2.4	4.8	24Vdc	22	motor/end switch		Position switch
TLR_VL110	Swagelok SS-43GHLVCR4-42dc	Left-right liquid inter connect	1/4"VCR male	100	172	-53	37	NA	2.4	4.8	24Vdc	22	motor/end switch		Position switch
TLR_VL111	Swagelok SS-43GHLVCR4-42dc	Left-right vapor inter connect	1/4"VCR male	100	172	-53	37	NA	2.4	4.8	24Vdc	22	motor/end switch		Position switch
SA_VL106	Danfoss AKV 10-2/068F1164+018F6701	Evaporator expansion valve and shut-off valve	3/8"x1/2" solder	20	42	-60	60	NA		0.6 5					
SA_VL110	Danfoss AKV 10-2/068F1164+018F6701	Expansion valve	3/8"x1/2" solder	20	42	-60	60	NA		0.6 5					
SA_VL114	Danfoss AKV 10-1/068F1161+018F6701	Evaporator expansion valve and shut-off valve	3/8"x1/2" solder	20	42	-60	60	NA		0.5					
SA_VL119	Danfoss AKV 10-1/068F1161+018F6701	Expansion valve	3/8"x1/2" solder	20	42	-60	60	NA		0.5					
SB_VL106	Danfoss AKV 10-2/068F1164+018F6701	Evaporator expansion valve and shut-off valve	3/8"x1/2" solder	20	42	-60	60	NA		0.6 5					
SB_VL110	Danfoss AKV 10-2/068F1164+018F6701	Expansion valve	3/8"x1/2" solder	20	42	-60	60	NA		0.6 5					
SB_VL114	Danfoss AKV 10-1/068F1161+018F6701	Evaporator expansion valve and shut-off valve	3/8"x1/2" solder	20	42	-60	60	NA		0.5					
SB_VL119	Danfoss AKV 10-1/068F1161+018F6701	Expansion valve	3/8"x1/2" solder	20	42	-60	60	NA		0.5					
TL_VL001	Swagelok SS-4UW-TW	Transfer tube shut-off	1/4" socket weld	100	172	-29	343	NA	0.36	4.4	NA	NA	NA	Proportiona l	NA
TL_VL002	Swagelok SS31RS4 (Modified)	Liquid expansion	1/4" Swagelok	100	212	-65	343	NA	0.012 Nom / 0.04 max	1.6	NA	NA	NA	Proportiona l	NA
TL_VL003	Swagelok SS-4UW-TW	Test evaporator inlet	1/4" socket weld	100	172	-29	343	NA	0.36	4.4	NA	NA	NA	Proportiona l	NA
TL_VL004	Swagelok SS-4UW-TW	Evaporator inlet	1/4"	100	172	-29	343	NA	0.36	4.4	NA	NA	NA	Proportiona l	NA

			socket weld										1	
TL_VL006	Swagelok SS-6UW-TW	Test evaporator outlet	3/8" socket weld	100	172	-29	343	NA	1	7.1	NA	NA	Proportiona l	NA
TL_VL007	Swagelok SS-58SW8T	Check valve with modified poppet	1/2" socket weld	100	307	-53	176	NA	2.2	11. 1	NA	NA	NA	NA
TL_VL008	Swagelok SS-6UW-TW	Transfer tube shut-off	3/8" socket weld	100	172	-29	343	NA	1	4.4	NA	NA	Proportiona l	NA
TL_VL009	TBV	Tert. vacuum evacuation	CF16	2	NA	NA	NA	NA	NA	NA	NA	NA	Proportiona l	NA
TL_VL101	Swagelok SS-43GHLVCR4	Transfer tube shut-off	1/4"VCR male	100	172	-53	37	NA	2.4	4.8	NA	NA	Open/Close	NA
TL_VL105	Swagelok SS-43GHLVCR4	Filling port	1/4"VCR male	100	172	-53	37	NA	2.4	4.8	NA	NA	Open/Close	NA
TL_VL106	Swagelok SS-43GHLVCR4	Pump shut-off	1/4"VCR male	100	172	-53	37	NA	2.4	4.8	NA	NA	Open/Close	NA
TL_VL107	Swagelok SS-43GHLVCR4	Filling port	1/4"VCR male	100	172	-53	37	NA	2.4	4.8	NA	NA	Open/Close	NA
TL_VL108	Swagelok SS-43GHLVCR4	Pump shut-off	1/4"VCR male	100	172	-53	37	NA	2.4	4.8	NA	NA	Open/Close	NA
TL_VL110	Swagelok SS31RS4	Liquid expansion	1/4" Swagelok	100	212	-65	343	NA	0.012 Nom / 0.04 max	1.6	NA	NA	Proportiona l	NA
TL_VL113	Swagelok SS-43GHLVCR4	Transfer tube shut-off	1/4"VCR male	100	172	-53	37	NA	2.4	4.8	NA	NA	Open/Close	NA
TR_VL001	Swagelok SS-4UW-TW	Transfer tube shut-off	1/4" socket weld	100	172	-29	343	NA	0.36	4.4	NA	NA	Proportiona l	NA
TR_VL002	Swagelok SS31RS4 (Modified)	Liquid expansion	1/4" Swagelok	100	212	-65	343	NA	0.012 Nom / 0.04 max	1.6	NA	NA	Proportiona l	NA
TR_VL003	Swagelok SS-4UW-TW	Test evaporator inlet	1/4" socket weld	100	172	-29	343	NA	0.36	4.4	NA	NA	Proportiona l	NA
TR_VL004	Swagelok SS-4UW-TW	Evaporator inlet	1/4" socket weld	100	172	-29	343	NA	0.36	4.4	NA	NA	Proportiona l	NA
TR_VL006	Swagelok SS-6UW-TW	Test evaporator outlet	3/8" socket weld	100	172	-29	343	NA	1	7.1	NA	NA	Proportiona l	NA
TR_VL007	Swagelok SS-58SW8T	Check valve with modified poppet	1/2" socket weld	100	307	-53	176	NA	2.2	11. 1	NA	NA	NA	NA

TR_VL008	Swagelok SS-6UW-TW	Transfer tube shut-off	1/4" socket weld	100	172	-29	343	NA	1	4.4	NA	NA	NA	Proportiona l	NA
TR_VL009	TBV	Tert. vacuum evacuation	CF16	2	NA	NA	NA	NA	N A	NA	NA	NA	NA	Proportiona l	NA
TR_VL101	Swagelok SS-43GHLVCR4	Transfer tube shut-off	1/4"VCR male	100	172	-53	37	NA	2.4	4.8	NA	NA	NA	Open/Close	NA
TR_VL105	Swagelok SS-43GHLVCR4	Filling port	1/4"VCR male	100	172	-53	37	NA	2.4	4.8	NA	NA	NA	Open/Close	NA
TR_VL106	Swagelok SS-43GHLVCR4	Pump shut-off	1/4"VCR male	100	172	-53	37	NA	2.4	4.8	NA	NA	NA	Open/Close	NA
TR_VL107	Swagelok SS-43GHLVCR4	Filling port	1/4"VCR male	100	172	-53	37	NA	2.4	4.8	NA	NA	NA	Open/Close	NA
TR_VL110	Swagelok SS31RS4	Liquid expansion	1/4" Swagelok	100	212	-65	343	NA	0.012 Nom / 0.04 max	1.6	NA	NA	NA	Proportiona l	NA
TR_VL113	Swagelok SS-43GHLVCR4	Transfer tube shut-off	1/4"VCR male	100	172	-53	37	NA	2.4	4.8	NA	NA	NA	Open/Close	NA
TLR_VL001	Swagelok SS-4UW-TW	Left right inter connect	1/4" socket weld	100	172	-29	343	NA	0.36	4.4	NA	NA	NA	Proportiona l	NA
TLR_VL002	Swagelok SS-6UW-TW	Left right inter connect	3/8" socket weld	100	172	-29	343	NA	1	7.1	NA	NA	NA	Proportiona l	NA
TLR_VL107	Swagelok SS-43GHLVCR4	Filling port	1/4"VCR male	100	172	-53	37	NA	2.4	4.8					
SA_VL101	Danfoss GBC10S/009G7051	Compressor section shut-off	3/8" solder	20	48	-40	150	NA							
SA_VL102	Danfoss NRD/020-1132	Condenser control	1/2" solder	20	28	-45	130	1.4 - 3							
SA_VL103	Danfoss/KVR-12/034L0093	Condenser pressure control	1/2" solder	20	28	-45	130	5 - 17.5							
SA_VL104	Integral in SA-AC102	Liquid line shut-off													
SA_VL107	Integral in SA-VL108	Schrader valve		20	TBV	TBV	TBV	NA							
SA_VL108	Danfoss GBC12S/009G7052	Evaporator shut-off	1/2" solder	20	48	-40	150	NA							
SA_VL111	Integral in SA-VL112	Schrader valve		20	TBV	TBV	TBV	NA							
SA_VL112	Danfoss GBC12S/009G7052	Evaporator shut-off	1/2" solder	20	48	-40	150	NA							
SA_VL115	Integral in SA-VL116	Schrader valve		20				NA							
SA_VL116	Danfoss GBC12S/009G7052	Accu evaporator shut-off	1/2" solder	20	48	-40	150	NA							
SA_VL117	Danfoss KVP-12	Accu	1/2"	18	28	-45	130	0 - 7		N					



SB_VL125	Integral in SB-PM101	Compressor discharge shut-off											
SB_VL127	Integral in SB-VL104	Schrader valve											
SB_VL128	Integral in SB-VL123	Schrader valve											

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## Medium-Flow Metering Valves, Cv up to 0.04



Part Number: SS-31RS4

Description: SS Medium-Flow High-Pressure (5000 psig (344 bar)) Metering Valve, 1/4 in. Swagelok Tube Fitting

## Product Specifications

## General

Body Material	316 Stainless Steel
Connection 1 Size	1/4 in.
Connection 1 Type	Swagelok® Tube Fitting
Connection 2 Size	1/4 in.
Connection 2 Type	Swagelok® Tube Fitting
eClass (4.1)	37010203
eClass (6.0)	37-01-02-03
UNSPSC (11.0501)	40141609
UNSPSC (4.03)	40141600
UNSPSC (SWG01)	40141600

## REVIEW PRODUCT CATALOG FOR COMPLETE SPECIFICATIONS INCLUDING WARNINGS AND CAUTIONS.

Safe Product Selection: When selecting a product, the total system design must be considered to ensure safe, trouble-free performance. Function, material compatibility, adequate ratings, proper installation, operation, and maintenance are the responsibilities of the system designer and user.

Caution: Do not mix or interchange valve components with those of other manufacturers.

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Figure 11.3-2: CO<sub>2</sub> expansion valve

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## Secondary Packed Bellows Valves, Manual and Actuated, up to 1200°F [648°C]



Part Number: SS-4UW-TW

Description: SS Secondary Packed Bellows-Sealed Valve, Welded, Spherical Stem Tip, 1/4 in. TSW and 3/8 in. TBW

## Product Specifications

## General

Actuator Type	Manual
Body Material	Stainless Steel
Body Type	Straight
Flow Pattern	Straight (2-way)
Series	U Series
Service Class	General
End Connection 1 Size	1/4 in
End Connection 1 Type	Tube socket weld
End Connection 2 Size	1/4 in
End Connection 2 Type	Tube socket weld
Handle Color	Green
Handle Style	Aluminum bar
Bellows Material	347 Stainless Steel
Body Seal	Welded
Cleaning	Swagelok SC-10
Gasket	None
ID Tag	No
Packing	Grafoil®
Stem Type	Spherical
Surface Finish	Standard
Testing	Helium leak testing according to SCS-00020
Stem Tip Material	Cobalt based alloy
Max Temperature Pressure Rating	900°F @ 600 PSIG /482°C @ 41.3 BAR
Room Temperature Pressure Rating	2500 PSIG @ 100°F /172 @ BAR 37°C

## REVIEW PRODUCT CATALOG FOR COMPLETE SPECIFICATIONS INCLUDING WARNINGS AND CAUTIONS.

Safe Product Selection: When selecting a product, the total system design must be considered to ensure safe, trouble-free performance. Function, material compatibility, adequate ratings, proper installation, operation, and maintenance are the responsibilities of the system designer and user.

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Figure 11.3-1: CO<sub>2</sub> shut-off valve in cooling bridge



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## 1-Piece, Instrumentation, 40G Series Ball Valves



**Part Number:** SS-43GVCR4  
**Description:** SS 1-Piece 40 Series Ball Valve, 2.4 Cv, 1/4 in. Male Swagelok VCR Metal Gasket Face Seal Fitting

## Product Specifications

## General

Actuator Type	Manual
Flow Path	Standard (2-way)
Flow Pattern	Straight (2-way)
Valve Material	Stainless Steel
End Connection 1 Size	1/4 in
End Connection 1 Type	Face seal (metal gasket) VCR
End Connection 2 Size	1/4 in
End Connection 2 Type	Face seal (metal gasket) VCR
Handle Color	Black
Handle Style	Lever
Approval	No Approval
Ball/Stem Material	Stainless Steel
Body Vent	No
Cleaning	Swagelok SC-10
Lubricant	Dow M111
Packing	Modified PTFE
Ring/Disc Material	Stainless Steel
Sour Gas	No
Testing	Testing according to WS-22
Max Temperature Pressure Rating	300°F @ 2500 PSIG /148°C @ 172 BAR
Orifice	0.187
Room Temperature Pressure Rating	3000 PSIG @ 100°F /206 @ BAR 37°C

## REVIEW PRODUCT CATALOG FOR COMPLETE SPECIFICATIONS INCLUDING WARNINGS AND CAUTIONS.

**Safe Product Selection:** When selecting a product, the total system design must be considered to ensure safe, trouble-free performance. Function, material compatibility, adequate ratings, proper installation, operation, and maintenance are the responsibilities of the system designer and user.

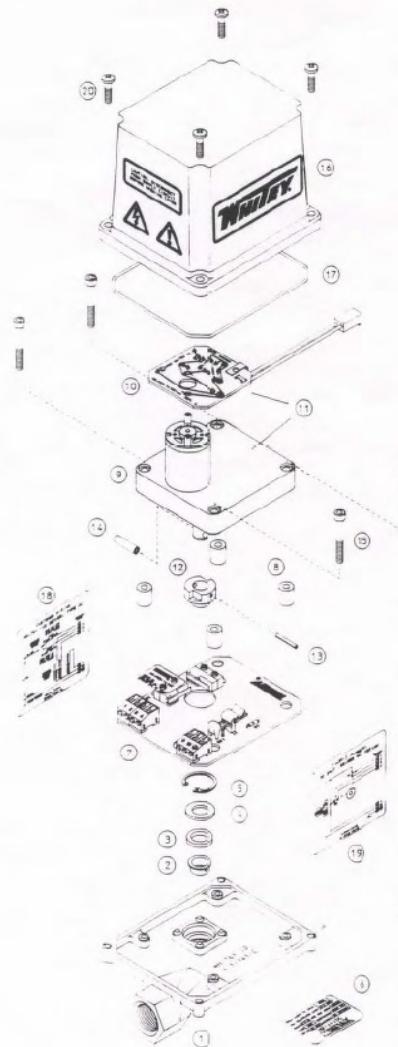
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Figure 11.3-3: CO<sub>2</sub> 2-way ball valve

## 1 CONSTRUCTION INFORMATION

## Exploded View of the 141 Series Type DC Actuator

Figure 11.3-4: CO<sub>2</sub> 2-way ball valve electric drive (1)

SERIES

## CONSTRUCTION INFORMATION 2

### Parts List and Materials of Construction

ITEM	QTY	DESCRIPTION	MATERIAL
1	1	Base	Die Cast Aluminum
2	1	Bushing	Nylon
3	1	Shaft Seal	Buna-N
4	1	Washer	Stainless Steel
5	1	Retaining Ring	Steel
6	1	Specification Label	Polyester
7	1	Assembled PC Board	
8	4	Motor Standoffs	Nickel Plated Brass
9	1	DC Gearmotor	Stainless Steel Shaft
10	1	Assembled PC Board	Stainless Steel Shaft
11	1	Gearmotor Assembly	Nylon
12	1	Dual Cam	Stainless Steel
13	1	Spring Pin	Stainless Steel
14	1	Roll Pin	Cadmium Plated Steel
15	4	Mounting Screws	Die Cast Aluminum
16	1	Cover	Buna-N
17	1	Cover Seal	Polyester
18	1	Wiring Label	Polyester
19	1	Schematic Label	
20	4	Cover Screws	Stainless Steel
	1	User's Manual	

### User Wiring and Internal Circuit

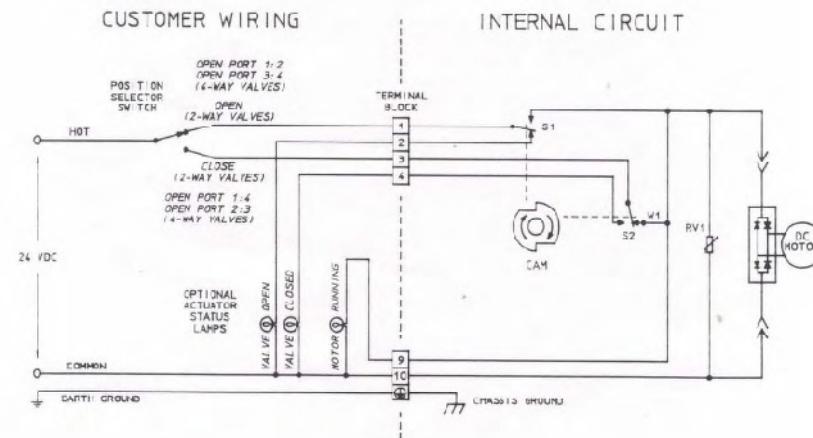
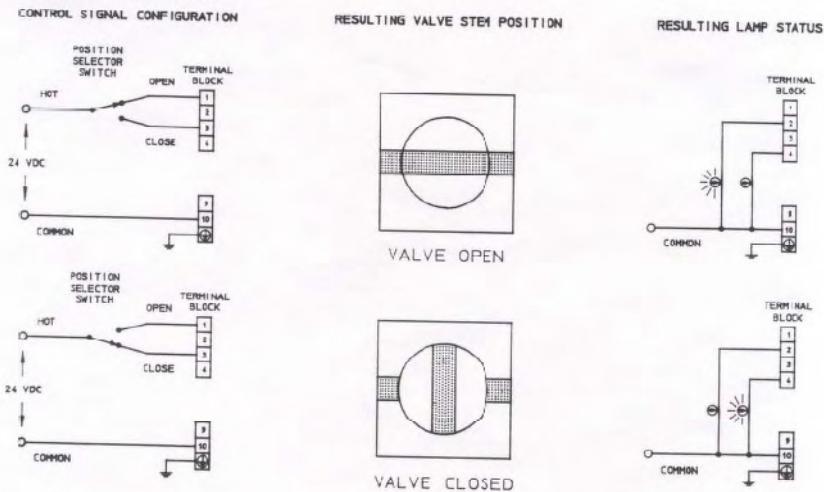


Figure 11.3-5: CO<sub>2</sub> 2-way ball valve electric drive (2)

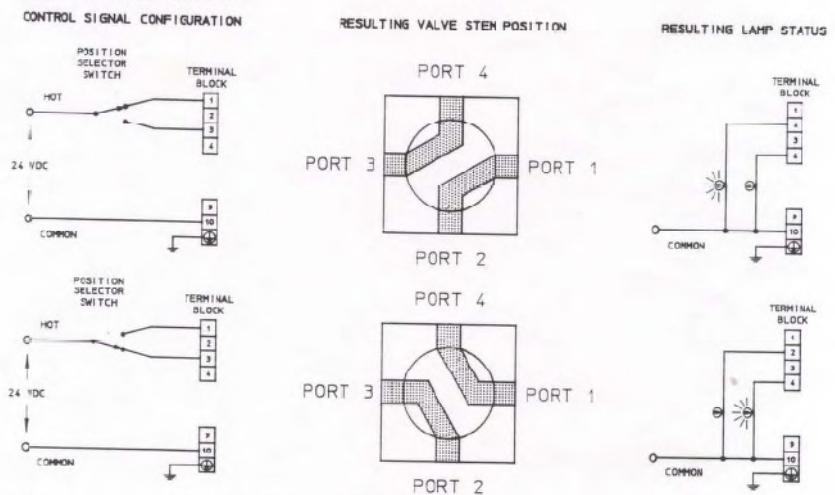
## 3 OPERATING CHARACTERISTICS

### Valve Stem Position vs. Applied Control Signal

#### 2-Way Ball Valves



#### 4-Way Ball Valves





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## 1-Piece, Instrumentation, 40G Series Ball Valves



Part Number: SS-43GXVCR4

Description: SS 1-Piece 40G Series 3-Way Ball Valve, 0.90 Cv, 1/4 in. Male Swagelok VCR Metal Gasket Face Seal Fitting

## Product Specifications

## General

Actuator Type	Manual
Flow Path	Standard (3-way)
Flow Pattern	Switching (3-way)
Valve Material	Stainless Steel
End Connection 1 Size	1/4 in
End Connection 1 Type	Face seal (metal gasket) VCR
End Connection 2 Size	1/4 in
End Connection 2 Type	Face seal (metal gasket) VCR
End Connection 3 Size	1/4 in
End Connection 3 Type	Face seal (metal gasket) VCR
Handle Color	Black
Handle Style	Lever
Approval	No Approval
Ball/Stem Material	Stainless Steel
Body Vent	No
Cleaning	Swagelok SC-10
Lubricant	Dow M111
Packing	Modified PTFE
Ring/Disc Material	Stainless Steel
Sour Gas	No
Testing	Testing according to WS-22
Max Temperature Pressure Rating	300°F @ 2500 PSIG /148°C @ 172 BAR
Orifice	0.187
Room Temperature Pressure Rating	2500 PSIG @ 100°F/172 @ BAR 37°C

REVIEW PRODUCT CATALOG FOR COMPLETE SPECIFICATIONS INCLUDING WARNINGS AND CAUTIONS.

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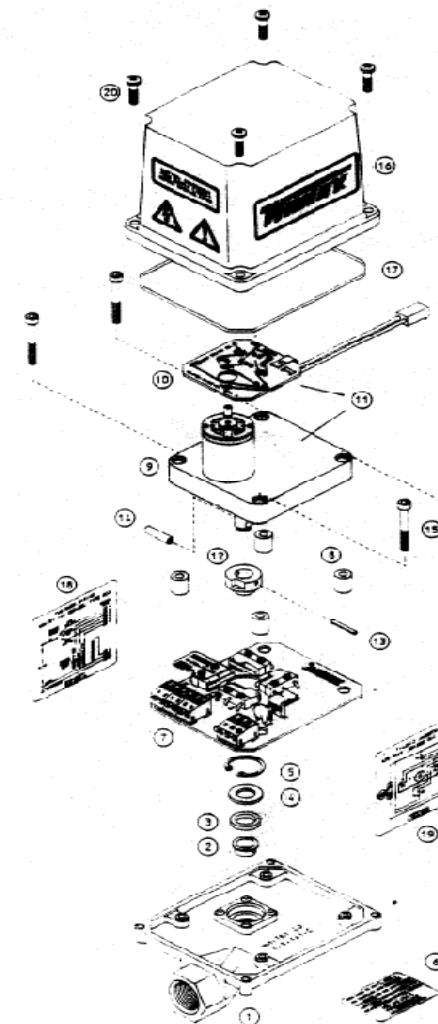
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Figure 11.3-6: CO<sub>2</sub> 3-way ball valve

## 1 CONSTRUCTION INFORMATION

## Exploded View of the 141 Series Type DCX Actuator



141DCX SERIES

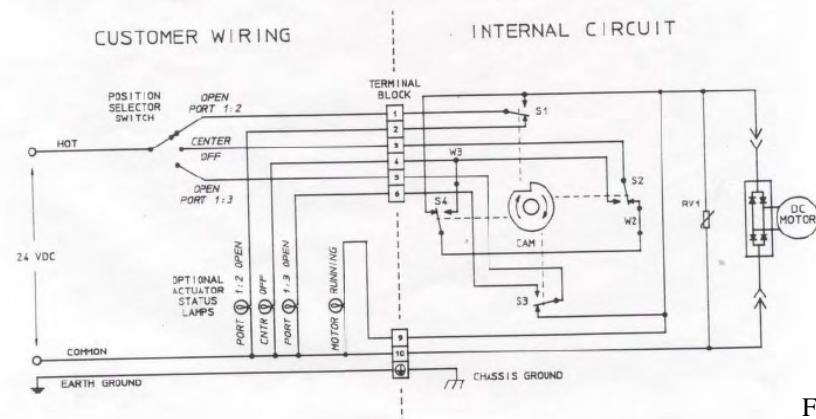
Figure 11.3-7: CO<sub>2</sub> 3-way ball valve electric drive (1)

## CONSTRUCTION INFORMATION 2

### Parts List and Materials of Construction

ITEM	QTY	DESCRIPTION	MATERIAL
1	1	Base	Die Cast Aluminum
2	1	Bushing	Nylon
3	1	Shaft Seal	Buna-N
4	1	Washer	Stainless Steel
5	1	Retaining Ring	Steel
6	1	Specification Label	Polyester
7	1	Assembled PC Board	
8	4	Motor Standoffs	Nickel Plated Brass
9	1	DC Gearmotor	Stainless Steel Shaft
10	1	Assembled PC Board	Stainless Steel Shaft
11	1	Gearmotor Assembly	Nylon
12	1	Single Cam	Stainless Steel
13	1	Spring Pin	Stainless Steel
14	1	Roll Pin	Stainless Steel
15	4	Mounting Screws	Cadmium Plated Steel
16	1	Cover	Die Cast Aluminum
17	1	Cover Seal	Buna-N
18	1	Wiring Label	Polyester
19	1	Schematic Label	Polyester
20	4	Cover Screws	Stainless Steel
	1	User's Manual	

### User Wiring and Internal Circuit



## 3 OPERATING CHARACTERISTICS

### Valve Stem Position vs. Applied Control Signal

#### 3-Way Ball Valves

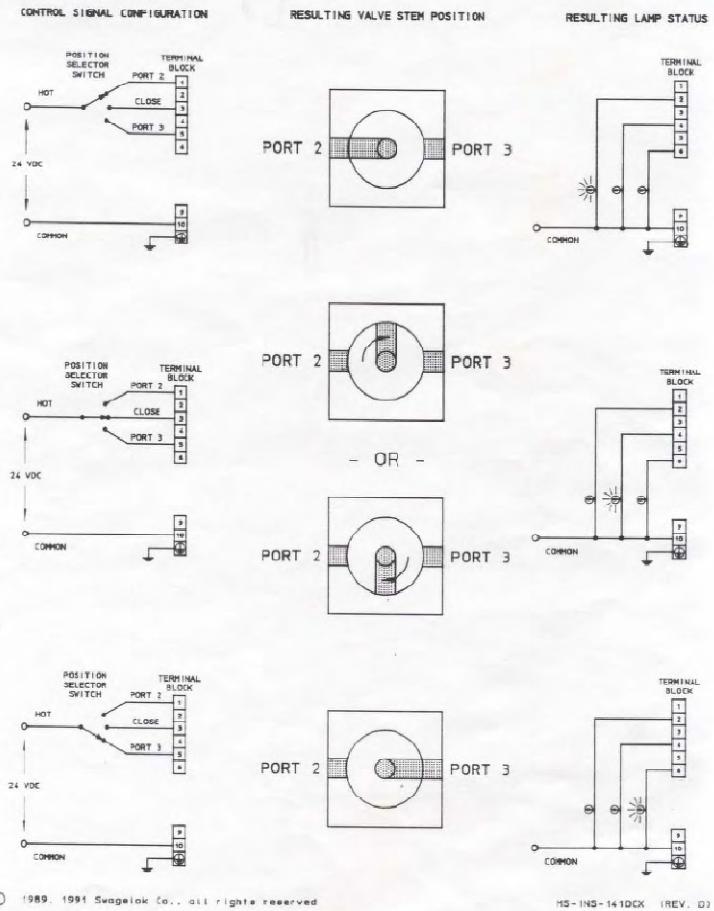


Figure 11.3-8: CO<sub>2</sub> 3-way ball valve electric drive (2)



MEET THE CHALLENGE™

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The Netherlands  
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**Lift Check Valves****Part Number:** SS-58SW8T**Description:** SS Lift Check Valve, 2.20 Cv, 1/2 in. Tube Socket Weld or Pipe Butt Weld**Product Specifications****General**

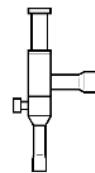
Body Material	316 Stainless Steel
Cleaning Process	Standard Cleaning and Packaging (SC-10)
Connection 1 Size	1/2 in.
Connection 1 Type	Tube Socket Weld
Connection 2 Size	1/2 in.
Connection 2 Type	Tube Socket Weld
eClass (4.1)	37010801
eClass (6.0)	27-29-20-01
UNSPSC (11.0501)	40141609
UNSPSC (4.03)	40141601
UNSPSC (SWG01)	40141601

**REVIEW PRODUCT CATALOG FOR COMPLETE SPECIFICATIONS INCLUDING WARNINGS AND CAUTIONS.**

**Gate Product Selection:** When selecting a product, the total system design must be considered to ensure safe, trouble-free performance. Function, material compatibility, adequate ratings, proper installation, operation, and maintenance are the responsibilities of the system designer and user.

**Caution:** Do not mix or interchange valve components with those of other manufacturers.

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Figure 11.3-9: CO<sub>2</sub> 1-way poppet valve (no-return valve)**034L0023**

Regulating range 0 - 5,5 bar,  
factory setting 2 bar, max.  
working pressure 18 bar. Access  
port: 1/8 in. Schraeder valve for  
pressure testing. Max. test  
pressure KVP 12 - 22 = 28 bar,  
KVP 28 - 35 = 25,6...

Characteristic	Value
Type	KVP 12
Weight	0,370 Kg
Access port	Yes
Approval	C UL US LISTED
Approval	GOST AN30
Approval file name	REFRIGERANT VALVE 53R0
Cv-value [USgal/min]	11,010
Factory setting [bar]	2,00 bar
Factory setting [psig]	29,0 psig
Identical product	034L0218
Inlet connection type	SOLDER, ODF
Inlet size [in]	1/2 IN
Kv-value [m <sup>3</sup> /h]	2,500
Max. test pressure [bar]	28,0 bar
Max. test pressure [psig]	405 psig
Max. Working Pressure ef	18,0 bar
Max. Working Pressure	260 Psig
Medium temperature range [°C]	-45 - 105 °C
Medium temperature range [°F]	-50 - 220 °F
Outlet connection type	SOLDER, ODF
Outlet size [in]	1/2 IN
P band max. [bar]	2,0 bar
P band max. [psi]	29,0 psi
Pack format	Multi pack
Product description	Evaporator Pres. Reg.
Quantity per pack format	12 pc
Rated capacity R134a [kW]	2,80 kW
Rated capacity R134a [TR]	0,90 TR
Rated capacity R22 [kW]	4,00 kW
Rated capacity R22 [TR]	1,30 TR
Rated capacity R404A/R507 [kW]	3,60 kW
Rated capacity R404A/R507 [TR]	1,20 TR
Rated capacity R407C [kW]	3,70 kW
Rated capacity R407C [TR]	1,20 TR
Refrigerant(s)	HCFC
Refrigerant(s)	HFC
Regulating range [bar]	0,0 - 5,5 bar
Regulation range [psig] Pe	0,00 - 80,00 psig

Figure 11.3-10: HFC evaporator pressure regulator

Figure 11.3-11: HFC 1kW expansion valve



Tolerance of coil voltage: +10 / -15%. Enclosure to IEC 529: Max. IP 67. Working principle: PWM (Pulse-width modulation). Recommended period of time: 6 Seconds. Capacity (R22): 1-16 kW. Regulation ra...

Characteristic	Value
Type	AKV 10-1
Weight	0.349 Kg
10W a.c. MOPD [bar]	18 bar
10W a.c. MOPD [psi]	260 psi
Ambient temperature	-50 - 50 °C
Ambient temperature range [°F]	-58 - 120 °F
Armature tube size	13,5 MM
Catalogue number	RD.8A
Coil type	None
Cv-value [USgal/min]	0,012
Direction	Angleway
Function	NC
Inlet size [in]	3/8 IN
Inlet type	SOLDER, ODF
Kv-value [m³/h]	0,010
Manual Operation	No
Max. Working Pressure ef	52,0 bar
Max. Working Pressure	754 psig
Medium temperature range [°C]	-50 - 60 °C
Medium temperature range [°F]	-58 - 140 °F
Min. ODP [bar]	0,000 bar
Min. ODP [psi]	0,000 psi
MOPD [bar/psi]	18 bar
Orifice size	0,50
Orifice / Piston no.	10-1
Outlet size [in]	1/2 IN
Outlet type	SOLDER, ODF
Pack format	Multi pack
Quantity per pack format	18 pc
Rated capacity R22 [kW]	1,00 kW
Refrigerant(s)	CFC
Refrigerant(s)	HCFC
Refrigerant(s)	HFC
Refrigerant(s)	R744
Standard product	Yes
Type designation	Electric Expansion Valve

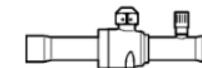
Figure 11.3-12: HFC 1.4kW expansion valve



Tolerance of coil voltage: +10 / -15%. Enclosure to IEC 529: Max. IP 67. Working principle: PWM (Pulse-width modulation). Recommended period of time: 6 Seconds. Capacity (R22): 1-16 kW. Regulation ra...

Characteristic	Value
Type	AKV 10-2
Weight	0.342 Kg
10W a.c. MOPD [bar]	18 bar
10W a.c. MOPD [psi]	260 psi
Ambient temperature	-50 - 50 °C
Ambient temperature range [°F]	-58 - 120 °F
Approval	GOST AN30
Armature tube size	13,5 MM
Catalogue number	RD.8A
Coil type	None
Cv-value [USgal/min]	0,020
Direction	Angleway
Function	NC
Inlet size [in]	3/8 IN
Inlet type	SOLDER, ODF
Kv-value [m³/h]	0,017
Manual Operation	No
Max. Working Pressure ef	52,0 bar
Max. Working Pressure	754 psig
Medium temperature range [°C]	-50 - 60 °C
Medium temperature range [°F]	-58 - 140 °F
Min. ODP [bar]	0,000 bar
Min. ODP [psi]	0,000 psi
MOPD [bar/psi]	18 bar
Orifice size	0,65
Orifice / Piston no.	10-2
Outlet size [in]	1/2 IN
Outlet type	SOLDER, ODF
Pack format	Multi pack
Quantity per pack format	18 pc
Rated capacity R22 [kW]	1,60 kW
Refrigerant(s)	CFC
Refrigerant(s)	HCFC
Refrigerant(s)	HFC
Refrigerant(s)	R744
Standard product	Yes
Type designation	Electric Expansion Valve

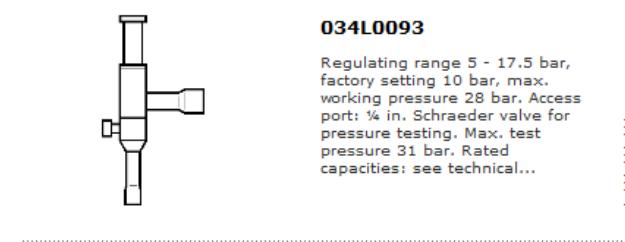
Figure 11.3-13: HFC 2-way ball valve (12mm)

**009G7052**

Refrigerants: CFC, HCFC, HFC. Temperature range: -40 - +150°C. Max. working pressure: 45 bar. Max. test pressure: 65 bar. Approvals: UL, CSA, CE

Characteristic	Value
Type	GBC 12s
Weight	0.320 Kg
Access port	Yes
Approval	CE
Approval	CSA
Approval	UL
Approval file name	REFRIGERANT VALVE 53R0
Cv-value [USgal/min]	46,580
Direction	Straightway
Flow direction	Bi-flow
Inlet connection type	SOLDER, ODF
Inlet size [in]	1/2 IN
Kv-value [m³/h]	10,580
Max. test pressure [bar]	65,0 bar
Max. test pressure [psig]	940 psig
Max. Working Pressure ef	45,0 bar
Max. Working Pressure	650 psig
Outlet connection type	SOLDER, ODF
Outlet size [in]	1/2 IN
Pack format	Multi pack
Product description	Ball Valve
Quantity per pack format	25 pc
Refrigerant(s)	CFC
Refrigerant(s)	HCFC
Refrigerant(s)	HFC
Temperature range [°C]	-40 - 150 °C
Temperature range [°F]	-40 - 300 °F

Figure 11.3-14: HFC 2-way valve (22mm)



Characteristic	Value
Type	KVR 12
Weight	0.394 Kg
Access port	Yes
Approval	C UL US LISTED
Approval	GOST AN30
Approval file name	REFRIGERANT VALVE 53R0
Factory setting [bar]	10,00 bar
Factory setting [psig]	145,0 psig
Identical product	034L1293
Inlet connection type	SOLDER, ODF
Inlet size [in]	1/2 IN
Max. test pressure [bar]	31,0 bar
Max. test pressure [psig]	450 Psig
Max. Working Pressure ef	28,0 bar
Max. Working Pressure	406 psig
Medium temperature range [°C]	-45 - 105 °C
Medium temperature range [°F]	-50 - 220 °F
Outlet connection type	SOLDER, ODF
Outlet size [in]	1/2 IN
P band max. [bar]	6,2 bar
P band max. [psi]	90,0 psi
Pack format	Multi pack
Product description	Condensing Pres. Reg.
Quantity per pack format	12 pc
Refrigerant(s)	HCFC
Refrigerant(s)	HFC
Regulating range [bar]	5,0 - 17,5 bar
Regulation range [psig] Pe	73,00 - 254,00 psig

Figure 11.3-15: HFC condenser pressure regulator



Characteristic	Value
Type	NRD 12s
Weight	-
Approval	C UL US
Approval file name	REFRIGERANT VALVE 53R0
Cv-value [USgal/min]	2,370
Direction	Straightway
Inlet connection type	SOLDER, ODF
Inlet size [in]	1/2 IN
Kv-value [m³/h]	2,050
Max. Working Pressure ef	46,0 bar
Max. Working Pressure	667 psig
Min. Pressure drop [bar]	1,40 bar
Min. pressure drop [psi]	20,3 psi
Outlet connection type	SOLDER, ODF
Outlet size [in]	1/2 IN
Pack format	Industrial pack
Product description	Diff. pressure reg.
Quantity per pack format	40 pc
Refrigerant(s)	CFC
Refrigerant(s)	HCFC
Refrigerant(s)	HFC
Temperature range [°C]	-50 - 140 °C
Temperature range [°F]	-60 - 285 °F

Figure 11.3-16: HFC condenser differential pressure regulator



Characteristic	Value
Type	GBC 22s
Weight	0.504 Kg
Access port	Yes
Approval	CE
Approval	CSA
Approval	UL
Approval file name	REFRIGERANT VALVE 53R0
Cv-value [USgal/min]	12,030
Direction	Straightway
Flow direction	Bi-flow
Inlet connection type	SOLDER, ODF
Inlet size [in]	7/8 in
Inlet size [mm]	22 MM
Kv-value [m³/h]	28,170
Max. test pressure [bar]	65,0 bar
Max. test pressure [psig]	940 psig
Max. Working Pressure ef	45,0 bar
Max. Working Pressure	650 psig
Outlet connection type	SOLDER, ODF
Outlet size [in]	7/8 in
Outlet size [mm]	22 MM
Pack format	Multi pack
Product description	Ball Valve
Quantity per pack format	25 pc
Refrigerant(s)	CFC
Refrigerant(s)	HCFC
Refrigerant(s)	HFC
Temperature range [°C]	-40 - 150 °C
Temperature range [°F]	-40 - 300 °F

### 11.3.1.1 Heaters

Table 11.3-2: VTCS Heaters

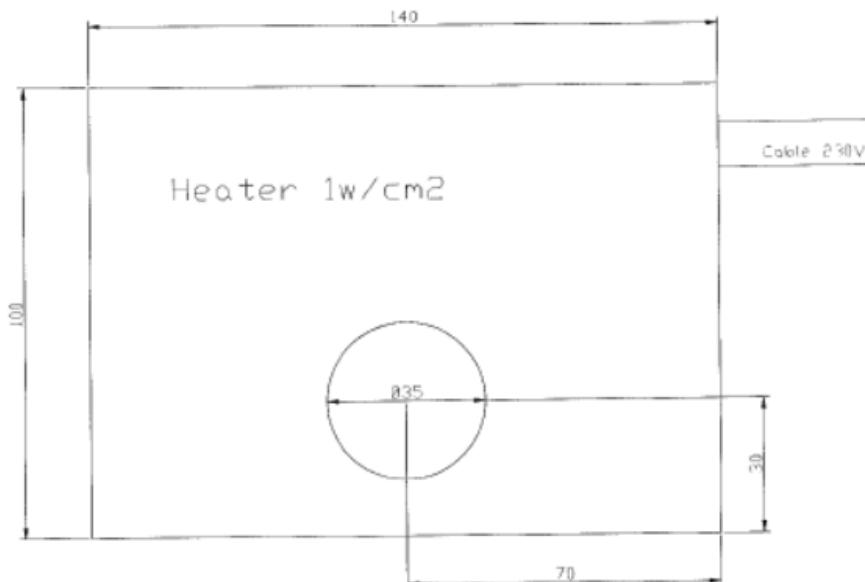
Code	Part number	Function	Supply (V)		Power (W)	Resistance (Ohm)	Electrical Control	Output signal	Diameter (mm)	Length (mm)	No-heat length (mm)	Heated area (cm <sup>2</sup> )	Thermocouple location	Heat flux (W/cm <sup>2</sup> )
TL_HT001	2 parallel / 3 serial Watlow K010030c500000	Module base temperature control	30	DC	34.8	$52.3\Omega/3*2 = 8.7\Omega$	DC Voltage regulation					19.4		1.8
TL_HT002	2 parallel / 3 serial Watlow K010030c500000	Module base temperature control	30	DC	34.8	$52.3\Omega/3*2 = 8.7\Omega$	DC Voltage regulation					19.4		1.8
TL_HT003	2 parallel / 3 serial Watlow K010030c500000	Module base temperature control	30	DC	34.8	$52.3\Omega/3*2 = 8.7\Omega$	DC Voltage regulation					19.4		1.8
TL_HT004	2 parallel / 3 serial Watlow K010030c500000	Module base temperature control	30	DC	34.8	$52.3\Omega/3*2 = 8.7\Omega$	DC Voltage regulation					19.4		1.8
TL_HT102	Watlow: Silicon Heater pads	Pump oil heater	240	AC	130	443.1	PWM					130.0		1.0
TL_HT103	Watlow: KFRJ016DM003A	Liquid line damper	220	AC	50	968	PWM	Internal Thermocouple K	12.7	410	350	23.9	center	2.1
TL_HT104	Watlow: KMFG1000M001A	By pass heater	220	AC	2000	24.2	PWM	Internal Thermocouple K	10	1000	100	282.7	center	7.1
TL_HT105	Watlow: KFRJ015AM001A	Accumulator heater	220	AC	1000	48.4	PWM	Internal Thermocouple K	12.7	380	85	117.7	center	8.5
TR_HT001	2 parallel / 3 serial Watlow K010030c500000	Module base temperature control	30	DC	34.8	$52.3\Omega/3*2 = 8.7\Omega$	DC Voltage regulation					19.4		1.8
TR_HT002	2 parallel / 3 serial Watlow K010030c500000	Module base temperature control	30	DC	34.8	$52.3\Omega/3*2 = 8.7\Omega$	DC Voltage regulation					19.4		1.8
TR_HT003	2 parallel / 3 serial Watlow K010030c500000	Module base temperature control	30	DC	34.8	$52.3\Omega/3*2 = 8.7\Omega$	DC Voltage regulation					19.4		1.8

TR_HT004	2 parallel / 3 serial Watlow K010030c500000	Module base temperature control	30	DC	34.8	$52.3\Omega/3*2 = 8.7\Omega$	DC Voltage regulation				19.4		1.8
TR_HT102	Watlow: TBD	Pump oil heater	240	AC	130	443.1	PWM				130.0		1.0
TR_HT103	Watlow: KFRJ016DM003A	Liquid line damper	220	AC	50	968	PWM	Internal Thermocouple K	12.7	410	350	23.9	center 2.1
TR_HT104	Watlow: KMFG1000M001A	By pass heater	220	AC	2000	24.2	PWM	Internal Thermocouple K	10	1000	100	282.7	center 7.1
TR_HT105	Watlow: KFRJ015AM001A	Accumulator heater	220	AC	1000	48.4	PWM	Internal Thermocouple K	12.7	380	85	117.7	center 8.5
TLR_HT102	Watlow: TBD	Pump oil heater	240	AC	130	443.1	PWM				130.0		1.0

Betr.: **Watlow** verwarmingselementen, uw e-mail aanvraag d.d. 07-12-2006. Offerte nr. 13183.

Geachte heer Munneke,

Hiermee komen wij terug op bovengenoemde aanvraag. Naar aanleiding van hetgeen besproken is, bieden wij u, overeenkomstig onze algemene verkoopvoorwaarden, vrijblijvend aan:



5 st. **Watlow** wire wound silicone rubber heater met de onderstaande specificatie:

- type nog onbekend
- dikte 1,4 mm (m.u.v. draadaansluiting)
- lengte 140 mm
- breedte 100 mm
- vermogen 130 watt
- waddichtheid 1,0 W/cm<sup>2</sup>
- aansluitspanning 240 volt
- aansluitingen met 4000 mm teflon geïsoleerd aansluitdraad en een gat Ø 35 mm, volgens uw tekening volgens de standaard fabrieksspecificatie
- uitvoering

prijs per stuk  
netto eenmalige aanmaakkosten

€ 48,25  
€ 90,-

De fabrikant waarborgt het materiaal en de constructie van de aangeboden componenten. Het is echter de verantwoordelijkheid van de gebruiker om zeker te stellen dat deze componenten juist zijn geselecteerd en geïnstalleerd in uw specifieke toepassing.

Figure 11.3-17: LEWA CO<sub>2</sub> pump oil heater

18P.05.2006 09:57 +51 2526/6104

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2087	1006788	04-AUG-06	EUR	38995	Heij C.	30 dagen	1 van 1
<hr/>							
Artikelnummer	Omschrijving	Verwachte leverdatum	Aantal	Eenheid	Prijs BTW %	Totaalprijs	
611335002	Metr.Frd KMFG1000M001A Ø10x1000mm 220V-2000W - koude zone 100mm - TC "K" (loc. A) - 3000mm SLT- (TC lds. 3000mm) - Epoxy afgedicht	18-SEP-06	4	STUK	189,85 19	755,40	<i>UTG by-pass heater</i>
600200040	Frd. KFRJ015AM001A Ø12"x380mm 220V-1000W - koude zone 85mm - TC "K" (loc. A) - 3000mm SLT- (TC lds. 3000mm) - Epoxy afgedicht	18-SEP-06	4	STUK	128,80 19	515,20	<i>UTG oceu heater</i>

Betr.: Watlow staafelementen, uw aanvraag d.d. 17-11-2008. Offerte nr. 30102-1.

Geachte heer Verlaat,

Hiermee komen wij terug op uw boven genoemde aanvraag. Wij hebben u verzoek om een thermokoppel in het verwarmde deel alsmede een thermokoppel in de koude zone met onze leveranciersdeskundige besproken. Helaas is dit technisch niet mogelijk. Derhalve bieden wij u, overeenkomstig onze algemene leveringsvoorwaarden, vrijblijvend aan:

3 st \* metrische Firerod staafelementen met de navolgende specificatie

- code KFRJ016DM003A
- afmeting Ø 1/2" x 410mm
- onverwarmd aan draadzijde 350mm
- aansluitwaarde 220 volt
- vermogen 50 watt
- aansluitdraad 150mm fiberglass aangekrimpt - *langer*
- thermokoppel type K in het midden - *eind in heated deel*
- afdichting epoxy hars

prijs per stuk

€ 103,-

Figure 11.3-18: CO<sub>2</sub> rod heaters

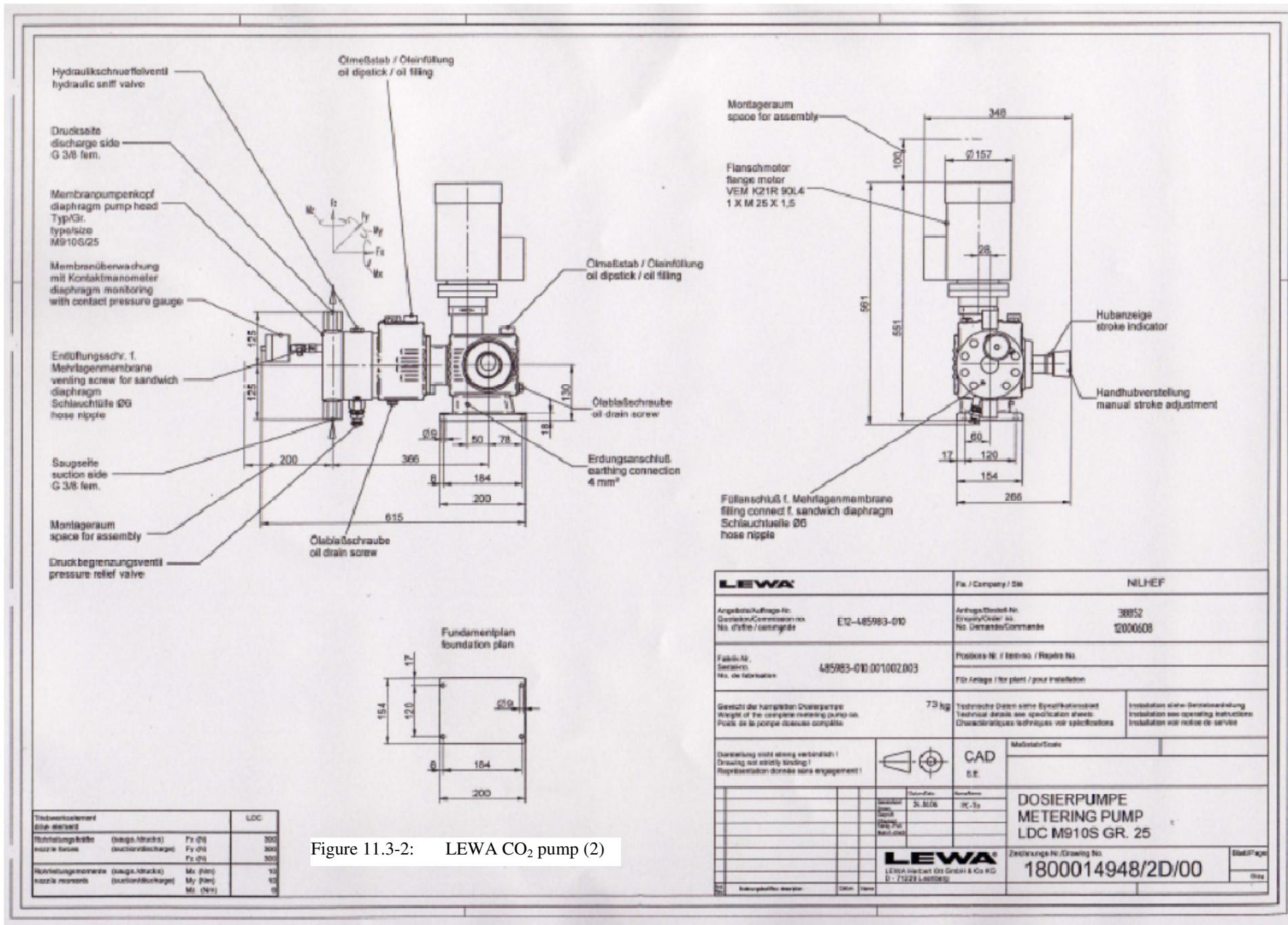
### 11.3.2 Pumps and Compressors

Table 11.3-3: VTCS Pumps and compressors

Code	Part number	Function	Connection	Pressure Head (Bar)	Flow range (mL/s)	Supply (V)	Power (W)	Electrical Control	Manual Control	Output signal	Remark
TL_PM101	LEWA 475967-010.001	Liquid pump	G 3/8 Fem	99 max	1 – 18 (4-65 l/h)	380 VAC 3p 50Hz	1500 max	on/off	Manual flow control	Membrane leak detection switch	
TR_PM101	LEWA 475967-010.001	Liquid pump	G 3/8 Fem	99 max	1 - 18 (4-65 l/h)	380 VAC 3p 50Hz	1500 max	on/off	Manual flow control	Membrane leak detection switch	
TLR_PM101	LEWA 475967-010.001	Liquid pump	G 3/8 Fem	99 max	1 - 18 (4-65 l/h)	380 VAC 3p 50Hz	1500 max	on/off	Manual flow control	Membrane leak detection switch	
SA_PM101	Bitzer 2CC-3.2Y	Gas Compressor	7/8" in / 5/8" out	28 max	4511 (16.2 m3/h) @ 50Hz	380 VAC 3p 25-70Hz		Frequency regulation			
SB_PM101	Bitzer 2KC-05.2y	Gas Compressor	5/8" in / 1/2" out	28 max	1130 (4.06 m3/h @ 50 Hz)	380 VAC 3p 50Hz		on/off			Integral in condensing aggregate: Bitzer LH32/2KC-05.2y

Technical Data Sheet					
Customer NIKHIEF Kruislaan 409 MBO 1098 SJ Amsterdam Netherlands		 Customer Reference No. P.O. No.: 38852 - Issued: 22/06/06 GEVEKE 120000608 LEWA-Quotation-No. E12-485933 LEWA-Commission-No. 010 LEWA-Position ~000			
<b>1 Element</b>					Page 1 of 1
<b>Enquiry Data (If operating data are incomplete LEWA takes no responsibility for the pump selection!)</b>					
2 Fluid	CO <sub>2</sub>		dangerous acc. 67/548/EEC		<input type="checkbox"/>
3		min	max	min	max
4 Concentration	[%]	100.00	100.00	Vapour pressure	[bar abs] 16.87
5 Fluid temperature	[°C]	-25	-25	Solidifying point	[°C] --
6 Density	[g/cm <sup>3</sup> ]	1.05	1.05	Solids	Concentration [%] --
7 Viscosity	[mPa s]	0.16	0.16	Density [g/cm <sup>3</sup> ] --	Solids sizes [mm] --
8 Required flow	[l/h]	4.00	65.00	Hardness [Mohs] --	Hardness [Mohs] --
9 Operating press. discharge [bar]	99.00	99.00	Setting rate [l/m/s] --	Setting rate [l/m/s] --	Compressibility [%] 0.51
10 Operating press. suction [bar]	50.0	50.0			
11 Area classification					
12 Ambient conditions (temperature, climate...)					
<b>Design data</b>					
13 No.	3		LEWA-Serial-No.	485983-010.	001.002.003
14 Type	LDC1	horiz. (h) / vertical (v)	Custom.-Item-No.		
15 Crankcase	Type	LDC	Driver	Make	VEN
17 Rod thrust	[N]	5000	Type	K21R 90LA	
18 Stroke adjustment	manual (H-W)		Power	[kW]	1.50
19 Eccentricity	[°]	0	Rpm	[min <sup>-1</sup> ]	1400
20 Gear reduction		8.33	Ex-protection		
21 Strokes per minute	[min <sup>-1</sup> ]	168	Protection / Insulation	[IP55]	/ F
22 Intermed elem.-TypeWidth	[mm]	=	Voltage	[V]	400
23 Pumphead	Type	M910S	Phases / Frequency	[Hz]	3 / 50
24 Plunger-Ø	[mm]	25	Size / Mounting		
25 Flow @ max. operating press.	[l/h]	62.69	Flange-Ø	[mm]	C140
26 Max. perm. operating press.	[bar]	100.0	Shaft-Ø	[mm] x [mm]	24Dx50
27 Diaphragm condition monitor	pressure contactor		Thermistots		3
28 Vent screw	No		design (VIK,CSA-)		
29 Type of plunger sealing	ground bush		Additional remarks:		
30 Plunger linkage	-				
31 Valve Suction / DN	K1	/ 10	Variable frequency drive		
32 Spring load	[bar]	-	Range	[Hz]	-
33 Valve Discharge / DN	K1	/ 10	Start-up against load		
34 Spring load	[bar]	-	Rated torque at max. press.	[Nm]	3.25
35 Setting PRV pumphead int.	[bar]	109	Start-up torque at max. press.	[Nm]	12.05
36 Setting PRV external	[bar]	100	Additional remarks:		
37 Inlet pressure loss	[bar]	0.06	General		
38 Min. required suction press. [bar abs]		16.93	Paint	RAL 5015	
39 Connection Suction	ISO G 3/8 fem.		Name plate	nl	
40 Connection Discharge	ISO G 3/8 fem.		Weight	[kg]	73
41 Connection Flushing	-		Sound pressure	[dB(A)]	-
42 Heating / Cooling	-		Ex-protection (pump)		
43 Materials LEWA material-Code	3		Accessories / Documentation / Remarks :		
44 Pumphead / Valve body	PTFE				
45 diaphragm					
46 Valve Seat / Insert ring	1.4122	/ -			
47 Guide / bal	1.4581BZ	/ 1.3541			
48 Spring / Sealing ring	-	/ -			
49 Type of plunger sealing					
50 Hydraulic fluid (diaphragm head)	M-5				
51 Intermed fluid (sandwich diaphr.)	Alkohol				
issued	24.06.06	Name PC-TG	Rev.(1)	Name	Rev.(4)
checked		Name Rev.(2)		Name Rev.(5)	Name
checked		Name Rev.(3)		Name Rev.(6)	Name

Figure 11.3-1: LEWA CO<sub>2</sub> pump (1)



## Piston compressors

Data Sheet: 2CC-3.2



- Leaflet: KP-100 (50Hz / SI)
- Leaflet: KP-105 (60Hz / IP)
- Operating Instruction: KB-100
- Spare Part List: KE-120
- Manufacturers Declaration // Decl. of Conformity // Decl. of Incorporation: KC-001
- Manufacturers Declaration // Decl. of Conformity // Decl. of Incorporation: KC-100
- Technical Information:  
KT-122 KT-140 KT-150 KT-410 KT-420 KT-500 KT-510 KT-601 KT-602 KT-680
- Show dimensional drawing
- Download CAD drawing
- Exploded View

### Technical Data

	SI	IP
Displacement (1450 RPM 50Hz)	18,24 m <sup>3</sup> /h	573.5 CFH
Displacement (1750 RPM 60Hz)	19,80 m <sup>3</sup> /h	692.2 CFH
No. of cylinder x bore x stroke	2 x 55 mm x 39,3 mm	2 x 2.17 inch x 1.55 inch
Motor voltage (more on request)	380..420V Y/3/50Hz	440..480V Y/3/60Hz
Max operating current	8.5A	8.5A
Winding ratio	--	--
Starting current (Rotor locked)	35.0A Y	35.0A Y
Weight	70 kg	154 lb
Max. pressure (LP/HP)	19 / 28 bar	275 / 403 psi
Connection suction line	22 mm - 7/8"	22 mm - 7/8"
Connection discharge line	16 mm - 5/8"	16 mm - 5/8"
Connection cooling water	--	--
Oil type R134a/R407C/R404A/R507A	to<55°C: BSE32 / to>55°C: BSE55 (Option)	to<130°F: BSE32 / to>130°F: BSE55 (Option)
Oil type R410A	--	--
Oil type R22 (R12/R502)	B5.2 (Standard)	B5.2 (Standard)
Oil type R744 (CO <sub>2</sub> )	--	--
Oil type R290/R1270	Clavus G68 (Standard)	Clavus G68 (Standard)
Oil charge	1,50 dm <sup>3</sup>	52.8 fl oz
Crankcase heater	0..120 W PTC (Option)	0..120 W PTC (Option)

Figure 11.3-3: SA-Main HFC compressor

## Piston compressors

Data Sheet: 2KC-05.2



- Leaflet: KP-100 (50Hz / SI)
- Leaflet: KP-105 (60Hz / IP)
- Operating Instruction: KB-100
- Spare Part List: KE-120
- Manufacturers Declaration // Decl. of Conformity // Decl. of Incorporation: KC-001
- Manufacturers Declaration // Decl. of Conformity // Decl. of Incorporation: KC-100
- Technical Information:  
KT-122 KT-140 KT-150 KT-410 KT-420 KT-500 KT-510 KT-601 KT-602 KT-680
- Show dimensional drawing
- Download CAD drawing
- Exploded View

### Technical Data

	SI	IP
Displacement (1450 RPM 50Hz)	4,06 m <sup>3</sup> /h	143.4 CFH
Displacement (1750 RPM 60Hz)	4,90 m <sup>3</sup> /h	173.0 CFH
No. of cylinder x bore x stroke	2 x 30 mm x 33 mm	2 x 1.18 inch x 1.3 inch
Motor voltage (more on request)	380..420V Y/3/50Hz	440..480V Y/3/60Hz
Max operating current	2.7A	2.7A
Starting current (Rotor locked)	12.0A Y	12.0A Y
Weight	43 kg	95 lb
Max. pressure (LP/HP)	19 / 28 bar	275 / 403 psi
Connection suction line	16 mm - 5/8"	16 mm - 5/8"
Connection discharge line	12 mm - 1/2"	12 mm - 1/2"
Oil type R134a/R407C/R404A/R507A	to<55°C: BSE32 / to>55°C: BSE55 (Option)	to<130°F: BSE32 / to>130°F: BSE55 (Option)
Oil type R22 (R12/R502)	B5.2 (Standard)	B5.2 (Standard)
Oil type R290/R1270	Clavus G68 (Standard)	Clavus G68 (Standard)
Oil charge	1,00 dm <sup>3</sup>	35.2 fl oz
Crankcase heater	0..60 W PTC (Option)	0..60 W PTC (Option)
Motor protection	SE-B1	SE-B1
Enclosure class	IP65	IP65
Additional fan	Option	Option
Vibration dampers	Standard	Standard

Figure 11.3-4: SB-Back-up HFC compressor

## 11.4 Passive line components

### 11.4.1 Accumulators

Table 11.4-1: VTCS accumulators

<b>Code</b>	<b>Part number</b>	<b>Function</b>	<b>Connection</b>	<b>Volume (Liter)</b>	<b>Operating Pressure (Bar)</b>	<b>Maximum Design Pressure (Bar)</b>	<b>Minimum design temperature (°C)</b>	<b>Maximum design temperature (°C)</b>	<b>Remark</b>
TL_AC101	TVC51	CO <sub>2</sub> pressure control	Multiple	14	74	135	-55	30	Nikhef engineered
TR_AC101	TVC51	CO <sub>2</sub> pressure control	Multiple	14	74	135	-55	30	Nikhef engineered
SA_AC101	Danfoss UOB 1/040B0010/040B0142	Oil separator	1/2" Solder	0.52	28	36	-40	120	
SA_AC102	Bitzer: F56	Liquid buffering	3/8" solder	5.6	20	33	-10	120	
SB_AC102	Bitzer: FS36	Liquid buffering	3/8" solder	3	20	33	-10	120	Integral in condensing aggregate: Bitzer LH32/2KC-05.2y

**Pressure vessels**

Data Sheet: FS056



Abb. ähnlich / Fig. similar, © Bitzer

- [Operating Instruction: DB-300](#)
- [Spare Part List: DE-110](#)
- [Manufacturers Declaration // Decl. of Conformity // Decl. of Incorporation: DC-300](#)
- [Download CAD drawing](#)

Technical Data		
	SI	IP
Weight	5,0 kg	11.0 lb
Total width	200 mm	7.9"
Total depth	--	--
Total height	353mm	13.9'
Receiver volume refrigerant	5,60 l	197.09 fl.oz
Max. refrigerant charge 90% at 20°C	20°C	68°F
R22	6,1 kg	13.4 lb
R134a	6,2 kg	13.6 lb
R407C	5,8 kg	12.8 lb
R404A/R507A	5,4 kg	11.9 lb
Connection inlet KL	10mm - 3/8"	10mm - 3/8"
Connection thread/-flange	--	--
Connection outlet FL	10 mm - 3/8"	10 mm - 3/8"
Gauge	7/16" 20 UNF	7/16" 20 UNF
Connection for pressure relief valve	1 1/4"-12 UNF (Option)	1 1/4"-12 UNF (Option)
Adapter for pressure relief valve	Option	Option
Minimum level control	--	--
Maximum level control	--	--
Electric liquid level control	--	--
Approval according PED 97/23/EC	Standard	Standard
Special Approvals (on request)	Option	Option

Figure 11.4-1: SA-Main HFC reservoir

**Pressure vessels**

Data Sheet: FS036

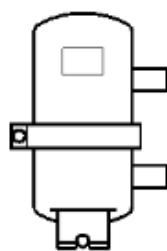


Abb. ähnlich / Fig. similar, © Bitzer

- [Operating Instruction: DB-300](#)
- [Spare Part List: DE-110](#)
- [Manufacturers Declaration // Decl. of Conformity // Decl. of Incorporation: DC-301](#)
- [Download CAD drawing](#)

Technical Data		
	SI	IP
Weight	3,0 kg	6.6 lb
Total width	129 mm	5.1"
Total depth	--	--
Total height	390mm	15.4'
Receiver volume refrigerant	3,0 l	105.59 fl.oz
Max. refrigerant charge 90% at 20°C	20°C	68°F
R22	3,3 kg	7.2 lb
R134a	3,3 kg	7.3 lb
R407C	3,1 kg	6.9 lb
R404A/R507A	2,9 kg	6.4 lb
Connection inlet KL	10mm - 3/8"	10mm - 3/8"
Connection thread/-flange	--	--
Connection outlet FL	10 mm - 3/8"	10 mm - 3/8"
Gauge	7/16" 20 UNF	7/16" 20 UNF
Connection for pressure relief valve	--	--
Adapter for pressure relief valve	--	--
Minimum level control	--	--
Maximum level control	--	--
Electric liquid level control	--	--
Approval according PED 97/23/EC	Standard	Standard
Special Approvals (on request)	Option	Option

Figure 11.4-2: SB-Back-up HFC reservoir

**040B0010**

Refrigerants: CFC, HCFC, HFC,  
Max. working pressure = 28  
bar. Max. test pressure = 36.5  
bar. Temperature of medium:  
-40 -120°C. Net volume: OUB  
1: 0.52 l, OUB 4: 2.46 l, Oil  
reservoir: OUB 1: 0.1 l.OU...  
...

SHARE

Characteristic	Value
Type	OUN 1
Weight	1.150 Kg
Approval	UL
Connection size	3/4-16 UNF-2B
Inlet connection type	UNION NUT
Max. Working Pressure ef	28,0 bar
Max. Working Pressure	406 psig
Net volume [USgal]	0,14 gal US
Net volume [l]	0,520 l
Outlet connection type	UNION NUT
Pack format	Multi pack
Product description	Oil Separator Excl. Unions
Quantity per pack format	6 PC
Refrigerant(s)	CFC
Refrigerant(s)	HCFC
Refrigerant(s)	HFC
Return connection size	7/16-20 UNF-1B
Return connection type	Flare

Figure 11.4-3: SA-Main oil separator

## 11.4.2 Heat exchangers

Table 11.4-2: VTCS heat exchangers

<b>Code</b>	<b>Contra HX</b>	<b>Part number</b>	<b>Function</b>	<b>Connection</b>	<b>Operating Pressure (Bar)</b>	<b>Maximum Design Pressure (Bar)</b>	<b>Minimum design temperature (°C)</b>	<b>Maximum design temperature (°C)</b>	<b>Heat exchange area (mm<sup>2</sup>)</b>
TL_HX001	PU01_A	TVD76	Module cooling	OD4mmx0.7mm weld	68	135	-40	60	1436
TL_HX002	PU02_A	TVD76	Module cooling	OD4mmx0.7mm weld	68	135	-40	60	1436
TL_HX003	VL01_A	TVD76	Module cooling	OD4mmx0.7mm weld	68	135	-40	60	1436
TL_HX004	VL02_A	TVD76	Module cooling	OD4mmx0.7mm weld	68	135	-40	60	1436
TL_HX005	VL03_A	TVD76	Module cooling	OD4mmx0.7mm weld	68	135	-40	60	1436
TL_HX006	VL04_A	TVD76	Module cooling	OD4mmx0.7mm weld	68	135	-40	60	1436
TL_HX007	VL05_A	TVD76	Module cooling	OD4mmx0.7mm weld	68	135	-40	60	1436
TL_HX008	VL06_A	TVD76	Module cooling	OD4mmx0.7mm weld	68	135	-40	60	1436
TL_HX009	VL07_A	TVD76	Module cooling	OD4mmx0.7mm weld	68	135	-40	60	1436
TL_HX010	VL08_A	TVD76	Module cooling	OD4mmx0.7mm weld	68	135	-40	60	1436
TL_HX011	VL09_A	TVD76	Module cooling	OD4mmx0.7mm weld	68	135	-40	60	1436
TL_HX012	VL10_A	TVD76	Module cooling	OD4mmx0.7mm weld	68	135	-40	60	1436
TL_HX013	VL11_A	TVD76	Module cooling	OD4mmx0.7mm weld	68	135	-40	60	1436
TL_HX014	VL12_A	TVD76	Module cooling	OD4mmx0.7mm weld	68	135	-40	60	1436
TL_HX015	VL13_A	TVD76	Module cooling	OD4mmx0.7mm weld	68	135	-40	60	1436
TL_HX016	VL14_A	TVD76	Module cooling	OD4mmx0.7mm weld	68	135	-40	60	1436
TL_HX017	VL15_A	TVD76	Module cooling	OD4mmx0.7mm weld	68	135	-40	60	1436
TL_HX018	VL16_A	TVD76	Module cooling	OD4mmx0.7mm weld	68	135	-40	60	1436
TL_HX021	VL19_A	TVD76	Module cooling	OD4mmx0.7mm weld	68	135	-40	60	1436
TL_HX024	VL22_A	TVD76	Module cooling	OD4mmx0.7mm weld	68	135	-40	60	1436
TL_HX025	VL23_A	TVD76	Module cooling	OD4mmx0.7mm weld	68	135	-40	60	1436
TL_HX026	VL24_A	TVD76	Module cooling	OD4mmx0.7mm weld	68	135	-40	60	1436
TL_HX027	VL25_A	TVD76	Module cooling	OD4mmx0.7mm weld	68	135	-40	60	1436
TL_HX028	TL_HX105	TVC12	Vapor transfer line	1/2" VCR female	90	135	-50	30	953568

TL_HX101	SA_HX103	TVC72 / SWEPB16DWHx12/1P-SC-H 4x1/2"INT.NPT	Main condenser	1/2"FNPT	68	135	-55	30	164000
TL_HX102	SB_HX103	TVC72 / SWEPB16DWHx6/1P-SC-H 4x1/2"INT.NPT	Back-up condenser	1/2"FNPT	68	135	-55	30	410000
TL_HX103	SA_HX107	3/8"x0.035"x10m SS Tube integral in TVC51	Main accu vaporator spiral	1/4HVCR male	-68	-135	-55	30	299080
TL_HX104	SB_HX107	3/8"x0.035"x10m SS Tube integral in TVC51	Back-up accu vaporator spiral	1/4HVCR male	-68	-135	-55	30	299080
TL_HX106	TL_HX028	TVC12	Liquid transfer line	1/2" VCR female	90	135	-50	30	686569
TR_HX001	PU01_C	TVD76	Module cooling	OD4mmx0.7mm weld	68	135	-40	60	1436
TR_HX002	PU02_C	TVD76	Module cooling	OD4mmx0.7mm weld	68	135	-40	60	1436
TR_HX003	VL01_C	TVD76	Module cooling	OD4mmx0.7mm weld	68	135	-40	60	1436
TR_HX004	VL02_C	TVD76	Module cooling	OD4mmx0.7mm weld	68	135	-40	60	1436
TR_HX005	VL03_C	TVD76	Module cooling	OD4mmx0.7mm weld	68	135	-40	60	1436
TR_HX006	VL04_C	TVD76	Module cooling	OD4mmx0.7mm weld	68	135	-40	60	1436
TR_HX007	VL05_C	TVD76	Module cooling	OD4mmx0.7mm weld	68	135	-40	60	1436
TR_HX008	VL06_C	TVD76	Module cooling	OD4mmx0.7mm weld	68	135	-40	60	1436
TR_HX009	VL07_C	TVD76	Module cooling	OD4mmx0.7mm weld	68	135	-40	60	1436
TR_HX010	VL08_C	TVD76	Module cooling	OD4mmx0.7mm weld	68	135	-40	60	1436
TR_HX011	VL09_C	TVD76	Module cooling	OD4mmx0.7mm weld	68	135	-40	60	1436
TR_HX012	VL10_C	TVD76	Module cooling	OD4mmx0.7mm weld	68	135	-40	60	1436
TR_HX013	VL11_C	TVD76	Module cooling	OD4mmx0.7mm weld	68	135	-40	60	1436
TR_HX014	VL12_C	TVD76	Module cooling	OD4mmx0.7mm weld	68	135	-40	60	1436
TR_HX015	VL13_C	TVD76	Module cooling	OD4mmx0.7mm weld	68	135	-40	60	1436
TR_HX016	VL14_C	TVD76	Module cooling	OD4mmx0.7mm weld	68	135	-40	60	1436
TR_HX017	VL15_C	TVD76	Module cooling	OD4mmx0.7mm weld	68	135	-40	60	1436
TR_HX018	VL16_C	TVD76	Module cooling	OD4mmx0.7mm weld	68	135	-40	60	1436
TR_HX021	VL19_C	TVD76	Module cooling	OD4mmx0.7mm weld	68	135	-40	60	1436
TR_HX024	VL22_C	TVD76	Module cooling	OD4mmx0.7mm weld	68	135	-40	60	1436
TR_HX025	VL23_C	TVD76	Module cooling	OD4mmx0.7mm weld	68	135	-40	60	1436
TR_HX026	VL24_C	TVD76	Module cooling	OD4mmx0.7mm weld	68	135	-40	60	1436
TR_HX027	VL25_C	TVD76	Module cooling	OD4mmx0.7mm weld	68	135	-40	60	1436
TR_HX028	TR_HX105	TVC12	Vapor transfer line	1/2" VCR female	90	135	-50	30	931624

TR_HX101	SA_HX105	TVC72 / SWEPB16DWHx12/1P-SC-H 4x1/2"INT.NPT	Main condenser	1/2"FNPT	68	135	-55	30	164000
TR_HX102	SB_HX105	TVC72 / SWEPB16DWHx6/1P-SC-H 4x1/2"INT.NPT	Back-up condenser	1/2"FNPT	68	135	-55	30	410000
TR_HX103	SA_HX108	3/8"x0.035"x10m SS Tube integral in TVC51	Main accu vaporator spiral	1/4HVCR male	-68	-135	-55	30	299080
TR_HX104	SB_HX108	3/8"x0.035"x10m SS Tube integral in TVC51	Back-up accu vaporator spiral	1/4HVCR male	-68	-135	-55	30	299080
TR_HX105	TLR_HX105	TVC135 / 6x 1.5mm*0.25mm*2m	TLR pump liquid inlet cooling	1/4HVCR female	90	135	-55	40	37699
TR_HX106	TL_HX028	TVC12	Liquid transfer line	1/2" VCR female	90	135	-50	30	670769
TLR_HX105	TR_HX105	TVC135 / 6x 1.5mm*0.25mm*2m	TLR pump liquid inlet cooling	orbital welding	90	135	-50	30	xxx
SA_HX101	CERN Cold water	SWEP B15Hx14 / 1P-SC-S	SA condenser	Soldering	23	32	0	120	504000
SA_HX102	SA_HX103 super heater	SWEP B5Hx16 / 1P-SC-S	SA superheater	Soldering	23	32	-50	30	168000
SA_HX103	TL_HX101	TVC72 / SWEPB16DWHx12/1P-SC-H 4x1/2"INT.NPT	SA main evaporator	1/2"FNPT	23	32	-50	30	164000
SA_HX104	SA_HX105 super heater	SWEP B5Hx16 / 1P-SC-S	SA superheater	Soldering	23	32	-50	30	168000
SA_HX105	TR_HX101	TVC72 / SWEPB16DWHx12/1P-SC-H 4x1/2"INT.NPT	SA main evaporator	1/2"FNPT	23	32	-50	30	164000
SA_HX106	Subcooler	SWEP B5Hx16 / 1P-SC-S	SA sub cooler	Soldering	23	32	-50	30	168000
SA_HX107	TL_HX103	3/8"x0.035"x10m SS Tube integral in TVC51	Main accu vaporator spiral	1/4HVCR male	-68	-135	-55	30	296881
SA_HX108	TR_HX103	3/8"x0.035"x10m SS Tube integral in TVC51	Main accu vaporator spiral	1/4HVCR male	-68	-135	-55	30	296881
SB_HX101	Ambient air	Bitzer LH32/2KC-05.2Y integral	SB condenser	Soldering	23	32	-50	30	249319
SB_HX103	TL_HX102	TVC72 / SWEPB16DWHx6/1P-SC-H 4x1/2"INT.NPT	SB main evaporator	1/2"FNPT	23	32	-50	30	410000
SB_HX105	TR_HX102	TVC72 / SWEPB16DWHx6/1P-SC-H 4x1/2"INT.NPT	SB main evaporator	1/2"FNPT	23	32	-50	30	410000
SB_HX106	Subcooler	SWEP B5Hx16 / 1P-SC-S	SB sub cooler	Soldering	23	32	-50	30	168000

SB_HX107	TL_HX104	3/8"x0.035"x10m SS Tube integral in TVC51	Main accu vaporator spiral	1/4HVCR male	-68	-135	-55	30	296881
SB_HX108	TR_HX104	3/8"x0.035"x10m SS Tube integral in TVC51	Main accu vaporator spiral	1/4HVCR male	-68	-135	-55	30	296881

**SWEP CBE Platenwarmtewisselaar(s):**

Positie	Type	Artikel-nummer	Nettoprijs per stuk	Toeslag <b>MSC</b> 24%	Aantal	Totaalprijs incl. toeslag
1	B15x14/1P-SC-S 4 x 22U	10041-014	€ 137,00	€ 32,88	1	€ 169,88
2	B16DWx12/1P-SC-S 2*3/4"+1/2"INT+3/4" / 1/2"INT	13656-012	€ 178,00	€ 42,72	2	€ 441,44
3	B5Hx16/1P-SC-S 2x22U+2x1/2"	10004-016	€ 77,00	€ 18,48	2	€ 190,96
4	B5Hx10/1P-SC-S 2*6.5+2*1/2"	10455-010 06227.0	€ 72,00	€ 17,28	1	€ 89,28
5	B5Hx10/1P-SC-S 2x12.8+2xR1/2"	L 10992-010	€ 72,00	€ 17,28	1	€ 89,28

**MSC = material surcharge:** wij berekenen **24% toeslag** materiaaltoeslag (MSC) vanwege de gestegen prijzen op de metaalmarkt. Dit percentage wordt per kwartaal aangepast bij wijzigingen op de metaalmarkt.

Figure 11.4-4: VTCS plate heatexchangers

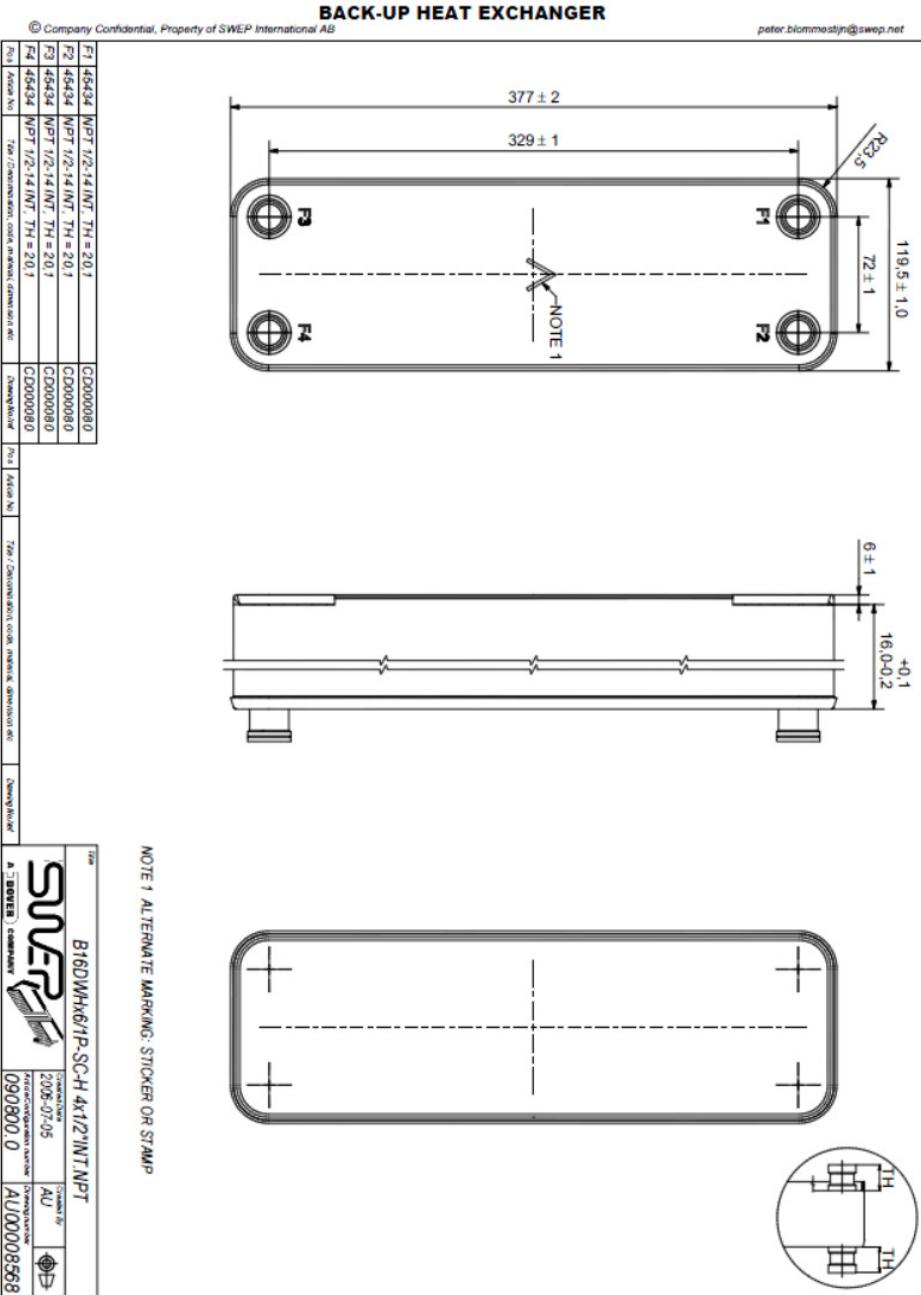


Figure 11.4-6: SB Back-up HFC evaporator

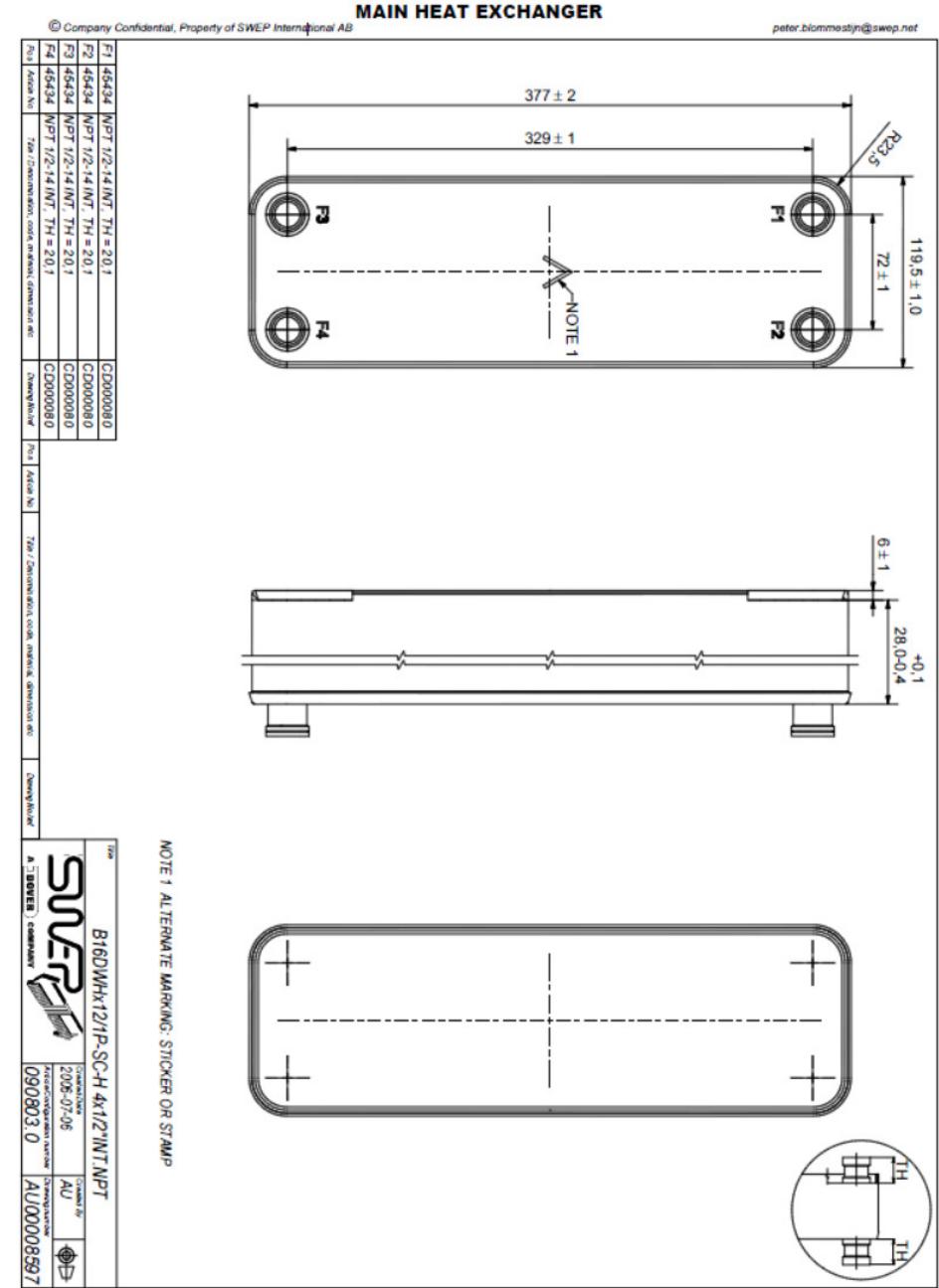


Figure 11.4-5: SA Main HFC evaporator

### 11.4.3 Relieve devices

Table 11.4-3: VTCS relieve devices

Code	Part number	Functionality	Burst Pressure (Bar)
TL_BD001	Swagelok SS-RDK-16-1900	Local control box liquid line safety	130+/- 7 bar
TL_BD002	Swagelok SS-RDK-16-1900	Local control box vapor line safety	130+/- 7 bar
TL_BD002	Swagelok SS-RDK-16-1900	Local control box vapor line safety	130+/- 7 bar
TL_BD004	TBD	Tertiary vacuum safety	1.5
TR_BD001	Swagelok SS-RDK-16-1900	Local control box liquid line safety	130+/- 7 bar
TR_BD002	Swagelok SS-RDK-16-1900	Local control box vapor line safety	130+/- 7 bar
TR_BD002	Swagelok SS-RDK-16-1900	Local control box vapor line safety	130+/- 7 bar
TR_BD004	TBD	Tertiary vacuum safety	1.5
TL_BD101	Swagelok SS-RDK-16-1900	Vapor line safety	130+/- 7 bar
TL_BD102	Swagelok SS-RDK-16-1900	Condenser safety	130+/- 7 bar
TL_BD103	Swagelok SS-RDK-16-1900	Accumulator safety	130+/- 7 bar
TL_BD104	Swagelok SS-RDK-16-1900	Suction line safety	130+/- 7 bar
TL_BD105	Swagelok SS-4R3A-EP	TL-PM101 safety	130 bar
TL_BD106	Swagelok SS-RDK-16-1900	Pump outlet safety	130+/- 7 bar
TL_BD107	Swagelok SS-RDK-16-1900	Liquid line safety	130+/- 7 bar
TR_BD101	Swagelok SS-RDK-16-1900	Vapor line safety	130+/- 7 bar
TR_BD102	Swagelok SS-RDK-16-1900	Condenser safety	130+/- 7 bar
TR_BD103	Swagelok SS-RDK-16-1900	Accumulator safety	130+/- 7 bar
TR_BD104	Swagelok SS-RDK-16-1900	Suction line safety	130+/- 7 bar
TR_BD105	Swagelok SS-4R3A-EP	TR-PM101 safety	130 bar
TR_BD106	Swagelok SS-RDK-16-1900	Pump outlet safety	130+/- 7 bar
TR_BD107	Swagelok SS-RDK-16-1900	Liquid line safety	130+/- 7 bar
TLR_BD105	Swagelok SS-4R3A-EP	TRL-PM101 safety	130 bar



**Swagelok Nederland**  
Coenecoop 770  
2741 PW Waddinxveen  
The Netherlands  
31-(0)182-624060

5/18/2010 8:03:25 AM

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### Spare Parts and Accessories



**Part Number:** SS-RDK-16-1900

**Description:** Stainless Steel Rupture Disc Kit for 16D Series Integral Bonnet Non-Rotating Stem Valves, 1900 ± 100 psig (130 ± 6.8 bar)

### Product Specifications

#### General

eClass (4.1)	37010904
eClass (6.0)	37-01-91-02
Feature	1900 PSI
UNSPSC (11.0501)	40141616
UNSPSC (4.03)	40141616
UNSPSC (SWG01)	40141616

#### REVIEW PRODUCT CATALOG FOR COMPLETE SPECIFICATIONS INCLUDING WARNINGS AND CAUTIONS.

**Safe Product Selection:** When selecting a product, the total system design must be considered to ensure safe, trouble-free performance. Function, material compatibility, adequate ratings, proper installation, operation, and maintenance are the responsibilities of the system designer and user.

**Caution:** Do not mix or interchange valve components with those of other manufacturers.

Figure 11.4-7: CO<sub>2</sub> Burst disc



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### Proportional Relief Valves, High Pressure



**Part Number:** SS-4R3A-EP

**Description:** SS High-Pressure Proportional Relief Valve, 1/4 in. Swagelok Tube Fitting, Ethylene Propylene Seal

### Product Specifications

#### General

Service Class	High Pressure
Size	1/8in
Valve Material	316 Stainless Steel
End Connection 1 Size	1/4 in
End Connection 1 Type	Swagelok tube fitting
End Connection 2 Size	1/4 in
End Connection 2 Type	Swagelok tube fitting
Approval	No Approval
Cleaning	Swagelok SC-10
Lubricant	Dow Corning Molykote 55 Grease
Manual Override	No
Seal Material	Ethylene Propylene
Testing	No Optional Testing
Max Temperature Pressure Rating	250°F @ 4910 PSIG /121°C @ 338 BAR
Room Temperature Pressure Rating	6000 PSIG @ 100°F /413 @ BAR 37°C

#### REVIEW PRODUCT CATALOG FOR COMPLETE SPECIFICATIONS INCLUDING WARNINGS AND CAUTIONS.

**Safe Product Selection:** When selecting a product, the total system design must be considered to ensure safe, trouble-free performance. Function, material compatibility, adequate ratings, proper installation, operation, and maintenance are the responsibilities of the system designer and user.

**Caution:** Do not mix or interchange valve components with those of other manufacturers.

Figure 11.4-8: CO<sub>2</sub> Spring relieve valve

## 11.4.4 Filters

Table 11.4-4: VTCS filters

Code	Part number	Function	Connection	Operating Pressure (Bar)	Maximum Design Pressure (Bar)	Minimum design temperature (°C)	Maximum design temperature (°C)	Pories (micron)
TL_FL001	Swagelok SS-4FW-VCR-15	TL-VL002 protection	1/4" male VCR	100	413	-28	37	15
TL_FL002	Swagelok element ss-4f-k4-15	Evaporator Capillary protection						15
TR_FL001	Swagelok SS-4FW-VCR-15	TL-VR002 protection	1/4" male VCR	100	413	-28	37	15
TR_FL002	Swagelok element ss-4f-k4-15	Evaporator Capillary protection		100	413	-28	37	15
TL_FL101	Swagelok ss-4TF-TW-15	Transfer tube filter	3/8" Weld	100	413	-28	37	15
TL_FL102	Swagelok ss-4TF-TW-15	TL-VL109 protection	1/4" Weld	100	413	-28	37	15
TR_FL101	Swagelok ss-4TF-TW-15	Transfer tube filter	3/8" Weld	100	413	-28	37	15
TR_FL102	Swagelok ss-4TF-TW-15	TL-VR109 protection	1/4" Weld	100	413	-28	37	15
TR_FL103	Swagelok SS-4FW-VCR-15	TLR pump culling capillary protection	1/4" male VCR	100	413	-28	37	15
SA_FL101	Danfoss DML 033s/023Z5050	Liquid line filtering	3/8 solder					
SB_FL101	Danfoss DML032s/023Z5048	Liquid line filtering	1/4 solder					

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## All-Welded In-Line Filters



**Part Number:** SS-4FW-VCR-15  
**Description:** Stainless Steel All-Welded In-Line Filter, 1/4 in. Male VCR, 15 Micron Pore Size

## Product Specifications

General	
Body Material	316 Stainless Steel
Cleaning Process	Special Cleaning and Packaging (SC-11)
Connection 1 Size	1/4 in.
Connection 1 Type	VCR® Metal Gasket Face Seal Fitting
Connection 2 Size	1/4 in.
Connection 2 Type	VCR® Metal Gasket Face Seal Fitting
eClass (4.1)	36101905
eClass (6.0)	36-10-20-00
Feature	15 Micron Element Pore Size
UNSPSC (11.0501)	40161516
UNSPSC (4.03)	40161500
UNSPSC (SWG01)	40161500

## REVIEW PRODUCT CATALOG FOR COMPLETE SPECIFICATIONS INCLUDING WARNINGS AND CAUTIONS.

Safe Product Selection: When selecting a product, the total system design must be considered to ensure safe, trouble-free performance. Function, material compatibility, adequate ratings, proper installation, operation, and maintenance are the responsibilities of the system designer and user.

Caution: Do not mix or interchange valve components with those of other manufacturers.

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Figure 11.4-9: CO<sub>2</sub> Inline filter

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## Tee-Type Filters

**Part Number:**

SS-4TF-TW-15

**Description:**

Stainless Steel Tee-Type Particulate Filter, 1/4 in. Tube Socket Weld and 3/8 in. Tube Butt Weld, 15 Micron Pore Size

## Product Specifications

General	
Body Material	316 Stainless Steel
Cleaning Process	Standard Cleaning and Packaging (SC-10)
Connection 1 Size	1/4 and 3/8 in.
Connection 1 Type	Tube Socket Weld and Tube Butt Weld
Connection 2 Size	1/4 and 3/8 in.
Connection 2 Type	Tube Socket Weld and Tube Butt Weld
eClass (4.1)	36101905
eClass (6.0)	36-10-20-90
Feature	15 Micron Element Pore Size
UNSPSC (11.0501)	40161500
UNSPSC (4.03)	40161500
UNSPSC (SWG01)	40161500

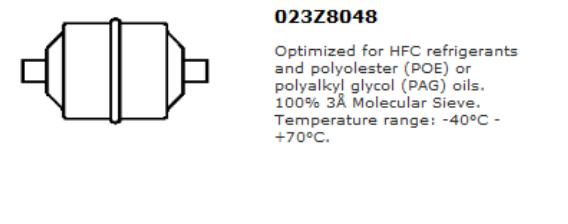
## REVIEW PRODUCT CATALOG FOR COMPLETE SPECIFICATIONS INCLUDING WARNINGS AND CAUTIONS.

Safe Product Selection: When selecting a product, the total system design must be considered to ensure safe, trouble-free performance. Function, material compatibility, adequate ratings, proper installation, operation, and maintenance are the responsibilities of the system designer and user.

Caution: Do not mix or interchange valve components with those of other manufacturers.

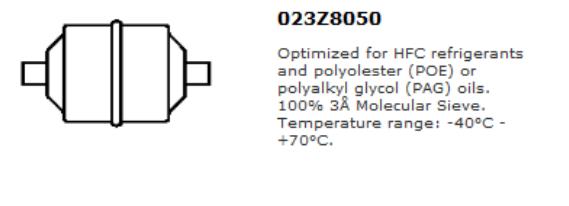
Figure 11.4-10: CO<sub>2</sub> T-filter

Figure 11.4-11: SB-Back-up filter



Characteristic	Value
Type	DML 0325
Weight	0,206 Kg
Acid capacity [g]	0,58 g
Acid capacity [oz]	0,021 oz
Approval	UL
Connection material	Cu
Core size	03 cu.in.
Felt mat/hole design	0
Inlet connection size [in]	1/4 IN
Inlet connection type	SOLDER, ODF
Max. Working Pressure ef	46,0 bar
Max. Working Pressure	667 psig
Net volume [fluid oz]	1,28 foz US
Net volume [l]	0,038 l
Outlet connection size [in]	1/4 IN
Outlet connection type	SOLDER, ODF
Pack format	Industrial pack
Product description	Liquid line filter drier
Quantity per pack format	28 pc
Refrigerant(s)	HCFC
Refrigerant(s)	HFC
Shell volume [foz US]	2,71 foz US
Shell volume [l]	0,08 l
Solid core surface [cm <sup>2</sup> ]	82 cm <sup>2</sup>
Solid core volume [cm <sup>3</sup> ]	41 cm <sup>3</sup>
Solid core surface [in <sup>2</sup> ]	12,71 in <sup>2</sup>
Solid core volume [in <sup>3</sup> ]	2,50 in <sup>3</sup>
Temperature range [°C]	-40 - 70 °C
Temperature range [°F]	-40 - 160 °F
Type designation	DML 0325

Figure 11.4-12: SA-Main filter



Characteristic	Value
Type	DML 0335
Weight	0,213 Kg
Acid capacity [g]	0,58 g
Acid capacity [oz]	0,021 oz
Approval	UL
Connection material	Cu
Core size	03 cu.in.
Felt mat/hole design	0
Inlet connection size [in]	3/8 IN
Inlet connection type	SOLDER, ODF
Max. Working Pressure ef	46,0 bar
Max. Working Pressure	667 psig
Net volume [fluid oz]	1,28 foz US
Net volume [l]	0,038 l
Outlet connection size [in]	3/8 IN
Outlet connection type	SOLDER, ODF
Pack format	Industrial pack
Product description	Liquid line filter drier
Quantity per pack format	28 pc
Refrigerant(s)	HCFC
Refrigerant(s)	HFC
Shell volume [foz US]	2,71 foz US
Shell volume [l]	0,08 l
Solid core surface [cm <sup>2</sup> ]	82 cm <sup>2</sup>
Solid core volume [cm <sup>3</sup> ]	41 cm <sup>3</sup>
Solid core surface [in <sup>2</sup> ]	12,71 in <sup>2</sup>
Solid core volume [in <sup>3</sup> ]	2,50 in <sup>3</sup>
Temperature range [°C]	-40 - 70 °C
Temperature range [°F]	-40 - 160 °F
Type designation	DML 0335

## 11.5 System analyses results

### 11.5.1 SA-Main Chiller

Model outcome of a nominal SA operation. Figure 11.5-1 shows the state points in the P-H diagram.

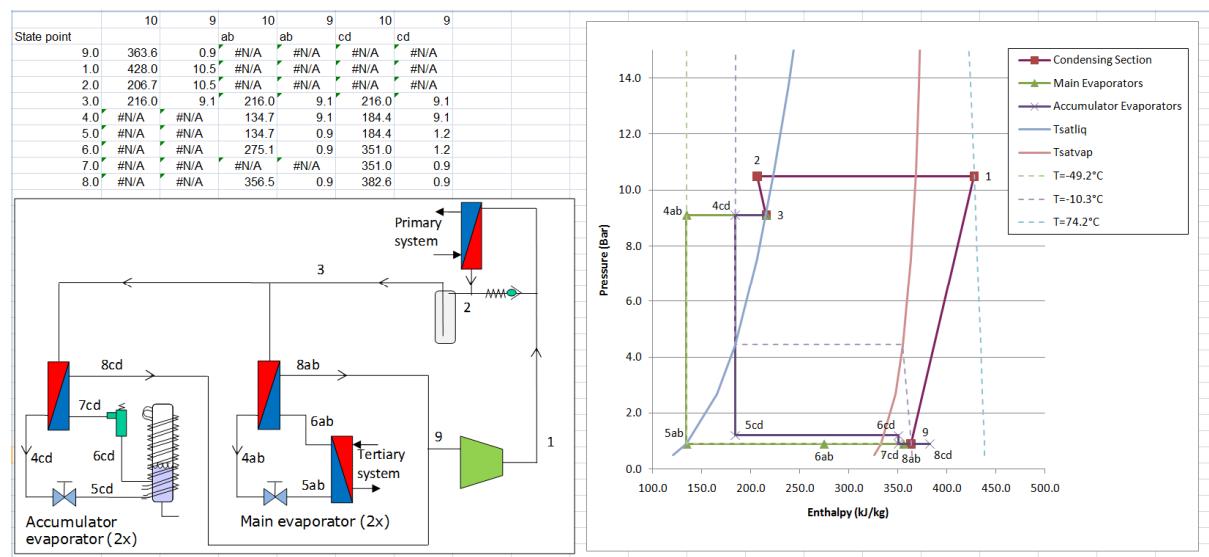


Figure 11.5-1: SA-chiller operation in the pressure enthalpy diagram.

Table 11.5-1 Volumes and operational states of the SA-Main chiller

Section	Volume (mL)	Pressure (Bar)	Enthalpy (kJ/kg)	Temp. (°C)	Rho (kg/m³)	Mass (g)
SA_S.01.01	649.9	10.5	427.9	74.1	40.2	26.1
SA_S.01.02	112.6	10.5	427.9	74.1	40.2	4.5
SA_S.01.03	441.0	10.5	317.3	17.6	83.1	36.7
SA_S.01.04	43.3	10.5	206.7	6.0	1134.6	49.1
SA_S.02.01	47.2	9.1	216.0	12.5	1105.2	52.1
SA_S.02.02	5600.0	9.1	216.0	12.5	566.1	3167.2
SA_S.02.03	130.4	9.1	216.0	12.5	1105.2	144.1
SA_S.03.01	200.0	9.1	175.4	-17.1	1222.1	244.4
SA_S.03.02	34.3	9.1	134.7	-49.2	1326.7	45.5
SA_S.03.03	49.0	0.9	134.7	-49.2	950.7	47.6
SA_S.03.04	366.0	0.9	204.9	-49.2	14.0	5.1
SA_S.03.05	96.2	0.9	275.2	-49.2	7.0	0.7
SA_S.03.06	48.1	0.9	275.2	-49.2	7.0	0.3
SA_S.03.07	175.0	0.9	315.8	-49.2	5.5	1.0
SA_S.03.08	63.5	0.9	356.5	-19.2	4.3	0.3
SA_S.04.01	200.0	9.1	175.4	-17.1	1222.1	244.4
SA_S.04.02	48.5	9.1	134.7	-49.2	1326.7	64.4
SA_S.04.03	81.4	0.9	134.7	-49.2	950.7	79.0
SA_S.04.04	366.0	0.9	245.6	-49.2	8.9	3.3
SA_S.04.05	159.8	0.9	275.2	-49.2	7.0	1.1
SA_S.04.06	76.0	0.9	275.2	-49.2	7.0	0.5
SA_S.04.07	175.0	0.9	315.8	-49.2	5.5	1.0
SA_S.04.08	63.5	0.9	356.5	-19.2	4.3	0.3

SA_S.05.01	200.0	9.1	200.2	1.3	1152.9	230.6
SA_S.05.02	25.5	9.1	184.4	-10.3	1197.6	30.5
SA_S.06.01	24.5	1.2	184.4	-43.2	29.5	0.7
SA_S.06.02	490.0	1.2	267.7	-43.2	10.1	5.0
SA_S.06.03	57.7	1.2	351.0	-25.0	6.0	0.3
SA_S.06.04	25.0	1.2	351.0	-25.0	6.0	0.1
SA_S.06.05	51.0	0.9	351.0	-26.0	4.5	0.2
SA_S.07.01	49.0	1.2	184.4	-43.2	29.5	1.4
SA_S.07.02	490.0	1.2	267.7	-43.2	10.1	5.0
SA_S.07.03	105.9	1.2	351.0	-25.0	6.0	0.6
SA_S.07.04	25.0	1.2	351.0	-25.0	6.0	0.1
SA_S.07.05	42.3	0.9	351.0	-26.0	4.5	0.2
SA_S.08.01	6.7	0.9	351.0	-26.0	4.5	0.0
SA_S.08.02	175.0	0.9	366.8	-6.4	4.1	0.7
SA_S.08.03	63.5	0.9	382.6	12.5	3.8	0.2
SA_S.09.01	1046.1	0.9	363.6	-10.4	4.2	4.4
SA_S.09.02	237.7	0.9	363.6	-10.4	4.2	1.0
SA_S.09.03	0.0	5.7	427.9	68.8	21.1	0.0
	=====					=====
Total volume	12.34				Total mass:	4500

Table 11.5-2 Overview of the volumes, charge and reservoir levels of the SA-Main chiller

Discharge and condensing section	1.25	Liter
Liquid and buffer section:	5.78	Liter
Branch 1 (to left condenser)	1.03	Liter
Branch 2 (to right condenser)	1.17	Liter
Branch 3&4 liquid inlet	0.23	Liter
Branch 3 (to left accu)	0.65	Liter
Branch 4 (to right accu)	0.71	Liter
Branch 3&4 vapor outlet	0.25	Liter
Cold gas section	1.28	Liter
System volume w.o. reservoir	6.74	Liter
Total system volume	12.34	Liter
Max flooded volume	2.85	Liter
Reservoir volume	5.60	Liter
Filling	4.5	kg
Homogeneous filling	0.36	kg/L
Maximum buffer level	74.10%	
Nominal buffer level	48.98%	
Minimum buffer level	14.25%	

### 11.5.2 SB-Back-up Chiller

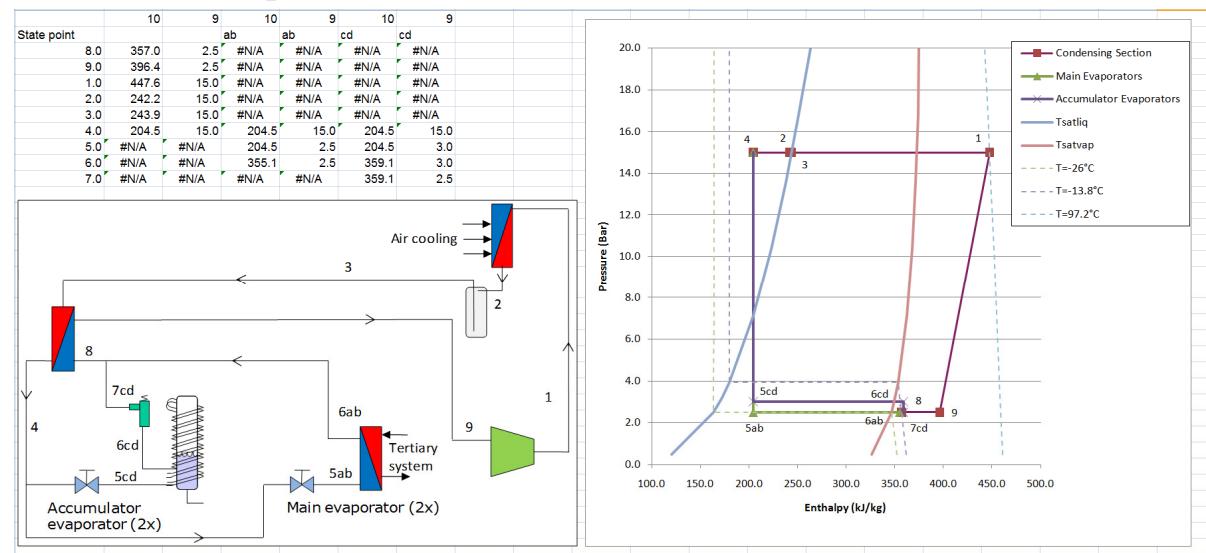


Figure 11.5-2: SB-chiller operation in the pressure enthalpy diagram.

Table 11.5-3 Volumes and operational states of the SB-Back-up chiller

Section	Volume (mL)	Pressure (Bar)	Enthalpy (kJ/kg)	Temp. ('C)	Rho (kg/m3)	Mass (g)
SB_S.01.01	132.8	15.0	447.6	97.2	54.7	7.3
SB_S.01.02	690.0	15.0	344.9	31.1	102.9	71.0
SB_S.02.01	4.7	15.0	242.2	30.0	1023.1	4.8
SB_S.02.02	3000.0	15.0	243.9	31.1	1017.0	2216.9
SB_S.02.03	106.4	15.0	243.9	31.1	1017.0	108.2
SB_S.05.01	200.0	15.0	224.7	18.5	1082.7	216.9
SB_S.05.02	11.6	15.0	205.5	5.1	1141.4	13.3
SB_S.03.03	63.7	2.5	205.5	-26.0	55.6	3.6

SB_S.03.04	183.0	2.5	280.3	-26.0	20.5	3.8
SB_S.03.05	125.1	2.5	355.1	-16.0	12.5	1.6
SB_S.03.08	37.5	2.5	355.1	-16.0	12.5	0.5
SB_S.04.03	81.4	2.5	205.5	-26.0	55.6	4.6
SB_S.04.04	183.0	2.5	280.3	-26.0	20.5	3.8
SB_S.04.05	159.8	2.5	355.1	-16.0	12.5	2.0
SB_S.04.08	37.5	2.5	355.1	-16.0	12.5	0.5
SB_S.06.01	39.2	2.5	205.5	-26.0	55.6	3.0
SB_S.06.02	490.0	2.5	282.9	-26.0	20.1	12.2
SB_S.06.03	86.6	2.5	3603	-10.0	12.1	1.3
SB_S.06.04	25.0	2.5	360.3	-10.0	12.1	0.4
SB_S.06.06	25.0	2.5	360.3	-10	12.1	0.3
SB_S.07.01	49.0	2.5	205.5	-26.0	55.6	3.8
SB_S.07.02	490.0	2.5	282.9	-26.0	20.1	12.2
SB_S.07.03	105.9	2.5	360.3	-10.0	12.1	1.6
SB_S.07.04	25.0	2.5	360.3	-10.0	12.1	0.4
SB_S.07.06	25.0	2.5	360.3	-10	12.1	0.3
SB_S.08.01	237.3	2.5	358.1	-12.6	12.3	2.9
SB_S.08.01	175.0	2.5	377.2	9.5	11.1	1.9
SB_S.09.01	112.4	2.5	396.4	31.1	10.2	1.1
SB_S.09.03	0.0	8.8	422.0	66.3	33.9	0.0
	=====				=====	
Total volume	6.90				Total mass:	2700

Table 11.5-4 Overview of the volumes, charge and reservoir levels of the SB-Back-up chiller

Discharge and condensing section	0.82	Liter
Liquid and buffer section:	3.32	Liter
Branch 1 (to left condenser)	0.41	Liter
Branch 2 (to right condenser)	0.46	Liter
Branch 3 (to left accu)	0.67	Liter
Branch 4 (to right accu)	0.69	Liter
Cold gas section	0.52	Liter
System volume w.o. buffer	3.90	Liter
Total system volume	6.90	Liter
Max flooded volume	1.90	Liter
Reservoir	3.00	Liter
Filling	2.7	kg
Homogeneous filling	0.39	kg/L
Maximum buffer level	83.75%	
Nominal buffer level	70.26%	
Minimum buffer level	14.00%	

### 11.5.3 Tertiary CO<sub>2</sub> systems

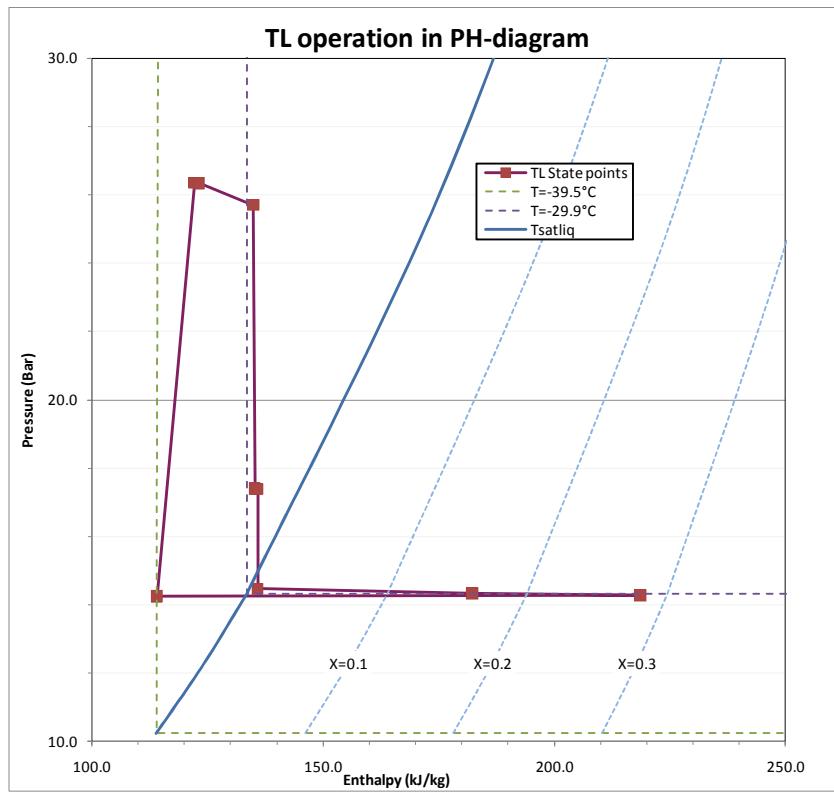


Figure 11.5-3: TL system in the PH-diagram. Detector power =489 Watt, Tsetpoint is -30°C

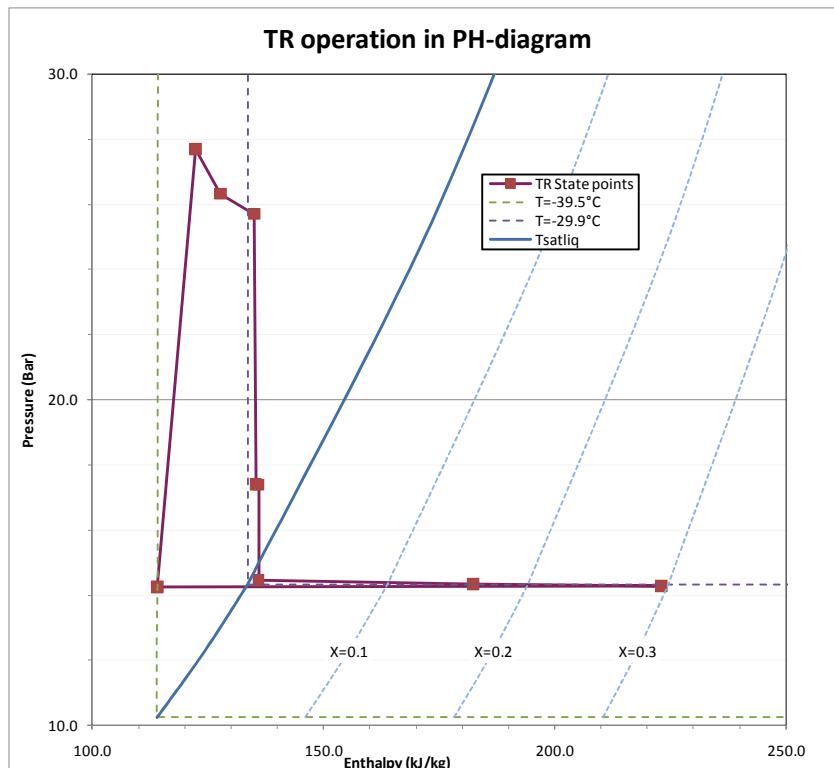


Figure 11.5-4: TR system in the PH-diagram. Detector power =489 Watt, Tsetpoint is -30°C

Table 11.5-5 Volumes and operational states of the TL and TRL System

Section	Volume (mL)	Pressure (Bar)	Enthalpy (kJ/kg)	Temp. ('C)	Rho (kg/m3)	Mass (g)
TL_S.01.01	25.1	26.4	122.2	-35.5	1103.0	27.7
TL_S.01.04	22.2	26.3	123.2	-35.0	1100.9	24.5
TL_S.01.05	605.0	26.4	526.5	70.0	44.4	26.9
TL_S.01.06	9.5	26.3	123.5	-34.8	1100.2	10.4
TL_S.02.01	38.3	26.3	124.5	-34.4	1098.3	42.0
TL_S.02.02	784.1	26.0	131.8	-30.8	1083.1	849.2
TL_S.03.01	38.7	25.7	135.0	-29.2	1076.4	41.7
TL_S.03.02	7.8	17.4	135.2	-29.1	1072.8	8.4
TL_S.03.03	18.7	17.4	135.8	-28.8	1071.5	20.1
TL_S.04.01-27	51.4	14.5	135.8	-29.6	929.6	47.8
TL_S.05.01-27	8.3	14.4	181.3	-29.8	201.1	1.7
TL_S.06.01-27	40.3	14.4	181.3	-29.8	200.0	8.1
TL_S.07.01	120.0	14.3	181.3	-29.9	199.8	24.0
TL_S.08.01	66.0	14.3	182.3	-29.9	196.5	13.0
TL_S.08.02	106.2	14.3	184.0	-29.9	190.9	20.3
TL_S.09.01	23.0	14.3	184.2	-29.9	190.1	4.4
TR_S.09.02	5844.4	14.3	204.4	-29.9	144.9	846.6
TL_S.09.99	93.2	14.3	217.1	-30.0	123.4	11.5
TL_S.10.01	44.8	14.3	218.0	-30.0	122.1	5.5
TL_S.10.02	36.0	14.3	218.5	-30.0	121.4	4.4
TL_S.11.01	305.0	14.3	222.7	-30.0	116.3	35.5
TL_S.11.02	6.4	14.3	113.0	-40.0	1117.6	7.1
TL_S.12.01	122.0	14.3	468.4	0.0	30.8	3.8
TL_S.12.02	6.4	14.3	468.4	0.0	30.8	0.2
TL_S.13.01	23.0	14.3	113.9	-39.5	1115.7	25.7
TL_S.13.02	36.0	14.3	114.3	-39.3	1114.9	40.1
TL_S.14.01	74.5	14.3	468.4	0.0	30.8	2.3
TL_S.14.02	75.4	14.3	468.4	0.0	30.8	2.3
TL_S.14.03	110.8	14.3	468.4	0.0	30.8	3.4
TL_S.15.01	23.4	14.3	436.8	-30.0	121.4	2.8
TL_S.15.02	14203.0	0.0	0.0	0.0	0.0	9828.3
TLR_S.01.01	29.1	17.4	463.9	0.0	38.6	1.1
TLR_S.13.02	32.3	14.3	284.1	-30.5	558.6	9.4
	=====					=====
Total Volume:	23030.3				Total CO <sub>2</sub> :	12000.0

Table 11.5-6 Volumes and operational states of the TR-System

Section	Volume (mL)	Pressure (Bar)	Enthalpy (kJ/kg)	Temp. ('C)	Rho (kg/m3)	Mass (g)
TR_S.01.01	41.5	27.7	122.3	-35.4	1103.1	45.8
TR_S.01.02	9.0	26.3	126.5	-33.4	1094.1	9.9
TR_S.01.03	5.5	26.3	126.7	-33.2	1093.7	6.1
TR_S.01.04	27.3	26.3	127.7	-32.8	1091.7	29.8
TR_S.01.05	605.0	26.3	526.5	70.0	44.4	26.9
TR_S.01.06	9.5	26.3	128.1	-32.6	1091.0	10.3

TR_S.02.01	26.1	26.3	129.0	-32.1	1089.0	28.5
TR_S.02.02	766.0	26.0	132.7	-30.3	1081.3	828.3
TR_S.03.01	46.3	25.7	135.1	-29.2	1076.2	49.9
TR_S.03.02	7.8	17.4	135.3	-29.0	1072.6	8.4
TR_S.03.03	18.7	17.4	135.9	-28.7	1071.3	20.1
TR_S.04.01-27	51.4	14.5	135.9	-29.6	921.6	47.4
TR_S.05.01-27	8.3	14.4	181.4	-29.8	200.7	1.7
TR_S.06.01-27	40.3	14.4	181.4	-29.8	199.6	8.1
TR_S.07.01	120.0	14.3	181.4	-29.9	199.4	23.9
TR_S.08.01	66.0	14.3	182.4	-29.9	196.1	12.9
TR_S.08.02	117.5	14.3	184.1	-29.9	190.5	22.4
TR_S.09.01	23.0	14.3	184.3	-29.9	189.7	4.4
TR_S.09.02	5710.0	14.3	205.7	-29.9	143.0	816.4
TR_S.09.99	72.7	14.3	221.7	-30.0	117.7	8.5
TR_S.10.01	37.2	14.3	222.6	-30.0	116.6	4.3
TR_S.10.02	36.0	14.3	223.1	-30.0	115.9	4.2
TR_S.11.01	305.0	14.3	227.3	-30.0	111.3	33.9
TR_S.11.02	5.8	14.3	113.0	-40.0	1117.6	6.4
TR_S.12.01	122.0	14.3	468.4	0.0	30.8	3.8
TR_S.12.02	5.8	14.3	468.4	0.0	30.8	0.2
TR_S.13.01	23.0	14.3	113.9	-39.5	1115.7	25.7
TR_S.13.02	36.0	14.3	114.3	-39.3	1114.9	40.1
TR_S.14.01	74.5	14.3	468.4	0.0	30.8	2.3
TR_S.14.02	75.4	14.3	468.4	0.0	30.8	2.3
TR_S.14.03	110.8	14.3	468.4	0.0	30.8	3.4
TR_S.15.01	16.1	14.3	436.8	-30.0	115.9	1.9
TR_S.15.02	14203.0	0.0	0.0	0.0	0.0	9862.0
	=====					=====
Total Volume:	22822.6				Total CO <sub>2</sub>	12000.0

Table 11.5-7 Summary of the Tertiary volume.

Subsystem	TL volume (mL)	TR Volume (mL)
Evaporator	220.0	220.0
Liquid feed	944.4	957.8
Vapor return	6213.7	6062.4
SA-Condenser	311.4	310.8
SB-Condenser	128.4	127.8
Liquid Suction	59.1	59.1
By-pass	260.7	260.7
Dampers	605.0	605.0
Accumulator section	14226.4	14219.1
Accumulator	14203.0	14203.0
Total Volume	22969.0	22822.6
Loop Volume	8766.0	8619.6
Plant Volume	15728.6	15748.5
Transfer Volume	7240.4	7074.2

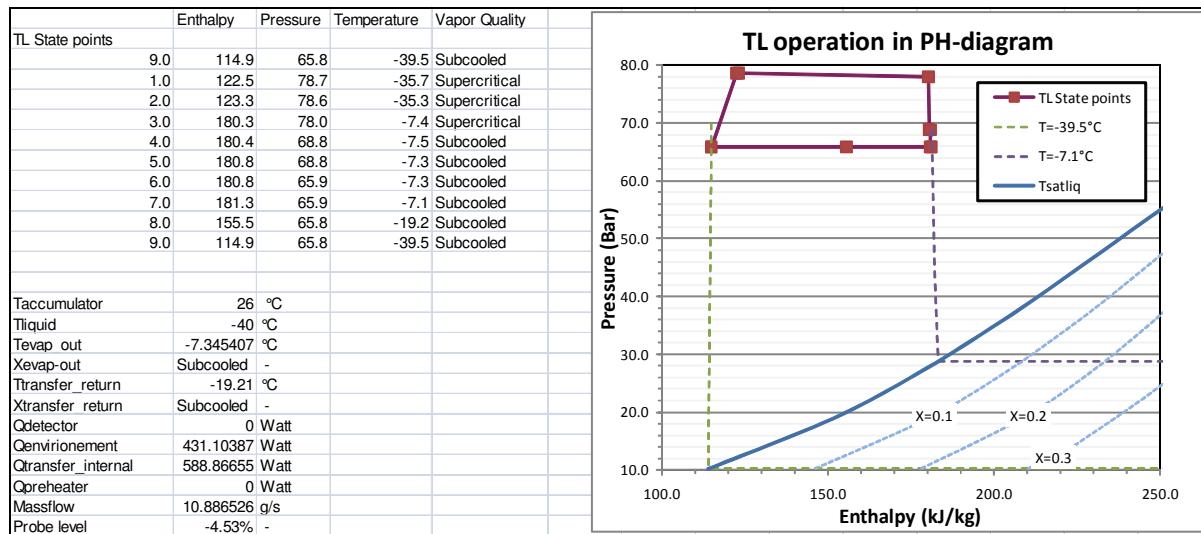


Figure 11.5-5: TL system Start-up. Detector power =0 Watt, SP = +26°C

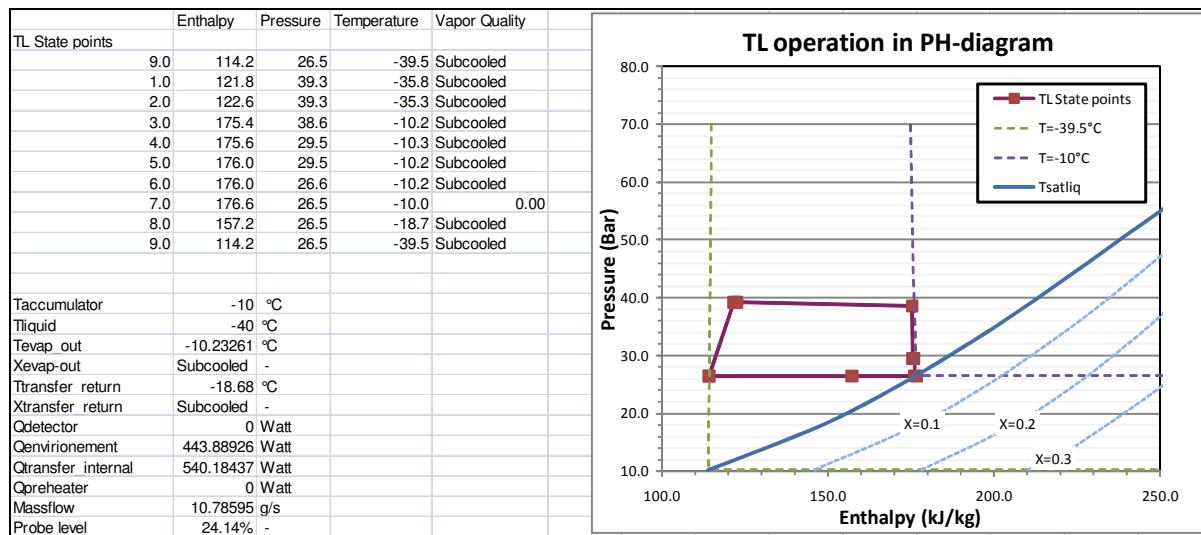


Figure 11.5-6: TL system operation. Detector power =0 Watt, SP = -10°C

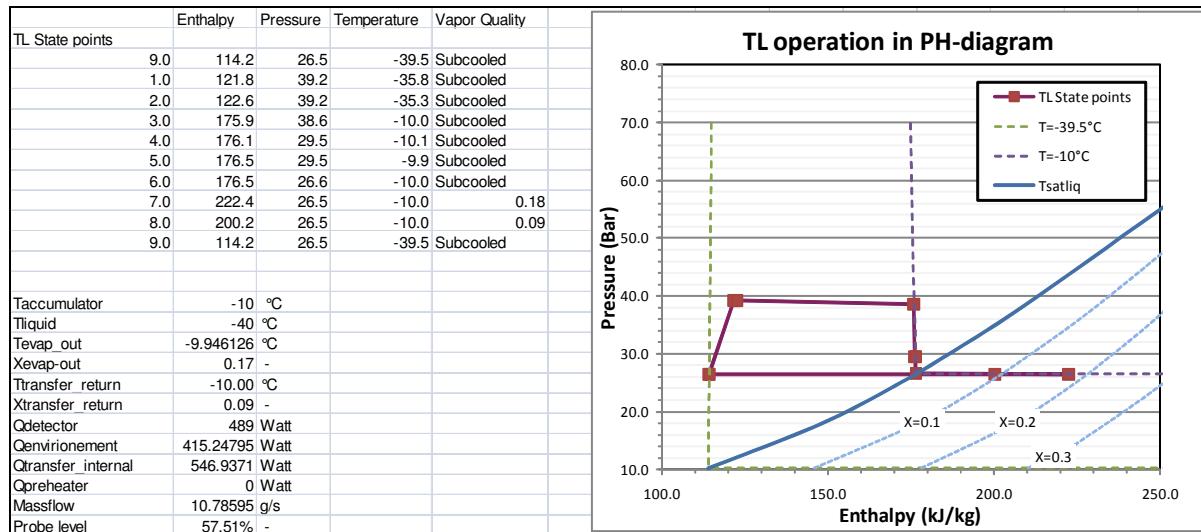


Figure 11.5-7: TL system operation. Detector power =489 Watt, SP = -10°C

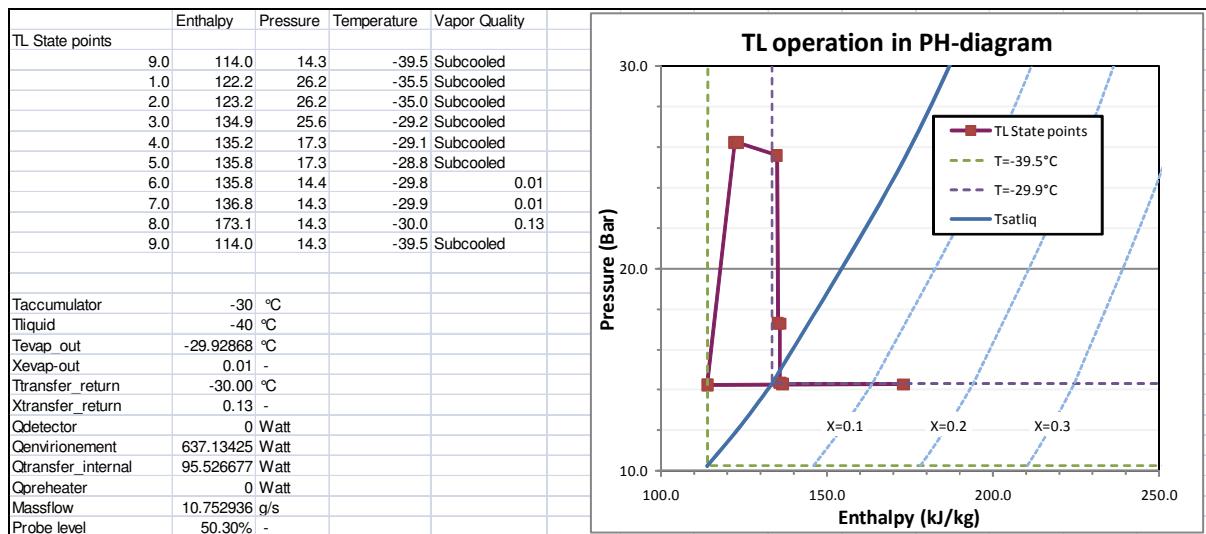


Figure 11.5-8: TL system operation. Detector power =0 Watt, SP = -30°C

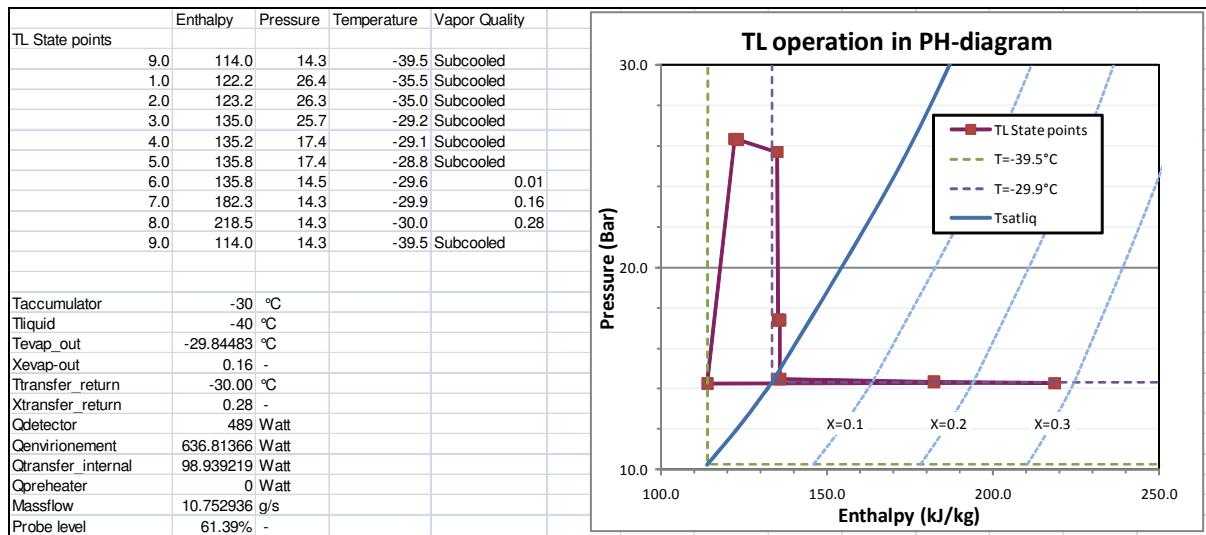


Figure 11.5-9: TL system operation. Detector power =489 Watt, SP = -30°C

## 11.6 PLC Alarms and warnings

Table 11.6-1 PLC alarms and corresponding values and actions.

Alarm Category	Alert Type	Alert Cause	PLC label	PVSS label	General actions / Failure Category	Proceeding	Triggered by	Timer involved	Timer setting PVSS label	Timer value	Running timer	Running Timer PVSS label	Threshold PLC variable	Threshold PVSS label	Threshold value	
Base plate	Alarm	Base plate freezing alarm	Tx_base_freezing	Tx_BA001---base_freezing	SA-Failure	restart	2 of TL_TT037, TL_TT038, TL_TT039, TL_TT040						BASEPLATE_FREEZING	Tx_BL001---BASEPLATE_FREEZING	0	
	Alarm	Base plate too hot	TLbase_too_hot_TT037	TL_BA002---base_too_hot_TT037	heater process termination	continue procedures	TL_TT037						MAX_TEMP_BASE_PLATE	TL_BL002---MAX_TEMP_BASEPLATE	27	
			TLbase_too_hot_TT038	TL_BA003---base_too_hot_TT038	heater process termination	continue procedures	TL_TT038						MAX_TEMP_BASE_PLATE	TL_BL002---MAX_TEMP_BASEPLATE	27	
			TLbase_too_hot_TT039	TL_BA004---base_too_hot_TT039	heater process termination	continue procedures	TL_TT039						MAX_TEMP_BASE_PLATE	TL_BL002---MAX_TEMP_BASEPLATE	27	
			TLbase_too_hot_TT040	TL_BA005---base_too_hot_TT040	heater process termination	continue procedures	TL_TT040						MAX_TEMP_BASE_PLATE	TL_BL002---MAX_TEMP_BASEPLATE	27	
	Alarm	FM455 error per channel	TLbase_TT037_error	TL_BA006---base_TT037_error	Switch off TL_HT001	continue procedures										
			TLbase_TT038_error	TL_BA007---base_TT038_error	Switch off TL_HT002											
			TLbase_TT039_error	TL_BA008---base_TT039_error	Switch off TL_HT003											
			TLbase_TT040_error	TL_BA009---base_TT040_error	Switch off TL_HT004											
Warning	Base plate too cold	TLbase_too_cold_TT037	TL_BW002---base_too_cold_TT037		continue procedures	TL_TT037							MIN_TEMP_BASE_PLATE	TL_BL003---MIN_TEMP_BASEPLATE	18	
			TLbase_too_cold_TT038	TL_BW003---base_too_cold_TT038			TL_TT038						MIN_TEMP_BASE_PLATE	TL_BL003---MIN_TEMP_BASEPLATE	18	
			TLbase_too_cold_TT039	TL_BW004---base_too_cold_TT039			TL_TT039						MIN_TEMP_BASE_PLATE	TL_BL003---MIN_TEMP_BASEPLATE	18	
			TLbase_too_cold_TT040	TL_BW005---base_too_cold_TT040			TL_TT040						MIN_TEMP_BASE_PLATE	TL_BL003---MIN_TEMP_BASEPLATE	18	
	Alarm	Base plate too hot	TRbase_too_hot_TT037	TR_BA002---base_too_hot_TT037	heater process termination	continue procedures	TR_TT037						MAX_TEMP_BASE_PLATE	TR_BL002---MAX_TEMP_BASEPLATE	27	
			TRbase_too_hot_TT038	TR_BA003---base_too_hot_TT038	heater process termination	continue procedures	TR_TT038						MAX_TEMP_BASE_PLATE	TR_BL002---MAX_TEMP_BASEPLATE	27	

			TRbase_too_hot_TT039	TR_BA004---base_too_hot_TT039	heater process termination	continue procedures	TR_TT039						MAX_TEMP_BASE_PLATE	TR_BL002---MAX TEMP_B ASEPLATE	27	
			TRbase_too_hot_TT040	TR_BA005---base_too_hot_TT040	heater process termination	continue procedures	TR_TT040						MAX_TEMP_BASE_PLATE	TR_BL002---MAX TEMP_B ASEPLATE	27	
Alarm	FM455 error per channel	TRbase_TT037_error	TR_BA006---base_TT037_error	Switch off TR_HT001	continue procedures											
		TRbase_TT038_error	TR_BA007---base_TT038_error	Switch off TR_HT002												
		TRbase_TT039_error	TR_BA008---base_TT039_error	Switch off TR_HT003												
		TRbase_TT040_error	TR_BA009---base_TT040_error	Switch off TR_HT004												
Warning	Base plate too cold	TRbase_too_cold_TT037	TR_BW002---base_too_cold_TT037		continue procedures	TR_TT037							MIN_TEMP_BASE_PLATE	TR_BL003---MIN TEMP_B ASEPLATE	18	
		TRbase_too_cold_TT038	TR_BW003---base_too_cold_TT038			TR_TT038							MIN_TEMP_BASE_PLATE	TR_BL003---MIN TEMP_B ASEPLATE	18	
		TRbase_too_cold_TT039	TR_BW004---base_too_cold_TT039			TR_TT039							MIN_TEMP_BASE_PLATE	TR_BL003---MIN TEMP_B ASEPLATE	18	
		TRbase_too_cold_TT040	TR_BW005---base_too_cold_TT040			TR_TT040							MIN_TEMP_BASE_PLATE	TR_BL003---MIN TEMP_B ASEPLATE	18	
	General FM455 alarm	Fm455_error	Tx_BA002---FM455_error													
Heater	Alarm	Tx Clixon alarm	Clixon_alarm	Tx_HA101---Clixon_alarm	Heater relais off	continue procedures	Clixon_status									1
	Alarm	TL Bridge heater too hot	bridge_htr2_too_hot_TL	TL_HA030---bridge_htr2_too_hot_TL	Bridge heater relais off	continue procedures	TL_TT045, smoke sniffer						BridgeHeater_max	Tx_HL030---BridgeHeater_max	40	
	Alarm	TL pump oil too cold	TL_HT102_too_cold	TL_HA101---HT102_too_cold	TL pump failure	restart	TL_TT122						TL_R_LR_HT102_MIN	Tx_HL101---R_LR_HT102_MIN	10	
	Alarm	TL pump oil too hot	TL_HT102_too_hot	TL_HA102---HT102_too_hot	Heater relais off	continue procedures	TL_TT122						TL_HT102_MAX	TL_HL102---HT102_MAX	50	
	Alarm	TL damper heater too hot	TL_HT103_too_hot	TL_HA103---HT103_too_hot	Heater relais off	continue procedures	TL_TT123						TL_HT103_MAX	TL_HL103---HT103_MAX	160	
	Alarm	TL by-pass heater too hot	TL_HT104_too_hot	TL_HA104---HT104_too_hot	Heater relais off, SA-failure	restart	TL_TT124						TL_HT104_MAX	TL_HL104---HT104_MAX	120	
	Alarm	TL accu heater too hot	TL_HT105_too_hot	TL_HA105---HT105_too_hot	Heater relais off	continue procedures	TL_TT125						TL_HT105_MAX	TL_HL105---HT105_MAX	160	
	Alarm	TL_HT102_thermocouple error	TL_TT122_error	TL_HA112---TT122_error	Heater relais off	continue procedures	TL_TT122_error									1
	Alarm	TL_HT103_thermocouple error	TL_TT123_error	TL_HA113---TT123_error	Heater relais off	continue procedures	TL_TT123_error									1
	Alarm	TL_HT104_thermocouple error	TL_TT124_error	TL_HA114---TT124_error	Heater relais off	continue procedures	TL_TT124_error									1
	Alarm	TL_HT105_thermocouple error	TL_TT125_error	TL_HA115---TT125_error	Heater relais off	continue procedures	TL_TT125_error									1
Warning	TL pump oil too warm	TL_HT102_hot_warning	TL_HW102---HT102_hot_warning	Switch off TL_HT102	continue procedures	TL_TT122							TL_HT102_MAX_WARN	TL_HL106---HT102_MAX_WARN	40	

	Warning	TL damper heater too warm	TL_HT103_hot_warning	TL_HW103---HT103_hot_warning	Switch off TL_HT103	continue procedures	TL_TT123						TL_HT103_MAX_WARN	TL_HL107---HT103_MAX_WARN	120
	Warning	TL by-pass heater too warm	TL_HT104_hot_warning	TL_HW104---HT104_hot_warning	Switch off TL_HT104, SA-failure	restart	TL_TT124						TL_HT104_MAX_WARN	TL_HL108---HT104_MAX_WARN	80
	Warning	TL accu heater too warm	TL_HT105_hot_warning	TL_HW105---HT105_hot_warning	Switch off TL_HT105	continue procedures	TL_TT125						TL_HT105_MAX_WARN	TL_HL109---HT105_MAX_WARN	120
	Alarm	TL Bridge heater too hot	bridge_htr1_too_hot_TR	TR_HA030---bridge_htr1_too_hot	Bridge heater relais off	continue procedures	TR_TT045_smoke_sniffer						BridgeHeater_max	Tx_HL030---BridgeHeater_max	40
	Alarm	TR pump oil too cold	TR_HT102_too_cold	TR_HA101---HT102_too_cold	TR pump failure	restart	TR_TT122						TR_R_LR_HT102_MIN	Tx_HL101---R_LR_HT102_MIN	10
	Alarm	TR pump oil too hot	TR_HT102_too_hot	TR_HA102---HT102_too_hot	Heater relais off	continue procedures	TR_TT122						TR_HT102_MAX	TR_HL102---HT102_MAX	50
	Alarm	TR damper heater too hot	TR_HT103_too_hot	TR_HA103---HT103_too_hot	Heater relais off	continue procedures	TR_TT123						TR_HT103_MAX	TR_HL103---HT103_MAX	160
	Alarm	TR by-pass heater too hot	TR_HT104_too_hot	TR_HA104---HT104_too_hot	Heater relais off, SA-failure	restart	TR_TT124						TR_HT104_MAX	TR_HL104---HT104_MAX	120
	Alarm	TR accu heater too hot	TR_HT105_too_hot	TR_HA105---HT105_too_hot	Heater relais off	continue procedures	TR_TT125						TR_HT105_MAX	TR_HL105---HT105_MAX	160
	Alarm	TR_HT102_thermocouple error	TR_TT122_error	TR_HA112---TT122_error	Heater relais off	continue procedures	TR_TT122_error								1
	Alarm	TR_HT103_thermocouple error	TR_TT123_error	TR_HA113---TT123_error	Heater relais off	continue procedures	TR_TT123_error								1
	Alarm	TR_HT104_thermocouple error	TR_TT124_error	TR_HA114---TT124_error	Heater relais off	continue procedures	TR_TT124_error								1
	Alarm	TR_HT105_thermocouple error	TR_TT125_error	TR_HA115---TT125_error	Heater relais off	continue procedures	TR_TT125_error								1
	Warning	TR pump oil too warm	TR_HT102_hot_warning	TR_HW102---HT102_hot_warning	Switch off TR_HT102	continue procedures	TR_TT122						TR_HT102_MAX_WARN	TR_HL106---HT102_MAX_WARN	40
	Warning	TR damper heater too warm	TR_HT103_hot_warning	TR_HW103---HT103_hot_warning	Switch off TR_HT103	continue procedures	TR_TT123						TR_HT103_MAX_WARN	TR_HL107---HT103_MAX_WARN	120
	Warning	TR by-pass heater too warm	TR_HT104_hot_warning	TR_HW104---HT104_hot_warning	Switch off TR_HT104, SA-failure	restart	TR_TT124						TR_HT104_MAX_WARN	TR_HL108---HT104_MAX_WARN	80
	Warning	TR accu heater too warm	TR_HT105_hot_warning	TR_HW105---HT105_hot_warning	Switch off TR_HT105	continue procedures	TR_TT125						TR_HT105_MAX_WARN	TR_HL109---HT105_MAX_WARN	120
	Alarm	TLR pump oil too cold	TLR_HT102_too_cold	TLR_HA101---HT102_too_cold	TLR pump failure	restart	TLR_TT122						TL_R_LR_HT102_MIN	Tx_HL101---R_LR_HT102_MIN	10
	Alarm	TLR pump oil too hot	TLR_HT102_too_hot	TLR_HA102---HT102_too_hot	Heater relais off	continue procedures	TLR_TT122						TLR_HT102_MAX	TLR_HL102---HT102_MAX	50
	Alarm	TLR_HT102_thermocouple error	TLR_TT122_error	TLR_HA112---TT122_error	Heater relais off	continue procedures	TLR_TT122_error								1
	Warning	TLR pump oil too warm	TLR_HT102_hot_warning	TLR_HW102---HT102_hot_warning	Switch off TLR_HT102	continue procedures	TLR_TT122						TLR_HT102_MAX_WARN	TLR_HL106---HT102_MAX_WARN	40
Pressure	Alarm	TL Pump head pressure too high	TL_PT104_TOO_HIGH	TL_PA101---PT104_TOO_HIGH	TL pump failure	restart	TL_PT104						TL_PT104_MAX	TL_PL101---PT104_MAX	85

	Alarm	TL Pump dP too high	TL_PT104_1_01_TOO_HI_GH	TL_PA102---PT104_101_TOO_HIGH	TL pump failure	restart	TL_PT104 - TL_PT101	WAIT_DISABLE_HIGHP_VL103	Tx_SC102---WAIT_DISABLE_HIGHP_VL103	20 sec	TL_sw_vl103_dis_high_p	TL_PC102---sw_vl103_dis_high_p	TL_PT104_101_MAXDIFF	TL_PL102---PT104_101_MAXDIFF	25
	Alarm	TL Pump dP too low	TL_PT104_1_01_TOO_LO_W	TL_PA103---PT104_101_TOO_LOW	TL pump failure	restart	TL_PT104 - TL_PT101	TL_MAX_STARTTIME	TL_SC103---TL_MAX_STARTTIME	5 min	TL_PM101_starttimmer	TL_PC103---PM101_starttimmer	TL_PT104_101_MINDIFF	TL_PL103---PT104_101_MINDIFF	2
								WAIT_DISABLE_LOW_P	Tx_SC104---WAIT_DISABLE_LOW_P	1 min	TL_sw_trans_dis_low_p	TL_PC104---sw_trans_dis_low_p			
								WAIT_DP_ALARM	Tx_SC105---WAIT_DP_ALARM	10 sec	TL_pump_wait_timer	TL_PC105---pump_wait_timer			
	Alarm	TL Membrane alarm	TL_PM101_membr_alarm	TL_PA106---PM101_membr_alarm	TL pump failure	restart	TL_PT103_stat_membr								1
	Alarm	TL Accu pressure too high	TL_ACCU_PRES_TOO_HI_GH	TL_PA107---ACCU_PRES_TOO_HIGH	Switch off TL_HT105	continue procedures	TL_PT102						TL_PT102_max	TL_PL107---PT102_max	68
	Alarm	TL any PT too high (closed volumes)	TL_ANY_PT_TOO_HIGH	TL_PA108---ANY_PT_TOO_HIGH	open all internal TL valves	reset procedures	TL_PT101, TL_PT102, TL_PT104						MAX_PRESS_CLOSED_VOLUME	TL_PL108---MAX_PRESS_CLOSED_VOLUME	99
	Alarm	TR Pump head pressure too high	TR_PT104_TOO_HIGH	TR_PA101---PT104_TOO_HIGH	TR pump failure	restart	TR_PT104						TR_PT104_MAX	TR_PL101---PT104_MAX	85
	Alarm	TR Pump dP too high	TR_PT104_1_01_TOO_HI_GH	TR_PA102---PT104_101_TOO_HIGH	TR pump failure	restart	TR_PT104 - TR_PT101	WAIT_DISABLE_HIGHP_VL103	Tx_SC102---WAIT_DISABLE_HIGHP_VL103	20 sec	TR_sw_vl103_dis_high_p	TR_PC102---sw_vl103_dis_high_p	TR_PT104_101_MAXDIFF	TR_PL102---PT104_101_MAXDIFF	25
	Alarm	TR Pump dP too low	TR_PT104_1_01_TOO_LO_W	TR_PA103---PT104_101_TOO_LOW	TR pump failure	restart	TR_PT104 - TR_PT101	TR_MAX_STARTTIME	TR_SC103---TR_MAX_STARTTIME	5 min	TR_PM101_starttimmer	TR_PC103---PM101_starttimmer	TR_PT104_101_MINDIFF	TR_PL103---PT104_101_MINDIFF	2
								WAIT_DISABLE_LOW_P	Tx_SC104---WAIT_DISABLE_LOW_P	1 min	TR_sw_trans_dis_low_p	TR_PC104---sw_trans_dis_low_p			
								WAIT_DP_ALARM	Tx_SC105---WAIT_DP_ALARM	10 sec	TR_pump_wait_timer	TR_PC105---pump_wait_timer			
	Alarm	TR Membrane alarm	TR_PM101_membr_alarm	TR_PA106---PM101_membr_alarm	TR pump failure	restart	TR_PT103_stat_membr								1
	Alarm	TR Accu pressure too high	TR_ACCU_PRES_TOO_HI_GH	TR_PA107---ACCU_PRES_TOO_HIGH	Switch off TR_HT105	continue procedures	TR_PT102						TR_PT102_max	TR_PL107---PT102_max	68
	Alarm	TR any PT too high (closed volumes)	TR_ANY_PT_TOO_HIGH	TR_PA108---ANY_PT_TOO_HIGH	open all internal TR valves	reset procedures	TL_PT101 or TL_PT102 or TL_PT104						MAX_PRESS_CLOSED_VOLUME	TR_PL108---MAX_PRESS_CLOSED_VOLUME	99
	Alarm	TLR Pump head pressure too high	TLR_PT104_TOO_HIGH	TLR_PA101---PT104_TOO_HIGH	TLR pump failure	restart	Tx_PT104						TLR_PT104_MAX	TLR_PL101---PT104_MAX	85

	Alarm	TLR Pump dP too high	TLR_PT104_101_TOO_HI_GH	TLR_PA102---PT104-101_TOO_HIGH	TLR pump failure	restart	Tx_PT104 - Tx_PT101	WAIT_DISABLE_HIGHPV_L103	Tx_SC102---WAIT_DISABLE_HIGHPV_L103	20 sec			TLR_PT104_101_MAXDIFF	TLR_PL102---Tx_PT104_101_MAXDIFF	25
	Alarm	TLR Pump dP too low	TLR_PT104_101_TOO_LO_W	TLR_PA103---PT104-101_TOO_LO_W	TLR pump failure	restart	Tx_PT104 - Tx_PT101	TLR_MAX_STARTTIME	TLR_SC103---TLR_MAX_S_TARTTIME	45 min	TLR_PM101_starttimer	TLR_PT104_101_MINDIFF	TLR_PL103---Tx_PT104_101_MINDIFF	2	
								WAIT_DISABLE_LOW_P	Tx_SC104---WAIT_DISABLE_LOW_P	1 min					
								WAIT_DP_A_ALARM	Tx_SC105---WAIT_DP_ALARM	10 sec					
	Alarm	TLR Membrane alarm	TLR_PM101_membr_alarm	TLR_PA106---PM101_membr_alarm	TLR pump failure	restart	TLR_PT103_stat_membr							1	
	Alarm	SA Discharge pressure too high	SA_PT108_TO_O_HIGH	SA_PA101---SA_PT108_TO_O_HIGH	SA-failure	restart	SA_PT108						Hardware setting	21.5	
	Alarm	SA Suction pressure too low	SA_PT108_TO_O_LOW	SA_PA102---SA_PT108_TO_O_LOW	SA-failure	restart	SA_PT108						Hardware setting	0.55	
	Alarm	SA liquid in compressor	SA_COMPRLIQUID_IN	SA_PA103---SA_COMPRLIQUID_IN	SA-failure	restart	SA_TT121 - SA_PT107_TSAT	SA_MAX_S_TARTTIME	SA_SC103---SA_MAX_STARTTIME	5 min	SA_PM101_starttimer	SA_PC103---PM101_starttimer			
								SA_WAIT_LIQUID_ALARM	SA_SC104---SA_WAIT_LIQUID_ALARM	30 sec	SA_wait_liquid_alarm	SA_PC104---wait_liquid_alarm	DIFF_SA_TT121_PT107_TSAT	2	
	Alarm	SB Discharge pressure too high	SB_PT108_TO_O_HIGH	SB_PA101---SB_PT108_TO_O_HIGH	SB-failure	restart	SB_PT108						Hardware setting	19.5	
	Alarm	SB Suction pressure too low	SB_PT108_TO_O_LOW	SB_PA102---SB_PT108_TO_O_LOW	SB-failure	restart	SB_PT108						Hardware setting	0.8	
	Alarm	SB liquid in compressor	SB_COMPRLIQUID_IN	SB_PA103---SB_COMPRLIQUID_IN	SB-failure	restart	SB_TT121 - SB_PT107_TSAT	SB_MAX_S_TARTTIME	SB_SC103---SB_MAX_STARTTIME	5 min	SB_PM101_starttimer	SB_PC103---PM101_starttimer			
								SB_WAIT_LIQUID_ALARM	SB_SC104---SB_WAIT_LIQUID_ALARM	30 sec	SB_wait_liquid_alarm	SB_PC104---wait_liquid_alarm	DIFF_SB_TT121_PT103_TSAT	2	
													DIFF_SB_TT121_PT104_TSAT	2	
Miscalaneou	Warning	TL Maximum set point reached	TL_accu_max_setpoint	TL_MW101---accu_max_setpoint	Saturate set point	continue procedures	TL_PT102						TL_max_accu_setp	TL_ML101---max_accu_setp	26
	Warning	TL Accu timeout	TL_accu_timeout	TL_MW102---accu_timeout_alarm	none	continue procedures	TL_PT102	TIMEOUT_ACCU_HTR	Tx_SC101---TIMEOUT_ACCU_HTR	30 min	TL_ACCU_TIMER	TL_MC102---ACCU_TIMER			
	Alarm	TL CO <sub>2</sub> frost alarm due to SA	TL_CO2_frost_alarm	TL_MA101---CO <sub>2</sub> _frost_alarm	SA-failure	restart	TL_TT112						CO <sub>2</sub> _lowest_temp	Tx_ML101---CO <sub>2</sub> _lowest_temp	-50



	Alarm	SA power group failure	exd1311_pwr(SA)_alarm	xx_MA101--- exd1311_pwr(SA)_alarm	SA-failure	restart	exd1311_pwrd(SA), exd1311_notpwr(SA)								
	Alarm	By-pass heater power failure	exd1306_pwr(htr)_alarm	xx_MA102--- exd1306_pwr(htr)_alarm	If used then SA-failure	If used then restart	exd1306_pwrd(heaters), exd1306_notpwr(heaters), tl_cooldown_power_by_pass, tr_cooldown_power_by_pass								
	Alarm	Diesel group power failure	esd205_pwr(diesel)_alarm	xx_MA103--- esd205_pwr(diesel)_alarm		reset procedures	esd205_pwr(diesel), esd205_notpwr(diesel)	xx-SC103--- WAIT_POWER_RETURN			xx_MC103--- PowerReturnTimer				
	Alarm	CO <sub>2</sub> vent alarm	venting_alarm	xx_MA104--- venting_alarm	Global enable off	reset procedures	Vacuum system					Hardware setting		1150 mbar	
	Alarm	General Haptas alarm	haptas_alarm	xx_MA105--- haptas_alarm		continue procedures									
	Alarm	TL Haptas alarm	TL_haptas_error_vector	TL_MA105--- haptas_error_vector		continue procedures					TL_haptas_timer	TL_MC105--- haptas_timer			
	Alarm	TR Haptas alarm	TR_haptas_error_vector	TR_MA105--- haptas_error_vector		continue procedures					TR_haptas_timer	TR_MC105--- haptas_timer			
	Alarm	TLR Haptas alarm	TLR_haptas_error_vector	TLR_MA105--- haptas_error_vector		continue procedures					TLR_haptas_timer	TLR_MC105--- haptas_timer			
Valve	Alarm	TL_VL102 timeout	TL_VL102_alarm	TL_VA102--- VL102_alarm		continue, procedure maybe get stucked	TIMEOUT_2 WAY_VALVE	Tx_SC106--- TIMEOUT_2 WAY_VALVE	5 sec	TL_VL102_timer	TL_VC102--- VL102_timer				
	Alarm	TL_VL103 timeout	TL_VL103_alarm	TL_VA103--- VL103_alarm		continue, procedure maybe get stucked	TIMEOUT_3 WAY_VALVE	Tx_SC107--- TIMEOUT_3 WAY_VALVE	10 sec	TL_VL103_timer	TL_VC103--- VL103_timer				
	Alarm	TL_VL104 timeout	TL_VL104_alarm	TL_VA104--- VL104_alarm		continue, procedure maybe get stucked	TIMEOUT_2 WAY_VALVE	Tx_SC106--- TIMEOUT_2 WAY_VALVE	5 sec	TL_VL104_timer	TL_VC104--- VL104_timer				
	Alarm	TL_VL109 timeout	TL_VL109_alarm	TL_VA109--- VL109_alarm		continue, procedure maybe get stucked	TIMEOUT_2 WAY_VALVE	Tx_SC106--- TIMEOUT_2 WAY_VALVE	5 sec	TL_VL109_timer	TL_VC109--- VL109_timer				
	Alarm	TL_VL111 timeout	TL_VL111_alarm	TL_VA111--- VL111_alarm		continue, procedure maybe get stucked	TIMEOUT_2 WAY_VALVE	Tx_SC106--- TIMEOUT_2 WAY_VALVE	5 sec	TL_VL111_timer	TL_VC111--- VL111_timer				
	Alarm	TL_VL112 timeout	TL_VL112_alarm	TL_VA112--- VL112_alarm		continue, procedure maybe get stucked	TIMEOUT_2 WAY_VALVE	Tx_SC106--- TIMEOUT_2 WAY_VALVE	5 sec	TL_VL112_timer	TL_VC112--- VL112_timer				

	Alarm	TR_VL102 timeout	TR_VL102_alarm	TR_VA102---VL102_alarm		continue, procedure maybe get stucked		TIMEOUT_2 WAY_VALVE	Tx_SC106---TIMEOUT_2 WAY_VALVE	5 sec	TR_VL102_timer	TR_VC102---VL102_timer	
	Alarm	TR_VL103 timeout	TR_VL103_alarm	TR_VA103---VL103_alarm		continue, procedure maybe get stucked		TIMEOUT_3 WAY_VALVE	Tx_SC107---TIMEOUT_3 WAY_VALVE	10 sec	TR_VL103_timer	TR_VC103---VL103_timer	
	Alarm	TR_VL104 timeout	TR_VL104_alarm	TR_VA104---VL104_alarm		continue, procedure maybe get stucked		TIMEOUT_2 WAY_VALVE	Tx_SC106---TIMEOUT_2 WAY_VALVE	5 sec	TR_VL104_timer	TR_VC104---VL104_timer	
	Alarm	TR_VL108 timeout	TR_VL108_alarm	TR_VA108---VL108_alarm		continue, procedure maybe get stucked		TIMEOUT_3 WAY_VALVE	Tx_SC107---TIMEOUT_3 WAY_VALVE	10 sec	TR_VL108_timer	TR_VC108---VL108_timer	
	Alarm	TR_VL109 timeout	TR_VL109_alarm	TR_VA109---VL109_alarm		continue, procedure maybe get stucked		TIMEOUT_2 WAY_VALVE	Tx_SC106---TIMEOUT_2 WAY_VALVE	5 sec	TR_VL109_timer	TR_VC109---VL109_timer	
	Alarm	TR_VL111 timeout	TR_VL111_alarm	TR_VA111---VL111_alarm		continue, procedure maybe get stucked		TIMEOUT_2 WAY_VALVE	Tx_SC106---TIMEOUT_2 WAY_VALVE	5 sec	TR_VL111_timer	TR_VC111---VL111_timer	
	Alarm	TR_VL112 timeout	TR_VL112_alarm	TR_VA112---VL112_alarm		continue, procedure maybe get stucked		TIMEOUT_2 WAY_VALVE	Tx_SC106---TIMEOUT_2 WAY_VALVE	5 sec	TR_VL112_timer	TR_VC112---VL112_timer	
	Alarm	TLR_VL101 timeout	TLR_VL101_alarm	TLR_VA101---VL101_alarm		continue, procedure maybe get stucked		TIMEOUT_2 WAY_VALVE	Tx_SC106---TIMEOUT_2 WAY_VALVE	5 sec	TLR_VL101_timer	TLR_VC101---VL101_timer	
	Alarm	TLR_VL109 timeout	TLR_VL109_alarm	TLR_VA109---VL109_alarm		continue, procedure maybe get stucked		TIMEOUT_3 WAY_VALVE	Tx_SC107---TIMEOUT_3 WAY_VALVE	10 sec	TLR_VL109_timer	TLR_VC109---VL109_timer	
	Alarm	TLR_VL110 timeout	TLR_VL110_alarm	TLR_VA110---VL110_alarm		continue, procedure maybe get stucked		TIMEOUT_3 WAY_VALVE	Tx_SC107---TIMEOUT_3 WAY_VALVE	10 sec	TLR_VL110_timer	TLR_VC110---VL110_timer	
	Alarm	TLR_VL111 timeout	TLR_VL111_alarm	TLR_VA111---VL111_alarm		continue, procedure maybe get stucked		TIMEOUT_2 WAY_VALVE	Tx_SC106---TIMEOUT_2 WAY_VALVE	5 sec	TLR_VL111_timer	TLR_VC111---VL111_timer	

## 11.7 PVSS logging of variables.

Most of the PLC variables are exported to PVSS for monitoring or logging. Most of the variables can be monitored using a preset trending page. The trending pages can be viewed by starting the trending monitor on one of the online computers using the following link: [G:\online\ecs\Shortcuts38\VELOVEDCSVMC\VEDCSVMC\\_UI\\_fwTrending.lnk](G:\online\ecs\Shortcuts38\VELOVEDCSVMC\VEDCSVMC_UI_fwTrending.lnk). Under the tree node **VEDCSVMC:VTCS\_DataExport** preset pages can be viewed. Table 11.7-3 shows the PVSS data points and the corresponding pages. From these pages CSV files can be exported for cooling data analyses.

Table 11.7-1: Sensor labeling and location of the A side detector

		Silicon Type	Module Number #	Temperature Board#	Repeater Location 1	Repeater Location 2	NTC00 (Cookie)	NTC01 (Silicon)	LV Branch Controller	LV Easycrate	LV Easyboard	LV channel	NTC00 label for cooling analyzes	NTC01 label for cooling analyzes	LV label for Cooling Analyses	VTCS heat exchanger #	VTCS Inlet tube sensor #	VTCS 1st cookie sensor #	VTCS last cookie sensor #	VTCS Outlet tube sensor #
PU01_A	B	R		1	0	1	2	3	9	2	4	0	VL_TT102	VL_TT103	VL_HT101	TL_HX001	TL_TT001	TL_TT002	TL_TT003	TL_TT004
PU02_A	T	R		1	4	5	6	7	9	2	4	0	VL_TT106	VL_TT107	VL_HT102	TL_HX002				TL_TT005
VL01_A	B	R		1	12	13	14	15	9	2	4	9	VL_TT114	VL_TT115	VL_HT103					TL_TT006
	T	Phi		1	8	9	10	11	9	2	4	6	VL_TT110	VL_TT111	VL_HT103	TL_HX003				TL_TT007
VL02_A	B	Phi		1	20	21	22	23	9	0	0	3	VL_TT122	VL_TT123	VL_HT104					TL_TT008
	T	R		1	16	17	18	19	9	0	0	0	VL_TT118	VL_TT119	VL_HT104	TL_HX004				TL_TT009
VL03_A	B	R		1	28	29	30	31	9	0	0	9	VL_TT130	VL_TT131	VL_HT105					TL_TT010
	T	Phi		1	24	25	26	27	9	0	0	6	VL_TT126	VL_TT127	VL_HT205	TL_HX005				TL_TT011
VL04_A	B	Phi		1	36	37	38	39	9	0	4	3	VL_TT138	VL_TT139	VL_HT106					TL_TT012
VL05_A	B	R		1	44	45	46	47	9	0	4	9	VL_TT146	VL_TT147	VL_HT107					TL_TT013
	T	Phi		1	40	41	42	43	9	0	4	6	VL_TT142	VL_TT143	VL_HT207	TL_HX007				TL_TT014
VL06_A	B	Phi		1	52	53	54	55	9	0	8	3	VL_TT154	VL_TT155	VL_HT108					TL_TT015
	T	R		1	48	49	50	51	9	0	8	0	VL_TT150	VL_TT151	VL_HT108	TL_HX008				TL_TT016
VL07_A	B	R		1	60	61	62	63	9	0	8	9	VL_TT162	VL_TT163	VL_HT109					TL_TT017
	T	Phi		1	56	57	58	59	9	0	8	6	VL_TT158	VL_TT159	VL_HT209	TL_HX009				TL_TT018
VL08_A	B	Phi		2	4	5	6	7	9	0	12	3	VL_TT206	VL_TT207	VL_HT110					TL_TT019
	T	R		2	0	1	2	3	9	0	12	0	VL_TT202	VL_TT203	VL_HT210	TL_HX010				TL_TT020
VL09_A	B	R		2	12	13	14	15	9	0	12	9	VL_TT214	VL_TT215	VL_HT111					TL_TT021
	T	Phi		2	8	9	10	11	9	0	12	6	VL_TT210	VL_TT211	VL_HT211	TL_HX011				TL_TT022
VL10_A	B	Phi		2	20	21	22	23	9	0	16	3	VL_TT222	VL_TT223	VL_HT112					TL_TT023
	T	R		2	16	17	18	19	9	0	16	0	VL_TT218	VL_TT219	VL_HT212	TL_HX012	TL_TT015	TL_TT016	TL_TT017	TL_TT018
VL11_A	B	R		2	28	29	30	31	9	0	16	9	VL_TT230	VL_TT231	VL_HT113					TL_TT019
	T	Phi		2	24	25	26	27	9	0	16	6	VL_TT226	VL_TT227	VL_HT213	TL_HX013				TL_TT020
VL12_A	B	Phi		2	36	37	38	39	9	1	0	3	VL_TT238	VL_TT239	VL_HT114					TL_TT021
	T	R		2	32	33	34	35	9	1	0	0	VL_TT234	VL_TT235	VL_HT214	TL_HX014				TL_TT022
VL13_A	B	R		2	44	45	46	47	9	1	0	9	VL_TT246	VL_TT247	VL_HT115					TL_TT023
	T	Phi		2	40	41	42	43	9	1	0	6	VL_TT242	VL_TT243	VL_HT215	TL_HX015				TL_TT024
VL14_A	B	Phi		2	52	53	54	55	9	1	4	3	VL_TT254	VL_TT255	VL_HT116					TL_TT025
	T	R		2	48	49	50	51	9	1	4	0	VL_TT250	VL_TT251	VL_HT216	TL_HX016				TL_TT026
VL15_A	B	R		2	60	61	62	63	9	1	4	9	VL_TT262	VL_TT263	VL_HT117					TL_TT027
	T	Phi		2	56	57	58	59	9	1	4	6	VL_TT258	VL_TT259	VL_HT217	TL_HX017				TL_TT028
VL16_A	B	Phi		3	4	5	6	7	9	1	8	3	VL_TT306	VL_TT307	VL_HT118					TL_TT029
	T	R		3	0	1	2	3	9	1	8	0	VL_TT302	VL_TT303	VL_HT218	TL_HX018				TL_TT030
VL17_A																			TL_HX019	
VL18_A																			TL_HX020	
VL19_A	B	R		3	12	13	14	15	9	1	8	9	VL_TT314	VL_TT315	VL_HT121					TL_TT025
	T	Phi		3	8	9	10	11	9	1	8	6	VL_TT310	VL_TT311	VL_HT221	TL_HX021				TL_TT026
VL20_A																			TL_HX022	
VL21_A																			TL_HX023	
VL22_A	B	Phi		3	20	21	22	23	9	1	12	3	VL_TT322	VL_TT323	VL_HT124					
	T	R		3	16	17	18	19	9	1	12	0	VL_TT318	VL_TT319	VL_HT224	TL_HX024				TL_TT026
VL23_A	B	R		3	28	29	30	31	9	1	12	9	VL_TT330	VL_TT331	VL_HT125					
	T	Phi		3	24	25	26	27	9	1	12	6	VL_TT326	VL_TT327	VL_HT225	TL_HX025				TL_TT027
VL24_A	B	Phi		3	36	37	38	39	9	1	16	3	VL_TT338	VL_TT339	VL_HT126					TL_TT028
	T	R		3	32	33	34	35	9	1	16	0	VL_TT334	VL_TT335	VL_HT226	TL_HX026				TL_TT029
VL25_A	B	R		3	44	45	46	47	9	1	16	9	VL_TT346	VL_TT347	VL_HT127					TL_TT030
	T	Phi		3	40	41	42	43	9	1	16	6	VL_TT342	VL_TT343	VL_HT227	TL_HX027	TL_TT029	TL_TT030	TL_TT031	TL_TT032

Table 11.7-2: Sensor labeling and location of the C side detector

			Silicon Type	Module Number #	Temperature Board#	Repeater Location 1	Repeater Location 2	NTC00 (Cookie)	NTC01 (Silicon)	LV Branch Controller	LV Easyboard	LV Easyboard	LV Current channel	NTC00 label for cooling analyzes	NTC01 label for cooling analyzes	VTCS heat exchanger #	VTCS Inlet tube sensor #	VTCS 1st cookie sensor #	VTCS last cookie sensor #	VTCS Outlet tube sensor #
PU01_C	T	R		1	0	1	2							VR_TT102	VR_TT103	VR_HT101				
PU02_C	B	R		1	4	5	6	7	9	2	0	3	VR_TT106	VR_TT107	VR_HT102	TR_HX001	TR_TT001	TR_TT002	TR_TT003	TR_TT004
VL01_C	T	Phi	36	1	8	9	10	11	9	2	0	6	VR_TT110	VR_TT111	VR_HF103					
	B	R		1	12	13	14	15	9	2	0	9	VR_TT114	VR_TT115	VR_HT203	TR_HX003				
VL02_C	T	R	32	1	16	17	18	19	6	0	0	0	VR_TT118	VR_TT119	VR_HT104					
	B	Phi		1	20	21	22	23	6	0	0	3	VR_TT122	VR_TT123	VR_HT204	TR_HX004				
VL03_C	T	Phi	51	1	24	25	26	27	6	0	0	6	VR_TT126	VR_TT127	VR_HT105					
	B	R		1	28	29	30	31	6	0	0	9	VR_TT130	VR_TT131	VR_HT205	TR_HX005				
VL04_C	T	R	45	1	32	33	34	35	6	0	4	0	VR_TT134	VR_TT135	VR_HT106					
	B	Phi		1	36	37	38	39	6	0	4	3	VR_TT138	VR_TT139	VR_HT206	TR_HX006				
VL05_C	T	Phi	50	1	40	41	42	43	6	0	4	6	VR_TT142	VR_TT143	VR_HT107					
	B	R		1	44	45	46	47	6	0	4	9	VR_TT146	VR_TT147	VR_HT207	TR_HX007				
VL06_C	T	R	42	1	48	49	50	51	6	0	8	0	VR_TT150	VR_TT151	VR_HT108					
	B	Phi		1	52	53	54	55	6	0	8	3	VR_TT154	VR_TT155	VR_HT208	TR_HX008				
VL07_C	T	Phi	33	1	56	57	58	59	6	0	8	6	VR_TT158	VR_TT159	VR_HT109					
	B	R		1	60	61	62	63	6	0	8	9	VR_TT162	VR_TT163	VR_HT209	TR_HX009				
VL08_C	T	R	38	2	0	1	2	3	6	0	12	0	VR_TT202	VR_TT203	VR_HT110					
	B	Phi		2	4	5	6	7	6	0	12	3	VR_TT206	VR_TT207	VR_HT210	TR_HX010				
VL09_C	T	Phi	44	2	8	9	10	11	6	0	12	6	VR_TT210	VR_TT211	VR_HT111					
	B	R		2	12	13	14	15	6	0	12	9	VR_TT214	VR_TT215	VR_HT211	TR_HX011				
VL10_C	T	R	35	2	16	17	18	19	6	0	16	0	VR_TT218	VR_TT219	VR_HT212					
	B	Phi		2	20	21	22	23	6	0	16	3	VR_TT222	VR_TT223	VR_HT212	TR_HX012	TR_TT015	TR_TT016	TR_TT017	TR_TT018
VL11_C	T	Phi	55	2	24	25	26	27	6	0	16	6	VR_TT226	VR_TT227	VR_HT113					
	B	R		2	28	29	30	31	6	0	16	9	VR_TT230	VR_TT231	VR_HT213	TR_HX013				
VL12_C	T	R	25	2	32	33	34	35	6	1	0	0	VR_TT234	VR_TT235	VR_HT114					
	B	Phi		2	36	37	38	39	6	1	0	3	VR_TT238	VR_TT239	VR_HT214	TR_HX014				
VL13_C	T	Phi	29	2	40	41	42	43	6	1	0	6	VR_TT242	VR_TT243	VR_HT115					
	B	R		2	44	45	46	47	6	1	0	9	VR_TT246	VR_TT247	VR_HT215	TR_HX015				
VL14_C	T	R	23	2	48	49	50	51	6	1	4	0	VR_TT250	VR_TT251	VR_HT116					
	B	Phi		2	52	53	54	55	6	1	4	3	VR_TT254	VR_TT255	VR_HT216	TR_HX016				
VL15_C	T	Phi	31	2	56	57	58	59	6	1	4	6	VR_TT258	VR_TT259	VR_HT117					
	B	R		2	60	61	62	63	6	1	4	9	VR_TT262	VR_TT263	VR_HT217	TR_HX017				
VL16_C	T	R	30	3	0	1	2	3	6	1	8	0	VR_TT302	VR_TT303	VR_HT118					
	B	Phi		3	4	5	6	7	6	1	8	3	VR_TT306	VR_TT307	VR_HT218	TR_HX018				
VL17_C																TR_HX019				
VL18_C																TR_HX020				
VL19_C	T	Phi	52	3	8	9	10	11	6	1	8	6	VR_TT310	VR_TT311	VR_HT121					
	B	R		3	12	13	14	15	6	1	8	9	VR_TT314	VR_TT315	VR_HT221	TR_HX021				
VL20_C																TR_HX022				
VL21_C																TR_HX023				
VL22_C	T	R	37	3	16	17	18	19	6	1	12	0	VR_TT318	VR_TT319	VR_HT124					
	B	Phi		3	20	21	22	23	6	1	12	3	VR_TT322	VR_TT323	VR_HT224	TR_HX024				
VL23_C	T	Phi	27	3	24	25	26	27	6	1	12	6	VR_TT326	VR_TT327	VR_HT125					
	B	R		3	28	29	30	31	6	1	12	9	VR_TT330	VR_TT331	VR_HT225	TR_HX025				
VL24_C	T	R	24	3	32	33	34	35	6	1	16	0	VR_TT334	VR_TT335	VR_HT126					
	B	Phi		3	36	37	38	39	6	1	16	3	VR_TT338	VR_TT339	VR_HT226	TR_HX026				
VL25_C	T	Phi	28	3	40	41	42	43	6	1	16	6	VR_TT342	VR_TT343	VR_HT127					
	B	R		3	44	45	46	47	6	1	16	9	VR_TT346	VR_TT347	VR_HT227	TR_HX027	TR_TT029	TR_TT030	TR_TT031	TR_TT032

Table 11.7-3: PVSS data points , corresponding monitoring pages and export labels.

PVSS label	PVSS identifier	Value	PVSS Data Point	PVSS Trending page	CSV export label
sniffer_overruled	StateBit	state	VEDCSVMC:VTCS_sniffer_overruled.state	PLC_States_1	IL_SNFov.stat
chilled_water_overruled	StateBit	state	VEDCSVMC:VTCS_chilled_water_overruled.state	PLC_States_1	IL_CHWov.stat
allowcooling_a_overruled	StateBit	state	VEDCSVMC:VTCS_allowcooling_a_overruled.state	PLC_States_1	IL_ALAov.stat
allowcooling_c_overruled	StateBit	state	VEDCSVMC:VTCS_allowcooling_c_overruled.state	PLC_States_1	IL_ALCov.stat
vacuum_ok_overruled	StateBit	state	VEDCSVMC:VTCS_vacuum_ok_overruled.state	PLC_States_1	IL_VACov.stat
coolingoff2vac_overruled	StateBit	state	VEDCSVMC:VTCS_coolingoff2vac_overruled.state	PLC_States_1	IL_C2Vov.stat
cooling_rdy_a_overruled	StateBit	state	VEDCSVMC:VTCS_cooling_rdy_a_overruled.state	PLC_States_1	IL_CRAov.stat
cooling_rdy_c_overruled	StateBit	state	VEDCSVMC:VTCS_cooling_rdy_c_overruled.state	PLC_States_1	IL_CRCov.stat
sniffer_ok	StateBit	state	VEDCSVMC:VTCS_sniffer_ok.state	PLC_States_1	IL_SNFok.stat
chilled_water_ok	StateBit	state	VEDCSVMC:VTCS_chilled_water_ok.state	PLC_States_1	IL_CHWok.stat
allowcooling_a	StateBit	state	VEDCSVMC:VTCS_allowcooling_a.state	PLC_States_1	IL_ALAok.stat
allowcooling_c	StateBit	state	VEDCSVMC:VTCS_allowcooling_c.state	PLC_States_1	IL_ALCok.stat
vacuum_ok	StateBit	state	VEDCSVMC:VTCS_vacuum_ok.state	PLC_States_1	IL_VACok.stat
coolingoff_to_vacuum	StateBit	state	VEDCSVMC:VTCS_coolingoff_to_vacuum.state	PLC_States_1	IL_C2Vok.stat
cooling_rdy_a	StateBit	state	VEDCSVMC:VTCS_cooling_rdy_a.state	PLC_States_1	IL_CRAok.stat
cooling_rdy_c	StateBit	state	VEDCSVMC:VTCS_cooling_rdy_c.state	PLC_States_1	IL_CRCok.stat
intlck_smoke_alert	StateBit	state	VEDCSVMC:VTCS_intlck_smoke_alert.state	PLC_States_1	IL_SNFa.stat
intlck_water_alert	StateBit	state	VEDCSVMC:VTCS_intlck_water_alert.state	PLC_States_1	IL_CHWa.stat
intlck_allowCoolA_alert	StateBit	state	VEDCSVMC:VTCS_intlck_allowCoolA_alert.state	PLC_States_1	IL_ALAal.stat
intlck_allowCoolC_alert	StateBit	state	VEDCSVMC:VTCS_intlck_allowCoolC_alert.state	PLC_States_1	IL_ALCal.stat
intlck_vacuum_alert	StateBit	state	VEDCSVMC:VTCS_intlck_vacuum_alert.state	PLC_States_1	IL_VACal.stat
global_enable	StateBit	state	VEDCSVMC:VTCS_global_enable.state	PLC_States_1	IL_GLBen.stat
venting_alarm	StateBit	state	VEDCSVMC:VTCS_venting_alarm.state	PLC_States_1	IL_VENal.stat
Aside_CO2status	StateDword	state	VEDCSVMC:VTCS_Aside_CO2status.state		
Cside_CO2status	StateDword	state	VEDCSVMC:VTCS_Cside_CO2status.state		
Chiller_status	StateDword	state	VEDCSVMC:VTCS_Chiller_status.state		
TL_valves2default_proc	StateDword	state	VEDCSVMC:VTCS_TL_valves2default_proc.state		
TR_valves2default_proc	StateDword	state	VEDCSVMC:VTCS_TR_valves2default_proc.state		
TLR_valves2default_proc	StateDword	state	VEDCSVMC:VTCS_TLR_valves2default_proc.state		
SwitchTransferLine_proc	StateDword	state	VEDCSVMC:VTCS_SwitchTransferLine_proc.state		
SASBswitchover_proc	StateWord	state	VEDCSVMC:VTCS_SASBswitchover_proc.state		
TLLTRswitchover_proc	StateWord	state	VEDCSVMC:VTCS_TLLTRswitchover_proc.state		
TRTLLTRswitchover_proc	StateWord	state	VEDCSVMC:VTCS_TRTLLTRswitchover_proc.state		
TLRswitchoff_proc	StateWord	state	VEDCSVMC:VTCS_TLRswitchoff_proc.state		
TL_CoolingOn	StateBit	state	VEDCSVMC:VTCS_TL_CoolingOn.state	PLC_States_1	TL_STcon.stat
TL_OverBypass	StateBit	state	VEDCSVMC:VTCS_TL_OverBypass.state	PLC_States_1	TL_ST2bp.stat
TL_overTLPump	StateBit	state	VEDCSVMC:VTCS_TL_overTLPump.state	PLC_States_1	TL_ST2lp.stat
TL_overTLRpump	StateBit	state	VEDCSVMC:VTCS_TL_overTLRpump.state	PLC_States_1	TL_ST2mp.stat
TL_overSA	StateBit	state	VEDCSVMC:VTCS_TL_overSA.state	PLC_States_1	TL_ST2sA.stat
TL_overSB	StateBit	state	VEDCSVMC:VTCS_TL_overSB.state	PLC_States_1	TL_ST2sB.stat
TL_overBridgeHeater	StateBit	state	VEDCSVMC:VTCS_TL_overBridgeHeater.state	PLC_States_1	TL_ST2bh.stat
TL_AccuCoolingSA	StateBit	state	VEDCSVMC:VTCS_TL_AccuCoolingSA.state	PLC_States_1	TL_STacA.stat
TL_AccuCoolingSB	StateBit	state	VEDCSVMC:VTCS_TL_AccuCoolingSB.state	PLC_States_1	TL_STacB.stat

TR_CoolingOn	StateBit	state	VEDCSVMC:VTCS_TR_CoolingOn.state	PLC_States_1	TR_STcon.stat
TR_OverBypass	StateBit	state	VEDCSVMC:VTCS_TR_OverBypass.state	PLC_States_1	TR_ST2bp.stat
TR_overTRpump	StateBit	state	VEDCSVMC:VTCS_TR_overTRpump.state	PLC_States_1	TR_ST2lp.stat
TR_overTRRpump	StateBit	state	VEDCSVMC:VTCS_TR_overTRRpump.state	PLC_States_1	TR_ST2mp.stat
TR_overSA	StateBit	state	VEDCSVMC:VTCS_TR_overSA.state	PLC_States_1	TR_ST2sA.stat
TR_overSB	StateBit	state	VEDCSVMC:VTCS_TR_overSB.state	PLC_States_1	TR_ST2sB.stat
TR_overBridgeHeater	StateBit	state	VEDCSVMC:VTCS_TR_overBridgeHeater.state	PLC_States_1	TR_ST2bh.stat
TR_AccuCoolingSA	StateBit	state	VEDCSVMC:VTCS_TR_AccuCoolingSA.state	PLC_States_1	TR_STacA.stat
TR_AccuCoolingSB	StateBit	state	VEDCSVMC:VTCS_TR_AccuCoolingSB.state	PLC_States_1	TR_STacB.stat
TLR_PumpClaimed	StateBit	state	VEDCSVMC:VTCS_TLR_PumpClaimed.state	PLC_States_1	TM_STpCL.stat
SA_CoolingOn	StateBit	state	VEDCSVMC:VTCS_SA_CoolingOn.state	PLC_States_1	SA_ST101.stat
SB_CoolingOn	StateBit	state	VEDCSVMC:VTCS_SB_CoolingOn.state	PLC_States_1	SB_ST101.stat
PVSS_FSM_A_OFF	StateBit	state	VEDCSVMC:VTCS_PVSS_FSM_A_OFF.state	PLC_States_2	PV_FSM01.stat
PVSS_FSM_A_STARTINGUP	StateBit	state	VEDCSVMC:VTCS_PVSS_FSM_A_STARTINGUP.state	PLC_States_2	PV_FSM02.stat
PVSS_FSM_A_READY	StateBit	state	VEDCSVMC:VTCS_PVSS_FSM_A_READY.state	PLC_States_2	PV_FSM03.stat
PVSS_FSM_A_ERROR	StateBit	state	VEDCSVMC:VTCS_PVSS_FSM_A_ERROR.state	PLC_States_2	PV_FSM04.stat
PVSS_FSM_C_OFF	StateBit	state	VEDCSVMC:VTCS_PVSS_FSM_C_OFF.state	PLC_States_2	PV_FSM05.stat
PVSS_FSM_C_STARTINGUP	StateBit	state	VEDCSVMC:VTCS_PVSS_FSM_C_STARTINGUP.state	PLC_States_2	PV_FSM06.stat
PVSS_FSM_C_READY	StateBit	state	VEDCSVMC:VTCS_PVSS_FSM_C_READY.state	PLC_States_2	PV_FSM07.stat
PVSS_FSM_C_ERROR	StateBit	state	VEDCSVMC:VTCS_PVSS_FSM_C_ERROR.state	PLC_States_2	PV_FSM08.stat
CO <sub>2</sub> _TL_mode	StateByte	state	VEDCSVMC:VTCS_CO <sub>2</sub> _TL_mode.state		
CO <sub>2</sub> _TR_mode	StateByte	state	VEDCSVMC:VTCS_CO <sub>2</sub> _TR_mode.state		
TLR_PM101_mode	StateByte	state	VEDCSVMC:VTCS_TLR_PM101_mode.state		
SA_mode	StateByte	state	VEDCSVMC:VTCS_SA_mode.state		
SB_mode	StateByte	state	VEDCSVMC:VTCS_SB_mode.state		
dr_an1_0	MiscalaneousBytes	byte	VEDCSVMC:VTCS_dr_an1_0.byte		
dr_an1_1	MiscalaneousBytes	byte	VEDCSVMC:VTCS_dr_an1_1.byte		
dr_an1_2	MiscalaneousBytes	byte	VEDCSVMC:VTCS_dr_an1_2.byte		
dr_an1_3	MiscalaneousBytes	byte	VEDCSVMC:VTCS_dr_an1_3.byte		
dr_an1_4	MiscalaneousBytes	byte	VEDCSVMC:VTCS_dr_an1_4.byte		
dr_an1_5	MiscalaneousBytes	byte	VEDCSVMC:VTCS_dr_an1_5.byte		
dr_an1_6	MiscalaneousBytes	byte	VEDCSVMC:VTCS_dr_an1_6.byte		
dr_an1_7	MiscalaneousBytes	byte	VEDCSVMC:VTCS_dr_an1_7.byte		
dr_an1_8	MiscalaneousBytes	byte	VEDCSVMC:VTCS_dr_an1_8.byte		
dr_an1_9	MiscalaneousBytes	byte	VEDCSVMC:VTCS_dr_an1_9.byte		
dr_an1_10	MiscalaneousBytes	byte	VEDCSVMC:VTCS_dr_an1_10.byte		
dr_an1_11	MiscalaneousBytes	byte	VEDCSVMC:VTCS_dr_an1_11.byte		
dr_an1_12	MiscalaneousBytes	byte	VEDCSVMC:VTCS_dr_an1_12.byte		
dr_an1_13	MiscalaneousBytes	byte	VEDCSVMC:VTCS_dr_an1_13.byte		
dr_an1_14	MiscalaneousBytes	byte	VEDCSVMC:VTCS_dr_an1_14.byte		
dr_an1_15	MiscalaneousBytes	byte	VEDCSVMC:VTCS_dr_an1_15.byte		
dr_an1_16	MiscalaneousBytes	byte	VEDCSVMC:VTCS_dr_an1_16.byte		
dr_an1_17	MiscalaneousBytes	byte	VEDCSVMC:VTCS_dr_an1_17.byte		
dr_an1_18	MiscalaneousBytes	byte	VEDCSVMC:VTCS_dr_an1_18.byte		
dr_an1_19	MiscalaneousBytes	byte	VEDCSVMC:VTCS_dr_an1_19.byte		
dr_an1_20	MiscalaneousBytes	byte	VEDCSVMC:VTCS_dr_an1_20.byte		
dr_an1_21	MiscalaneousBytes	byte	VEDCSVMC:VTCS_dr_an1_21.byte		
dr_an1_22	MiscalaneousBytes	byte	VEDCSVMC:VTCS_dr_an1_22.byte		
dr_an1_23	MiscalaneousBytes	byte	VEDCSVMC:VTCS_dr_an1_23.byte		

dr_an1_24	MiscalaneousBytes	byte	VEDCSVMC:VTCS_dr_an1_24.byte		
dr_an2_0	MiscalaneousBytes	byte	VEDCSVMC:VTCS_dr_an2_0.byte		
dr_an2_1	MiscalaneousBytes	byte	VEDCSVMC:VTCS_dr_an2_1.byte		
dr_an2_2	MiscalaneousBytes	byte	VEDCSVMC:VTCS_dr_an2_2.byte		
dr_an2_3	MiscalaneousBytes	byte	VEDCSVMC:VTCS_dr_an2_3.byte		
dr_an2_4	MiscalaneousBytes	byte	VEDCSVMC:VTCS_dr_an2_4.byte		
dr_an2_5	MiscalaneousBytes	byte	VEDCSVMC:VTCS_dr_an2_5.byte		
dr_an2_6	MiscalaneousBytes	byte	VEDCSVMC:VTCS_dr_an2_6.byte		
dr_an2_7	MiscalaneousBytes	byte	VEDCSVMC:VTCS_dr_an2_7.byte		
dr_an2_8	MiscalaneousBytes	byte	VEDCSVMC:VTCS_dr_an2_8.byte		
dr_an2_9	MiscalaneousBytes	byte	VEDCSVMC:VTCS_dr_an2_9.byte		
dr_an2_10	MiscalaneousBytes	byte	VEDCSVMC:VTCS_dr_an2_10.byte		
dr_an2_11	MiscalaneousBytes	byte	VEDCSVMC:VTCS_dr_an2_11.byte		
dr_an2_12	MiscalaneousBytes	byte	VEDCSVMC:VTCS_dr_an2_12.byte		
dr_an2_13	MiscalaneousBytes	byte	VEDCSVMC:VTCS_dr_an2_13.byte		
dr_an2_14	MiscalaneousBytes	byte	VEDCSVMC:VTCS_dr_an2_14.byte		
dr_an2_15	MiscalaneousBytes	byte	VEDCSVMC:VTCS_dr_an2_15.byte		
dr_an2_16	MiscalaneousBytes	byte	VEDCSVMC:VTCS_dr_an2_16.byte		
dr_an2_17	MiscalaneousBytes	byte	VEDCSVMC:VTCS_dr_an2_17.byte		
dr_an2_18	MiscalaneousBytes	byte	VEDCSVMC:VTCS_dr_an2_18.byte		
dr_an2_19	MiscalaneousBytes	byte	VEDCSVMC:VTCS_dr_an2_19.byte		
dr_an2_20	MiscalaneousBytes	byte	VEDCSVMC:VTCS_dr_an2_20.byte		
dr_an2_21	MiscalaneousBytes	byte	VEDCSVMC:VTCS_dr_an2_21.byte		
dr_an2_22	MiscalaneousBytes	byte	VEDCSVMC:VTCS_dr_an2_22.byte		
dr_an2_23	MiscalaneousBytes	byte	VEDCSVMC:VTCS_dr_an2_23.byte		
dr_an2_24	MiscalaneousBytes	byte	VEDCSVMC:VTCS_dr_an2_24.byte		
dr_an3_0	MiscalaneousBytes	byte	VEDCSVMC:VTCS_dr_an3_0.byte		
dr_an3_1	MiscalaneousBytes	byte	VEDCSVMC:VTCS_dr_an3_1.byte		
dr_an3_2	MiscalaneousBytes	byte	VEDCSVMC:VTCS_dr_an3_2.byte		
dr_an3_3	MiscalaneousBytes	byte	VEDCSVMC:VTCS_dr_an3_3.byte		
dr_an3_4	MiscalaneousBytes	byte	VEDCSVMC:VTCS_dr_an3_4.byte		
dr_an3_5	MiscalaneousBytes	byte	VEDCSVMC:VTCS_dr_an3_5.byte		
dr_an3_6	MiscalaneousBytes	byte	VEDCSVMC:VTCS_dr_an3_6.byte		
dr_an3_7	MiscalaneousBytes	byte	VEDCSVMC:VTCS_dr_an3_7.byte		
dr_an3_8	MiscalaneousBytes	byte	VEDCSVMC:VTCS_dr_an3_8.byte		
dr_an3_9	MiscalaneousBytes	byte	VEDCSVMC:VTCS_dr_an3_9.byte		
dr_an3_10	MiscalaneousBytes	byte	VEDCSVMC:VTCS_dr_an3_10.byte		
dr_an3_11	MiscalaneousBytes	byte	VEDCSVMC:VTCS_dr_an3_11.byte		
dr_an3_12	MiscalaneousBytes	byte	VEDCSVMC:VTCS_dr_an3_12.byte		
dr_an3_13	MiscalaneousBytes	byte	VEDCSVMC:VTCS_dr_an3_13.byte		
dr_an3_14	MiscalaneousBytes	byte	VEDCSVMC:VTCS_dr_an3_14.byte		
dr_an3_15	MiscalaneousBytes	byte	VEDCSVMC:VTCS_dr_an3_15.byte		
dr_an3_16	MiscalaneousBytes	byte	VEDCSVMC:VTCS_dr_an3_16.byte		
dr_an3_17	MiscalaneousBytes	byte	VEDCSVMC:VTCS_dr_an3_17.byte		
dr_an3_18	MiscalaneousBytes	byte	VEDCSVMC:VTCS_dr_an3_18.byte		
dr_an3_19	MiscalaneousBytes	byte	VEDCSVMC:VTCS_dr_an3_19.byte		
dr_an3_20	MiscalaneousBytes	byte	VEDCSVMC:VTCS_dr_an3_20.byte		
dr_an3_21	MiscalaneousBytes	byte	VEDCSVMC:VTCS_dr_an3_21.byte		
dr_an3_22	MiscalaneousBytes	byte	VEDCSVMC:VTCS_dr_an3_22.byte		

dr_an3_23	MiscalaneousBytes	byte	VEDCSVMC:VTCS_dr_an3_23.byte		
dr_an3_24	MiscalaneousBytes	byte	VEDCSVMC:VTCS_dr_an3_24.byte		
dr_an4_0	MiscalaneousBytes	byte	VEDCSVMC:VTCS_dr_an4_0.byte		
dr_an4_1	MiscalaneousBytes	byte	VEDCSVMC:VTCS_dr_an4_1.byte		
dr_an4_2	MiscalaneousBytes	byte	VEDCSVMC:VTCS_dr_an4_2.byte		
dr_an4_3	MiscalaneousBytes	byte	VEDCSVMC:VTCS_dr_an4_3.byte		
dr_an4_4	MiscalaneousBytes	byte	VEDCSVMC:VTCS_dr_an4_4.byte		
dr_an4_5	MiscalaneousBytes	byte	VEDCSVMC:VTCS_dr_an4_5.byte		
dr_an4_6	MiscalaneousBytes	byte	VEDCSVMC:VTCS_dr_an4_6.byte		
dr_an4_7	MiscalaneousBytes	byte	VEDCSVMC:VTCS_dr_an4_7.byte		
dr_an4_8	MiscalaneousBytes	byte	VEDCSVMC:VTCS_dr_an4_8.byte		
dr_an4_9	MiscalaneousBytes	byte	VEDCSVMC:VTCS_dr_an4_9.byte		
dr_an4_10	MiscalaneousBytes	byte	VEDCSVMC:VTCS_dr_an4_10.byte		
dr_an4_11	MiscalaneousBytes	byte	VEDCSVMC:VTCS_dr_an4_11.byte		
dr_an4_12	MiscalaneousBytes	byte	VEDCSVMC:VTCS_dr_an4_12.byte		
dr_an4_13	MiscalaneousBytes	byte	VEDCSVMC:VTCS_dr_an4_13.byte		
dr_an4_14	MiscalaneousBytes	byte	VEDCSVMC:VTCS_dr_an4_14.byte		
dr_an4_15	MiscalaneousBytes	byte	VEDCSVMC:VTCS_dr_an4_15.byte		
dr_an4_16	MiscalaneousBytes	byte	VEDCSVMC:VTCS_dr_an4_16.byte		
dr_an4_17	MiscalaneousBytes	byte	VEDCSVMC:VTCS_dr_an4_17.byte		
dr_an4_18	MiscalaneousBytes	byte	VEDCSVMC:VTCS_dr_an4_18.byte		
dr_an4_19	MiscalaneousBytes	byte	VEDCSVMC:VTCS_dr_an4_19.byte		
dr_an4_20	MiscalaneousBytes	byte	VEDCSVMC:VTCS_dr_an4_20.byte		
dr_an4_21	MiscalaneousBytes	byte	VEDCSVMC:VTCS_dr_an4_21.byte		
dr_an4_22	MiscalaneousBytes	byte	VEDCSVMC:VTCS_dr_an4_22.byte		
dr_an4_23	MiscalaneousBytes	byte	VEDCSVMC:VTCS_dr_an4_23.byte		
dr_an4_24	MiscalaneousBytes	byte	VEDCSVMC:VTCS_dr_an4_24.byte		
dr_fm455_0	MiscalaneousBytes	byte	VEDCSVMC:VTCS_dr_fm455_0.byte		
dr_fm455_1	MiscalaneousBytes	byte	VEDCSVMC:VTCS_dr_fm455_1.byte		
dr_fm455_2	MiscalaneousBytes	byte	VEDCSVMC:VTCS_dr_fm455_2.byte		
dr_fm455_3	MiscalaneousBytes	byte	VEDCSVMC:VTCS_dr_fm455_3.byte		
dr_fm455_4	MiscalaneousBytes	byte	VEDCSVMC:VTCS_dr_fm455_4.byte		
dr_fm455_5	MiscalaneousBytes	byte	VEDCSVMC:VTCS_dr_fm455_5.byte		
dr_fm455_6	MiscalaneousBytes	byte	VEDCSVMC:VTCS_dr_fm455_6.byte		
dr_fm455_7	MiscalaneousBytes	byte	VEDCSVMC:VTCS_dr_fm455_7.byte		
dr_fm455_8	MiscalaneousBytes	byte	VEDCSVMC:VTCS_dr_fm455_8.byte		
dr_fm455_9	MiscalaneousBytes	byte	VEDCSVMC:VTCS_dr_fm455_9.byte		
dr_fm455_10	MiscalaneousBytes	byte	VEDCSVMC:VTCS_dr_fm455_10.byte		
dr_fm455_11	MiscalaneousBytes	byte	VEDCSVMC:VTCS_dr_fm455_11.byte		
dr_fm455_12	MiscalaneousBytes	byte	VEDCSVMC:VTCS_dr_fm455_12.byte		
dr_fm455_13	MiscalaneousBytes	byte	VEDCSVMC:VTCS_dr_fm455_13.byte		
dr_fm455_14	MiscalaneousBytes	byte	VEDCSVMC:VTCS_dr_fm455_14.byte		
dr_fm455_15	MiscalaneousBytes	byte	VEDCSVMC:VTCS_dr_fm455_15.byte		
dr_fm455_16	MiscalaneousBytes	byte	VEDCSVMC:VTCS_dr_fm455_16.byte		
dr_fm455_17	MiscalaneousBytes	byte	VEDCSVMC:VTCS_dr_fm455_17.byte		
dr_fm455_18	MiscalaneousBytes	byte	VEDCSVMC:VTCS_dr_fm455_18.byte		
dr_fm455_19	MiscalaneousBytes	byte	VEDCSVMC:VTCS_dr_fm455_19.byte		
dr_fm455_20	MiscalaneousBytes	byte	VEDCSVMC:VTCS_dr_fm455_20.byte		
dr_fm455_21	MiscalaneousBytes	byte	VEDCSVMC:VTCS_dr_fm455_21.byte		





TL_TT047	TemperatureTransmitter	status	VEDCSVMC:VTCS_TL_TT047.status		
TL_TT048	TemperatureTransmitter	T	VEDCSVMC:VTCS_TL_TT048.T	TL_Detector_Temperature	TL_TT048.temp
TL_TT048	TemperatureTransmitter	status	VEDCSVMC:VTCS_TL_TT048.status		
TL_TT101	TemperatureTransmitter	T	VEDCSVMC:VTCS_TL_TT101.T	TL_System_Sensor_A	TL_TT101.temp
TL_TT101	TemperatureTransmitter	status	VEDCSVMC:VTCS_TL_TT101.status		
TL_TT102	TemperatureTransmitter	T	VEDCSVMC:VTCS_TL_TT102.T	TL_System_Sensor_A	TL_TT102.temp
TL_TT102	TemperatureTransmitter	status	VEDCSVMC:VTCS_TL_TT102.status		
TL_TT103	TemperatureTransmitter	T	VEDCSVMC:VTCS_TL_TT103.T	TL_System_Sensor_A	TL_TT103.temp
TL_TT103	TemperatureTransmitter	status	VEDCSVMC:VTCS_TL_TT103.status		
TL_TT104	TemperatureTransmitter	T	VEDCSVMC:VTCS_TL_TT104.T	TL_System_Sensor_A	TL_TT104.temp
TL_TT104	TemperatureTransmitter	status	VEDCSVMC:VTCS_TL_TT104.status		
TL_TT105	TemperatureTransmitter	T	VEDCSVMC:VTCS_TL_TT105.T	TL_System_Sensor_A	TL_TT105.temp
TL_TT105	TemperatureTransmitter	status	VEDCSVMC:VTCS_TL_TT105.status		
TL_TT106	TemperatureTransmitter	T	VEDCSVMC:VTCS_TL_TT106.T	TL_System_Sensor_A	TL_TT106.temp
TL_TT106	TemperatureTransmitter	status	VEDCSVMC:VTCS_TL_TT106.status		
TL_TT107	TemperatureTransmitter	T	VEDCSVMC:VTCS_TL_TT107.T	TL_System_Sensor_A	TL_TT107.temp
TL_TT107	TemperatureTransmitter	status	VEDCSVMC:VTCS_TL_TT107.status		
TL_TT108	TemperatureTransmitter	T	VEDCSVMC:VTCS_TL_TT108.T	TL_System_Sensor_A	TL_TT108.temp
TL_TT108	TemperatureTransmitter	status	VEDCSVMC:VTCS_TL_TT108.status		
TL_TT109	TemperatureTransmitter	T	VEDCSVMC:VTCS_TL_TT109.T	TL_System_Sensor_A	TL_TT109.temp
TL_TT109	TemperatureTransmitter	status	VEDCSVMC:VTCS_TL_TT109.status		
TL_TT110	TemperatureTransmitter	T	VEDCSVMC:VTCS_TL_TT110.T	TL_System_Sensor_A	TL_TT110.temp
TL_TT110	TemperatureTransmitter	status	VEDCSVMC:VTCS_TL_TT110.status		
xx_TTamb	TemperatureTransmitter	T	VEDCSVMC:VTCS_xx_TTamb.T	TL_System_Sensor_A	xx_TTamb.temp
xx_TTamb	TemperatureTransmitter	status	VEDCSVMC:VTCS_xx_TTamb.status		
TL_TT112	TemperatureTransmitter	T	VEDCSVMC:VTCS_TL_TT112.T	TL_System_Sensor_A	TL_TT112.temp
TL_TT112	TemperatureTransmitter	status	VEDCSVMC:VTCS_TL_TT112.status		
TL_TT113	TemperatureTransmitter	T	VEDCSVMC:VTCS_TL_TT113.T	TL_System_Sensor_A	TL_TT113.temp
TL_TT113	TemperatureTransmitter	status	VEDCSVMC:VTCS_TL_TT113.status		
TL_TT114	TemperatureTransmitter	T	VEDCSVMC:VTCS_TL_TT114.T	TL_System_Sensor_A	TL_TT114.temp
TL_TT114	TemperatureTransmitter	status	VEDCSVMC:VTCS_TL_TT114.status		
TL_TT115	TemperatureTransmitter	T	VEDCSVMC:VTCS_TL_TT115.T	TL_System_Sensor_A	TL_TT115.temp
TL_TT115	TemperatureTransmitter	status	VEDCSVMC:VTCS_TL_TT115.status		
TL_TT116	TemperatureTransmitter	T	VEDCSVMC:VTCS_TL_TT116.T	TL_System_Sensor_A	TL_TT116.temp
TL_TT116	TemperatureTransmitter	status	VEDCSVMC:VTCS_TL_TT116.status		
TL_TT117	TemperatureTransmitter	T	VEDCSVMC:VTCS_TL_TT117.T	TL_System_Sensor_A	TL_TT117.temp
TL_TT117	TemperatureTransmitter	status	VEDCSVMC:VTCS_TL_TT117.status		
TL_TT118	TemperatureTransmitter	T	VEDCSVMC:VTCS_TL_TT118.T	TL_System_Sensor_A	TL_TT118.temp
TL_TT118	TemperatureTransmitter	status	VEDCSVMC:VTCS_TL_TT118.status		
TL_TT119	TemperatureTransmitter	T	VEDCSVMC:VTCS_TL_TT119.T	TL_System_Sensor_A	TL_TT119.temp
TL_TT119	TemperatureTransmitter	status	VEDCSVMC:VTCS_TL_TT119.status		
TL_TT120	TemperatureTransmitter	T	VEDCSVMC:VTCS_TL_TT120.T	TL_System_Sensor_A	TL_TT120.temp
TL_TT120	TemperatureTransmitter	status	VEDCSVMC:VTCS_TL_TT120.status		
TL_TT121	TemperatureTransmitter	T	VEDCSVMC:VTCS_TL_TT121.T	TL_System_Sensor_A	TL_TT121.temp
TL_TT121	TemperatureTransmitter	status	VEDCSVMC:VTCS_TL_TT121.status		
TL_TT122	TemperatureTransmitter	T	VEDCSVMC:VTCS_TL_TT122.T	TL_System_Sensor_A	TL_TT122.temp
TL_TT122	TemperatureTransmitter	status	VEDCSVMC:VTCS_TL_TT122.status		
TL_TT123	TemperatureTransmitter	T	VEDCSVMC:VTCS_TL_TT123.T	TL_System_Sensor_A	TL_TT123.temp
TL_TT123	TemperatureTransmitter	status	VEDCSVMC:VTCS_TL_TT123.status		







TR_TT124	TemperatureTransmitter	status	VEDCSVMC:VTCS_TR_TT124.status		
TR_TT125	TemperatureTransmitter	T	VEDCSVMC:VTCS_TR_TT125.T	TR_System_Sensor_A	TR_TT125.temp
TR_TT125	TemperatureTransmitter	status	VEDCSVMC:VTCS_TR_TT125.status		
TLR_TT112	TemperatureTransmitter	T	VEDCSVMC:VTCS_TLR_TT112.T	TLR_SystemSensors	TM_TT112.temp
TLR_TT112	TemperatureTransmitter	status	VEDCSVMC:VTCS_TLR_TT112.status		
TLR_TT113	TemperatureTransmitter	T	VEDCSVMC:VTCS_TLR_TT113.T	TLR_SystemSensors	TM_TT113.temp
TLR_TT113	TemperatureTransmitter	status	VEDCSVMC:VTCS_TLR_TT113.status		
TLR_TT114	TemperatureTransmitter	T	VEDCSVMC:VTCS_TLR_TT114.T	TLR_SystemSensors	TM_TT114.temp
TLR_TT114	TemperatureTransmitter	status	VEDCSVMC:VTCS_TLR_TT114.status		
TLR_TT115	TemperatureTransmitter	T	VEDCSVMC:VTCS_TLR_TT115.T	TLR_SystemSensors	TM_TT115.temp
TLR_TT115	TemperatureTransmitter	status	VEDCSVMC:VTCS_TLR_TT115.status		
TLR_TT122	TemperatureTransmitter	T	VEDCSVMC:VTCS_TLR_TT122.T	TLR_SystemSensors	TM_TT122.temp
TLR_TT122	TemperatureTransmitter	status	VEDCSVMC:VTCS_TLR_TT122.status		
SA_TT101	TemperatureTransmitter	T	VEDCSVMC:VTCS_SA_TT101.T	SA_SystemValues	SA_TT101.temp
SA_TT101	TemperatureTransmitter	status	VEDCSVMC:VTCS_SA_TT101.status		
SA_TT102	TemperatureTransmitter	T	VEDCSVMC:VTCS_SA_TT102.T	SA_SystemValues	SA_TT102.temp
SA_TT102	TemperatureTransmitter	status	VEDCSVMC:VTCS_SA_TT102.status		
SA_TT103	TemperatureTransmitter	T	VEDCSVMC:VTCS_SA_TT103.T	SA_SystemValues	SA_TT103.temp
SA_TT103	TemperatureTransmitter	status	VEDCSVMC:VTCS_SA_TT103.status		
SA_TT104	TemperatureTransmitter	T	VEDCSVMC:VTCS_SA_TT104.T	SA_SystemValues	SA_TT104.temp
SA_TT104	TemperatureTransmitter	status	VEDCSVMC:VTCS_SA_TT104.status		
SA_TT105	TemperatureTransmitter	T	VEDCSVMC:VTCS_SA_TT105.T	SA_SystemValues	SA_TT105.temp
SA_TT105	TemperatureTransmitter	status	VEDCSVMC:VTCS_SA_TT105.status		
SA_TT106	TemperatureTransmitter	T	VEDCSVMC:VTCS_SA_TT106.T	SA_SystemValues	SA_TT106.temp
SA_TT106	TemperatureTransmitter	status	VEDCSVMC:VTCS_SA_TT106.status		
SA_TT107	TemperatureTransmitter	T	VEDCSVMC:VTCS_SA_TT107.T	SA_SystemValues	SA_TT107.temp
SA_TT107	TemperatureTransmitter	status	VEDCSVMC:VTCS_SA_TT107.status		
SA_TT108	TemperatureTransmitter	T	VEDCSVMC:VTCS_SA_TT108.T	SA_SystemValues	SA_TT108.temp
SA_TT108	TemperatureTransmitter	status	VEDCSVMC:VTCS_SA_TT108.status		
SA_TT109	TemperatureTransmitter	T	VEDCSVMC:VTCS_SA_TT109.T	SA_SystemValues	SA_TT109.temp
SA_TT109	TemperatureTransmitter	status	VEDCSVMC:VTCS_SA_TT109.status		
SA_TT110	TemperatureTransmitter	T	VEDCSVMC:VTCS_SA_TT110.T	SA_SystemValues	SA_TT110.temp
SA_TT110	TemperatureTransmitter	status	VEDCSVMC:VTCS_SA_TT110.status		
SA_TT111	TemperatureTransmitter	T	VEDCSVMC:VTCS_SA_TT111.T	SA_SystemValues	SA_TT111.temp
SA_TT111	TemperatureTransmitter	status	VEDCSVMC:VTCS_SA_TT111.status		
SA_TT112	TemperatureTransmitter	T	VEDCSVMC:VTCS_SA_TT112.T	SA_SystemValues	SA_TT112.temp
SA_TT112	TemperatureTransmitter	status	VEDCSVMC:VTCS_SA_TT112.status		
SA_TT113	TemperatureTransmitter	T	VEDCSVMC:VTCS_SA_TT113.T	SA_SystemValues	SA_TT113.temp
SA_TT113	TemperatureTransmitter	status	VEDCSVMC:VTCS_SA_TT113.status		
SA_TT114	TemperatureTransmitter	T	VEDCSVMC:VTCS_SA_TT114.T	SA_SystemValues	SA_TT114.temp
SA_TT114	TemperatureTransmitter	status	VEDCSVMC:VTCS_SA_TT114.status		
SA_TT115	TemperatureTransmitter	T	VEDCSVMC:VTCS_SA_TT115.T	SA_SystemValues	SA_TT115.temp
SA_TT115	TemperatureTransmitter	status	VEDCSVMC:VTCS_SA_TT115.status		
SA_TT116	TemperatureTransmitter	T	VEDCSVMC:VTCS_SA_TT116.T	SA_SystemValues	SA_TT116.temp
SA_TT116	TemperatureTransmitter	status	VEDCSVMC:VTCS_SA_TT116.status		
SA_TT117	TemperatureTransmitter	T	VEDCSVMC:VTCS_SA_TT117.T	SA_SystemValues	SA_TT117.temp
SA_TT117	TemperatureTransmitter	status	VEDCSVMC:VTCS_SA_TT117.status		
SA_TT118	TemperatureTransmitter	T	VEDCSVMC:VTCS_SA_TT118.T	SA_SystemValues	SA_TT118.temp
SA_TT118	TemperatureTransmitter	status	VEDCSVMC:VTCS_SA_TT118.status		

SA_TT119	TemperatureTransmitter	T	VEDCSVMC:VTCS_SA_TT119.T	SA_SystemValues	SA_TT119.temp
SA_TT119	TemperatureTransmitter	status	VEDCSVMC:VTCS_SA_TT119.status		
SA_TT120	TemperatureTransmitter	T	VEDCSVMC:VTCS_SA_TT120.T	SA_SystemValues	SA_TT120.temp
SA_TT120	TemperatureTransmitter	status	VEDCSVMC:VTCS_SA_TT120.status		
SA_TT121	TemperatureTransmitter	T	VEDCSVMC:VTCS_SA_TT121.T	SA_SystemValues	SA_TT121.temp
SA_TT121	TemperatureTransmitter	status	VEDCSVMC:VTCS_SA_TT121.status		
SA_TT122	TemperatureTransmitter	T	VEDCSVMC:VTCS_SA_TT122.T	SA_SystemValues	SA_TT122.temp
SA_TT122	TemperatureTransmitter	status	VEDCSVMC:VTCS_SA_TT122.status		
SB_TT101	TemperatureTransmitter	T	VEDCSVMC:VTCS_SB_TT101.T	SB_SystemValues	SB_TT101.temp
SB_TT101	TemperatureTransmitter	status	VEDCSVMC:VTCS_SB_TT101.status		
SB_TT102	TemperatureTransmitter	T	VEDCSVMC:VTCS_SB_TT102.T	SB_SystemValues	SB_TT102.temp
SB_TT102	TemperatureTransmitter	status	VEDCSVMC:VTCS_SB_TT102.status		
SB_TT104	TemperatureTransmitter	T	VEDCSVMC:VTCS_SB_TT104.T	SB_SystemValues	SB_TT104.temp
SB_TT104	TemperatureTransmitter	status	VEDCSVMC:VTCS_SB_TT104.status		
SB_TT105	TemperatureTransmitter	T	VEDCSVMC:VTCS_SB_TT105.T	SB_SystemValues	SB_TT105.temp
SB_TT105	TemperatureTransmitter	status	VEDCSVMC:VTCS_SB_TT105.status		
SB_TT107	TemperatureTransmitter	T	VEDCSVMC:VTCS_SB_TT107.T	SB_SystemValues	SB_TT107.temp
SB_TT107	TemperatureTransmitter	status	VEDCSVMC:VTCS_SB_TT107.status		
SB_TT109	TemperatureTransmitter	T	VEDCSVMC:VTCS_SB_TT109.T	SB_SystemValues	SB_TT109.temp
SB_TT109	TemperatureTransmitter	status	VEDCSVMC:VTCS_SB_TT109.status		
SB_TT111	TemperatureTransmitter	T	VEDCSVMC:VTCS_SB_TT111.T	SB_SystemValues	SB_TT111.temp
SB_TT111	TemperatureTransmitter	status	VEDCSVMC:VTCS_SB_TT111.status		
SB_TT113	TemperatureTransmitter	T	VEDCSVMC:VTCS_SB_TT113.T	SB_SystemValues	SB_TT113.temp
SB_TT113	TemperatureTransmitter	status	VEDCSVMC:VTCS_SB_TT113.status		
SB_TT114	TemperatureTransmitter	T	VEDCSVMC:VTCS_SB_TT114.T	SB_SystemValues	SB_TT114.temp
SB_TT114	TemperatureTransmitter	status	VEDCSVMC:VTCS_SB_TT114.status		
SB_TT115	TemperatureTransmitter	T	VEDCSVMC:VTCS_SB_TT115.T	SB_SystemValues	SB_TT115.temp
SB_TT115	TemperatureTransmitter	status	VEDCSVMC:VTCS_SB_TT115.status		
SB_TT116	TemperatureTransmitter	T	VEDCSVMC:VTCS_SB_TT116.T	SB_SystemValues	SB_TT116.temp
SB_TT116	TemperatureTransmitter	status	VEDCSVMC:VTCS_SB_TT116.status		
SB_TT117	TemperatureTransmitter	T	VEDCSVMC:VTCS_SB_TT117.T	SB_SystemValues	SB_TT117.temp
SB_TT117	TemperatureTransmitter	status	VEDCSVMC:VTCS_SB_TT117.status		
SB_TT118	TemperatureTransmitter	T	VEDCSVMC:VTCS_SB_TT118.T	SB_SystemValues	SB_TT118.temp
SB_TT118	TemperatureTransmitter	status	VEDCSVMC:VTCS_SB_TT118.status		
SB_TT119	TemperatureTransmitter	T	VEDCSVMC:VTCS_SB_TT119.T	SB_SystemValues	SB_TT119.temp
SB_TT119	TemperatureTransmitter	status	VEDCSVMC:VTCS_SB_TT119.status		
SB_TT121	TemperatureTransmitter	T	VEDCSVMC:VTCS_SB_TT121.T	SB_SystemValues	SB_TT121.temp
SB_TT121	TemperatureTransmitter	status	VEDCSVMC:VTCS_SB_TT121.status		
SB_TT122	TemperatureTransmitter	T	VEDCSVMC:VTCS_SB_TT122.T	SB_SystemValues	SB_TT122.temp
SB_TT122	TemperatureTransmitter	status	VEDCSVMC:VTCS_SB_TT122.status		
PA_TT101	TemperatureTransmitter	T	VEDCSVMC:VTCS_PA_TT101.T	SA_SystemValues	PA_TT101.temp
PA_TT101	TemperatureTransmitter	status	VEDCSVMC:VTCS_PA_TT101.status		
PA_TT102	TemperatureTransmitter	T	VEDCSVMC:VTCS_PA_TT102.T	SA_SystemValues	PA_TT102.temp
PA_TT102	TemperatureTransmitter	status	VEDCSVMC:VTCS_PA_TT102.status		
PB_TT101	TemperatureTransmitter	T	VEDCSVMC:VTCS_PB_TT101.T	SB_SystemValues	PB_TT101.temp
PB_TT101	TemperatureTransmitter	status	VEDCSVMC:VTCS_PB_TT101.status		
TL_PT001	PressureTransmitter	P	VEDCSVMC:VTCS_TL_PT001.P	TL_System_Sensors_A	TL_PT001.pres
TL_PT001	PressureTransmitter	status	VEDCSVMC:VTCS_TL_PT001.status		
TL_PT001	PressureTransmitter	Tsat	VEDCSVMC:VTCS_TL_PT001.Tsat	TL_System_Sensors_A	TL_PT001.tsat

TL_PT002	PressureTransmitter	P	VEDCSVMC:VTCS_TL_PT002.P	TL_System_Sensors_A	TL_PT002.pres
TL_PT002	PressureTransmitter	status	VEDCSVMC:VTCS_TL_PT002.status		
TL_PT002	PressureTransmitter	Tsat	VEDCSVMC:VTCS_TL_PT002.Tsat	TL_System_Sensors_A	TL_PT002.tsat
TL_PT003	PressureTransmitter	P	VEDCSVMC:VTCS_TL_PT003.P	TL_System_Sensors_A	TL_PT003.pres
TL_PT003	PressureTransmitter	status	VEDCSVMC:VTCS_TL_PT003.status		
TL_PT003	PressureTransmitter	Tsat	VEDCSVMC:VTCS_TL_PT003.Tsat	TL_System_Sensors_A	TL_PT003.tsat
TL_PT004	PressureTransmitter	P	VEDCSVMC:VTCS_TL_PT004.P	TL_System_Sensors_A	TL_PT004.pres
TL_PT004	PressureTransmitter	status	VEDCSVMC:VTCS_TL_PT004.status		
TL_PT004	PressureTransmitter	NA			
TL_PT101	PressureTransmitter	P	VEDCSVMC:VTCS_TL_PT101.P	TL_System_Sensors_A	TL_PT101.pres
TL_PT101	PressureTransmitter	status	VEDCSVMC:VTCS_TL_PT101.status		
TL_PT101	PressureTransmitter	Tsat	VEDCSVMC:VTCS_TL_PT101.Tsat	TL_System_Sensors_A	TL_PT101.tsat
TL_PT102	PressureTransmitter	P	VEDCSVMC:VTCS_TL_PT102.P	TL_System_Sensors_A	TL_PT102.pres
TL_PT102	PressureTransmitter	status	VEDCSVMC:VTCS_TL_PT102.status		
TL_PT102	PressureTransmitter	Tsat	VEDCSVMC:VTCS_TL_PT102.Tsat	TL_System_Sensors_A	TL_PT102.tsat
TL_PT103	PressureSwitch	P	VEDCSVMC:VTCS_TL_PT103.P		
TL_PT103	PressureSwitch	status	VEDCSVMC:VTCS_TL_PT103.status		
TL_PT103	PressureSwitch	NA			
TL_PT104	PressureTransmitter	P	VEDCSVMC:VTCS_TL_PT104.P	TL_System_Sensors_A	TL_PT104.pres
TL_PT104	PressureTransmitter	status	VEDCSVMC:VTCS_TL_PT104.status		
TL_PT104	PressureTransmitter	Tsat	VEDCSVMC:VTCS_TL_PT104.Tsat	TL_System_Sensors_A	TL_PT104.tsat
TR_PT001	PressureTransmitter	P	VEDCSVMC:VTCS_TR_PT001.P	TR_System_Sensors_A	TR_PT001.pres
TR_PT001	PressureTransmitter	status	VEDCSVMC:VTCS_TR_PT001.status		
TR_PT001	PressureTransmitter	Tsat	VEDCSVMC:VTCS_TR_PT001.Tsat	TR_System_Sensors_A	TR_PT001.tsat
TR_PT002	PressureTransmitter	P	VEDCSVMC:VTCS_TR_PT002.P	TR_System_Sensors_A	TR_PT002.pres
TR_PT002	PressureTransmitter	status	VEDCSVMC:VTCS_TR_PT002.status		
TR_PT002	PressureTransmitter	Tsat	VEDCSVMC:VTCS_TR_PT002.Tsat	TR_System_Sensors_A	TR_PT002.tsat
TR_PT003	PressureTransmitter	P	VEDCSVMC:VTCS_TR_PT003.P	TR_System_Sensors_A	TR_PT003.pres
TR_PT003	PressureTransmitter	status	VEDCSVMC:VTCS_TR_PT003.status		
TR_PT003	PressureTransmitter	Tsat	VEDCSVMC:VTCS_TR_PT003.Tsat	TR_System_Sensors_A	TR_PT003.tsat
TR_PT004	PressureTransmitter	P	VEDCSVMC:VTCS_TR_PT004.P	TR_System_Sensors_A	TR_PT004.pres
TR_PT004	PressureTransmitter	status	VEDCSVMC:VTCS_TR_PT004.status		
TR_PT004	PressureTransmitter	Tsat	VEDCSVMC:VTCS_TR_PT004.Tsat	TR_System_Sensors_A	TR_PT004.tsat
TR_PT101	PressureTransmitter	P	VEDCSVMC:VTCS_TR_PT101.P	TR_System_Sensors_A	TR_PT101.pres
TR_PT101	PressureTransmitter	status	VEDCSVMC:VTCS_TR_PT101.status		
TR_PT101	PressureTransmitter	Tsat	VEDCSVMC:VTCS_TR_PT101.Tsat	TR_System_Sensors_A	TR_PT101.tsat
TR_PT102	PressureTransmitter	P	VEDCSVMC:VTCS_TR_PT102.P	TR_System_Sensors_A	TR_PT102.pres
TR_PT102	PressureTransmitter	status	VEDCSVMC:VTCS_TR_PT102.status		
TR_PT102	PressureTransmitter	Tsat	VEDCSVMC:VTCS_TR_PT102.Tsat	TR_System_Sensors_A	TR_PT102.tsat
TR_PT103	PressureSwitch	P	VEDCSVMC:VTCS_TR_PT103.P		
TR_PT103	PressureSwitch	status	VEDCSVMC:VTCS_TR_PT103.status		
TR_PT104	PressureTransmitter	P	VEDCSVMC:VTCS_TR_PT104.P	TR_System_Sensors_A	TR_PT104.pres
TR_PT104	PressureTransmitter	status	VEDCSVMC:VTCS_TR_PT104.status		
TR_PT104	PressureTransmitter	Tsat	VEDCSVMC:VTCS_TR_PT104.Tsat	TR_System_Sensors_A	TR_PT104.tsat
TLR_PT103	PressureSwitch	P	VEDCSVMC:VTCS_TLR_PT103.P		
TLR_PT103	PressureSwitch	status	VEDCSVMC:VTCS_TLR_PT103.status		
SA_PT101	PressureTransmitter	P	VEDCSVMC:VTCS_SA_PT101.P	SA_SystemValues	SA_PT101.pres
SA_PT101	PressureTransmitter	status	VEDCSVMC:VTCS_SA_PT101.status		
SA_PT101	PressureTransmitter	Tsat	VEDCSVMC:VTCS_SA_PT101.Tsat	SA_SystemValues	SA_PT101.tsat
SA_PT102	PressureTransmitter	P	VEDCSVMC:VTCS_SA_PT102.P	SA_SystemValues	SA_PT102.pres

SA_PT102	PressureTransmitter	status	VEDCSVMC:VTCS_SA_PT102.status		
SA_PT102	PressureTransmitter	Tsat	VEDCSVMC:VTCS_SA_PT102.Tsat	SA_SystemValues	SA_PT102.tsat
SA_PT103	PressureTransmitter	P	VEDCSVMC:VTCS_SA_PT103.P	SA_SystemValues	SA_PT103.pres
SA_PT103	PressureTransmitter	status	VEDCSVMC:VTCS_SA_PT103.status		
SA_PT103	PressureTransmitter	Tsat	VEDCSVMC:VTCS_SA_PT103.Tsat	SA_SystemValues	SA_PT103.tsat
SA_PT104	PressureTransmitter	P	VEDCSVMC:VTCS_SA_PT104.P	SA_SystemValues	SA_PT104.pres
SA_PT104	PressureTransmitter	status	VEDCSVMC:VTCS_SA_PT104.status		
SA_PT104	PressureTransmitter	Tsat	VEDCSVMC:VTCS_SA_PT104.Tsat	SA_SystemValues	SA_PT104.tsat
SA_PT105	PressureTransmitter	P	VEDCSVMC:VTCS_SA_PT105.P	SA_SystemValues	SA_PT105.pres
SA_PT105	PressureTransmitter	status	VEDCSVMC:VTCS_SA_PT105.status		
SA_PT105	PressureTransmitter	Tsat	VEDCSVMC:VTCS_SA_PT105.Tsat	SA_SystemValues	SA_PT105.tsat
SA_PT106	PressureTransmitter	P	VEDCSVMC:VTCS_SA_PT106.P	SA_SystemValues	SA_PT106.pres
SA_PT106	PressureTransmitter	status	VEDCSVMC:VTCS_SA_PT106.status		
SA_PT106	PressureTransmitter	Tsat	VEDCSVMC:VTCS_SA_PT106.Tsat	SA_SystemValues	SA_PT106.tsat
SA_PT107	PressureTransmitter	P	VEDCSVMC:VTCS_SA_PT107.P	SA_SystemValues	SA_PT107.pres
SA_PT107	PressureTransmitter	status	VEDCSVMC:VTCS_SA_PT107.status		
SA_PT107	PressureTransmitter	Tsat	VEDCSVMC:VTCS_SA_PT107.Tsat	SA_SystemValues	SA_PT107.tsat
SA_PT108	PressureSwitch	P	VEDCSVMC:VTCS_SA_PT108.P	SA_SystemValues	SA_PT108.pres
SA_PT108	PressureSwitch	status	VEDCSVMC:VTCS_SA_PT108.status		
SB_PT102	PressureTransmitter	P	VEDCSVMC:VTCS_SB_PT102.P	SB_SystemValues	SB_PT102.pres
SB_PT102	PressureTransmitter	status	VEDCSVMC:VTCS_SB_PT102.status		
SB_PT102	PressureTransmitter	Tsat	VEDCSVMC:VTCS_SB_PT102.Tsat	SB_SystemValues	SB_PT102.tsat
SB_PT103	PressureTransmitter	P	VEDCSVMC:VTCS_SB_PT103.P	SB_SystemValues	SB_PT103.pres
SB_PT103	PressureTransmitter	status	VEDCSVMC:VTCS_SB_PT103.status		
SB_PT103	PressureTransmitter	Tsat	VEDCSVMC:VTCS_SB_PT103.Tsat	SB_SystemValues	SB_PT103.tsat
SB_PT104	PressureTransmitter	P	VEDCSVMC:VTCS_SB_PT104.P	SB_SystemValues	SB_PT104.pres
SB_PT104	PressureTransmitter	status	VEDCSVMC:VTCS_SB_PT104.status		
SB_PT104	PressureTransmitter	Tsat	VEDCSVMC:VTCS_SB_PT104.Tsat	SB_SystemValues	SB_PT104.tsat
SB_PT105	PressureTransmitter	P	VEDCSVMC:VTCS_SB_PT105.P	SB_SystemValues	SB_PT105.pres
SB_PT105	PressureTransmitter	status	VEDCSVMC:VTCS_SB_PT105.status		
SB_PT105	PressureTransmitter	Tsat	VEDCSVMC:VTCS_SB_PT105.Tsat	SB_SystemValues	SB_PT105.tsat
SB_PT106	PressureTransmitter	P	VEDCSVMC:VTCS_SB_PT106.P	SB_SystemValues	SB_PT106.pres
SB_PT106	PressureTransmitter	status	VEDCSVMC:VTCS_SB_PT106.status		
SB_PT106	PressureTransmitter	Tsat	VEDCSVMC:VTCS_SB_PT106.Tsat	SB_SystemValues	SB_PT106.tsat
SB_PT108	PressureSwitch	P	VEDCSVMC:VTCS_SB_PT108.P	SB_SystemValues	SB_PT108.pres
SB_PT108	PressureSwitch	status	VEDCSVMC:VTCS_SB_PT108.status		
TL_VL102	Automatic2WayValve	status	VEDCSVMC:VTCS_TL_VL102.status		
TL_VL103	Automatic3WayValve	status	VEDCSVMC:VTCS_TL_VL103.status		
TL_VL104	Automatic2WayValve	status	VEDCSVMC:VTCS_TL_VL104.status		
TL_VL109	Automatic2WayValve	status	VEDCSVMC:VTCS_TL_VL109.status		
TL_VL111	Automatic2WayValve	status	VEDCSVMC:VTCS_TL_VL111.status		
TL_VL112	Automatic2WayValve	status	VEDCSVMC:VTCS_TL_VL112.status		
TR_VL102	Automatic2WayValve	status	VEDCSVMC:VTCS_TR_VL102.status		
TR_VL103	Automatic3WayValve	status	VEDCSVMC:VTCS_TR_VL103.status		
TR_VL104	Automatic2WayValve	status	VEDCSVMC:VTCS_TR_VL104.status		
TR_VL108	Automatic3WayValve	status	VEDCSVMC:VTCS_TR_VL108.status		
TR_VL109	Automatic2WayValve	status	VEDCSVMC:VTCS_TR_VL109.status		
TR_VL111	Automatic2WayValve	status	VEDCSVMC:VTCS_TR_VL111.status		
TR_VL112	Automatic2WayValve	status	VEDCSVMC:VTCS_TR_VL112.status		

TLR_VL101	Automatic3WayValve	status	VEDCSVMC:VTCS_TLR_VL101.status		
TLR_VL109	Automatic3WayValve	status	VEDCSVMC:VTCS_TLR_VL109.status		
TLR_VL110	Automatic2WayValve	status	VEDCSVMC:VTCS_TLR_VL110.status		
TLR_VL111	Automatic2WayValve	status	VEDCSVMC:VTCS_TLR_VL111.status		
SA_VL106	AutomaticRegulatingValve	Position	VEDCSVMC:VTCS_SA_VL106.Position	SA_SystemValues	SA_VL106.posi
SA_VL106	AutomaticRegulatingValve	status	VEDCSVMC:VTCS_SA_VL106.status		
SA_VL110	AutomaticRegulatingValve	Position	VEDCSVMC:VTCS_SA_VL110.Position	SA_SystemValues	SA_VL110.posi
SA_VL110	AutomaticRegulatingValve	status	VEDCSVMC:VTCS_SA_VL110.status		
SA_VL114	AutomaticRegulatingValve	Position	VEDCSVMC:VTCS_SA_VL114.Position	SA_SystemValues	SA_VL114.posi
SA_VL114	AutomaticRegulatingValve	status	VEDCSVMC:VTCS_SA_VL114.status		
SA_VL119	AutomaticRegulatingValve	Position	VEDCSVMC:VTCS_SA_VL119.Position	SA_SystemValues	SA_VL119.posi
SA_VL119	AutomaticRegulatingValve	status	VEDCSVMC:VTCS_SA_VL119.status		
SB_VL106	AutomaticRegulatingValve	Position	VEDCSVMC:VTCS_SB_VL106.Position	SB_SystemValues	SB_VL106.posi
SB_VL106	AutomaticRegulatingValve	status	VEDCSVMC:VTCS_SB_VL106.status		
SB_VL110	AutomaticRegulatingValve	Position	VEDCSVMC:VTCS_SB_VL110.Position	SB_SystemValues	SB_VL110.posi
SB_VL110	AutomaticRegulatingValve	status	VEDCSVMC:VTCS_SB_VL110.status		
SB_VL114	AutomaticRegulatingValve	Position	VEDCSVMC:VTCS_SB_VL114.Position	SB_SystemValues	SB_VL114.posi
SB_VL114	AutomaticRegulatingValve	status	VEDCSVMC:VTCS_SB_VL114.status		
SB_VL119	AutomaticRegulatingValve	Position	VEDCSVMC:VTCS_SB_VL119.Position	SB_SystemValues	SB_VL119.posi
SB_VL119	AutomaticRegulatingValve	status	VEDCSVMC:VTCS_SB_VL119.status		
TL_LT101	LevelTransmitter	Level	VEDCSVMC:VTCS_TL_LT101.Level	TL_System_Sensors_A	TL_LT101.level
TL_LT101	LevelTransmitter	status	VEDCSVMC:VTCS_TL_LT101.status		
TL_LT101	LevelTransmitter	raw	VEDCSVMC:VTCS_TL_LT101.raw	TL_System_Sensors_A	TL_LT101.rawl
TR_LT101	LevelTransmitter	Level	VEDCSVMC:VTCS_TR_LT101.Level	TR_System_Sensors_A	TR_LT101.level
TR_LT101	LevelTransmitter	status	VEDCSVMC:VTCS_TR_LT101.status		
TR_LT101	LevelTransmitter	raw	VEDCSVMC:VTCS_TR_LT101.raw	TR_System_Sensors_A	TR_LT101.rawl
TL_HT001	BasePlateHeater	Power	VEDCSVMC:VTCS_TL_HT001.Power	TL_System_Sensors_B	TL_HT001.powr
TL_HT002	BasePlateHeater	Power	VEDCSVMC:VTCS_TL_HT002.Power	TL_System_Sensors_B	TL_HT002.powr
TL_HT003	BasePlateHeater	Power	VEDCSVMC:VTCS_TL_HT003.Power	TL_System_Sensors_B	TL_HT003.powr
TL_HT004	BasePlateHeater	Power	VEDCSVMC:VTCS_TL_HT004.Power	TL_System_Sensors_B	TL_HT004.powr
TL_HT001	BasePlateHeater	Power	VEDCSVMC:VTCS_TL_HT001.Power	TL_System_Sensors_B	TL_HT001.powr
TL_HT002	BasePlateHeater	Power	VEDCSVMC:VTCS_TL_HT002.Power	TL_System_Sensors_B	TL_HT002.powr
TL_HT003	BasePlateHeater	Power	VEDCSVMC:VTCS_TL_HT003.Power	TL_System_Sensors_B	TL_HT003.powr
TL_HT004	BasePlateHeater	Power	VEDCSVMC:VTCS_TL_HT004.Power	TL_System_Sensors_B	TL_HT004.powr
TL_HT001	BasePlateHeater	Power	VEDCSVMC:VTCS_TL_HT001.Power	TL_System_Sensors_B	TL_HT001.powr
TL_HT002	BasePlateHeater	Power	VEDCSVMC:VTCS_TL_HT002.Power	TL_System_Sensors_B	TL_HT002.powr
TL_HT003	BasePlateHeater	Power	VEDCSVMC:VTCS_TL_HT003.Power	TL_System_Sensors_B	TL_HT003.powr
TL_HT004	BasePlateHeater	Power	VEDCSVMC:VTCS_TL_HT004.Power	TL_System_Sensors_B	TL_HT004.powr
TL_HT030	HeaterSwitch	bit	VEDCSVMC:VTCS_TL_HT030.bit	TL_System_Sensors_A	TL_HT030.PWon
TL_HT101	Heater	Power	VEDCSVMC:VTCS_TL_HT101.Power	TL_System_Sensors_B	TL_HT101.powr
TL_HT102	Heater	Power	VEDCSVMC:VTCS_TL_HT102.Power	TL_System_Sensors_B	TL_HT102.powr
TL_HT103	Heater	Power	VEDCSVMC:VTCS_TL_HT103.Power	TL_System_Sensors_B	TL_HT103.powr
TL_HT104	Heater	Power	VEDCSVMC:VTCS_TL_HT104.Power	TL_System_Sensors_B	TL_HT104.powr
TL_HT105	Heater	Power	VEDCSVMC:VTCS_TL_HT105.Power	TL_System_Sensors_B	TL_HT105.powr
TR_HT001	BasePlateHeater	Power	VEDCSVMC:VTCS_TR_HT001.Power	TR_System_Sensors_B	TR_HT001.powr
TR_HT002	BasePlateHeater	Power	VEDCSVMC:VTCS_TR_HT002.Power	TR_System_Sensors_B	TR_HT002.powr
TR_HT003	BasePlateHeater	Power	VEDCSVMC:VTCS_TR_HT003.Power	TR_System_Sensors_B	TR_HT003.powr
TR_HT004	BasePlateHeater	Power	VEDCSVMC:VTCS_TR_HT004.Power	TR_System_Sensors_B	TR_HT004.powr
TR_HT001	BasePlateHeater	Power	VEDCSVMC:VTCS_TR_HT001.Power	TR_System_Sensors_B	TR_HT001.powr

TR_HT002	BasePlateHeater	Power	VEDCSVMC:VTCS_TR_HT002.Power	TR_System_Sensors_B	TR_HT002.pwr
TR_HT003	BasePlateHeater	Power	VEDCSVMC:VTCS_TR_HT003.Power	TR_System_Sensors_B	TR_HT003.pwr
TR_HT004	BasePlateHeater	Power	VEDCSVMC:VTCS_TR_HT004.Power	TR_System_Sensors_B	TR_HT004.pwr
TR_HT001	BasePlateHeater	Power	VEDCSVMC:VTCS_TR_HT001.Power	TR_System_Sensors_B	TR_HT001.pwr
TR_HT002	BasePlateHeater	Power	VEDCSVMC:VTCS_TR_HT002.Power	TR_System_Sensors_B	TR_HT002.pwr
TR_HT003	BasePlateHeater	Power	VEDCSVMC:VTCS_TR_HT003.Power	TR_System_Sensors_B	TR_HT003.pwr
TR_HT004	BasePlateHeater	Power	VEDCSVMC:VTCS_TR_HT004.Power	TR_System_Sensors_B	TR_HT004.pwr
TR_HT030	HeaterSwitch	bit	VEDCSVMC:VTCS_TR_HT030.bit	TR_System_Sensors_A	TR_HT030.PWon
TR_HT101	Heater	Power	VEDCSVMC:VTCS_TR_HT101.Power	TR_System_Sensors_B	TR_HT101.pwr
TR_HT102	Heater	Power	VEDCSVMC:VTCS_TR_HT102.Power	TR_System_Sensors_B	TR_HT102.pwr
TR_HT103	Heater	Power	VEDCSVMC:VTCS_TR_HT103.Power	TR_System_Sensors_B	TR_HT103.pwr
TR_HT104	Heater	Power	VEDCSVMC:VTCS_TR_HT104.Power	TR_System_Sensors_B	TR_HT104.pwr
TR_HT105	Heater	Power	VEDCSVMC:VTCS_TR_HT105.Power	TR_System_Sensors_B	TR_HT105.pwr
TLR_HT102	Heater	Power	VEDCSVMC:VTCS_TLR_HT102.Power	TLR_SystemSensors	TM_HT102.pwr
Tx_HTenb	HeaterSwitch	bit	VEDCSVMC:VTCS_Tx_HTenb.bit	TL_System_Sensors_B	Tx_HTenb.stat
Tx_HTclx	HeaterSwitch	bit	VEDCSVMC:VTCS_Tx_HTclx.bit	TL_System_Sensors_B	Tx_HTclx.stat
TL_PM101	Pump	On	VEDCSVMC:VTCS_TL_PM101.On	TL_System_Sensors_B	TL_PM101.SWon
TL_PM101	Pump	Th_rel_status	VEDCSVMC:VTCS_TL_PM101.Th_rel_status	TL_System_Sensors_B	TL_PM101.TRon
TL_PM101	Pump	pres_ok	VEDCSVMC:VTCS_TL_PM101.pres_ok	TL_System_Sensors_B	TL_PM101.PRok
TL_PM101	Pump	valves_ok	VEDCSVMC:VTCS_TL_PM101.valves_ok	TL_System_Sensors_B	TL_PM101.VLok
TR_PM101	Pump	On	VEDCSVMC:VTCS_TR_PM101.On	TR_System_Sensors_B	TR_PM101.SWon
TR_PM101	Pump	Th_rel_status	VEDCSVMC:VTCS_TR_PM101.Th_rel_status	TR_System_Sensors_B	TR_PM101.TRon
TR_PM101	Pump	pres_ok	VEDCSVMC:VTCS_TR_PM101.pres_ok	TR_System_Sensors_B	TR_PM101.PRok
TR_PM101	Pump	valves_ok	VEDCSVMC:VTCS_TR_PM101.valves_ok	TR_System_Sensors_B	TR_PM101.VLok
TLR_PM101	Pump	On	VEDCSVMC:VTCS_TLR_PM101.On	TLR_SystemSensors	TM_PM101.SWon
TLR_PM101	Pump	Th_rel_status	VEDCSVMC:VTCS_TLR_PM101.Th_rel_status	TLR_SystemSensors	TM_PM101.TRon
TLR_PM101	Pump	pres_ok	VEDCSVMC:VTCS_TLR_PM101.pres_ok	TLR_SystemSensors	TM_PM101.PRok
TLR_PM101	Pump	valves_ok	VEDCSVMC:VTCS_TLR_PM101.valves_ok	TLR_SystemSensors	TM_PM101.VLok
TLR_PM101	Pump	NA			
SA_PM101	ControlledCompressor	FREQ_ACTUAL	VEDCSVMC:VTCS_SA_PM101.FREQ_ACTUAL	SA_SystemValues	SA_PM101.FRac
SA_PM101	ControlledCompressor	FREQ_SETP	VEDCSVMC:VTCS_SA_PM101.FREQ_SETP	SA_SystemValues	SA_PM101.FRtr
SA_PM101	ControlledCompressor	On	VEDCSVMC:VTCS_SA_PM101.On	SA_SystemValues	SA_PM101.SWon
SA_PM101	ControlledCompressor	motor_protect_ok	VEDCSVMC:VTCS_SA_PM101.motor_protect_ok	SA_SystemValues	SA_PM101.MPok
SA_PM101	ControlledCompressor	pres_ok	VEDCSVMC:VTCS_SA_PM101.pres_ok	SA_SystemValues	SA_PM101.PRok
SA_PM101	ControlledCompressor	CURRENT	VEDCSVMC:VTCS_SA_PM101.CURRENT	SA_SystemValues	SA_PM101.curr
SA_PM101	ControlledCompressor	CTRL_WORD1	VEDCSVMC:VTCS_SA_PM101 CTRL_WORD1		
SA_PM101	ControlledCompressor	CTRL_WORD2	VEDCSVMC:VTCS_SA_PM101 CTRL_WORD2		
SA_PM101	ControlledCompressor	STATUS_WORD1	VEDCSVMC:VTCS_SA_PM101 STATUS_WORD1		
SA_PM101	ControlledCompressor	STATUS_WORD2	VEDCSVMC:VTCS_SA_PM101 STATUS_WORD2		
SB_PM101	Compressor	On	VEDCSVMC:VTCS_SB_PM101.On	SB_SystemValues	SB_PM101.SWon
SB_PM101	Compressor	Th_rel_status	VEDCSVMC:VTCS_SB_PM101.Th_rel_status	SB_SystemValues	SB_PM101.TRon
SB_PM101	Compressor	pres_ok	VEDCSVMC:VTCS_SB_PM101.pres_ok	SB_SystemValues	SB_PM101.PRok
TL_BA001---base_freezing	AlarmBit	Alarm	VEDCSVMC:VTCS_TL_BA001---base_freezing.Alarm	TL_Alarms	TL_BA001.alrm
TL_BA002---base_too_hot_TT037	AlarmBit	Alarm	VEDCSVMC:VTCS_TL_BA002---base_too_hot_TT037.Alarm	TL_Alarms	TL_BA002.alrm
TL_BA003---base_too_hot_TT038	AlarmBit	Alarm	VEDCSVMC:VTCS_TL_BA003---base_too_hot_TT038.Alarm	TL_Alarms	TL_BA003.alrm
TL_BA004---base_too_hot_TT039	AlarmBit	Alarm	VEDCSVMC:VTCS_TL_BA004---base_too_hot_TT039.Alarm	TL_Alarms	TL_BA004.alrm
TL_BA005---base_too_hot_TT040	AlarmBit	Alarm	VEDCSVMC:VTCS_TL_BA005---	TL_Alarms	TL_BA005.alrm

			base_too_hot_TT040.Alarm		
TL_BA006---base_TT037_error	AlarmBit	Alarm	VEDCSVMC:VTCS_TL_BA006---base_TT037_error.Alarm	TL_Alarms	TL_BA006.alrm
TL_BA007---base_TT038_error	AlarmBit	Alarm	VEDCSVMC:VTCS_TL_BA007---base_TT038_error.Alarm	TL_Alarms	TL_BA007.alrm
TL_BA008---base_TT039_error	AlarmBit	Alarm	VEDCSVMC:VTCS_TL_BA008---base_TT039_error.Alarm	TL_Alarms	TL_BA008.alrm
TL_BA009---base_TT040_error	AlarmBit	Alarm	VEDCSVMC:VTCS_TL_BA009---base_TT040_error.Alarm	TL_Alarms	TL_BA009.alrm
TL_BW002---base_too_cold_TT037	AlarmBit	Alarm	VEDCSVMC:VTCS_TL_BW002---base_too_cold_TT037.Alarm	TL_Alarms	TL_BW002.alrm
TL_BW003---base_too_cold_TT038	AlarmBit	Alarm	VEDCSVMC:VTCS_TL_BW003---base_too_cold_TT038.Alarm	TL_Alarms	TL_BW003.alrm
TL_BW004---base_too_cold_TT039	AlarmBit	Alarm	VEDCSVMC:VTCS_TL_BW004---base_too_cold_TT039.Alarm	TL_Alarms	TL_BW004.alrm
TL_BW005---base_too_cold_TT040	AlarmBit	Alarm	VEDCSVMC:VTCS_TL_BW005---base_too_cold_TT040.Alarm	TL_Alarms	TL_BW005.alrm
TR_BA001---base_freezing	AlarmBit	Alarm	VEDCSVMC:VTCS_TR_BA001---base_freezing.Alarm	TR_Alarms	TR_BA001.alrm
TR_BA002---base_too_hot_TT037	AlarmBit	Alarm	VEDCSVMC:VTCS_TR_BA002---base_too_hot_TT037.Alarm	TR_Alarms	TR_BA002.alrm
TR_BA003---base_too_hot_TT038	AlarmBit	Alarm	VEDCSVMC:VTCS_TR_BA003---base_too_hot_TT038.Alarm	TR_Alarms	TR_BA003.alrm
TR_BA004---base_too_hot_TT039	AlarmBit	Alarm	VEDCSVMC:VTCS_TR_BA004---base_too_hot_TT039.Alarm	TR_Alarms	TR_BA004.alrm
TR_BA005---base_too_hot_TT040	AlarmBit	Alarm	VEDCSVMC:VTCS_TR_BA005---base_too_hot_TT040.Alarm	TR_Alarms	TR_BA005.alrm
TR_BA006---base_TT037_error	AlarmBit	Alarm	VEDCSVMC:VTCS_TR_BA006---base_TT037_error.Alarm	TR_Alarms	TR_BA006.alrm
TR_BA007---base_TT038_error	AlarmBit	Alarm	VEDCSVMC:VTCS_TR_BA007---base_TT038_error.Alarm	TR_Alarms	TR_BA007.alrm
TR_BA008---base_TT039_error	AlarmBit	Alarm	VEDCSVMC:VTCS_TR_BA008---base_TT039_error.Alarm	TR_Alarms	TR_BA008.alrm
TR_BA009---base_TT040_error	AlarmBit	Alarm	VEDCSVMC:VTCS_TR_BA009---base_TT040_error.Alarm	TR_Alarms	TR_BA009.alrm
TR_BW002---base_too_cold_TT037	AlarmBit	Alarm	VEDCSVMC:VTCS_TR_BW002---base_too_cold_TT037.Alarm	TR_Alarms	TR_BW002.alrm
TR_BW003---base_too_cold_TT038	AlarmBit	Alarm	VEDCSVMC:VTCS_TR_BW003---base_too_cold_TT038.Alarm	TR_Alarms	TR_BW003.alrm
TR_BW004---base_too_cold_TT039	AlarmBit	Alarm	VEDCSVMC:VTCS_TR_BW004---base_too_cold_TT039.Alarm	TR_Alarms	TR_BW004.alrm
TR_BW005---base_too_cold_TT040	AlarmBit	Alarm	VEDCSVMC:VTCS_TR_BW005---base_too_cold_TT040.Alarm	TR_Alarms	TR_BW005.alrm
Tx_BA002---FM455_error	AlarmBit	Alarm	VEDCSVMC:VTCS_Tx_BA002---FM455_error.Alarm	TLR_SA_SB_xx_Alarms	Tx_BA002.alrm
Tx_BA003---baseplate_alarm	AlarmBit	Alarm	VEDCSVMC:VTCS_Tx_BA003---baseplate_alarm.Alarm	TLR_SA_SB_xx_Alarms	Tx_BA003.alrm
Tx_HA101---Clixon_alarm	AlarmBit	Alarm	VEDCSVMC:VTCS_Tx_HA101---Clixon_alarm.Alarm	TLR_SA_SB_xx_Alarms	Tx_HA101.alrm
TL_HA030---bridge_htr2_too_hot	AlarmBit	Alarm	VEDCSVMC:VTCS_TL_HA030---bridge_htr2_too_hot.Alarm	TL_Alarms	TL_HA030.alrm
TL_HA101---HT102_too_cold	AlarmBit	Alarm	VEDCSVMC:VTCS_TL_HA101---HT102_too_cold.Alarm	TL_Alarms	TL_HA101.alrm
TL_HA102---HT102_too_hot	AlarmBit	Alarm	VEDCSVMC:VTCS_TL_HA102---HT102_too_hot.Alarm	TL_Alarms	TL_HA102.alrm
TL_HA103---HT103_too_hot	AlarmBit	Alarm	VEDCSVMC:VTCS_TL_HA103---HT103_too_hot.Alarm	TL_Alarms	TL_HA103.alrm
TL_HA104---HT104_too_hot	AlarmBit	Alarm	VEDCSVMC:VTCS_TL_HA104---HT104_too_hot.Alarm	TL_Alarms	TL_HA104.alrm
TL_HA105---HT105_too_hot	AlarmBit	Alarm	VEDCSVMC:VTCS_TL_HA105---HT105_too_hot.Alarm	TL_Alarms	TL_HA105.alrm
TL_HA111---TT121_error	AlarmBit	Alarm	VEDCSVMC:VTCS_TL_HA111---TT121_error.Alarm	TL_Alarms	TL_HA111.alrm
TL_HA112---TT122_error	AlarmBit	Alarm	VEDCSVMC:VTCS_TL_HA112---TT122_error.Alarm	TL_Alarms	TL_HA112.alrm
TL_HA113---TT123_error	AlarmBit	Alarm	VEDCSVMC:VTCS_TL_HA113---TT123_error.Alarm	TL_Alarms	TL_HA113.alrm
TL_HA114---TT124_error	AlarmBit	Alarm	VEDCSVMC:VTCS_TL_HA114---TT124_error.Alarm	TL_Alarms	TL_HA114.alrm
TL_HA115---TT125_error	AlarmBit	Alarm	VEDCSVMC:VTCS_TL_HA115---TT125_error.Alarm	TL_Alarms	TL_HA115.alrm
TL_HW102---HT102_hot_warning	AlarmBit	Alarm	VEDCSVMC:VTCS_TL_HW102---HT102_hot_warning.Alarm	TL_Alarms	TL_HW102.alrm
TL_HW103---HT103_hot_warning	AlarmBit	Alarm	VEDCSVMC:VTCS_TL_HW103---	TL_Alarms	TL_HW103.alrm

			HT103_hot_warning.Alarm		
TL_HW104---HT104_hot_warning	AlarmBit	Alarm	VEDCSVMC:VTCS_TL_HW104---HT104_hot_warning.Alarm	TL_Alarms	TL_HW104.alrm
TL_HW105---HT105_hot_warning	AlarmBit	Alarm	VEDCSVMC:VTCS_TL_HW105---HT105_hot_warning.Alarm	TL_Alarms	TL_HW105.alrm
TR_HA030---bridge_htr1_too_hot	AlarmBit	Alarm	VEDCSVMC:VTCS_TR_HA030---bridge_htr1_too_hot.Alarm	TR_Alarms	TR_HA030.alrm
TR_HA101---HT102_too_cold	AlarmBit	Alarm	VEDCSVMC:VTCS_TR_HA101---HT102_too_cold.Alarm	TR_Alarms	TR_HA101.alrm
TR_HA102---HT102_too_hot	AlarmBit	Alarm	VEDCSVMC:VTCS_TR_HA102---HT102_too_hot.Alarm	TR_Alarms	TR_HA102.alrm
TR_HA103---HT103_too_hot	AlarmBit	Alarm	VEDCSVMC:VTCS_TR_HA103---HT103_too_hot.Alarm	TR_Alarms	TR_HA103.alrm
TR_HA104---HT104_too_hot	AlarmBit	Alarm	VEDCSVMC:VTCS_TR_HA104---HT104_too_hot.Alarm	TR_Alarms	TR_HA104.alrm
TR_HA105---HT105_too_hot	AlarmBit	Alarm	VEDCSVMC:VTCS_TR_HA105---HT105_too_hot.Alarm	TR_Alarms	TR_HA105.alrm
TR_HA111---TT121_error	AlarmBit	Alarm	VEDCSVMC:VTCS_TR_HA111---TT121_error.Alarm	TR_Alarms	TR_HA111.alrm
TR_HA112---TT122_error	AlarmBit	Alarm	VEDCSVMC:VTCS_TR_HA112---TT122_error.Alarm	TR_Alarms	TR_HA112.alrm
TR_HA113---TT123_error	AlarmBit	Alarm	VEDCSVMC:VTCS_TR_HA113---TT123_error.Alarm	TR_Alarms	TR_HA113.alrm
TR_HA114---TT124_error	AlarmBit	Alarm	VEDCSVMC:VTCS_TR_HA114---TT124_error.Alarm	TR_Alarms	TR_HA114.alrm
TR_HA115---TT125_error	AlarmBit	Alarm	VEDCSVMC:VTCS_TR_HA115---TT125_error.Alarm	TR_Alarms	TR_HA115.alrm
TR_HW102---HT102_hot_warning	AlarmBit	Alarm	VEDCSVMC:VTCS_TR_HW102---HT102_hot_warning.Alarm	TR_Alarms	TR_HW102.alrm
TR_HW103---HT103_hot_warning	AlarmBit	Alarm	VEDCSVMC:VTCS_TR_HW103---HT103_hot_warning.Alarm	TR_Alarms	TR_HW103.alrm
TR_HW104---HT104_hot_warning	AlarmBit	Alarm	VEDCSVMC:VTCS_TR_HW104---HT104_hot_warning.Alarm	TR_Alarms	TR_HW104.alrm
TR_HW105---HT105_hot_warning	AlarmBit	Alarm	VEDCSVMC:VTCS_TR_HW105---HT105_hot_warning.Alarm	TR_Alarms	TR_HW105.alrm
TLR_HA101---HT102_too_cold	AlarmBit	Alarm	VEDCSVMC:VTCS_TLR_HA101---HT102_too_cold.Alarm	TLR_SA_SB_xx_Alarms	TM_HA101.alrm
TLR_HA102---HT102_too_hot	AlarmBit	Alarm	VEDCSVMC:VTCS_TLR_HA102---HT102_too_hot.Alarm	TLR_SA_SB_xx_Alarms	TM_HA102.alrm
TLR_HA112---TT122_error	AlarmBit	Alarm	VEDCSVMC:VTCS_TLR_HA112---TT122_error.Alarm	TLR_SA_SB_xx_Alarms	TM_HA112.alrm
TLR_HW102---HT102_hot_warning	AlarmBit	Alarm	VEDCSVMC:VTCS_TLR_HW102---HT102_hot_warning.Alarm	TLR_SA_SB_xx_Alarms	TM_HW102.alrm
TL_PA101---PT104_TOO_HIGH	AlarmBit	Alarm	VEDCSVMC:VTCS_TL_PA101---PT104_TOO_HIGH.Alarm	TL_Alarms	TL_PA101.alrm
TL_PA102---PT104_101_TOO_HIGH	AlarmBit	Alarm	VEDCSVMC:VTCS_TL_PA102---PT104_101_TOO_HIGH.Alarm	TL_Alarms	TL_PA102.alrm
TL_PA103---PT104_101_TOO_LOW	AlarmBit	Alarm	VEDCSVMC:VTCS_TL_PA103---PT104_101_TOO_LOW.Alarm	TL_Alarms	TL_PA103.alrm
TL_PA106---PM101_membr_alarm	AlarmBit	Alarm	VEDCSVMC:VTCS_TL_PA106---PM101_membr_alarm.Alarm	TL_Alarms	TL_PA106.alrm
TL_PA107---ACCU_PRES_TOO_HIGH	AlarmBit	Alarm	VEDCSVMC:VTCS_TL_PA107---ACCU_PRES_TOO_HIGH.Alarm	TL_Alarms	TL_PA107.alrm
TL_PA108---ANY_PT_TOO_HIGH	AlarmBit	Alarm	VEDCSVMC:VTCS_TL_PA108---ANY_PT_TOO_HIGH.Alarm	TL_Alarms	TL_PA108.alrm
TR_PA101---PT104_TOO_HIGH	AlarmBit	Alarm	VEDCSVMC:VTCS_TR_PA101---PT104_TOO_HIGH.Alarm	TR_Alarms	TR_PA101.alrm
TR_PA102---PT104_101_TOO_HIGH	AlarmBit	Alarm	VEDCSVMC:VTCS_TR_PA102---PT104_101_TOO_HIGH.Alarm	TR_Alarms	TR_PA102.alrm
TR_PA103---PT104_101_TOO_LOW	AlarmBit	Alarm	VEDCSVMC:VTCS_TR_PA103---PT104_101_TOO_LOW.Alarm	TR_Alarms	TR_PA103.alrm
TR_PA106---PM101_membr_alarm	AlarmBit	Alarm	VEDCSVMC:VTCS_TR_PA106---PM101_membr_alarm.Alarm	TR_Alarms	TR_PA106.alrm
TR_PA107---ACCU_PRES_TOO_HIGH	AlarmBit	Alarm	VEDCSVMC:VTCS_TR_PA107---ACCU_PRES_TOO_HIGH.Alarm	TR_Alarms	TR_PA107.alrm
TR_PA108---ANY_PT_TOO_HIGH	AlarmBit	Alarm	VEDCSVMC:VTCS_TR_PA108---ANY_PT_TOO_HIGH.Alarm	TR_Alarms	TR_PA108.alrm

TLR_PA101---PT104_TOO_HIGH	AlarmBit	Alarm	VEDCSVMC:VTCS_TLR_PA101---PT104_TOO_HIGH.Alarm	TLR_SA_SB_xx_Alarms	TM_PA101.alrm
TLR_PA102---PT104-101_TOO_HIGH	AlarmBit	Alarm	VEDCSVMC:VTCS_TLR_PA102---PT104-101_TOO_HIGH.Alarm	TLR_SA_SB_xx_Alarms	TM_PA102.alrm
TLR_PA103---PT104-101_TOO_LOW	AlarmBit	Alarm	VEDCSVMC:VTCS_TLR_PA103---PT104-101_TOO_LOW.Alarm	TLR_SA_SB_xx_Alarms	TM_PA103.alrm
TLR_PA106---PM101_membr_alarm	AlarmBit	Alarm	VEDCSVMC:VTCS_TLR_PA106---PM101_membr_alarm.Alarm	TLR_SA_SB_xx_Alarms	TM_PA106.alrm
SA_PA101---SA_PT108_TOO_HIGH	AlarmBit	Alarm	VEDCSVMC:VTCS_SA_PA101---SA_PT108_TOO_HIGH.Alarm	TLR_SA_SB_xx_Alarms	SA_PA101.alrm
SA_PA102---SA_PT108_TOO_LOW	AlarmBit	Alarm	VEDCSVMC:VTCS_SA_PA102---SA_PT108_TOO_LOW.Alarm	TLR_SA_SB_xx_Alarms	SA_PA102.alrm
SA_PA103---SA_COMPR_LIQUID_IN	AlarmBit	Alarm	VEDCSVMC:VTCS_SA_PA103---SA_COMPR_LIQUID_IN.Alarm	TLR_SA_SB_xx_Alarms	SA_PA103.alrm
SB_PA101---SB_PT108_TOO_HIGH	AlarmBit	Alarm	VEDCSVMC:VTCS_SB_PA101---SB_PT108_TOO_HIGH.Alarm	TLR_SA_SB_xx_Alarms	SB_PA101.alrm
SB_PA102---SB_PT108_TOO_LOW	AlarmBit	Alarm	VEDCSVMC:VTCS_SB_PA102---SB_PT108_TOO_LOW.Alarm	TLR_SA_SB_xx_Alarms	SB_PA102.alrm
SB_PA103---SB_COMPR_LIQUID_IN	AlarmBit	Alarm	VEDCSVMC:VTCS_SB_PA103---SB_COMPR_LIQUID_IN.Alarm	TLR_SA_SB_xx_Alarms	SB_PA103.alrm
TL_MW101---accu_max_setpoint	AlarmBit	Alarm	VEDCSVMC:VTCS_TL_MW101---accu_max_setpoint.Alarm	TL_Alarms	TL_MW101.alrm
TL_MW102---accu_timeout_alarm	AlarmBit	Alarm	VEDCSVMC:VTCS_TL_MW102---accu_timeout_alarm.Alarm	TL_Alarms	TL_MW102.alrm
TL_MA101---CO <sub>2</sub> _frost_alarm	AlarmBit	Alarm	VEDCSVMC:VTCS_TL_MA101---CO <sub>2</sub> _frost_alarm.Alarm	TL_Alarms	TL_MA101.alrm
TL_MA102---CO <sub>2</sub> _frost_alarm_SB	AlarmBit	Alarm	VEDCSVMC:VTCS_TL_MA102---CO <sub>2</sub> _frost_alarm_SB.Alarm	TL_Alarms	TL_MA102.alrm
TL_MA103---PM101_therm_relay_on	AlarmBit	Alarm	VEDCSVMC:VTCS_TL_MA103---PM101_therm_relay_on.Alarm	TL_Alarms	TL_MA103.alrm
TL_MA104---too_warm_accu	AlarmBit	Alarm	VEDCSVMC:VTCS_TL_MA104---too_warm_accu.Alarm	TL_Alarms	TL_MA104.alrm
TL_MA105---too_warm_cookie	AlarmBit	Alarm	VEDCSVMC:VTCS_TL_MA105---too_warm_cookie.Alarm	TL_Alarms	TL_MA105.alrm
TL_MA106---too_warm	AlarmBit	Alarm	VEDCSVMC:VTCS_TL_MA106---too_warm.Alarm	TL_Alarms	TL_MA106.alrm
TR_MW101---accu_max_setpoint	AlarmBit	Alarm	VEDCSVMC:VTCS_TR_MW101---accu_max_setpoint.Alarm	TR_Alarms	TR_MW101.alrm
TR_MW102---accu_timeout_alarm	AlarmBit	Alarm	VEDCSVMC:VTCS_TR_MW102---accu_timeout_alarm.Alarm	TR_Alarms	TR_MW102.alrm
TR_MA101---CO <sub>2</sub> _frost_alarm	AlarmBit	Alarm	VEDCSVMC:VTCS_TR_MA101---CO <sub>2</sub> _frost_alarm.Alarm	TR_Alarms	TR_MA101.alrm
TR_MA102---CO <sub>2</sub> _frost_alarm_SB	AlarmBit	Alarm	VEDCSVMC:VTCS_TR_MA102---CO <sub>2</sub> _frost_alarm_SB.Alarm	TR_Alarms	TR_MA102.alrm
TR_MA103---PM101_therm_relay_on	AlarmBit	Alarm	VEDCSVMC:VTCS_TR_MA103---PM101_therm_relay_on.Alarm	TR_Alarms	TR_MA103.alrm
TR_MA104---too_warm_accu	AlarmBit	Alarm	VEDCSVMC:VTCS_TR_MA104---too_warm_accu.Alarm	TR_Alarms	TR_MA104.alrm
TR_MA105---too_warm_cookie	AlarmBit	Alarm	VEDCSVMC:VTCS_TR_MA105---too_warm_cookie.Alarm	TR_Alarms	TR_MA105.alrm
TR_MA106---too_warm	AlarmBit	Alarm	VEDCSVMC:VTCS_TR_MA106---too_warm.Alarm	TR_Alarms	TR_MA106.alrm
TLR_MA103---PM101_therm_relay_on	AlarmBit	Alarm	VEDCSVMC:VTCS_TLR_MA103---PM101_therm_relay_on.Alarm	TLR_SA_SB_xx_Alarms	TM_MA10.alrm
SA_MA101---SA_drive_fault	AlarmBit	Alarm	VEDCSVMC:VTCS_SA_MA101---SA_drive_fault.Alarm	TLR_SA_SB_xx_Alarms	SA_MA101.alrm
SA_MA102---SA_drive_alarm	AlarmBit	Alarm	VEDCSVMC:VTCS_SA_MA102---SA_drive_alarm.Alarm	TLR_SA_SB_xx_Alarms	SA_MA102.alrm
SA_MA103---SA_PM101_motorprotection	AlarmBit	Alarm	VEDCSVMC:VTCS_SA_MA103---SA_PM101_motorprotection.Alarm	TLR_SA_SB_xx_Alarms	SA_MA103.alrm
SA_MA104---PA_coolingwater_too_hot	AlarmBit	Alarm	VEDCSVMC:VTCS_SA_MA104---PA_coolingwater_too_hot.Alarm	TLR_SA_SB_xx_Alarms	SA_MA104.alrm
SB_MA103---SB_PM101_therm_relay_on	AlarmBit	Alarm	VEDCSVMC:VTCS_SB_MA103---SB_PM101_therm_relay_on.Alarm	TLR_SA_SB_xx_Alarms	SB_MA103.alrm
xx_MA101---extd1311_pwr(SA)_alarm	AlarmBit	Alarm	VEDCSVMC:VTCS_xx_MA101---	TLR_SA_SB_xx_Alarms	xx_MA101.alrm

xx_MA102---exd1306_pwr(htr)_alarm	AlarmBit	Alarm	exd1311_pwr(SA)_alarm.Alarm		
xx_MA103---esd205_pwr(diesel)_alarm	AlarmBit	Alarm	VEDCSVMC:VTCS_xx_MA102--- exd1306_pwr(htr)_alarm.Alarm	TLR_SA_SB_xx_Alarms	xx_MA102.alrm
xx_MA104---venting_alarm	AlarmBit	Alarm	VEDCSVMC:VTCS_xx_MA103--- esd205_pwr(diesel)_alarm.Alarm	TLR_SA_SB_xx_Alarms	xx_MA103.alrm
xx_MA105---haptas_alarm	AlarmBit	Alarm	VEDCSVMC:VTCS_xx_MA104---venting_alarm.Alarm	TLR_SA_SB_xx_Alarms	xx_MA104.alrm
xx_MA106---ref_pt100_error	AlarmBit	Alarm	VEDCSVMC:VTCS_xx_MA105---haptas_alarm.Alarm	TLR_SA_SB_xx_Alarms	xx_MA105.alrm
TL_MA105---haptas_error_vector	AlarmByte	Alarm	VEDCSVMC:VTCS_TL_MA105---haptas_error_vector.Alarm		
TR_MA105---haptas_error_vector	AlarmByte	Alarm	VEDCSVMC:VTCS_TR_MA105--- haptas_error_vector.Alarm		
TLR_MA105---haptas_error_vector	AlarmByte	Alarm	VEDCSVMC:VTCS_TLR_MA105--- haptas_error_vector.Alarm		
TL_VA102---VL102_alarm	AlarmByte	Alarm	VEDCSVMC:VTCS_TL_VA102---VL102_alarm.Alarm		
TL_VA103---VL103_alarm	AlarmByte	Alarm	VEDCSVMC:VTCS_TL_VA103---VL103_alarm.Alarm		
TL_VA104---VL104_alarm	AlarmByte	Alarm	VEDCSVMC:VTCS_TL_VA104---VL104_alarm.Alarm		
TL_VA109---VL109_alarm	AlarmByte	Alarm	VEDCSVMC:VTCS_TL_VA109---VL109_alarm.Alarm		
TL_VA111---VL111_alarm	AlarmByte	Alarm	VEDCSVMC:VTCS_TL_VA111---VL111_alarm.Alarm		
TL_VA112---VL112_alarm	AlarmByte	Alarm	VEDCSVMC:VTCS_TL_VA112---VL112_alarm.Alarm		
TR_VA102---VL102_alarm	AlarmByte	Alarm	VEDCSVMC:VTCS_TR_VA102---VL102_alarm.Alarm		
TR_VA103---VL103_alarm	AlarmByte	Alarm	VEDCSVMC:VTCS_TR_VA103---VL103_alarm.Alarm		
TR_VA104---VL104_alarm	AlarmByte	Alarm	VEDCSVMC:VTCS_TR_VA104---VL104_alarm.Alarm		
TR_VA108---VL108_alarm	AlarmByte	Alarm	VEDCSVMC:VTCS_TR_VA108---VL108_alarm.Alarm		
TR_VA109---VL109_alarm	AlarmByte	Alarm	VEDCSVMC:VTCS_TR_VA109---VL109_alarm.Alarm		
TR_VA111---VL111_alarm	AlarmByte	Alarm	VEDCSVMC:VTCS_TR_VA111---VL111_alarm.Alarm		
TR_VA112---VL112_alarm	AlarmByte	Alarm	VEDCSVMC:VTCS_TR_VA112---VL112_alarm.Alarm		
TLR_VA101---VL101_alarm	AlarmByte	Alarm	VEDCSVMC:VTCS_TLR_VA101---VL101_alarm.Alarm		
TLR_VA109---VL109_alarm	AlarmByte	Alarm	VEDCSVMC:VTCS_TLR_VA109---VL109_alarm.Alarm		
TLR_VA110---VL110_alarm	AlarmByte	Alarm	VEDCSVMC:VTCS_TLR_VA110---VL110_alarm.Alarm		
TLR_VA111---VL111_alarm	AlarmByte	Alarm	VEDCSVMC:VTCS_TLR_VA111---VL111_alarm.Alarm		
TL_PC102---sw_vl103_dis_high_p	ClockTimer	timer	VEDCSVMC:VTCS_TL_PC102---sw_vl103_dis_high_p.timer	TL_TR_Timers	TL_PC102.CLtm
TL_PC103---PM101_starttimer	ClockTimer	timer	VEDCSVMC:VTCS_TL_PC103---PM101_starttimer.timer	TL_TR_Timers	TL_PC103.CLtm
TL_PC104---sw_trans_dis_low_p	ClockTimer	timer	VEDCSVMC:VTCS_TL_PC104---sw_trans_dis_low_p.timer	TL_TR_Timers	TL_PC104.CLtm
TL_PC105---pump_wait_timer	ClockTimer	timer	VEDCSVMC:VTCS_TL_PC105---pump_wait_timer.timer	TL_TR_Timers	TL_PC105.CLtm
TR_PC102---sw_vl103_dis_high_p	ClockTimer	timer	VEDCSVMC:VTCS_TR_PC102--- sw_vl103_dis_high_p.timer	TL_TR_Timers	TR_PC102.CLtm
TR_PC103---PM101_starttimer	ClockTimer	timer	VEDCSVMC:VTCS_TR_PC103---PM101_starttimer.timer	TL_TR_Timers	TR_PC103.CLtm
TR_PC104---sw_trans_dis_low_p	ClockTimer	timer	VEDCSVMC:VTCS_TR_PC104---sw_trans_dis_low_p.timer	TL_TR_Timers	TR_PC104.CLtm
TR_PC105---pump_wait_timer	ClockTimer	timer	VEDCSVMC:VTCS_TR_PC105---pump_wait_timer.timer	TL_TR_Timers	TR_PC105.CLtm
TLR_PC103---PM101_starttimer	ClockTimer	timer	VEDCSVMC:VTCS_TLR_PC103---PM101_starttimer.timer	xx_Timers	TM_PC103.CLtm
SA_PC103---PM101_starttimer	ClockTimer	timer	VEDCSVMC:VTCS_SA_PC103---PM101_starttimer.timer	xx_Timers	SA_PC103.CLtm
SA_PC104---wait_liquid_alarm	ClockTimer	timer	VEDCSVMC:VTCS_SA_PC104---wait_liquid_alarm.timer	xx_Timers	SA_PC104.CLtm
SB_PC103---PM101_starttimer	ClockTimer	timer	VEDCSVMC:VTCS_SB_PC103---PM101_starttimer.timer	xx_Timers	SB_PC103.CLtm
SB_PC104---wait_liquid_alarm	ClockTimer	timer	VEDCSVMC:VTCS_SB_PC104---wait_liquid_alarm.timer	xx_Timers	SB_PC104.CLtm
TL_MC102---ACCU_TIMER	ClockTimer	timer	VEDCSVMC:VTCS_TL_MC102---ACCU_TIMER.timer	TL_TR_Timers	TL_MC102.CLtm
TL_MC103---wait_frost_alarm	ClockTimer	timer	VEDCSVMC:VTCS_TL_MC103---wait_frost_alarm.timer	TL_TR_Timers	TL_MC103.CLtm
TR_MC102---ACCU_TIMER	ClockTimer	timer	VEDCSVMC:VTCS_TR_MC102---ACCU_TIMER.timer	TL_TR_Timers	TR_MC102.CLtm
TR_MC103---wait_frost_alarm	ClockTimer	timer	VEDCSVMC:VTCS_TR_MC103---wait_frost_alarm.timer	TL_TR_Timers	TR_MC103.CLtm
TL_MC105---haptas_timer	ClockTimer	timer	VEDCSVMC:VTCS_TL_MC105---haptas_timer.timer	TL_TR_Timers	TL_MC105.CLtm
TR_MC105---haptas_timer	ClockTimer	timer	VEDCSVMC:VTCS_TR_MC105---haptas_timer.timer	TL_TR_Timers	TR_MC105.CLtm

TLR_MC105---haptas_timer	ClockTimer	timer	VEDCSVMC:VTCS_TLR_MC105---haptas_timer.timer	xx_Timers	TM_MC105.CLtm
TL_VC102---VL102_timer	ClockTimer	timer	VEDCSVMC:VTCS_TL_VC102---VL102_timer.timer	TL_TR_Timers	TL_VC102.CLtm
TL_VC103---VL103_timer	ClockTimer	timer	VEDCSVMC:VTCS_TL_VC103---VL103_timer.timer	TL_TR_Timers	TL_VC103.CLtm
TL_VC104---VL104_timer	ClockTimer	timer	VEDCSVMC:VTCS_TL_VC104---VL104_timer.timer	TL_TR_Timers	TL_VC104.CLtm
TL_VC109---VL109_timer	ClockTimer	timer	VEDCSVMC:VTCS_TL_VC109---VL109_timer.timer	TL_TR_Timers	TL_VC109.CLtm
TL_VC111---VL111_timer	ClockTimer	timer	VEDCSVMC:VTCS_TL_VC111---VL111_timer.timer	TL_TR_Timers	TL_VC111.CLtm
TL_VC112---VL112_timer	ClockTimer	timer	VEDCSVMC:VTCS_TL_VC112---VL112_timer.timer	TL_TR_Timers	TL_VC112.CLtm
TR_VC102---VL102_timer	ClockTimer	timer	VEDCSVMC:VTCS_TR_VC102---VL102_timer.timer	TL_TR_Timers	TR_VC102.CLtm
TR_VC103---VL103_timer	ClockTimer	timer	VEDCSVMC:VTCS_TR_VC103---VL103_timer.timer	TL_TR_Timers	TR_VC103.CLtm
TR_VC104---VL104_timer	ClockTimer	timer	VEDCSVMC:VTCS_TR_VC104---VL104_timer.timer	TL_TR_Timers	TR_VC104.CLtm
TR_VC108---VL108_timer	ClockTimer	timer	VEDCSVMC:VTCS_TR_VC108---VL108_timer.timer	TL_TR_Timers	TR_VC108.CLtm
TR_VC109---VL109_timer	ClockTimer	timer	VEDCSVMC:VTCS_TR_VC109---VL109_timer.timer	TL_TR_Timers	TR_VC109.CLtm
TR_VC111---VL111_timer	ClockTimer	timer	VEDCSVMC:VTCS_TR_VC111---VL111_timer.timer	TL_TR_Timers	TR_VC111.CLtm
TR_VC112---VL112_timer	ClockTimer	timer	VEDCSVMC:VTCS_TR_VC112---VL112_timer.timer	TL_TR_Timers	TR_VC112.CLtm
TLR_VC101---VL101_timer	ClockTimer	timer	VEDCSVMC:VTCS_TLR_VC101---VL101_timer.timer	xx_Timers	TM_VC110.CLtm
TLR_VC109---VL109_timer	ClockTimer	timer	VEDCSVMC:VTCS_TLR_VC109---VL109_timer.timer	xx_Timers	TM_VC109.CLtm
TLR_VC110---VL110_timer	ClockTimer	timer	VEDCSVMC:VTCS_TLR_VC110---VL110_timer.timer	xx_Timers	TM_VC110.CLtm
TLR_VC111---VL111_timer	ClockTimer	timer	VEDCSVMC:VTCS_TLR_VC111---VL111_timer.timer	xx_Timers	TM_VC111.CLtm
TL_HC101---Rth_update_timer	ClockTimer	timer	VEDCSVMC:VTCS_TL_HC101---Rth_update_timer.timer	TL_TR_Timers	TL_HC101.CLtm
TR_HC101---Rth_update_timer	ClockTimer	timer	VEDCSVMC:VTCS_TR_HC101---Rth_update_timer.timer	TL_TR_Timers	TR_HC101.CLtm
TL_MC106---PM101_maintenance	ClockTimer	timer	VEDCSVMC:VTCS_TL_MC106---PM101_maintenance.timer	TL_TR_Timers	TL_MC106.CLtm
TR_MC106---PM101_maintenance	ClockTimer	timer	VEDCSVMC:VTCS_TR_MC106---PM101_maintenance.timer	TL_TR_Timers	TR_MC106.CLtm
TLR_MC106---PM101_maintenance	ClockTimer	timer	VEDCSVMC:VTCS_TLR_MC106---PM101_maintenance.timer	xx_Timers	TM_MC106.CLtm
TL_MC107---wait_cool_transf	ClockTimer	timer	VEDCSVMC:VTCS_TL_MC107---wait_cool_transf.timer	TL_TR_Timers	TL_MC107.CLtm
TR_MC107---wait_cool_transf	ClockTimer	timer	VEDCSVMC:VTCS_TR_MC107---wait_cool_transf.timer	TL_TR_Timers	TR_MC107.CLtm
TL_PC106---wait_low_p	ClockTimer	timer	VEDCSVMC:VTCS_TL_PC106---wait_low_p.timer	TL_TR_Timers	TL_PC106.CLtm
TR_PC106---wait_low_p	ClockTimer	timer	VEDCSVMC:VTCS_TR_PC106---wait_low_p.timer	TL_TR_Timers	TR_PC106.CLtm
xx_MC103---PowerReturnTlimer	ClockTimer	timer	VEDCSVMC:VTCS_xx_MC103---PowerReturnTlimer.timer	xx_Timers	xx_MC103.CLtm
TR_PC106---wait_low_p	ClockTimer	timer	VEDCSVMC:VTCS_TR_PC106---wait_low_p.timer	TL_TR_Timers	TR_PC106.CLtm
Tx_SC101---TIMEOUT_ACCU_HTR	ClockSetting	timer	VEDCSVMC:VTCS_Tx_SC101---TIMEOUT_ACCU_HTR.timer	xx_Timers	Tx_SC101.CLsp
Tx_SC102---WAIT_DISABLE_HIGHP_VL103	ClockSetting	timer	VEDCSVMC:VTCS_Tx_SC102---WAIT_DISABLE_HIGHP_VL103.timer	xx_Timers	Tx_SC102.CLsp
Tx_SC103---WAITTIME_PUMP_SUBCOOL	ClockSetting	timer	VEDCSVMC:VTCS_Tx_SC103---WAITTIME_PUMP_SUBCOOL.timer	xx_Timers	Tx_SC103.CLsp
Tx_SC104---WAIT_DISABLE_LOWP	ClockSetting	timer	VEDCSVMC:VTCS_Tx_SC104---WAIT_DISABLE_LOWP.timer	xx_Timers	Tx_SC104.CLsp
Tx_SC105---WAIT_DP_ALARM	ClockSetting	timer	VEDCSVMC:VTCS_Tx_SC105---WAIT_DP_ALARM.timer	xx_Timers	Tx_SC105.CLsp
Tx_SC106---TIMEOUT_2WAY_VALVE	ClockSetting	timer	VEDCSVMC:VTCS_Tx_SC106---TIMEOUT_2WAY_VALVE.timer	xx_Timers	Tx_SC106.CLsp
Tx_SC107---TIMEOUT_3WAY_VALVE	ClockSetting	timer	VEDCSVMC:VTCS_Tx_SC107---TIMEOUT_3WAY_VALVE.timer	xx_Timers	Tx_SC107.CLsp
Tx_SC108---MAX_TIME_COOL_TRANS_LINE	ClockSetting	timer	VEDCSVMC:VTCS_Tx_SC108---MAX_TIME_COOL_TRANS_LINE.timer	xx_Timers	Tx_SC108.CLsp
Tx_SC109---WAIT_DP_ALARM	ClockSetting	timer	VEDCSVMC:VTCS_Tx_SC109---WAIT_DP_ALARM.timer	xx_Timers	Tx_SC109.CLsp
xx_SC103---WAIT_POWER_RETURN	ClockSetting	timer	VEDCSVMC:VTCS_xx_SC103---WAIT_POWER_RETURN.timer	xx_Timers	xx_SC103.CLsp
TL_SC103---MAX_STARTTIME	ClockSetting	timer	VEDCSVMC:VTCS_TL_SC103---MAX_STARTTIME.timer	TL_TR_Timers	TL_SC103.CLsp
TR_SC103---MAX_STARTTIME	ClockSetting	timer	VEDCSVMC:VTCS_TR_SC103---MAX_STARTTIME.timer	TL_TR_Timers	TR_SC103.CLsp

TLR_SC103---MAX_STARTTIME	ClockSetting	timer	VEDCSVMC:VTCS_TLR_SC103--- MAX_STARTTIME.timer	xx_Timers	TM_SC103.CLsp
SA_SC103---MAX_STARTTIME	ClockSetting	timer	VEDCSVMC:VTCS_SA_SC103---MAX_STARTTIME.timer	xx_Timers	SA_SC103.CLsp
SA_SC104---WAIT_LIQUID_ALARM	ClockSetting	timer	VEDCSVMC:VTCS_SA_SC104--- WAIT_LIQUID_ALARM.timer	xx_Timers	SA_SC104.CLsp
SB_SC102---WAIT_FROST_ALARM	ClockSetting	timer	VEDCSVMC:VTCS_SB_SC102--- WAIT_FROST_ALARM.timer	xx_Timers	SB_SC102.CLsp
SB_SC103---MAX_STARTTIME	ClockSetting	timer	VEDCSVMC:VTCS_SB_SC103---MAX_STARTTIME.timer	xx_Timers	SB_SC103.CLsp
SB_SC104---WAIT_LIQUID_ALARM	ClockSetting	timer	VEDCSVMC:VTCS_SB_SC104--- WAIT_LIQUID_ALARM.timer	xx_Timers	SB_SC104.CLsp
Tx_BL001---BASEPLATE_FREEZING	Limit	Limit	VEDCSVMC:VTCS_Tx_BL001--- BASEPLATE_FREEZING.Limit	Tx_Limits	Tx_BL001.lmit
TL_BL002--- MAX_TEMP_BASEPLATE	Limit	Limit	VEDCSVMC:VTCS_TL_BL002--- MAX_TEMP_BASEPLATE.Limit	Tx_Limits	TL_BL002.lmit
TL_BL003--- MIN_TEMP_BASEPLATE	Limit	Limit	VEDCSVMC:VTCS_TL_BL003--- MIN_TEMP_BASEPLATE.Limit	Tx_Limits	TL_BL003.lmit
TR_BL002--- MAX_TEMP_BASEPLATE	Limit	Limit	VEDCSVMC:VTCS_TR_BL002--- MAX_TEMP_BASEPLATE.Limit	Tx_Limits	TR_BL002.lmit
TR_BL003--- MIN_TEMP_BASEPLATE	Limit	Limit	VEDCSVMC:VTCS_TR_BL003--- MIN_TEMP_BASEPLATE.Limit	Tx_Limits	TR_BL003.lmit
Tx_HL030---BridgeHeater_max	Limit	Limit	VEDCSVMC:VTCS_Tx_HL030---BridgeHeater_max.Limit	Tx_Limits	Tx_HL030.lmit
Tx_HL101---HT102_MIN	Limit	Limit	VEDCSVMC:VTCS_Tx_HL101---HT102_MIN.Limit	Tx_Limits	Tx_HL101.lmit
TL_HL102---HT102_MAX	Limit	Limit	VEDCSVMC:VTCS_TL_HL102---HT102_MAX.Limit	Tx_Limits	TL_HL102.lmit
TL_HL103---HT103_MAX	Limit	Limit	VEDCSVMC:VTCS_TL_HL103---HT103_MAX.Limit	Tx_Limits	TL_HL103.lmit
TL_HL104---HT104_MAX	Limit	Limit	VEDCSVMC:VTCS_TL_HL104---HT104_MAX.Limit	Tx_Limits	TL_HL104.lmit
TL_HL105---HT105_MAX	Limit	Limit	VEDCSVMC:VTCS_TL_HL105---HT105_MAX.Limit	Tx_Limits	TL_HL105.lmit
TL_HL106---HT102_MAX_WARN	Limit	Limit	VEDCSVMC:VTCS_TL_HL106--- HT102_MAX_WARN.Limit	Tx_Limits	TL_HL106.lmit
TL_HL107---HT103_MAX_WARN	Limit	Limit	VEDCSVMC:VTCS_TL_HL107--- HT103_MAX_WARN.Limit	Tx_Limits	TL_HL107.lmit
TL_HL108---HT104_MAX_WARN	Limit	Limit	VEDCSVMC:VTCS_TL_HL108--- HT104_MAX_WARN.Limit	Tx_Limits	TL_HL108.lmit
TL_HL109---HT105_MAX_WARN	Limit	Limit	VEDCSVMC:VTCS_TL_HL109--- HT105_MAX_WARN.Limit	Tx_Limits	TL_HL109.lmit
TR_HL102---HT102_MAX	Limit	Limit	VEDCSVMC:VTCS_TR_HL102---HT102_MAX.Limit	Tx_Limits	TR_HL102.lmit
TR_HL103---HT103_MAX	Limit	Limit	VEDCSVMC:VTCS_TR_HL103---HT103_MAX.Limit	Tx_Limits	TR_HL103.lmit
TR_HL104---HT104_MAX	Limit	Limit	VEDCSVMC:VTCS_TR_HL104---HT104_MAX.Limit	Tx_Limits	TR_HL104.lmit
TR_HL105---HT105_MAX	Limit	Limit	VEDCSVMC:VTCS_TR_HL105---HT105_MAX.Limit	Tx_Limits	TR_HL105.lmit
TR_HL106---HT102_MAX_WARN	Limit	Limit	VEDCSVMC:VTCS_TR_HL106--- HT102_MAX_WARN.Limit	Tx_Limits	TR_HL106.lmit
TR_HL107---HT103_MAX_WARN	Limit	Limit	VEDCSVMC:VTCS_TR_HL107--- HT103_MAX_WARN.Limit	Tx_Limits	TR_HL107.lmit
TR_HL108---HT104_MAX_WARN	Limit	Limit	VEDCSVMC:VTCS_TR_HL108--- HT104_MAX_WARN.Limit	Tx_Limits	TR_HL108.lmit
TR_HL109---HT105_MAX_WARN	Limit	Limit	VEDCSVMC:VTCS_TR_HL109--- HT105_MAX_WARN.Limit	Tx_Limits	TR_HL109.lmit
TLR_HL102---HT102_MAX	Limit	Limit	VEDCSVMC:VTCS_TLR_HL102---HT102_MAX.Limit	Tx_Limits	TM_HL10.lmit
TLR_HL106---HT102_MAX_WARN	Limit	Limit	VEDCSVMC:VTCS_TLR_HL106--- HT102_MAX_WARN.Limit	Tx_Limits	TM_HL10.lmit
TL_PL101---PT104_MAX	Limit	Limit	VEDCSVMC:VTCS_TL_PL101---PT104_MAX.Limit	Tx_Limits	TL_PL101.lmit
TL_PL102---PT104_101_MAXDIFF	Limit	Limit	VEDCSVMC:VTCS_TL_PL102--- PT104_101_MAXDIFF.Limit	Tx_Limits	TL_PL102.lmit

TL_PL103---PT104_101_MINDIFF	Limit	Limit	VEDCSVMC:VTCS_TL_PL103--- PT104_101_MINDIFF.Limit	Tx_Limits	TL_PL103.lmit
TL_PL107---PT102_max	Limit	Limit	VEDCSVMC:VTCS_TL_PL107---PT102_max.Limit	Tx_Limits	TL_PL107.lmit
Tx_PL108--- MAX_PRESS_CLOSED_VOLUME	Limit	Limit	VEDCSVMC:VTCS_Tx_PL108--- MAX_PRESS_CLOSED_VOLUME.Limit	Tx_Limits	Tx_PL108.lmit
TR_PL101---PT104_MAX	Limit	Limit	VEDCSVMC:VTCS_TR_PL101---PT104_MAX.Limit	Tx_Limits	TR_PL101.lmit
TR_PL102---PT104_101_MAXDIFF	Limit	Limit	VEDCSVMC:VTCS_TR_PL102--- PT104_101_MAXDIFF.Limit	Tx_Limits	TR_PL102.lmit
TR_PL103---PT104_101_MINDIFF	Limit	Limit	VEDCSVMC:VTCS_TR_PL103--- PT104_101_MINDIFF.Limit	Tx_Limits	TR_PL103.lmit
TR_PL107---PT102_max	Limit	Limit	VEDCSVMC:VTCS_TR_PL107---PT102_max.Limit	Tx_Limits	TR_PL107.lmit
TLR_PL101---PT104_MAX	Limit	Limit	VEDCSVMC:VTCS_TLR_PL101---PT104_MAX.Limit	Tx_Limits	TM_PL101.lmit
TLR_PL102---PT104_101_MAXDIFF	Limit	Limit	VEDCSVMC:VTCS_TLR_PL102--- PT104_101_MAXDIFF.Limit	Tx_Limits	TM_PL102.lmit
TLR_PL103---PT104_101_MINDIFF	Limit	Limit	VEDCSVMC:VTCS_TLR_PL103--- PT104_101_MINDIFF.Limit	Tx_Limits	TM_PL103.lmit
SL_PL104--- DIFF_SA_TT121_PT107_TSAT	Limit	Limit	VEDCSVMC:VTCS_SL_PL104--- DIFF_SA_TT121_PT107_TSAT.Limit	Sx_Limits	SL_PL104.lmit
SB_PL104--- DIFF_SB_TT121_PT103_TSAT	Limit	Limit	VEDCSVMC:VTCS_SB_PL104--- DIFF_SB_TT121_PT103_TSAT.Limit	Sx_Limits	SB_PL104.lmit
SB_PL105--- DIFF_SB_TT121_PT104_TSAT	Limit	Limit	VEDCSVMC:VTCS_SB_PL105--- DIFF_SB_TT121_PT104_TSAT.Limit	Sx_Limits	SB_PL105.lmit
TL_ML101---max_accu_setp	Limit	Limit	VEDCSVMC:VTCS_TL_ML101---max_accu_setp.Limit	Tx_Limits	TL_ML101.lmit
Tx_ML101---CO <sub>2</sub> _lowest_temp	Limit	Limit	VEDCSVMC:VTCS_Tx_ML101---CO <sub>2</sub> _lowest_temp.Limit	Tx_Limits	Tx_ML101.lmit
Tx_ML104---Too_Warm_Threshold	Limit	Limit	VEDCSVMC:VTCS_Tx_ML104--- Too_Warm_Threshold.Limit	Tx_Limits	Tx_ML104.lmit
Tx_ML105---Rth_MAX	Limit	Limit	VEDCSVMC:VTCS_Tx_ML105---Rth_MAX.Limit	Tx_Limits	Tx_ML105.lmit
Tx_ML106---Rth_MIN	Limit	Limit	VEDCSVMC:VTCS_Tx_ML106---Rth_MIN.Limit	Tx_Limits	Tx_ML106.lmit
Tx_ML107---HT105_MAX_HLM	Limit	Limit	VEDCSVMC:VTCS_Tx_ML107---HT105_MAX_HLM.Limit	Tx_Limits	Tx_ML107.lmit
Tx_ML107---HT105_MIN_HLM	Limit	Limit	VEDCSVMC:VTCS_Tx_ML107---HT105_MIN_HLM.Limit	Tx_Limits	Tx_ML107.lmit
TR_ML101---max_accu_setp	Limit	Limit	VEDCSVMC:VTCS_TR_ML101---max_accu_setp.Limit	Tx_Limits	TR_ML101.lmit
PA_ML101---TT101_MAX	Limit	Limit	VEDCSVMC:VTCS_PA_ML101---TT101_MAX.Limit	Sx_Limits	PA_ML101.lmit
xx_ML101--- MAX_HAPTAS_CALIBR_ERROR	Limit	Limit	VEDCSVMC:VTCS_xx_ML101--- MAX_HAPTAS_CALIBR_ERROR.Limit	Tx_Limits	xx_ML101.lmit
Sx_ML101---SASB_takeover_threshold	Limit	Limit	VEDCSVMC:VTCS_Sx_ML101--- SASB_takeover_threshold.Limit	Sx_Limits	Sx_ML101.lmit
TL_AC101	Accumulator	SETPOINT	VEDCSVMC:VTCS_TL_AC101.SETPOINT	TL_System_Sensors_A	TL_AC101.SPac
TL_AC101	Accumulator	TARGET_SETPOINT	VEDCSVMC:VTCS_TL_AC101.TARGET_SETPOINT	TL_System_Sensors_A	TL_AC101.SPtr
TL_AC101	Accumulator	Rth	VEDCSVMC:VTCS_TL_AC101.Rth	TL_System_Sensors_A	TL_AC101.Rthm
TR_AC101	Accumulator	SETPOINT	VEDCSVMC:VTCS_TR_AC101.SETPOINT	TR_System_Sensors_A	TR_AC101.SPac
TR_AC101	Accumulator	TARGET_SETPOINT	VEDCSVMC:VTCS_TR_AC101.TARGET_SETPOINT	TR_System_Sensors_A	TR_AC101.Sptr
TR_AC101	Accumulator	Rth	VEDCSVMC:VTCS_TR_AC101.Rth	TR_System_Sensors_A	TR_AC101.Rthm

## 11.8 Additional base plate heater information

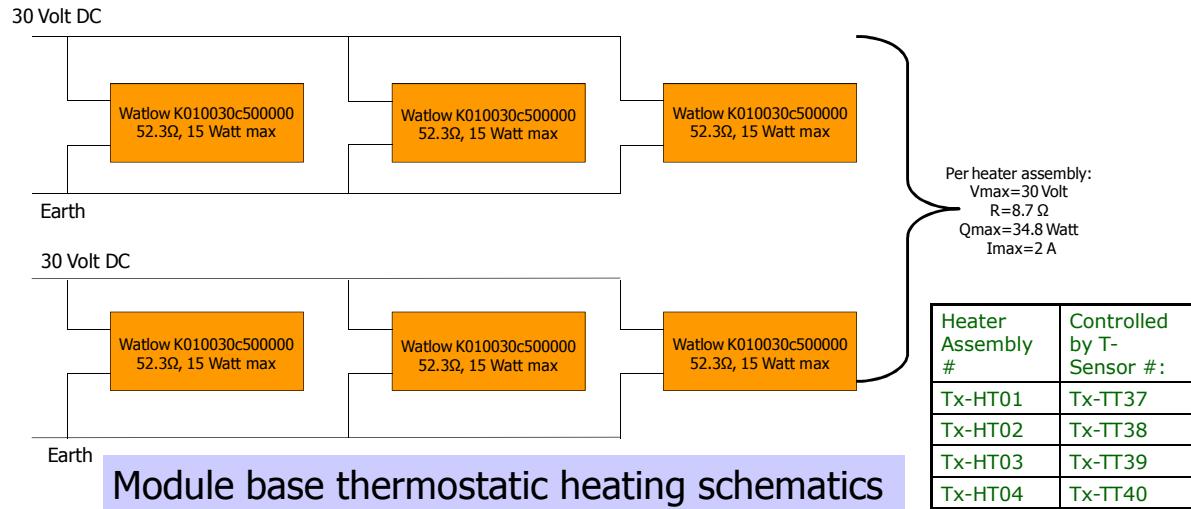


Figure 11.8-1: Baseplate heater electrical layout

## Module Base Slow Control Interface Board Layout

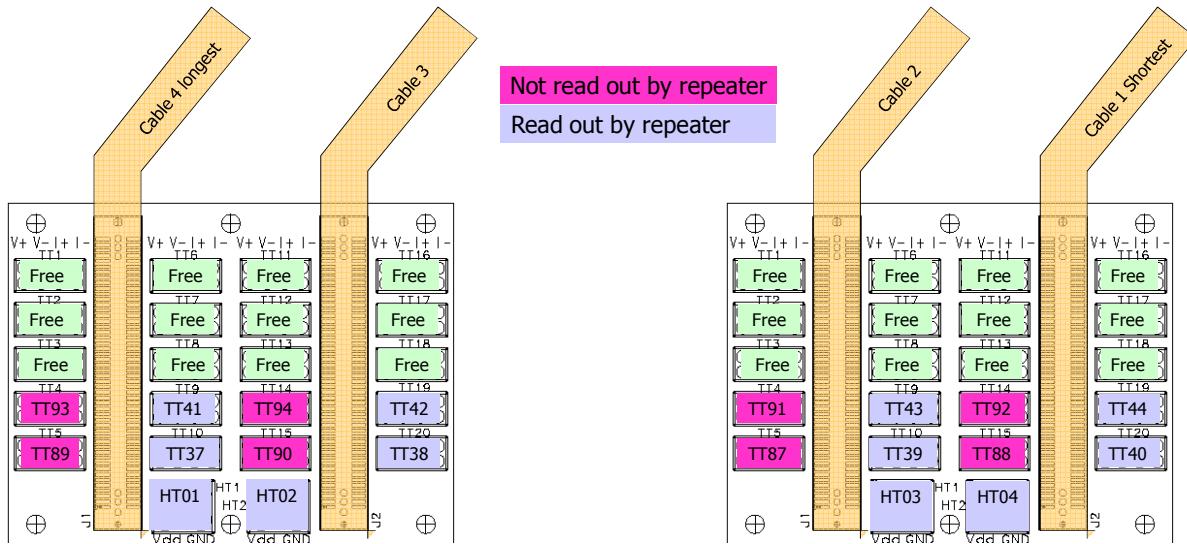


Figure 11.8-2: Baseplate heater cable connectors

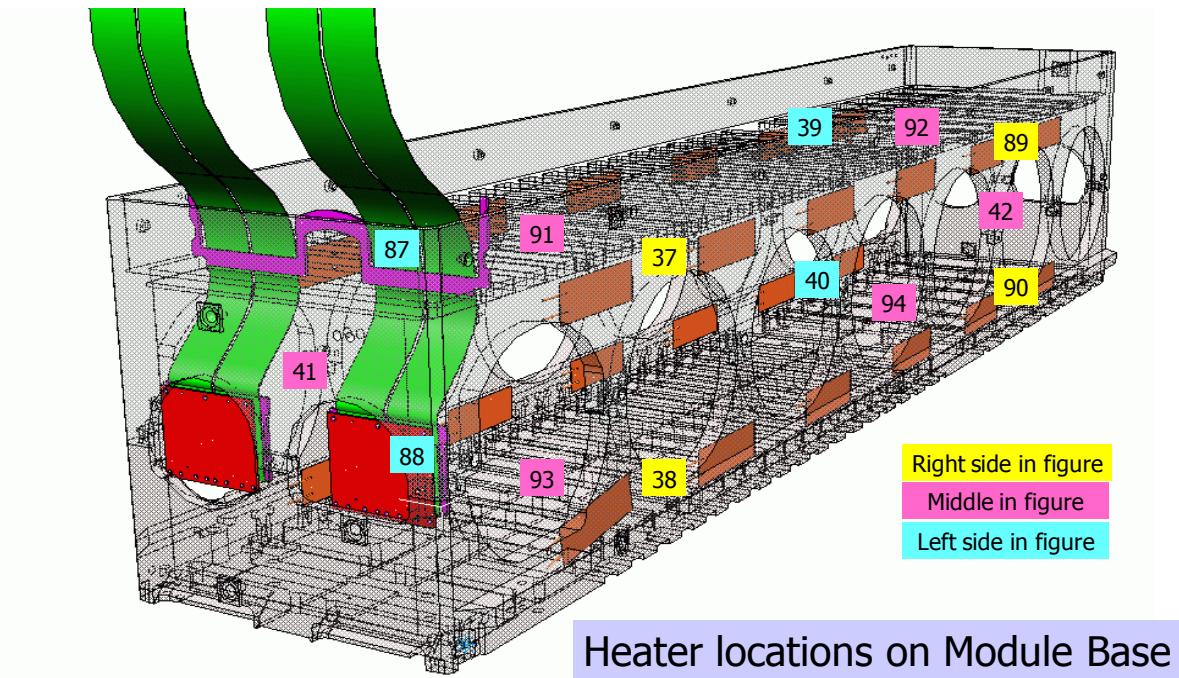


Figure 11.8-3: Base plate heater temperature sensor locations

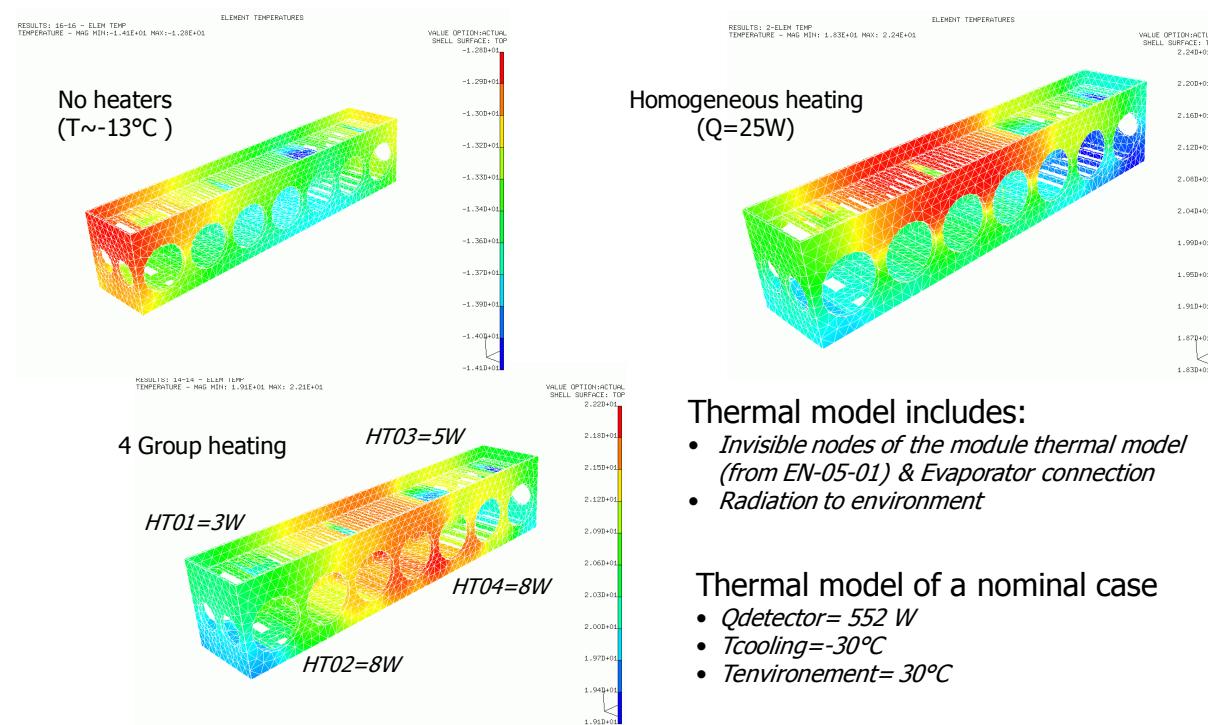


Figure 11.8-4: Base plate thermal simulation

## 11.9 Additional evaporator information

### INPUT

$$\boxed{\text{bar} := 0.1 \frac{\text{N}}{\text{mm}^2}}$$

Conversion factor

$$k := 1.5$$

Safety factor

$$P := 100\text{bar}$$

Pressure

$$H_2 := 18.5\text{mm}$$

Diameter conflat knife

$$n := 6$$

Number of bolts

$$C := 500 \frac{\text{N}}{\text{mm}}$$

Sealing force ( $C=300-500\text{N/mm}$ )

$$C_{\min} := 300 \frac{\text{N}}{\text{mm}}$$

Minimum sealing force

$$d_{\text{m4}} := 4\text{mm}$$

Diameter bolts

$$d_{\text{m4A}} := 3.5\text{mm}$$

Minor diameter bolts

$$k\text{N} := 1000\text{N}$$

Conversion factor

$$p := 0.7\text{mm}$$

Pitch

$$\beta := 60\text{deg}$$

apex angle

$$\phi := \arctan\left(\frac{p}{\pi \cdot d_{\text{m4A}}}\right)$$

Pitch angle

$$\phi = 3.6\text{ deg}$$

$$\mu_k := 0.15$$

Friction factor

$$\rho := \arctan\left(\frac{\mu_k}{\cos\left(\frac{\beta}{2}\right)}\right)$$

Friction angle

$$\rho = 9.83\text{ deg}$$

$$\text{Nm} := \text{N mm}$$

Conversion factor

### CALCULATION

$$P_B := k P$$

Internal pressure

$$P_B = 15 \frac{\text{N}}{\text{mm}^2}$$

$$\text{Pressure load}$$

$$A_p := 0.25 \cdot \pi \cdot H_2^2$$

$$F_p := P_B A_p$$

$$F_p = 4 \times 10^3 \text{ N}$$

$$F_{p,b} := \frac{F_p}{n}$$

$$F_{p,b} = 672 \text{ N}$$

$$\text{Sealing force}$$

$$\text{circumferential} := \pi \cdot H_2$$

$$\text{circumferential} = 58.1\text{mm}$$

$$F_{\text{seal}} := C \cdot \text{circumferential}$$

$$F_{\text{seal}} = 2.9 \times 10^4 \text{ N}$$

$$F_{\text{seal,b}} := \frac{F_{\text{seal}}}{n}$$

$$F_{\text{seal,b}} = 4.8 \times 10^3 \text{ N}$$

$$\sigma := \frac{(F_{p,b} + F_{\text{seal,b}})}{0.25 \cdot \pi \cdot d_{\text{m4}}^2}$$

$$\sigma = 438.9 \frac{\text{N}}{\text{mm}^2}$$

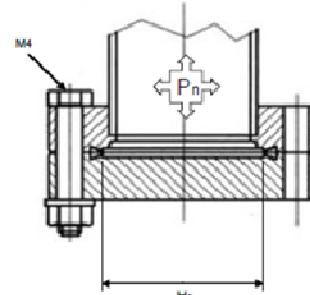
$$F_{\text{bol,tot}} := F_{\text{seal,b}} + F_{p,b}$$

$$F_{\text{bol,tot}} = 5.51\text{ kN}$$

Max.negative force in m4 bolt (12.9): 6.8 kN

Yield stress of m4 bolt (12.9): 1100 N/mm<sup>2</sup>

Bolt strength is sufficient



flange surface

pressure load

force per bolt

Minimum Sealing force:

$$F_{\text{seal,min}} := C_{\min} \cdot \text{circumferential}$$

$$F_{\text{seal,min}} = 1.7 \times 10^4 \text{ N}$$

$$F_{\text{seal}} - F_p > F_{\text{seal,min}}$$

$$F_{\text{seal}} - F_p = 2.5 \times 10^4 \text{ N}$$

circumferential conflat knife

sealing force in bolt

tensile stress per bolt

$$T_t := \left( F_{\text{bol,tot}} \tan(\phi + \rho) \cdot \frac{d_{\text{m4A}}}{2} \right)$$

$$T_t = 2.3 \text{ Nm} \quad \text{Torque from turning}$$

$$T_f := \mu_k \cdot F_{\text{bol,tot}} \cdot 1.3 \cdot \frac{d_{\text{m4}}}{2}$$

$$T_f = 2.2 \text{ Nm} \quad \text{Torque from friction}$$

$$T := T_t + T_f$$

$$T = 4.5 \text{ Nm} \quad \text{Total torque}$$

Max. Torque on m4 bolt(12.9): 5.2Nm

Figure 11.9-1: Calculation of the evaporator inlet connector connection

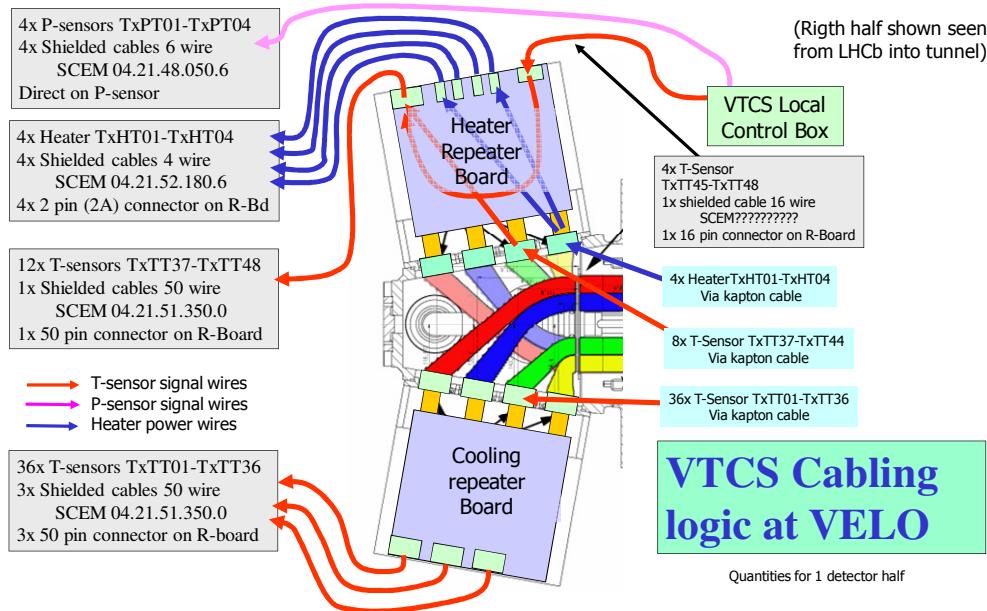


Figure 11.9-2: Evaporator and module base cabling to PLC

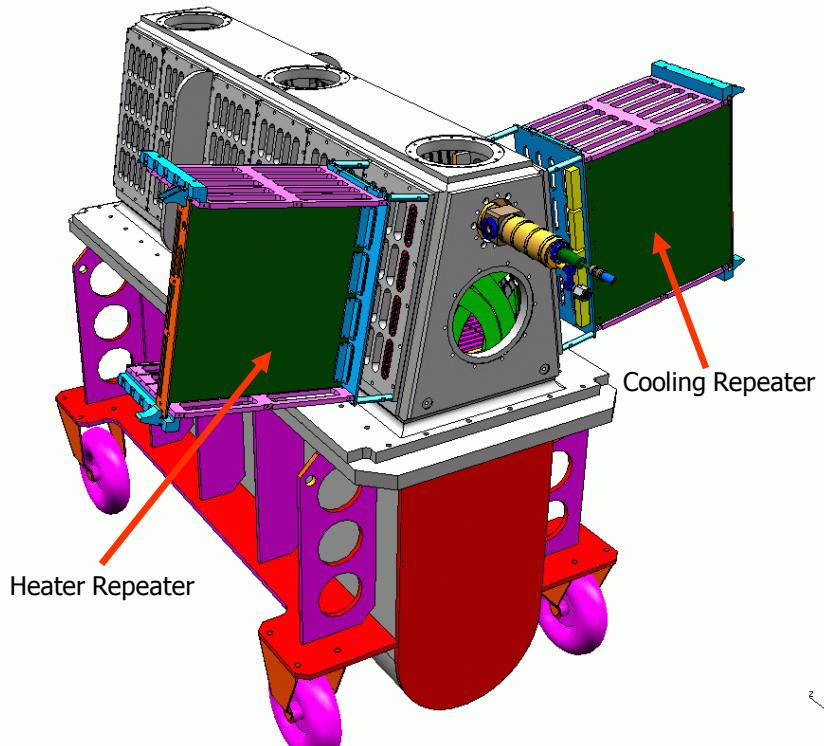


Figure 11.9-3: Cooling repeaterboards

**Evaporator Temperature sensor cabling situation in side the secondary vacuum**

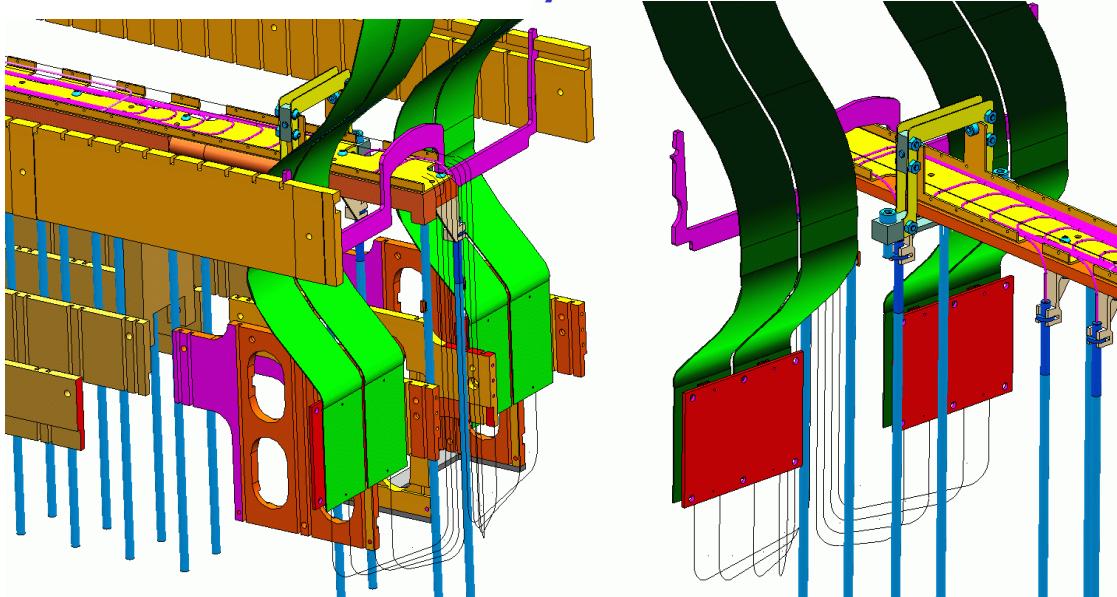


Figure 11.9-4: Evaporator kapton cable 1

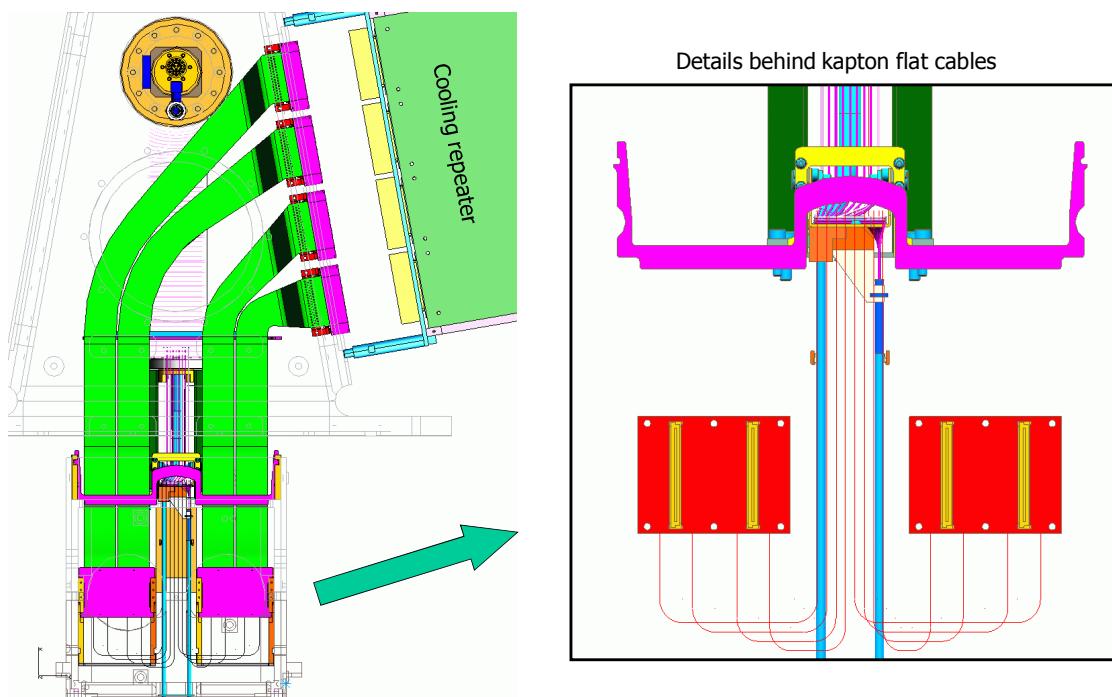


Figure 11.9-5: Evaporator kapton cable 2

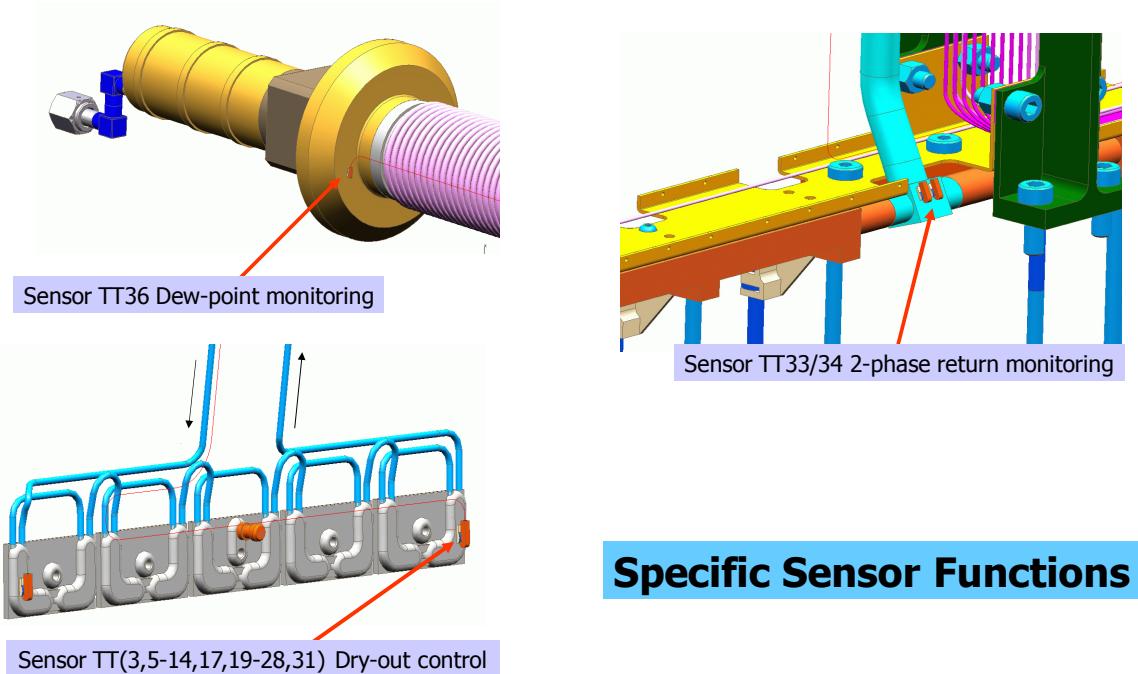


Figure 11.9-6: Evaporator temperature sensor locations

## Evaporator Slow Control Interface Board Layout

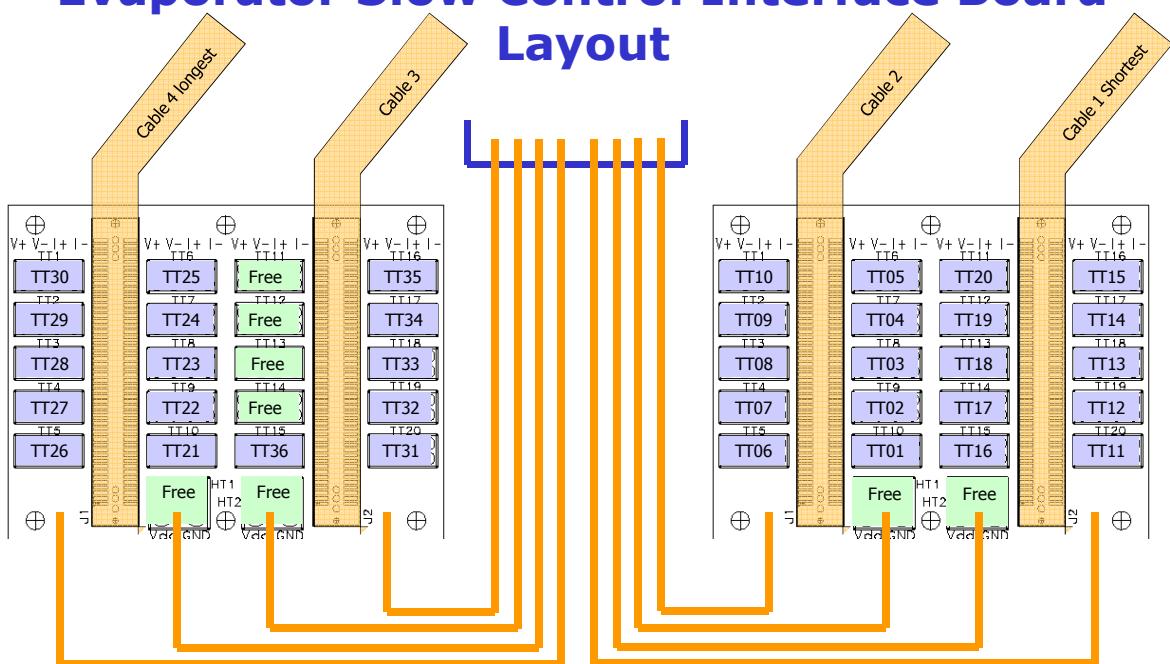


Figure 11.9-7: Evaporator temperature sensor interface board layout

Senor Label	Length (mm)		Senor Label	Length (mm)
TT 1	430		TT 20	1340
TT 2	860		TT 21	1380
TT 3	850		TT 22	1410
TT 4	410		TT 23	1430
TT 5	890		TT 24	1450
TT 6	1010		TT 25	1610
TT 7	1030		TT 26	1780
TT 8	1060		TT 27	1820
TT 9	1080		TT 28	1870
TT 10	1100		TT 29	1480
TT 11	1170		TT 30	1900
TT 12	1200		TT 31	1920
TT 13	1220		TT 32	1490
TT 14	1250		TT 33	1380
TT 15	840		TT 34	1370
TT 16	1300		TT 35	1370
TT 17	1300		TT 36	2260
TT 18	860			=====
TT 19	1310		total (mm)	46430
			Average (mm)	1290

- Cable lengths are from TT sensor to soldering patch on interface board. Over length is included

- All shown lengths are similar for the left and right detector. Shown are the sensors of 1 detector half. Every sensor need to be fabricated 2 times.

- Sensor ID TT37 – TT48, will be cut to length when assembled. Pre made length for all will be **1500 mm**

Figure 11.9-8: Evaporator temperature senosor cabling length