

Signals Correlation Algorithms For Cheaper Surveys: Using Windowing Functions.

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ABSTRACT

This paper investigates the use of baseline dependent windowing functions in interferometry data to minimize the loss of signal amplitude (smearing) when the correlated data is averaged over wide bandwidth and long time. In radio interferometry smearing is reduced when a cross-correlator averages the correlated data over narrower bandwidth and shorter integration times. Unfortunately, this leads to a huge amount of data to manage and it is becoming a bottleneck for further data processing such as calibration and imaging. With future generation surveys, it is important to investigate the reduction of the output data rate. Therefore, the focus of this paper is on the use of baselines dependent windowing functions to keep smearing down at an acceptable extent and at the same time significantly suppress signals from out field of view sources, while the nominal sensitivity is conserved.

Key words: Instrumentation: interferometers, Methods: data analysis, Methods: numerical, Techniques: interferometric

1 INTRODUCTION

The recent radio astronomy techniques is to build a single, gigantic instrument called *interferometer*, from the combination of several small parabolic antennas separated over kilometres (?). The signal from each antenna is combined at the level of a cross-correlator to form the interferometer data output. The cross-correlator carries out data reduction and filters out an amount of noise by averaging the signal of each baseline over discrete time and/or frequency bins. It is well known in interferometry that averaging can lead to the loss of signal amplitude when the cross correlator integrate over a longer period of time and a wider bandwidth. This effect is known as time-average smearing and bandwidth smearing (Thompson *et al.* ?). The above effects cause the distortion of sources within the field of interest by decreasing their intensity.

To keep smearing down at acceptable levels, a correlator must cross-correlate the signal over a shorter period of time and a narrower bandwidth, hence producing a large amount of data for subsequence stage such as imaging (Martí-Vidal & Marcaide 2008; Linfield 1986), calibration (?), etc. This huge amount of data is becoming an increasingly serious

problem and becoming more challenging as the computational demands of the next generation radio telescopes will rise significantly (see the SKA phase 1 specification ?). Similarly, the next generation of radio telescopes will require an unprecedented level of SNR while mapping large regions of the sky. Thus, a substantial increase in SNR can only be achieved by observing for longer time at wider bandwidth without loss of signal: this is not realisable with averaging. Therefore, it becomes urgent to develop new decorrelation algorithm techniques that will allow the required SNR of the future radio telescopes.

In this paper, we investigate the efficiency of correlator windowing functions for the reduction of interferometric data and the recovery of interferometers arrays desire FoV, with the ultimate goal of reaching higher SNR. The main idea is to achieve a high SNR by conserving the astrophysical signal and by limiting the noise. Thermal noise can be driven arbitrary low by increasing the observing time¹, but in radio astronomy confusion noise is a major problem and can even cause calibration to fail. Therefore, we seek to use a windowing function that will conserve the useful signal while also limiting sidelobes confusion from out of FoV sources.

$$SNR = \frac{S_{use}}{N_{ter} + N_{con}} \quad (1)$$

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- "Useful signal", S_{use} the signal from source in the field of interest. These sources should be accurately recovered over the instrument entire FoV : correlator windowing functions maximized this signal by allowing the interferometer array to map a large region of the sky.

- "Sidelobe confusion", N_{con} signal from out field of view sources received from their sidelobes. These sources are not of interest and should be removed : correlator windowing functions acts as a remover of these signals when the array is mapping a large region of the sky.

- "Thermal noise", N_{ter} the thermal noise from the instrument, ionosphere, etc. Averaging presents theoretically a maximum sensitivity, but the use of extended correlator windowing functions can reduce or eliminate the loss of the nominal sensitivity.

The proposed techniques are applied to MeerKAT (Karoo Array Telescope) ? and the Very Large Array (VLA)? and could also be used for future radio telescopes such as the SKA.

2 OVERVIEWS AND DEFINITIONS

2.1 Visibility and relation with the sky

An interferometer array measured a quantity $V = V(u, v, w)$ known classically as the visibility function (see ?). The variables u, v and w are in unit of wavelength and they are the coordinates of the vector of which the norm is the distance between two antennas, known in interferometry as a baseline. A source in the sky will see u and v oriented towards the direction East-West and South-North respectively and w is directed towards the phase centre of the source plane or image plane. The projection of u and v in the image plane are l and m respectively. They are the observed source coordinates, measured in radian. The ideal measurement of interferometric wide-field imaging also known as the van Cittert-Zernike theorem (Thompson *et al.* 2001, Eq.6) is given by

$$V_{pq,(u,v,w)} = \iint \frac{I(l,m)}{\sqrt{1-l^2-m^2}} e^{-2\pi i \phi(u,v,w)} dl dm, \quad (2)$$

where $I(l,m)$ is the sky brightness and $\phi(u,v,w) = ul + vm + w(\sqrt{1-l^2-m^2}-1)$ is a term from the cross-correlator that models the direction in the sky and the separation of the two antennas. The term $\sqrt{1-l^2-m^2}$ is the result of the projection of the celestial sphere on the image plane.

2.2 Averaging and convolution

The Earth rotation causes the phase, $\phi(u,v,w)$ to variate in time. The baseline coordinates are defined in units of wavelength, and making $\phi(u,v,w)$ to variate in frequency. To take this effect into account, Eq. 2 is rewritten as an integration over time and frequency interval. If we consider that $[t_s, t_e]$ is the time integration interval and $[v_s, v_e]$ the frequency integration interval, then Eq.2 can be rewritten as:

$$V_{pq,(t_e,v_e)}^{corr} = \frac{1}{\Delta t \Delta v} \int_{t_s}^{t_e} \int_{v_s}^{v_e} V_{pq,(t,v)} dv dt. \quad (3)$$

Here, $V_{pq,(t,v)}$ is a continuous function, in reality we know only the sampled visibility. Nevertheless, when measuring

the sampled visibility, the antennas reception pattern or "primary beam", $A_{t,v}$ which describes the sensitivity of the interferometer elements p and q , with radius from the centre of the dish beam is taken into account. With this assumption, the sampled visibility measured at discrete spaces is:

$$V_{pq,(t,v)}^{samp} = S_{pq,(t,v)} \left(V_{pq,(t,v)} \circ A_{t,v} \right), \quad (4)$$

where \circ denote the convolution operator and $S_{pq,(t,v)}$ is a sampling function that indicates where the (u,v) data for the baseline (p,q) are measured during the integration. It is unity where measurement have been made, and zero otherwise. Therefore, Eq.3 holds for many sources, when the signal at the centre frequency and at the centre time is restricted to a narrow frequency interval and to a short time interval, this is the current efficient observing mode. However, the mathematics behind is as follows:

$$V_{pq,(t_e,v_e)}^{corr} = \frac{1}{n_t n_v} \sum_{i=1}^{n_t} \sum_{j=1}^{n_v} V_{pq,(t_i,v_j)}^{samp}. \quad (5)$$

Here, n_t and n_v are the number of discrete times within the time interval and the number of discrete frequency within the frequency interval respectively. For convenience, lets introduce a normalized *Boxcar* windowing function, $\Pi_{pq,(t_e-t_i,v_e-v_j)}$ that will attribute an equal weight (in this case $1/n_t n_v$) to all sampling visibilities points. We can therefore rewrite Eq. 5 as:

$$V_{pq,(t_e,v_e)}^{corr} = \sum_{i=1}^{n_t} \sum_{j=1}^{n_v} \Pi_{pq,(t_e-t_i,v_e-v_j)} V_{pq,(t_i,v_j)}^{samp}. \quad (6)$$

It is worth noting that Eq.6 is a naturally weighted visibility and is a two dimensional convolution between the *Boxcar* windowing function and the sampled visibility. Thus, averaging is equivalent to convolving the sampled visibility with a *Boxcar* windowing function. Mathematically, this is described as follows:

$$V_{pq,(t_e,v_e)}^{corr} = c_{pq,(t,v)} \cdot \left(\left(\Pi_{pq} \circ V_{pq}^{samp} \right)_{(t,v)} \right). \quad (7)$$

Here, $c_{pq,(t,v)}$ is a function that samples the result of $\left(\Pi_{pq} \circ V_{pq}^{samp} \right)_{(t,v)}$ at the centre time interval and centre frequency interval.

Nevertheless, we note that this is not an efficient mode of attributing the weight of baselines visibilities. This mean that, the baselines of the array are all suppose equally in term of the statistical analyse of the signals from the astronomical source. Unfortunately, this is not the case, since we lost informations on some baselines than order due to the incomplete sampling of the Fourier component that differ from one baseline to another.

2.3 Effect of time and bandwidth averaging

During imaging (Martí-Vidal & Marcaide 2008), Eq.7 is inverse Fourier transform, and the convolution theorem is applied, the *sinc* function therefore multiply the sky (see appendixB for a short discussion and illustration). Thus, the sky map is tapered by the *sinc* function in the l and m direction, the response is maximal for sources at the phase

centre ($l = 0, m = 0$), while for off-phase centre sources, the response is smeared (decreased) for larger Δt and $\Delta \nu$. The Fourier phase components $2\pi\phi(u, v, w)$ is a function of the direction in the sky, the wavelength, the separation of antennas as well as the integration time and frequency. Therefore, a maximal phase will occurs on longer baselines while a small phase on shorter baselines. Thus, this explained while the degree of smearing increases with the position of a source and the baseline length (see Thompson et al.).

- Fig.1 shows the attenuation of a source at various coordinates in the sky for various integration time interval. More than 90% of the source brightness is measured for integration less than or equal to 25s when this source is within $[0^\circ, 3^\circ]$. We can noticed on this figure that, we could not maintained the 90% of the source brightness within $[0^\circ, 1^\circ]$ if the desire FoV is 2° and suppressed the source within $[1^\circ, 3^\circ]$ with these short integration. Therefore, as mention earlier in this work, a small integration produced large data and maintained sidelobes contamination from out field of view sources.

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Fortunately, since the response is maximal only for sources at the phase centre, an interesting approach is achieved by convolving the observed visibility with a windowing function that depends on (u, v) coordinates spacing (baseline dependent windowing function). However, a windowing function with a wide dynamic range spectrum is preferable in this work.

2.4 Imaging

Recall from the previous section that, the boxcar windowing function can be replaced by a windowing function, $W_{pq,(t,\nu)}$ that depends on (u, v) spacing. Now, consider that $\mathbf{W}_{pq,(t,\nu)}$ is a $n_t \times n_\nu$ matrix of elements $W_{pq,(t_i, \nu_j)}^{j=1, n_\nu}_{i=1, n_t}$, the weights of (u, v) points. From the full sky Radio Interferometry Measurement Equation (RIME) formalism (see Hamaka et al, O.M. Smirnov (2010a)), the sampled visibilities can be presented mathematically as a $4 \times n_t \times n_\nu$ matrix of four polarizations time and frequency dependent matrices each of size $n_t \times n_\nu$.

$$\mathbf{V}_{pq,(t,\nu)}^{samp} = \left(\mathbf{V}_{pq,(t,\nu)}^0, \mathbf{V}_{pq,(t,\nu)}^1, \mathbf{V}_{pq,(t,\nu)}^2, \mathbf{V}_{pq,(t,\nu)}^3 \right)^{\dagger},$$

where the symbol † stand for the transpose operation. The convolution operator is linear, therefore we can rewrite Eq.7 in terms of a series of linear transformations or functional model as:

$$\mathbf{V}_{pq,(t_c, \nu_c)}^{corr} = \mathbf{C}_{pq,(t,\nu)}^{block} \cdot \mathbf{W}_{pq,(t,\nu)}^{block} \cdot \mathbf{V}_{pq,(t,\nu)}^{samp}. \quad (8)$$

Here, $\mathbf{C}_{pq,(t,\nu)}^{block}$ and $\mathbf{W}_{pq,(t,\nu)}^{block}$ are blocks diagonals matrices of size $(4n_t n_\nu) \times (4n_t n_\nu)$, the block elements are $\mathbf{W}_{pq,(t,\nu)}$ and $\mathbf{C}_{pq,(t,\nu)}$ respectively, where $\mathbf{C}_{pq,(t,\nu)}$ is the centre time interval and centre frequency interval sampling matrix of size $n_t \times n_\nu$. This is the result of the time and frequency integration for the baseline (p, q) . For a synthesis, the baseline (p, q) made a full coverage in the (u, v) plane. Therefore, we can package into a single matrix, $\mathbf{V}_{pq,(t', \nu')}^{corr}$ of size $(4N_t N_\nu) \times (4N_t N_\nu)$ the weighted average visibilities of the baseline (p, q) during the synthesis as follows:

$$\mathbf{V}_{pq,(t', \nu')}^{corr} = \mathbf{C}_{pq,(t,\nu)}^{block, n} \cdot \mathbf{W}_{pq,(t,\nu)}^{block, n} \cdot \mathbf{V}_{pq,(t,\nu)}^{samp, n}, \quad (9)$$

where N_t and N_ν are the number of time sample and frequency channels entering the Fourier domain. If the synthesis time is T and the frequency range is F , then $T = N_t \times \Delta t$ and $F = N_\nu \times \Delta \nu$. The size of $\mathbf{V}_{pq,(t', \nu')}^{corr}$ can also be written as $(4N_v^{pq}) \times (4N_v^{pq})$, where N_v^{pq} is the number of time and frequency visibilities for the baseline (p, q) . The matrices $\mathbf{C}_{pq,(t,\nu)}^{block, n}$ and $\mathbf{W}_{pq,(t,\nu)}^{block, n}$ are diagonals blocks matrices of size $(4N_v^{pq} n_t n_\nu) \times (4N_v^{pq} n_t n_\nu)$ where each diagonal block is the block diagonal matrix $\mathbf{C}_{pq,(t,\nu)}^{block}$ and $\mathbf{W}_{pq,(t,\nu)}^{block}$ respectively. n is the number of blocks elements. The sampled visibilities $\mathbf{V}_{pq,(t,\nu)}^{samp, n} = \mathbf{S}_{pq,(t,\nu)}^n \cdot \mathbf{V}_{pq,(t,\nu)}^n$ is a one row matrix of size $(N_v^{pq} 4n_t n_\nu) \times (4n_t n_\nu)$ made of $\mathbf{V}_{pq,(t,\nu)}^{samp}$ on top of each other and the matrix $\mathbf{S}_{pq,(t,\nu)}^n$ is the (u, v) plane sampling function for the visibilities $\mathbf{V}_{pq,(t,\nu)}^n$ of size $(N_v^{pq} 4n_t n_\nu) \times (4n_t n_\nu)$. We can write:

$$\mathbf{V}_{pq,(t', \nu')}^{corr} = \mathbf{C}_{pq,(t,\nu)}^{block, n} \cdot \mathbf{W}_{pq,(t,\nu)}^{block, n} \cdot \mathbf{S}_{pq,(t,\nu)}^n \cdot \mathbf{F} \cdot \mathcal{I}_{l,m}^{sky}, \quad (10)$$

if the number of pixel in the sky model is N_{pix} , then the true sky image vector $\mathcal{I}_{l,m}^{sky}$ has a size of $4N_{pix}$ and \mathbf{F} is a block diagonal Fourier transform operator of size $(4N_{pix}) \times (4N_{pix})$.

We are generally interested in using the total set of visibilities over baselines, time and frequencies, having $4 \times N_v$ visibilities measured over all baselines and $N_v = n_{bl} \times N_v^{pq}$ in this case. Here, n_{bl} is the number of baseline. We then have:

$$\mathbf{V}_{array,(t', \nu')}^{corr} = \mathbf{A} \cdot \mathcal{I}_{l,m}^{sky} + \epsilon. \quad (11)$$

Our data is always corrupted by a random error component or noise, ϵ and \mathbf{A} is the design matrix of size $(4N_v) \times (4N_{pix})$ corresponding to N_v visibilities weights, defined as

$$\mathbf{A} = \begin{bmatrix} \mathbf{C}_{(t,\nu)}^{block, n} \cdot \mathbf{W}_{01,(t,\nu)}^{block, n} \cdot \mathbf{S}_{01,(t,\nu)}^n \cdot \mathbf{F} \\ \vdots \\ \mathbf{C}_{(t,\nu)}^{block, n} \cdot \mathbf{W}_{ik,(t,\nu)}^{block, n} \cdot \mathbf{S}_{ik,(t,\nu)}^n \cdot \mathbf{F} \\ \vdots \\ \mathbf{C}_{(t,\nu)}^{block, n} \cdot \mathbf{W}_{jl,(t,\nu)}^{block, n} \cdot \mathbf{S}_{jl,(t,\nu)}^n \cdot \mathbf{F} \end{bmatrix}$$

The dirty image, $\mathcal{I}_{l,m}^D$ of size $4N_{pix}$ can then be derived as follow:

$$\mathcal{I}_{l,m}^D = \mathbf{F}^H \cdot \mathbf{A} \cdot \mathcal{I}_{l,m}^{sky} + \epsilon. \quad (12)$$

Here, H represents the the conjugate transpose operation

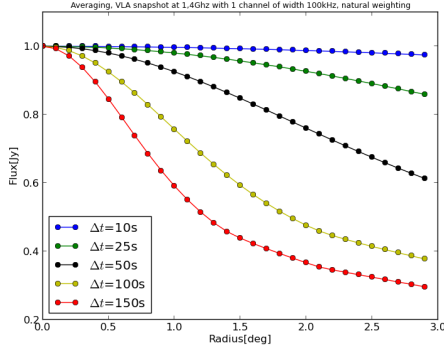


Figure 1. The attenuation of the intensity of a 1Jy source move from the phase centre for Δt integration synthesis at 100KHz bandwidth.

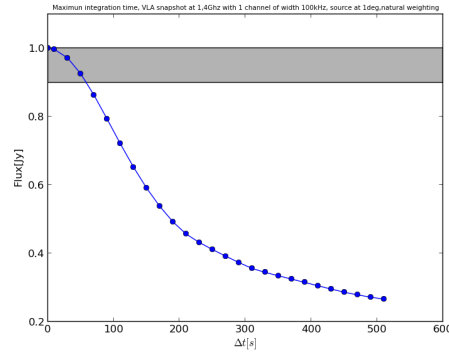


Figure 2. (b) Response to a 1Jy source at 1deg, as a function of Δt with 100KHz bandwidth

also known as a Hermitian transpose and \mathbf{F}^H is a block diagonal inverse Fourier transform operator of size $(4N_{pix}) \times (4N_{pix})$. The estimate of ϵ , for the map centre pixel is given by:

$$\begin{aligned} \tilde{\epsilon}_{0,0} &= \tilde{\mathcal{I}}_{0,0} - \mathbf{F}^H \cdot \mathbf{A} \cdot \tilde{\mathcal{I}}_{0,0} \\ &= \frac{1}{N_v} \sum_{k=1}^{N_v^{pq}} \left\{ \mathbf{B} \cdot \mathbf{V}_{array,(t,v)}^n - \mathbf{F}^H \mathbf{H} \cdot \mathbf{A} \cdot \mathbf{B} \cdot \mathbf{V}_{array,(t,v)}^n \right\} \end{aligned} \quad (13)$$

Here, \mathbf{B} and $\mathbf{V}_{array,(t,v)}^n$ are one row matrix of size $(N_v 4n_t n_v) \times (4n_t n_v)$ made of $\mathbf{C}_{(t,v)}^{block,n} \cdot \mathbf{W}_{01,(t,v)}^{block,n} \cdot \mathbf{S}_{01,(t,v)}^n$ and $\mathbf{V}_{pq,(t,v)}^n$ on top of each other respectively (see appendix A for the derivation of these complex matrices).

3 ALGORITHM 1: FOV SIGNALS RECOVERY

3.1 Description

Missing spaces between sampled (u, v) coordinates has an important dependences on the baseline length. However, the spacing between longer baselines (u, v) coordinates are wider then the one on shorter baselines, this is the obvious effect that explained while sources are more distorted on longer baselines compare to shorter one. Therefore, if one have to attribute a (u, v) weight, it may be as a function of the baseline length, in such a way that the distortion rate is taken into account over baselines. We aims in this section, to describe an algorithm that we used with a baseline-dependent windowing function to assign a proper weight to a data reference by a (u, v) coordinate considering the *spacing*² between the baseline (u, v) coordinates.

Fig.?? shows a snapshot coverage of an integration interval. For shorter baselines, the tracks are closer to the centre of rotation and for longer baselines the tracks are farther away from this centre. The *dot marks* are the data for a sampled (u, v) data, and the arrows indicates the separation between (u, v) coordinates and the centre (u, v) coordinate. It

is trivial to see on this figure that these separations are wider on longer baselines. The results of averaging is assigned to the centre (u, v) coordinate coloured in red.

3.2 Methods

Depending on the arrays, we show here that we can use the fact that, the spacing of long baselines (u, v) coordinates are wider and design a high dynamic range filter on longer baseline that will recover the desire FoV of the interferometer, and at the same time reducing the data rate. During an integration, the Earth rotation makes baselines coordinates u and v to variates in time and frequency. We can therefore package the (u, v) coordinates changes and the frequency changes of a baseline pq into a single matrix of size $n_t \times 2$ and into a single vector of dimension n_v respectively.

$$\begin{aligned} \mathbf{U}_{pq,t} &= \left(\mathbf{u}_{pq,t_s}, \dots, \mathbf{u}_{pq,t_c}, \dots, \mathbf{u}_{pq,t_e} \right)^{\dagger} \\ \mathbf{v} &= \left(v_s, \dots, v_c, \dots, v_e \right)^{\dagger} \end{aligned}$$

where the indexes s , c and e references the integration interval starting, centre, and ending time respectively. The elements of $\mathbf{U}_{pq,t}$ are functions of time and frequency representing a (u, v) coordinate. We defined the function, $\bar{\cdot}$ on a $n_t \times 2$ matrix as follow:

$$\bar{\mathbf{U}}_{pq,t} = \left(\|\mathbf{u}_{pq,t_s}\|, \dots, \|\mathbf{u}_{pq,t_c}\|, \dots, \|\mathbf{u}_{pq,t_e}\| \right)^{\dagger}, \quad (14)$$

where $\|\cdot\|$ is the Euclidean norm.

Definition 1.1. (Time direction spacing) The matrix that model the spacing between the (u, v) coordinates and the centre (u, v) coordinate of a baseline (p, q) across the time direction is defined as

$$\mathbf{U}_{pq,t}^s = \frac{v_c}{c} \cdot \left\{ \mathbf{U}_{pq,t} - \mathbf{H}_{pq,t} \right\},$$

where c is the speed of the light and \mathbf{H}_{pq} is a matrix of size $n_t \times 2$ that model the centre uv -coordinate, $\mathbf{H}_{pq,t} = (\mathbf{u}_{pq,t_s}, \dots, \mathbf{u}_{pq,t_c}, \dots, \mathbf{u}_{pq,t_e})^{\dagger}$.

² The *distance* has also huge dependences on the baseline length and allow us to formally define the data weight of a uv point over the entire uv plane.

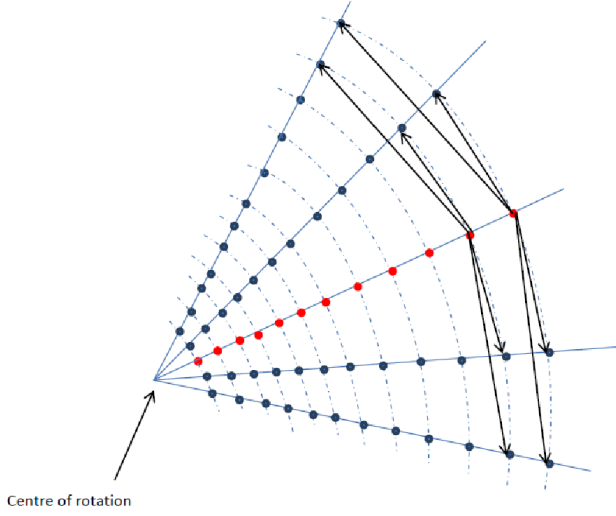


Figure 3. Coverage of one integration

Definition 1.2. (Frequency direction spacing) The vector of size n_v that model the spacing between the (u, v) coordinates and the centre (u, v) coordinate of a baseline (p, q) across the frequency direction is defined as

$$\mathbf{d}_v = \frac{\|\mathbf{u}_{pq,t_c}\|}{c} \cdot \left\{ \mathbf{v} - v_c \cdot \mathbf{g}_v \right\},$$

where \mathbf{g} is a $n_v \times 1$ unity matrix. The weight of a (u, v) data point is considered as follow:

Definition 1.3. (Baseline dependent windowing function)

If f_{pq} is a baseline dependent windowing function, then:

$$f_{pq} : \{\mathcal{R}, \mathcal{R}\} \rightarrow \mathcal{R}$$

$$d_{t_i}, d_{v_j} \mapsto \frac{w_{t_i, v_j}}{\sum_{i=1}^{n_t} \sum_{j=1}^{n_v} w_{t_i, v_j}}.$$

where d_{t_i} is an element of the vector $\mathbf{d}_t = \overline{\mathbf{U}}_{pq,t}^s$ and d_{v_j} is an element of the vector \mathbf{d}_v .

The previous algorithm is correct. But unfortunately, the algorithm does not suppressed out FoV sources and we loosed in sensitivity. Although simple averaging "means high sensitivity", we do need to eliminate at a certain rate out FoV sources in such a way that the overall SNR becomes higher than the one of averaging. We described such an algorithm in the following section.

4 ALGORITHM 2: FOV SIGNALS RECOVERY AND OUT FOV SUPPRESSION

4.1 Description

In theory, windowing functions and signals generally extend to infinity. Unfortunately, in practice, filtering a signal with a low pass filter, one need to define a cut-off interval. Therefore, if one wants to achieve sufficiently an accurate estimate of the windowing function ideal spectrum, one need a wide cut-off interval as far as the spectrum approaches the ideal when the windowing function order increases. An

overlap baseline dependent windowing function aims to extend the order of the baseline dependent windowing function in such a way that, we approaches the ideal spectrum. The only drawback of this technique is the increased of the time needed for processing the output sample of the signals being integrate.

4.2 Methods

The weight of a visibility is not defined by a unique baseline dependent windowing, but by the strength of the correlation between the overall overlapping baseline dependent windowing functions on the visibility. Now, consider that f_{pq}^a is an overlap-BDWF of width Δt and Δv across the time and frequency direction respectively.

Definition 1.4. (Left hand side overlapping functions) if Δt and Δv are the overlap time interval and frequency interval of the baseline dependent windowing function $f_{pq}^{a_0}$ respectively and $\{f_{pq}^{a_1}, f_{pq}^{a_2}, f_{pq}^{a_3}, \dots\}$ the set of BDWF overlapping on the *left hand side* of $f_{pq}^{a_0}$ then the resulting BDWF within Δt and Δv is defined as

$$g_{pq}^{lhs} : \{\mathcal{R}, \mathcal{R}\} \rightarrow \mathcal{R}$$

$$d_{t_i}, d_{v_j} \mapsto \frac{1}{N_{lhs}} \left(\sum_k f_{pq, (d_{t_i}, d_{v_j})}^{a_k} + f_{pq, (d_{t_i}, d_{v_j})}^{a_0} \right).$$

Here, N_{lhs} is the normalization term defined as

$$N_{lhs} = \sum_{i=1}^{n_{lt}} \sum_{j=1}^{n_{lv}} \left(\sum_k f_{pq, (d_{t_i}, d_{v_j})}^{a_k} + f_{pq, (d_{t_i}, d_{v_j})}^{a_0} \right),$$

where n_{lt} and n_{lv} are the number of (u, v) coordinates changes and frequency changes within Δt and Δv respectively.

Definition 1.5. (Right hand side overlapping functions)

if Δt and Δv are the overlap time and frequency interval of a BDWF $f_{pq}^{a_0}$ respectively and $\{f_{pq}^{a_1}, f_{pq}^{a_2}, f_{pq}^{a_3}, \dots\}$ the set of BDWF overlapping on the *right hand side* of $f_{pq}^{a_0}$, then the resulting BDWF within Δt and Δv is defined as

$$g_{pq}^{rhs} : \{\mathcal{R}, \mathcal{R}\} \rightarrow \mathcal{R}$$

$$d_{t_i}, d_{v_j} \mapsto \frac{1}{N_{rhs}} \left(f_{pq, (d_{t_i}, d_{v_j})}^{a_0} + \sum_k f_{pq, (d_{t_i}, d_{v_j})}^{a_k} \right).$$

Here, N_{rhs} is the normalization term defined as

$$N_{rhs} = \sum_{i=1}^{n_{rt}} \sum_{j=1}^{n_{rv}} \left(f_{pq, (d_{t_i}, d_{v_j})}^{a_0} + \sum_k f_{pq, (d_{t_i}, d_{v_j})}^{a_k} \right),$$

where n_{rt} and n_{rv} are the number of (u, v) coordinates changes and frequency changes within Δt and Δv respectively.

Definition 1.6. (Overlap baseline dependent windowing functions)

If $f_{pq}^{a_0}$ is a baseline dependent windowing function defined within the time interval Δt and the frequency interval Δv , g_{pq}^{lhs} the result of the left hand side of $f_{pq}^{a_0}$ overlapping windowing functions within the time interval Δt and the frequency interval Δv , and g_{pq}^{rhs} the result of the right hand side of $f_{pq}^{a_0}$ overlapping windowing functions within the

time interval $\Delta_r t$ and the frequency interval $\Delta_r \nu$, then the overlap baseline dependent windowing function within Δt and $\Delta \nu$ is defined as:

$$\mathcal{G}_{pq} : \{\mathcal{R}, \mathcal{R}\} \rightarrow \mathcal{R}$$

$$d_{t_i}, d_{\nu_j} \mapsto \begin{cases} \mathcal{G}_{pq}^{lhs} & \text{if } (t_i, \nu_j) \in (\Delta_l t, \Delta_l \nu) \\ \mathcal{f}_{pq}^{a_0} & \text{if } (t_i, \nu_j) \in (\Delta_m t, \Delta_m \nu) \\ \mathcal{G}_{pq}^{rhs} & \text{if } (t_i, \nu_j) \in (\Delta_r t, \Delta_r \nu) \end{cases}$$

where $\Delta_m t$ and $\Delta_m \nu$ are $\mathcal{f}_{pq}^{a_0}$ uncorrelated time and frequency interval respectively. From the above definitions, the following derivation is trivial

$$\{\Delta t, \Delta \nu\} = \{\Delta_l t \cup \Delta_m t \cup \Delta_r t, \Delta_l \nu \cup \Delta_m \nu \cup \Delta_r \nu\}.$$

They follows the below rules:

$$\Delta_m t = \begin{cases} \cup \{t_i\}_{i=s', s' \geq s+1}^{e', e' \leq e-1} & \text{if } n_{lt} + n_{rt} < n_t \\ \{t_c\} & \text{if } n_{lt} + n_{rt} = n_t \\ \emptyset & \text{otherwise} \end{cases}$$

and

$$\Delta_m \nu = \begin{cases} \cup \{\nu_i\}_{i=s', s' \geq s+1}^{e', e' \leq e-1} & \text{if } n_{lv} + n_{rv} < n_\nu \\ \{\nu_c\} & \text{if } n_{lv} + n_{rv} = n_\nu \\ \emptyset & \text{otherwise} \end{cases}$$

4.3 Windowing functions

In signal processing a windowing function is a mathematical function that is zero-values outside of some chosen interval, and when another function or a signal is multiplied by the windowing function, the product is also zero-values outside the interval. In this section, we evaluation the Peak Sidelobe Level (PSL), the Main Lobe width (MLW) and the Sidelobes Roll-off (SLR) of some windowing functions spectrum. This study will allow us to make a suitable choice of the window that by tapering with the sky, we conserve the brightness of sources in the field of interest and attenuate sidelobes confusion from strong sources out of the field of interest. Conventional signal processing literature and baseline dependent windowing functions:

Table of terms

Signal processing	BDWFs
Frequency domain	Image plane
Time domain	Fourier plane
Spectral response	Image taper
Cut-off interval or pass band	FoV
Stop band	Outside edges of FoV

4.3.1 Boxcar window

This window take a hunk of the data without modification, and this leads to discontinuities at the edges³. For a cut-off time interval $[-t_a, t_a]$ the boxcar window is defined as:

$$\Pi_t = \begin{cases} 1 & -t_a \leq t \leq t_a \\ 0 & \text{otherwise} \end{cases} \quad (15)$$

³ unless it happens that the signal fit exactly with the window width. Nevertheless, it is rare to find such a situation.

Fig.4 and Fig.5 gives the graph of Π_t and its spectrum respectively. The blue and the red curve of Fig.5 are the spectrum of Π_t for a time cut-off interval, $[-t_a, t_a]$ and $[-t_a/2, t_a/2]$ respectively. We noticed that when the cut-off interval is large, the MLW of the spectrum is narrower, the PSL is lower and the SLR drop faster.

4.3.2 Gaussian window

A Gaussian window centred at mean zero with standard deviation, σ is given by:

$$G_t = e^{-bt^2}. \quad (16)$$

Here, $b = (2\sigma^2)^{-1}$ and $\mathcal{F}^{-1}\{G_t\} = \sqrt{\frac{b}{\pi}} e^{-cl^2}$, where $c = \pi^2/b$. This shows us that the inverse Fourier transform of a Gaussian with standard deviation σ is a Gaussian with a standard deviation $\sigma' = (2\pi\sigma)^{-1}$. Fig.10 and Fig.?? gives the graph of G_t and its spectrum respectively, where G_t is truncate within the cut-off frequency interval $[-t_a, t_a]$, with $b = 3$ for the blue curve and $b = 5$ for the red one. We noticed that when the standard deviation is large, the MLW of the spectrum is narrower, the PSL is higher and the SLR drop slowly compare to a smaller standard deviation.

4.3.3 Butterworth window

The time response of the Butterworth window is flat in the pass band, and rolls off towards zero in the stop band, and it is characterized by two independent parameters, the cut-off time t_a and the order p . These two parameters controls the bandwidth and side lobes attenuation. The time response of the Butterworth window is given by:

$$BW_t = \left(1 + (t/t_a)^{2p}\right)^{-1}. \quad (17)$$

For the same frequency interval $[-t_a, t_a]$, we plotted three curves $\{p = 1, p = 3, p = 5\}$ of BW_t in Fig.8 and their corresponding spectrum in Fig.9. We noticed that when the other p is getting bigger, the MLW of the spectrum is conserved, while the PSL is getting higher and the SLR is dropping faster.

4.3.4 Sinc Window

The sinc window is an infinitely large convolution window as it is non zero everywhere. The sinc is defined as follow:

$$S_t = \text{sinc}(\pi bt). \quad (18)$$

Fig.6 and Fig.7 gives the graph of S_t and its spectrum respectively, where S_t is truncate within the cut-off time interval $[-t_a, t_a]$. We noticed that when the cut-off time interval is large (Fig.7, blue curve), the spectrum becomes perfectly flat at the passband while the MLW becomes narrower, the PSL becomes lower and the SLR drop faster compare to a cut-off interval of $[-t_a, t_a]$ (Fig.7, red curve).

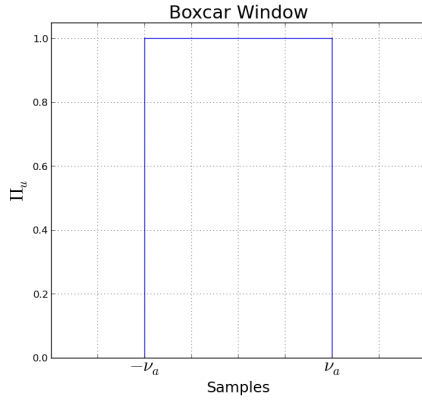


Figure 4. Boxcar windowing function.

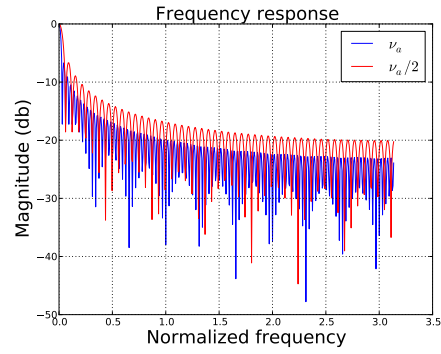


Figure 5. Frequency response of a boxcar window

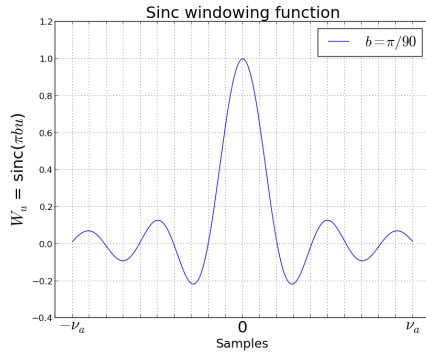


Figure 6. Sinc window

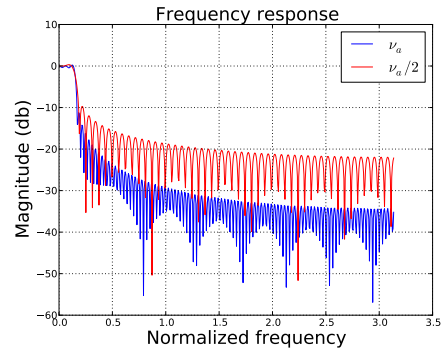


Figure 7. Frequency response of the sinc window

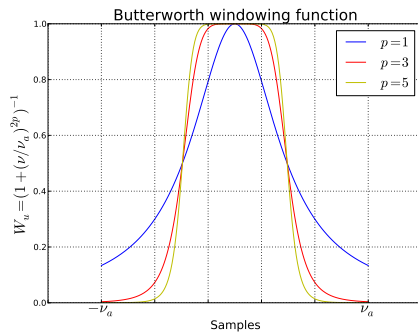


Figure 8. Butterworth windows

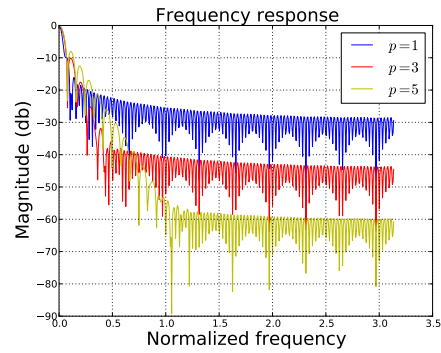


Figure 9. Frequency response of the Butterworth windows

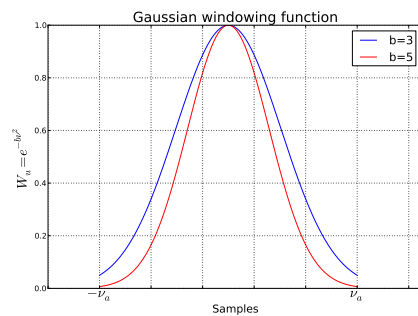


Figure 10. Gaussian windows

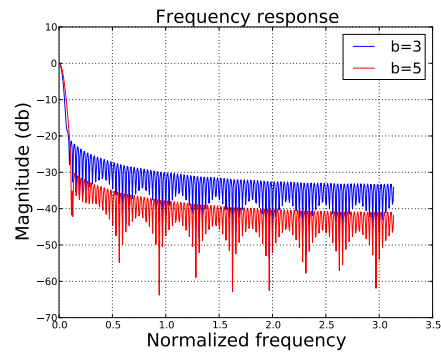


Figure 11. Frequency response of Gaussian windows

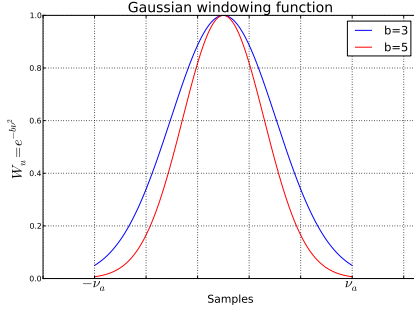


Figure 12. Bessel first King windows NB: this figure is coming very soon

4.3.5 Bessel Function of the First Kind

discuss the Bessel here

Windows	MLL (-3db)	PSL (db)	SLR (db/octave)
Π_t	$\approx 0,073$	-6,68	-6,78
S_t	$\approx 0,306$	-11,22	-12,42
G_t	$\approx 0,0736$	-30,28	-14,5
BW_t	$\approx 0,079$	-10,08	-15,39
J_{0t}	$\approx -$	-	-

A windowing function with a narrower main lobe width for a better spectral resolution, lower PSL to have less masking of nearby sources, and faster SLR to have less masking for far away sources is preferably in this work. Nevertheless, The energy is more concentrated in the frequency domain main lobe when the lobe width is narrower. Therefore, the frequency domain of the boxcar and the Butterworth window look similar, but the other of the Butterworth frequency domain can be control with the goal to concentrate more energy in the frequency main lobe. However, the sinc window is preferable as we expect in this work, signals in a wide dynamic range.

5 NOISE AND COMPARISON

Several windowing functions were described in the previous section, the sinc window, the Bessel of the first kind and the Butterworth approaches well our specifications, and they are taken under consideration throughout the rest of this paper. We show in this section that, applying our methods means that you are filtering the Fourier plane with a sort of hybrids filters (boxcar window on shorter baselines and the window you actually considered on longer baselines). We furthermore evaluate the theoretical noise predicted in Eq.13.

Fig.14, Fig.15 and Fig.16 are the baseline dependent windowing functions obtained using the sinc, the Bessel first kind and the Butterworth respectively. It appears on these figures that the baseline dependent windowing functions differ from the baseline (u, v) spacing, and for shorter baselines the window gets closer to the boxcar window. Nevertheless, we reduced the thermal noise on shorter baselines while we increased the spectral dynamic range on longer baselines.

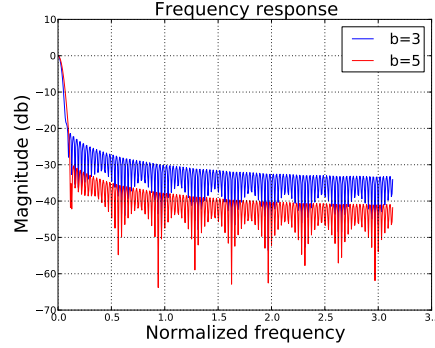


Figure 13. Frequency response of Bessel first kind window

Fig.17, Fig.18 and Fig.19 shows the three cases of an overlap baseline dependent windowing function obtained with the sinc.

- In Fig.20, Fig.21 and 22 we plotted the ratio $\frac{\sigma_{pq,w}}{\sigma_{pq,avg}}$ of the theoretical noise as a function of \bar{d}_t (the mean of (u, v) distance) using the sinc, the Bessel first kind and the Butterworth respectively. Here, $\sigma_{pq,w}$ and $\sigma_{pq,avg}$ are the per baseline theoretical rms noise of the baseline dependent windowing function and the one of averaging respectively. These figures shows that, the noise increases with baseline (u, v) distances.

- On shorter baselines, the noise is approximately the same with the one of averaging and drop significantly with the number of overlap time and frequency bins. This is because on shorter baselines, the baseline dependent windowing function are closer to the boxcar window, and when the number of overlap time and frequency bins increases, we have:

$$\frac{\sigma_{pq,w}}{\sigma_{pq,avg}} \approx \left(\frac{n_t n_v}{(n_t + n_{lt} + n_{rt})(n_v + n_{lv} + n_{rv})} \right)^{\frac{1}{2}}$$

The tables below summarized the array overall theoretical rms noise ratio and the simulation one.

f_{pq}	Theoretical	Simulation
Bl-sinc-W0×0	1.17	1.23
Bl-J0-W0×0	1.11	1.14
Bl-BW-W0×0	1.16	—

g_{pq}	Theoretical	Simulation
Bl-sinc-W100×25	1.02	1.18
Bl-J0-W100×25	0.91	1.08
Bl-BW-W100×25	1.44	—
Bl-sinc-W150×50	1.03	1.27
Bl-J0-W150×50	0.92	1.13
Bl-BW-W150×50	1.42	—

6 SIMULATIONS AND RESULTS

In order to test the algorithms described in section 3 and section 4, we performed multiple tests on JVLA simulated

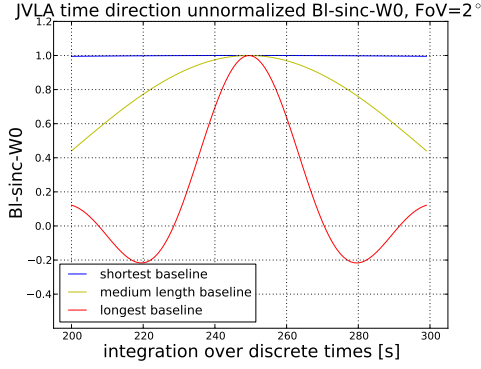


Figure 14. Time direction BI-sinc-W0 of the shortest, medium and longest baseline

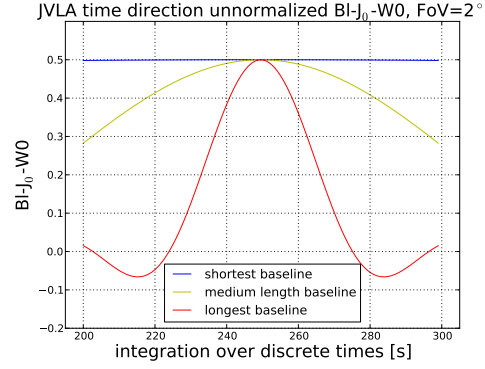


Figure 15. Time direction BI-J0-W0 of the shortest, medium and longest baseline

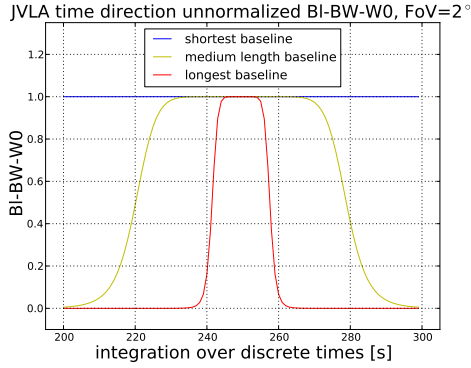


Figure 16. Time direction BI-BW-W0 of the shortest, medium and longest baseline

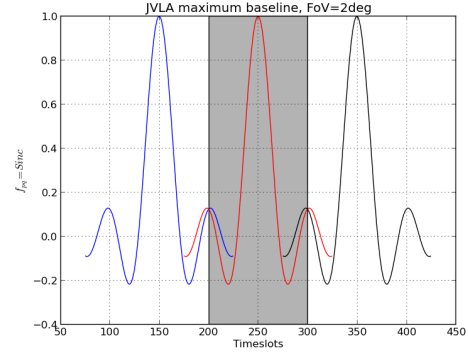


Figure 17. Overlap BDWF's: $\Delta_u t = [225, 250]$.

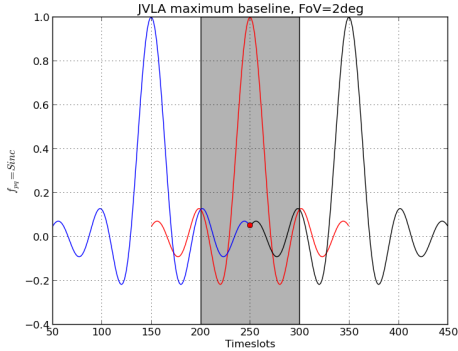


Figure 18. Overlap BDWF's: $\Delta_u t = \{250\}$.

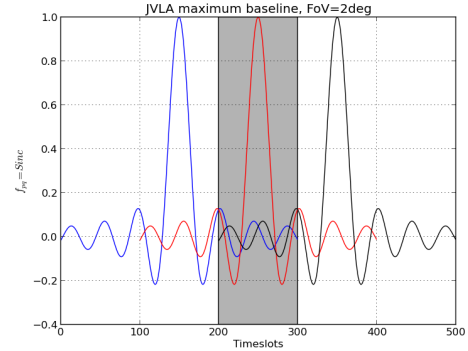


Figure 19. Overlap BDWF's: $\Delta_u t = \emptyset$.

measurement sets (MS). In this section we summarized and discussed those results. Two MS is used in our simulation, a high resolution MS (HR-MS) that contained the observed JVLA data of short integration time and frequency, a low resolution MS (LR-MS), where the results of simple averaging or the weighted averaging are saved. To apply the second algorithm described in section 4, the following conditions are satisfied:

(i) If t_{start}^{hrms} and t_{start}^{lrms} are the starting time of the HR-MS and LR-MS respectively. $n_{t,ovlp}$ the number of timeslots ex-

tended across the time direction, and Δt^{hrms} the HR-MS integration time, then $t_{start}^{lrms} \geq t_{start}^{hrms} + n_{t,ovlp} \times \Delta t^{hrms}$.

(ii) If t_{end}^{hrms} and t_{end}^{lrms} are the ending time of the HR-MS and LR-MS respectively, then $t_{end}^{lrms} \leq t_{end}^{hrms} + n_{t,ovlp} \times \Delta t^{hrms}$.

(iii) If ν_{start}^{hrms} and ν_{start}^{lrms} are the starting frequency of the HR-MS and LR-MS respectively. $n_{\nu,ovlp}$ the number of channels extended across the frequency direction, and $\Delta \nu^{hrms}$ the HR-MS width, then $\nu_{start}^{lrms} \geq \nu_{start}^{hrms} + n_{\nu,ovlp} \times \Delta \nu^{hrms}$.

(iv) If ν_{end}^{hrms} and ν_{end}^{lrms} are the ending frequency of the HR-

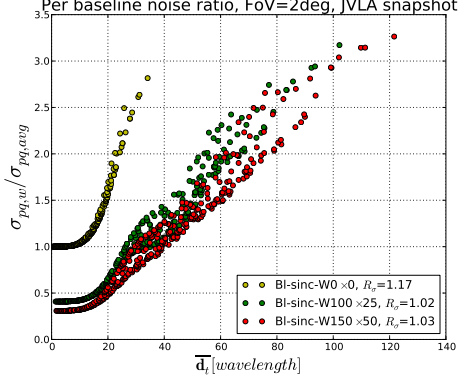


Figure 20. Per baseline noise ratio of $\text{BI-sinc-}Wn_{lt} \times n_{lv}$ and averaging

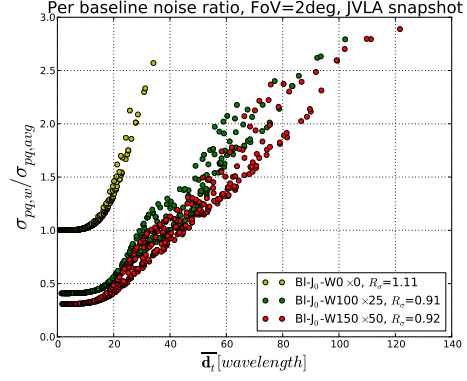


Figure 21. Per baseline noise ratio of $\text{BI-J0-}Wn_{lt} \times n_{lv}$ and averaging

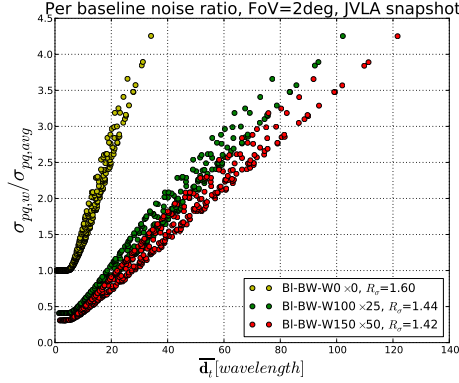


Figure 22. Per baseline noise ratio of $\text{BI-BW-}Wn_{lt} \times n_{lv}$ and averaging

MS and LR-MS respectively, then $v_{end}^{lrms} \leq v_{end}^{lrms} + n_{v,ovlp} \times \Delta v^{lrms}$.

6.1 Smearing elimination and out FoV suppression

We considered 40 different sky models each containing a 1Jy source; the sky models differ from each other by the source coordinates. The reason for having only one source in the sky model is to avoid standard imaging artefacts in the sky maps (cite here ?), which can affect the brightness of sources. Another obvious problem is the CLEAN algorithm (cite here ?), which does not created perfect clean maps. Therefore we need to avoid sidelobes confusion. Each of the sky model is simulated with a JVLA HR-MS of 7min30s snapshot synthesis, with a $\Delta t^{lrms} = 1.5s$ integration time at 1.4GHz, with 150 channels of width $\Delta v^{lrms} = 125kHz$. We therefore applied the actual method (simple averaging) and our methods, each result is save into a LR-MS of 1min30s synthesis, with a 150s integration time, with 1 channels of width 6.25MHz. We considered, $\{t_{start}^{lrms}, v_{start}^{lrms}\} = \{0s, 125kHz\}$, $\{t_{start}^{lrms}, v_{start}^{lrms}\} = \{1min30s, 6250kHz\}$, $\{t_{end}^{lrms}, v_{end}^{lrms}\} = \{7min30s, xxxkHz\}$, $\{t_{end}^{lrms}, v_{end}^{lrms}\} = \{6min, xxxkHz\}$, $n_{t,ovlp} = \{0, 100, 150\}$ and $n_{v,ovlp} = \{0, 25, 50\}$.

Fig.23, Fig.24, Fig.25 and Fig.26 show the results of the simulation, where we represented the brightness of the source as a function of the source coordinates in the sky model.

In these figures, we considered three cases of the sinc window, and three of the Bessel first kind ($\text{BI-sinc } Wn_{t,ovlp} \times n_{v,ovlp}$, $\text{BI-J0 } Wn_{t,ovlp} \times n_{v,ovlp}$ with $n_{t,ovlp} = \{0, 100, 150\}$ and $n_{v,ovlp} = \{0, 25, 50\}$). We evaluated the loss in signal amplitude with longer LR-MS integration time interval $\Delta t^{lrms} = 150s$ and wider LR-MS integration frequency interval $\Delta v^{lrms} = 6250kHz$. We furthermore evaluated the noise ratio, $\mathcal{R}_\sigma = \frac{\sigma_w}{\sigma_{Avg}}$ (with σ_w the resulting noise of the filter under consideration and σ_{Avg} the noise of simple averaging). These results shows that:

- We measured more than 90% of the source brightness within $\approx 75\%$ of the FoV using $\text{BI-sinc } W0 \times 0$ and $\text{BI-J0 } W0 \times 0$. Unfortunately, the attenuation rate of the source out of the FoV is approximately the same when performing with simple averaging.
- We measured more than 90% of the source brightness within $\approx 95\%$ of the FoV with the overlap filters. However, as mention in section 4.3 the reason for this is that, the overlap filter is an accurate practical evaluation of the window theoretical representation⁴.
- Another obvious effect of the overlap filters is the suppression of the source when this source is out of the FoV. When looking at these figures, it appears that the curves

⁴ windowing function theoretically extend to infinitely

of the overlaps filters are below the one of simple averaging. However, the overlaps filters attenuated $\approx 99\%$ of the source brightness out of the FoV.

- When looking at these figures, it appears that the sinc window conserved the signal within the FoV compared to the Bessel of the first kind window, while the Bessel of the first kind suppressed the signal out of the FoV compare to the sinc. However, the reason for this is that the main lobe width of the sinc is narrower than the one of the Bessel first kind and the Bessel first kind has low sidelobes level compared to the sinc.

When performing the baseline dependent filters, smearing is eliminated within the FoV while we compressed the data by integrating over a large time interval and wider frequency interval of a LR-MS. However, under some assumptions, the overlap baseline dependent filters significantly attenuate the source out of the FoV to a greater extent than simple averaging. Thus, in all cases the SNR obtained using these methods are greater than the one using the simple averaging method even as there is loss in sensitivity.

6.2 Maximal integration

In this section, the maximal frequency and time integration that can be consider in the frequency direction and the time direction without smearing in the FoV while the methods accurately suppressed the source when this is out of the FoV is evaluated. However, we considered 6 sky models of a 1Jy source with different coordinates ($r = \{0.09^\circ, 0.25^\circ, 0.5^\circ, 1^\circ, 1.5^\circ, 2^\circ\}$). The methods are performed with a 2° FoV sinc and Bessel first kind filters centered in the phase centre.

6.2.1 Frequency direction

In this case, each of these sky model is simulated with a JVLA HR-MS of 1 timeslots synthesis, with a short integration time of $\Delta t^{hrms} = 0.1s$ at 1.4GHz. The aims of a short HR-MS integration time is to avoid time direction smearing and therefore accurately evaluate smearing in the frequency direction. We considered 150 channels, and varied the width, $\Delta \nu^{hrms}$ in the interval $[125, 1187.5]$ kHz. We therefore applied the actual method (simple averaging) and our methods both in the frequency direction, each result is save into a LR-MS of 1 timeslot synthesis, with 0.1s integration time and 1 channels of width $\Delta \nu^{hrms} \times 50$ kHz. We considered, $\nu_{start}^{hrms} = \Delta \nu^{hrms} \text{kHz}$, $\nu_{start}^{hrms} = \nu_{start}^{hrms} \times 50 \text{kHz}$, $\nu_{end}^{hrms} = \nu_{start}^{hrms} \times 150 \text{kHz}$ and $\nu_{end}^{hrms} = \nu_{start}^{hrms} \times 100 \text{kHz}$. We compared in Fig.27 and Fig.28 the results of simple frequency averaging and the one of *Bl-sinc* $Wn_{\nu,ovlp}$ performed in the frequency direction. We compared in Fig.29 and Fig.30 the results of simple frequency averaging and the one of *Bl-J0* $Wn_{\nu,ovlp}$. Here we took $n_{\nu,ovlp} = \{0, 50\}$ frequency overlap bins. These results shows that:

- Firstly, these results show that, we can significantly integrate over a wider LR-MS frequency interval without a lost of signal amplitude. However, looking at these figures, the curves of the source at $0.09^\circ, 0.25^\circ, 0.5^\circ$ from the phase centre are closer to the affine equation $y = 1$, which differ from

the curves when the source is at $1^\circ, 1.5^\circ, 2^\circ$ from the phase centre.

- Secondly, looking on Fig.28 and 30, when the source is at 1.5° and 2° , the attenuation is significant within $[6.2, 12.6] \text{MHz}$ with the overlap frequency direction filters compare to simple frequency averaging.

- Finally, the sinc filter performed well on signal recovery compare to the Bessel first kind and the Bessel first kind suppressed the source when this is out of the FoV compare to the sinc.

6.2.2 Time direction

In this case, each of these sky model is simulated with a JVLA HR-MS of 300 timeslots synthesis, and we varied the integration time Δt^{hrms} in the interval $[0.5, 5.5]s$ at 1.4GHz. We considered 1 channels of width, $\Delta \nu^{hrms} = 125 \text{kHz}$. We therefore applied the actual method (simple averaging) and our methods both in the time direction then the result of each simulation is saved into a LR-MS of $100 \times \Delta t^{hrms}s$ synthesis, with a $100 \times \Delta t^{hrms}s$ integration time, with 1 channels of width 125kHz. We considered, $t_{start}^{hrms} = 0s$, $t_{start}^{hrms} = 100 \text{timeslots} \times \Delta t^{hrms}s$, $t_{end}^{hrms} = 300 \text{timeslots} \times \Delta t^{hrms}s$ and $t_{end}^{hrms} = 200 \text{timeslots} \times \Delta t^{hrms}s$.

We compared in Fig.31 and Fig.32 the results of simple time averaging and the one of *Bl-sinc* $Wn_{t,ovlp}$ performed in the time direction. We compared in Fig.33 and Fig.34 the results of simple time averaging and the one of *Bl-J0* $Wn_{t,ovlp}$. Here, we took $n_{t,ovlp} = \{0, 100\}$ time overlap bins. These results shows that:

- Firstly, we can significantly integrate over a longer LR-MS time interval without a lost of signal amplitude. However, looking at these figures, the curves of the source at $0.09^\circ, 0.25^\circ, 0.5^\circ$ from the phase centre are closer to the affine equation $y = 1$, which differ from the curves when the source is at $1^\circ, 1.5^\circ, 2^\circ$ from the phase centre.

- Secondly, looking on Fig.28 and 30, when the source is at 1.5° and 2° , the attenuation is significant within $[50, 150]$ with the overlap time direction filters compare to simple time averaging.

- Finally, the sinc filter performed well on signal recovery compare to the Bessel first kind and the Bessel first kind suppressed the source when this is out of the FoV compare to the sinc.

6.2.3 Time and frequency direction

In this case, each sky model is simulated with a JVLA HR-MS of 300 timeslots synthesis, and varied the integration time Δt^{hrms} in $[0.5, 5.5]s$ at 1.4GHz. We considered 150 channels and varied the width $\Delta \nu^{hrms}$ within the interval $[125, 750] \text{kHz}$. We therefore applied the actual method (simple averaging) and our methods both in the frequency direction and time direction, each result is save into a LR-MS of $100 \text{timeslots} \times \Delta t^{hrms}s$ synthesis, with $100 \text{timeslots} \times \Delta t^{hrms}$ integration time and 1 channels of width $50 \text{channels} \times \Delta \nu^{hrms} \text{kHz}$. We considered, $t_{start}^{hrms} = 0s$, $t_{start}^{hrms} = 100 \text{timeslots} \times \Delta t^{hrms}s$, $t_{end}^{hrms} = 300 \text{timeslots} \times \Delta t^{hrms}s$ and $t_{end}^{hrms} = 200 \text{timeslots} \times \Delta t^{hrms}s$, $\nu_{start}^{hrms} = \Delta \nu^{hrms} \text{kHz}$, $\nu_{start}^{hrms} = \nu_{start}^{hrms} \times 50 \text{kHz}$, $\nu_{end}^{hrms} = \nu_{start}^{hrms} \times 150 \text{kHz}$ and $\nu_{end}^{hrms} = \nu_{start}^{hrms} \times 100 \text{kHz}$.

We compared in Fig.35 and Fig.36 the results of simple time and frequency averaging and the one of *Bl-sinc* $Wn_{t,ovlp} \times n_{v,ovlp}$ performed in the time and frequency direction. We compared in Fig.37 and Fig.38 the results of simple time and frequency averaging and the one of *Bl-J0* $Wn_{t,ovlp} \times n_{v,ovlp}$ performed in the time and frequency direction. Here, we took $n_{t,ovlp} = \{0, 100\}$ time overlap bins and $n_{v,ovlp} = \{0, 50\}$ frequency overlap bins. These results shows that:

- Firstly, we can significantly integrate over a longer LR-MS time interval and frequency interval at the same time without a lost of signal amplitude. However, looking at these figures, the curves of the source at $0.09^\circ, 0.25^\circ, 0.5^\circ$ from the phase centre are closer to the affine equation $y = 1$, which differ from the curves when the source is at $1^\circ, 1.5^\circ, 2^\circ$ from the phase centre.
- Secondly, looking on Fig.36 and 38, when the source is at 1.5° and 2° , it appears that the curves of the overlaps filters are below the one of simple averaging. These suggest that, when we are integrating both over a wider LR-MS time interval and frequency interval, the source is suppressed significantly out of the FoV without any constraint on the integration time and frequency.
- Finally, the sinc filter performed well on signal recovery compare to the Bessel first kind and the Bessel first kind suppressed the source when this is out of the FoV compare to the sinc.

6.3 One strong source in the sky model and attenuation efficiency

6.4 Discussion

7 CONCLUSIONS

The goal of this paper was threefold. The first objective was to investigate **** windowing functions***

The second objective was to study ****first algorithm data compression***

The final objective was to ****second algorithm data compression and out field suppression***

Drawback and futures works*** drawback and futures works****

ACKNOWLEDGEMENTS

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Martí-Vidal I., Marcaide J., 2008, A&A, 480, 289

APPENDIX A: DERIVATION OF COMPLEX MATRICES

The complex matrices used in section 2.4 are explicitly derived in this appendix. In Eq.8, the matrices $\mathbf{C}_{(t,v)}^{block}$ and $\mathbf{W}_{pq,(t,v)}^{block}$ are blocks diagonals both of size $(4n_t n_v) \times (4n_t n_v)$, and the sampled visibilities $\mathbf{V}_{pq,(t,v)}^{samp}$ is a vector of size

$4 \times (n_t n_v)$. These matrices are explicitly expressed as follow:

$$\mathbf{C}_{(t,v)}^{block} = \begin{bmatrix} \mathbf{c}_{(t,v)} & 0 & 0 & 0 \\ 0 & \mathbf{c}_{(t,v)} & 0 & 0 \\ 0 & 0 & \mathbf{c}_{(t,v)} & 0 \\ 0 & 0 & 0 & \mathbf{c}_{(t,v)} \end{bmatrix}$$

$$\mathbf{W}_{pq,(t,v)}^{block} = \begin{bmatrix} \mathbf{W}_{pq,(t,v)} & 0 & 0 & 0 \\ 0 & \mathbf{W}_{pq,(t,v)} & 0 & 0 \\ 0 & 0 & \mathbf{W}_{pq,(t,v)} & 0 \\ 0 & 0 & 0 & \mathbf{W}_{pq,(t,v)} \end{bmatrix}$$

$$\mathbf{V}_{pq,(t,v)}^{samp} = \left[\mathcal{V}_{pq,(t,v)}^0, \mathcal{V}_{pq,(t,v)}^1, \mathcal{V}_{pq,(t,v)}^2, \mathcal{V}_{pq,(t,v)}^3 \right]^T.$$

In Eq.??, the matrices $\mathbf{C}_{(t,v)}^{block,n}$ and $\mathbf{W}_{pq,(t,v)}^{block,n}$ are blocks diagonals both of size $(4N_v^{pq} n_t n_v) \times (4N_v^{pq} n_t n_v)$, and the sampled visibilities $\mathbf{V}_{pq,(t,v)}^{samp,n}$ is a one row matrix of size $(N_v^{pq} 4n_t n_v) \times (4n_t n_v)$ made of $\mathbf{V}_{pq,(t,v)}^{samp}$. These matrices are explicitly expressed as follow:

$$\mathbf{C}_{(t,v)}^{block,n} = \begin{bmatrix} \mathbf{C}_{(t,v)}^{block} & \dots & 0 & \dots & 0 \\ \vdots & \vdots & \vdots & \vdots & \vdots \\ 0 & \dots & \mathbf{C}_{(t,v)}^{block} & \dots & 0 \\ \vdots & \vdots & \vdots & \vdots & \vdots \\ 0 & \dots & 0 & \dots & \mathbf{C}_{(t,v)}^{block} \end{bmatrix}$$

$$\mathbf{W}_{pq,(t,v)}^{block,n} = \begin{bmatrix} \mathbf{W}_{pq,(t,v)}^{block} & \dots & 0 & \dots & 0 \\ \vdots & \vdots & \vdots & \vdots & \vdots \\ 0 & \dots & \mathbf{W}_{pq,(t,v)}^{block} & \dots & 0 \\ \vdots & \vdots & \vdots & \vdots & \vdots \\ 0 & \dots & 0 & \dots & \mathbf{W}_{pq,(t,v)}^{block} \end{bmatrix}$$

$$\mathbf{V}_{pq,(t,v)}^{samp,n} = \left[\mathbf{V}_{pq,(t,v)}^{samp}, \dots, \mathbf{V}_{pq,(t,v)}^{samp}, \dots, \mathbf{V}_{pq,(t,v)}^{samp} \right]^T.$$

In Eq.11, the matrix \mathbf{A} of size $(4N_v) \times (4N_{pix})$ is defined as follow

$$\mathbf{A} = \begin{bmatrix} \mathbf{C}_{(t,v)}^{block,n} \cdot \mathbf{W}_{01,(t,v)}^{block,n} \cdot \mathbf{S}_{01,(t,v)}^{block,n} \cdot \mathbf{F} \\ \vdots \\ \mathbf{C}_{(t,v)}^{block,n} \cdot \mathbf{W}_{ik,(t,v)}^{block,n} \cdot \mathbf{S}_{ik,(t,v)}^{block,n} \cdot \mathbf{F} \\ \vdots \\ \mathbf{C}_{(t,v)}^{block,n} \cdot \mathbf{W}_{jl,(t,v)}^{block,n} \cdot \mathbf{S}_{jl,(t,v)}^{block,n} \cdot \mathbf{F} \end{bmatrix}$$

APPENDIX B: SIMILAR WAY OF IMAGING

Each baseline has his own baseline dependent windowing functions during integration. Unfortunately, we can not accurately estimate the resulting spectrum of all windowing functions that multiply the sky seen by these baselines (if we supposed that all baselines are seen the same sky). The

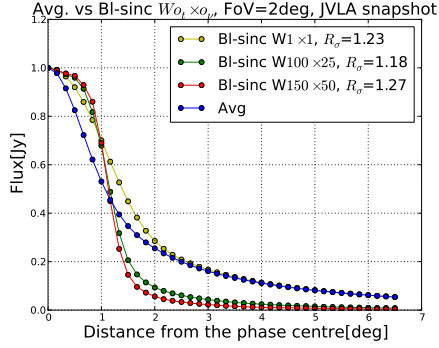


Figure 23. Time and frequency direction sinc filter applied on a 2° FoV JVLA surveys observing a 1Jy source move from the phase centre for 150s integration synthesis at 6.25MHz bandwidth.

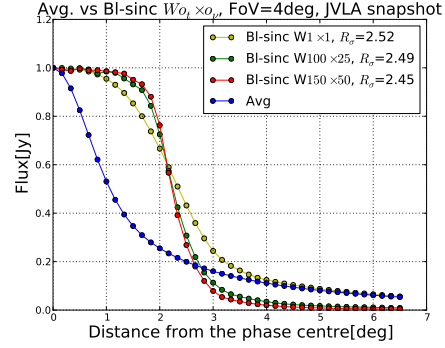


Figure 24. Time and frequency direction sinc filter applied on a 4° FoV JVLA surveys observing a 1Jy source move from the phase centre for 150s integration synthesis at 6.25MHz bandwidth.

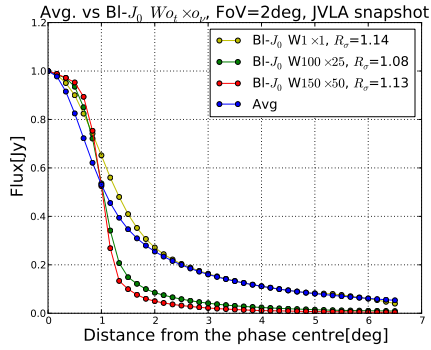


Figure 25. Time and frequency direction Bessel first kind filter applied on a 2° FoV JVLA surveys observing a 1Jy source move from the phase centre for 150s integration synthesis at 6.25MHz bandwidth.

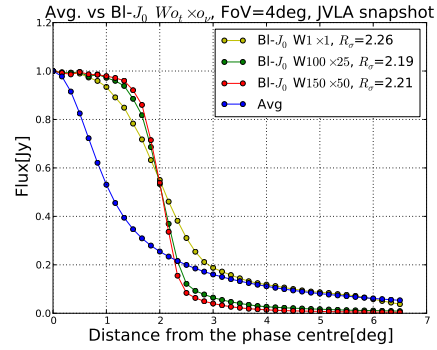


Figure 26. Time and frequency direction Bessel first kind filter applied on a 2° FoV JVLA surveys observing a 1Jy source move from the phase centre for 150s integration synthesis at 6.25MHz bandwidth.

measured sky intensity of the array is derived from the inverse Fourier transform of the sum of the sample visibilities measured at each baseline. The mathematics behind this is as follow:

$$\mathcal{I}_{l,m}^D = \mathcal{F}^{-1} \left\{ \sum_{pq} \mathcal{S}_{pq} \cdot \left(c_{pq} \cdot (\mathcal{W}_{pq} \circ \mathcal{V}) \right) \right\}_{(l,m)}$$

where \mathcal{S}_{pq} is the sampling function of the baseline pq . This can be rewritten as

$$\mathcal{I}_{l,m}^D = \sum_{pq} \mathcal{B}_{pq} \circ \left(\mathcal{F}^{-1} \{c\}_{pq} \circ (\mathcal{R}_{pq} \cdot \mathcal{I}^{sky}) \right)_{(l,m)}$$

Here, $\mathcal{R}_{pq} = \mathcal{W}_{pq}$ is the sky response or smearing response for the baseline pq . The same sky seen by all baselines is \mathcal{I}^{sky} and \mathcal{B}_{pq} is the synthesized beam or point spread function of the baseline pq .

$\left(\mathcal{F}^{-1} \{c\}_{pq} \circ (\mathcal{R}_{pq} \cdot \mathcal{I}^{sky}) \right)_{(l,m)} = (\mathcal{R}_{pq} \cdot \mathcal{I}^{sky})_{(l,m)}$. Therefore, the dirty beam can be written as:

$$\mathcal{I}_{l,m}^D = \left(\sum_{pq} \mathcal{B}_{pq} \circ (\mathcal{R}_{pq} \cdot \mathcal{I}) \right)_{(l,m)}$$

If the integration windowing function were the same in all baseline, then we can write:

$$\mathcal{I}_{l,m}^D = \left(\left(\sum_{pq} \mathcal{B}_{pq} \right) \circ (\mathcal{R} \cdot \mathcal{I}) \right)_{(l,m)}$$

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by the author.

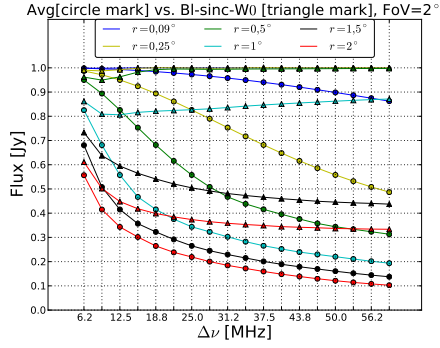


Figure 27. Response to a 1Jy source at different positions, as a function of bandwidth with 2° frequency sinc filter.

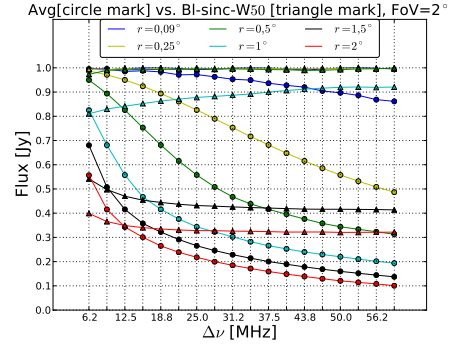


Figure 28. Response to a 1Jy source at different positions, as a function of bandwidth with 2° frequency overlap sinc filter.

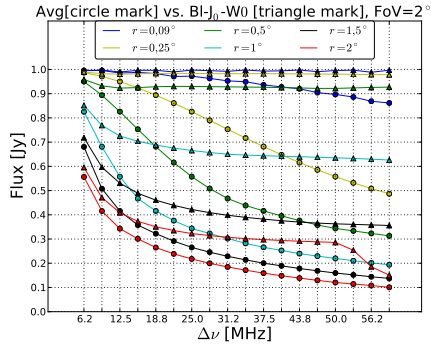


Figure 29. Response to a 1Jy source at different positions, as a function of bandwidth with 2° frequency Bessel first kind filter.

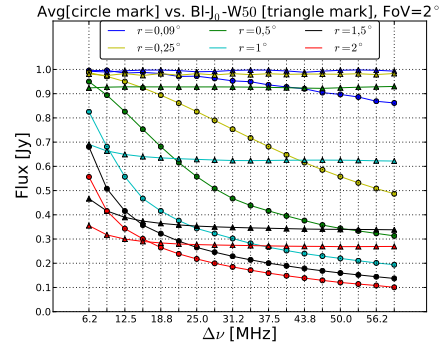


Figure 30. Response to a 1Jy source at different positions, as a function of bandwidth with 2° frequency overlap Bessel first kind filter.

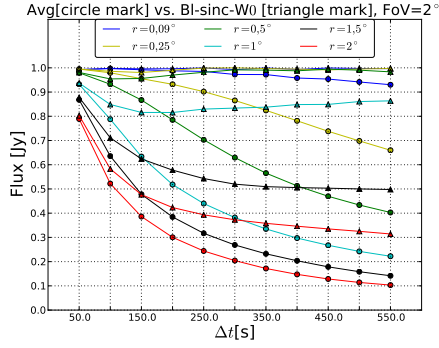


Figure 31. Response to a 1Jy source at different positions, as a function of integration time with 2° frequency sinc filter.

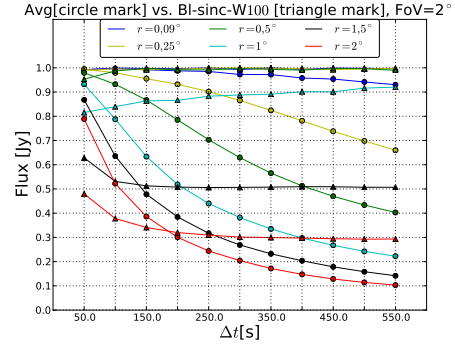


Figure 32. Response to a 1Jy source at different positions, as a function of integration time with 2° frequency overlap sinc filter.

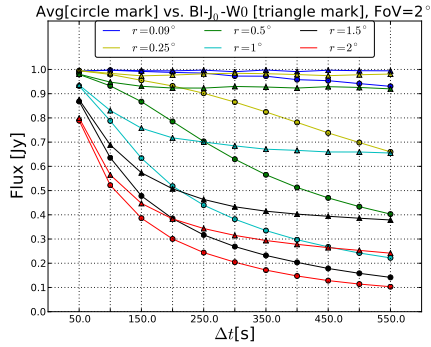


Figure 33. Response to a 1Jy source at different positions, as a function of integration time with 2° frequency Bessel first kind filter.

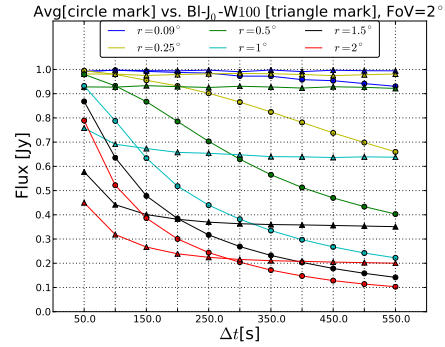


Figure 34. Response to a 1Jy source at different positions, as a function of integration time with 2° frequency overlap Bessel first kind filter.

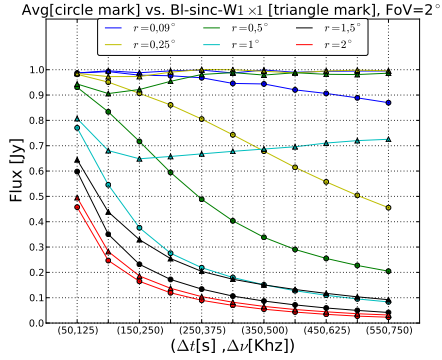


Figure 35. Response to a 1Jy source at different positions, as a function of integration time and bandwidth; with 2° frequency sinc filter.

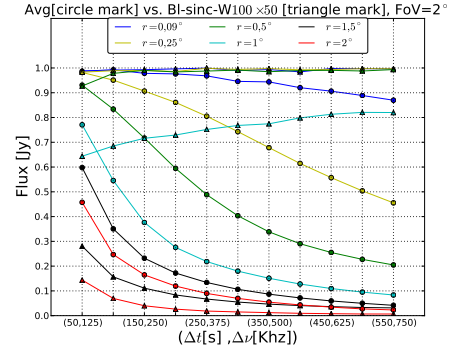


Figure 36. Response to a 1Jy source at different positions, as a function of integration time and bandwidth; with 2° frequency overlap sinc filter.

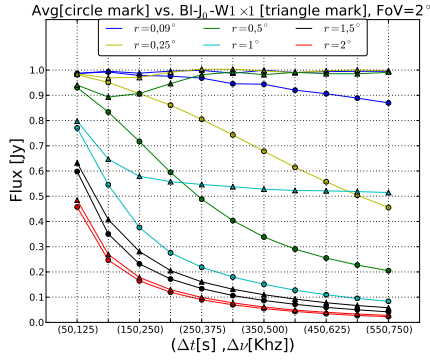


Figure 37. Response to a 1Jy source at different positions, as a function of integration time and bandwidth; with 2° frequency Bessel first kind filter.

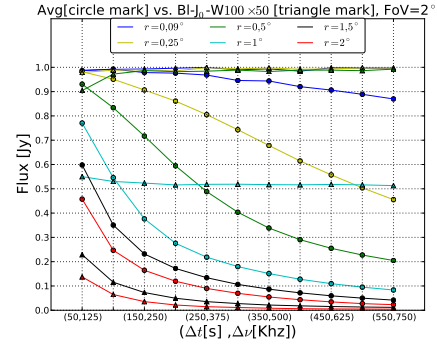


Figure 38. Response to a 1Jy source at different positions, as a function of integration time and bandwidth; with 2° frequency overlap Bessel first kind filter.