Sapienza
Università di Roma

# Vibration Suppression Design for Virtual Compliance Control in Bilateral Teleoperation

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Locomotion and haptic interfaces for VR exploration

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# Introduction

# Problem statement

## Goal

Development of a controller able to suppress the vibration and unwanted inputs in a bilateral control system.

## Idea

Application of one degree of freedom *virtual* spring-damper system with an additional inertia.

The disturbance suppression performances depend on the value of these virtual parameters, determined from the desired cut-off frequencies.

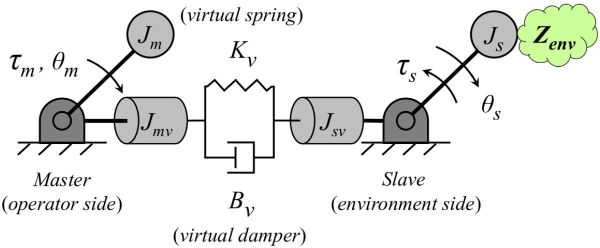
# Goal of the teleoperation

1. **Stability** of the closed loop system irrespective to the behaviour of the human and the environment

2. **Transparency** of the teleoperation task: same forces and displacements on the two sides of the system

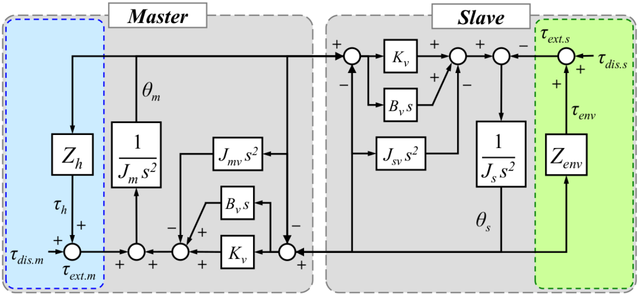
# System Modeling

# Inertia-Spring-Damper System




- Real inertiae: $J_m, J_s$
- Virtual inertiae: $J_{mv}, J_{sv}$
- Virtual damper and spring: $B_v, K_v$

# Bilateral Control Scheme




Dynamics equations of the system:

$$(J_m + J_{mv})\ddot{\theta}_m + B_v(\dot{\theta}_m - \dot{\theta}_s) + K_v(\theta_m - \theta_s) = \tau_m$$
$$(J_s + J_{sv})\ddot{\theta}_s + B_v(\dot{\theta}_s - \dot{\theta}_m) + K_v(\theta_s - \theta_m) = -\tau_s$$

# Bilateral Controller

The virtual parameters are considered elements of the controller. Equations are rearranged:

$$J_m s^2\theta_m = \tau_m - (B_v s + K_v)(\theta_m - \theta_s) - J_{mv} s^2\theta_m$$
$$J_s s^2\theta_s = -\tau_s - (B_v s + K_v)(\theta_s - \theta_m) - J_{sv} s^2\theta_s$$

where the external torques are action and reaction forces of the human and the environment.

System represented by:

$$\begin{bmatrix}\tau_m \\ \theta_s\end{bmatrix} = \underbrace{\begin{bmatrix}H_{11} & H_{12} \\ H_{21} & H_{22}\end{bmatrix}}_{\textit{Hybrid matrix}} \begin{bmatrix}\theta_m \\ -\tau_s\end{bmatrix}$$

# Bilateral Controller

Hybrid parameters $H_{ij}$:

$$
\begin{aligned}
H_{11} &= \frac{1}{Z_s}[Z_m Z_s - (B_v s + K_v)^2] \\
H_{12} &= -\frac{1}{Z_s}[B_v s + K_v] \\
H_{21} &= \frac{1}{Z_s}[B_v s + K_v] \\
H_{22} &= \frac{1}{Z_s}
\end{aligned}
$$

where:

$$
\begin{aligned}
Z_m &= (J_m + J_{mv})s^2 + B_v s + K_v \\
Z_s &= (J_s + J_{sv})s^2 + B_v s + K_v
\end{aligned}
$$

# Bilateral Controller

*Condition of transparency*: trasmitted impedance $Z_t$ transferred to the operator should be equal to environment impedance $Z_{env}$:

$$\frac{\tau_m}{\theta_m} = Z_t = Z_{env} = \frac{\tau_s}{\theta_s}$$

Relationship between $Z_t$ and $Z_{env}$:

$$Z_t = (\frac{-H_{12}H_{21}}{1 + H_{22}Z_{env}})Z_{env} + H_{11}$$

# Vibration Suppression Design

# Parameters Selection and Design

Assume system disturbed by environment vibration noise.

Inspect $H_{22}$ for the relationship of position response $\theta_s$ and external torque input $\tau_{ext}$:

$$\frac{\theta_s}{\tau_{ext}} = \frac{1}{(J_s + J_{sv})s^2 + B_v s + K_v}$$

Virtual parameters $J_v, B_v$ and $K_v$ determined from the characteristic equation:

$$s^2 + (g_1 + g_2)s + (g_1 \cdot g_2) = 0$$

where the poles $g_1$ and $g_2$ represent the desired cut-off frequencies.

# Parameters Selection and Design

Spring stiffness $K_v$ influences the transparency.

It regulates the *compliance* of the system, achieving **rigid coupling** (high spring stiffness) or **spring coupling** (low spring stiffness).

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Spring stiffness $K_v$ influences the transparency.

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$$\boxed{\text{We want to chose } K_v \text{ beforehand!}}$$

Virtual parameters $B_v$ and $J_v$ computed according to $K_v$:

$$B_v = \left(\frac{g_1 + g_2}{g_1 \cdot g_2}\right) K_v$$

and

$$J_{sv} = \left(\frac{1}{g_1 \cdot g_2}\right) K_v - J_s$$

# Simulations

# Simulation conditions

Simulation are done in ideal condition:

- the communication between master and slave have no critical aspects;
- instantaneous and loss-less signal transfer.

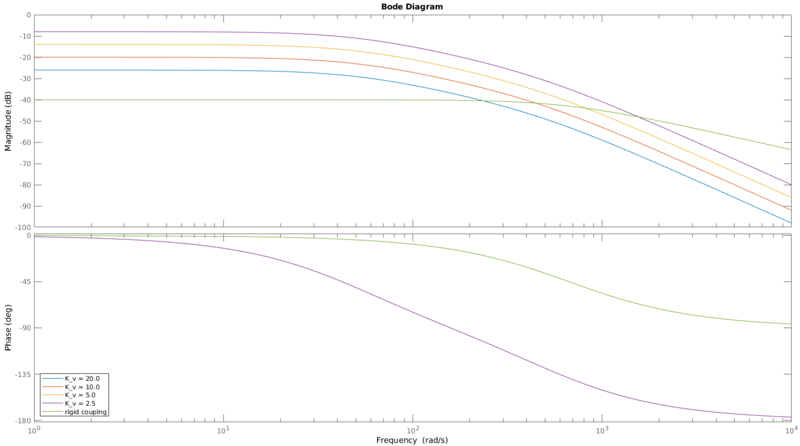
We will compare two different settings:

| Behaviour | $K_v$ | $B_v$ | $J_v$ |
|---|---|---|---|
| Virtual compliance | $20.0\ \frac{\mathrm{N\,m}}{\mathrm{rad}}$ | $4.4 \cdot 10^{-1}\ \frac{\mathrm{N\,m}}{\mathrm{rad/s}}$ | $3 \cdot 10^{-4}$ kg m$^2$ |
| Rigid coupling | $10^2\ \frac{\mathrm{N\,m}}{\mathrm{rad}}$ | $1.5 \cdot 10^{-1}\ \frac{\mathrm{N\,m}}{\mathrm{rad/s}}$ | $0$ kg m$^2$ |

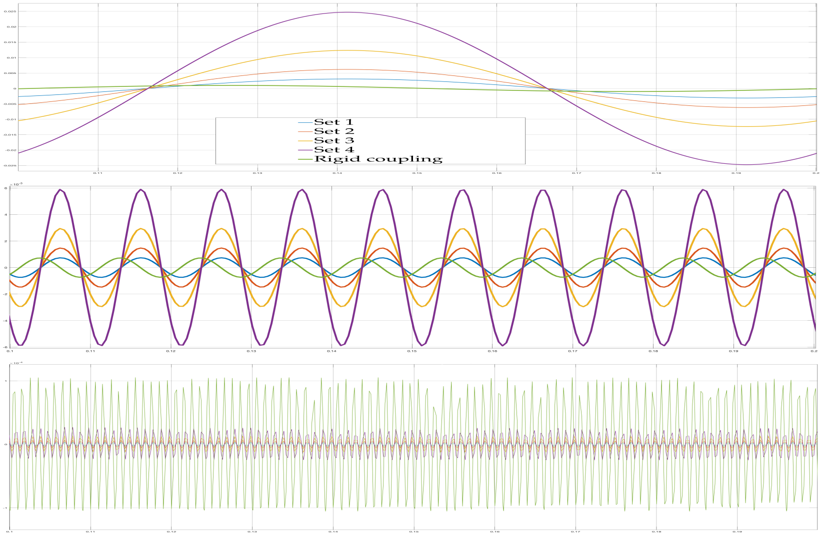
**Table 1:** Sets of chosen virtual parameters.

# Disturbance response

$$\frac{\theta_s}{\tau_{ext}} = \frac{1}{(J_s + J_{sv})s^2 + B_v s + K_v}$$



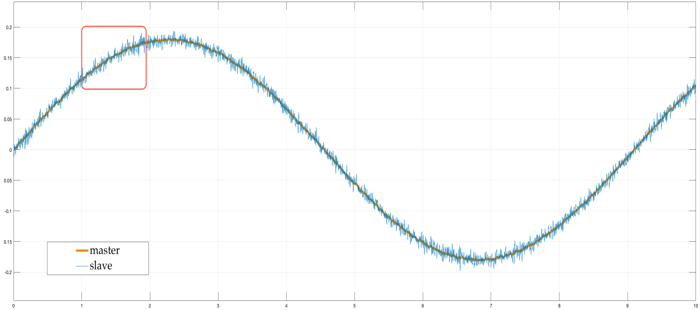
# Vibration suppression




Noise frequency : 10 Hz | $10^2$ Hz | $10^3$ Hz

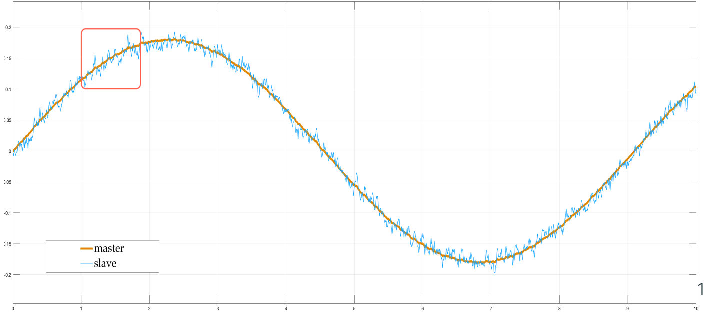
# Free Motion: High frequency noise

Rigid coupling:



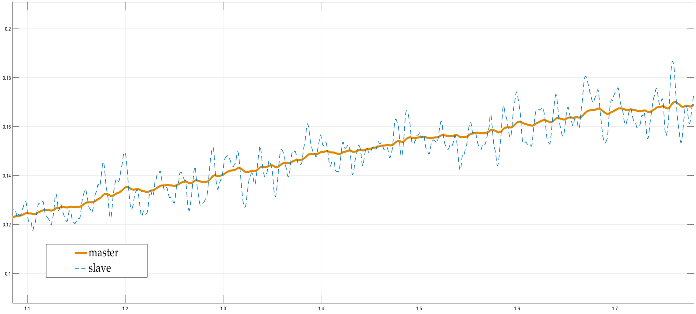

High frequency: 50 Hz

Virtual compliance:



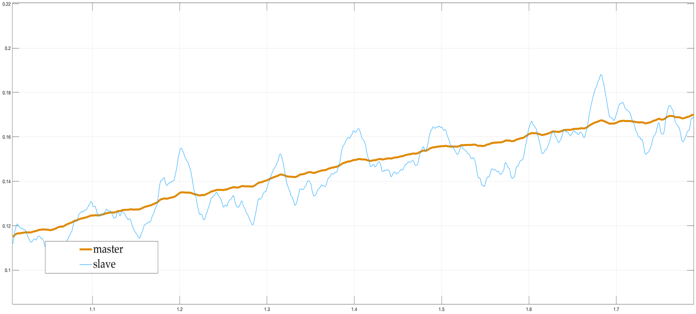
# Free Motion: High frequency noise

Rigid coupling:



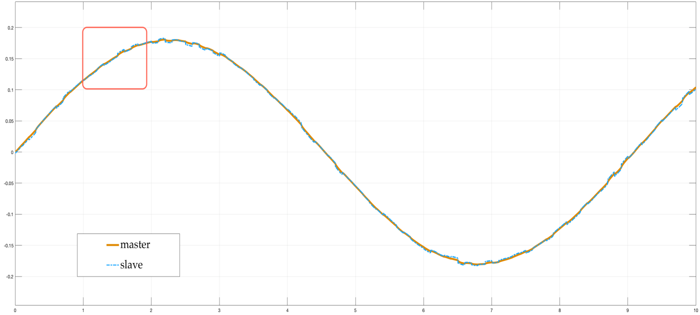

High frequency: 50 Hz

Virtual compliance:



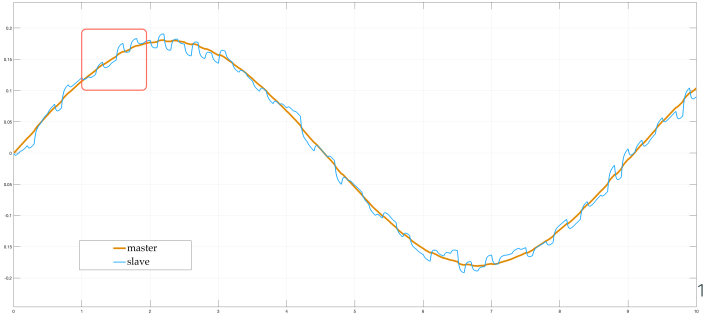
# Free Motion: Low frequency noise 20 Hz

Rigid coupling:



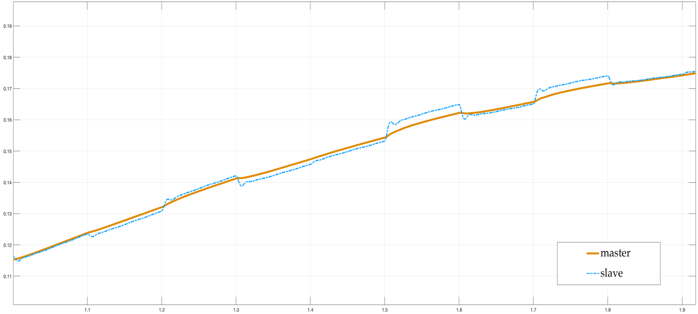

Low frequency: 20 Hz

Virtual compliance:



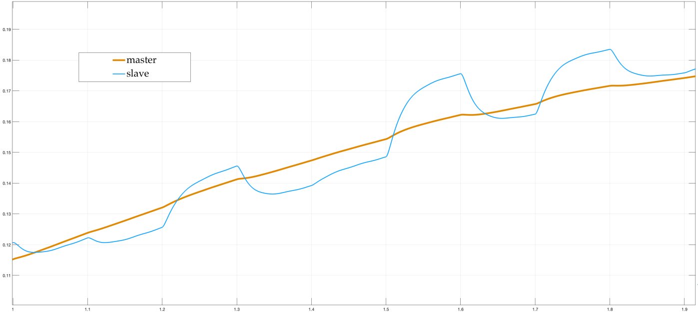
# Free Motion: Low frequency noise 20 Hz

Rigid coupling:



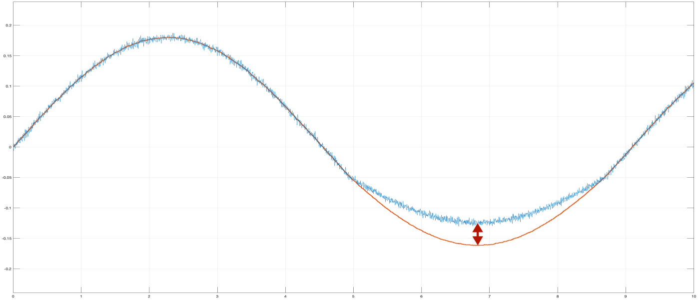

Low frequency: 20 Hz

Virtual compliance:



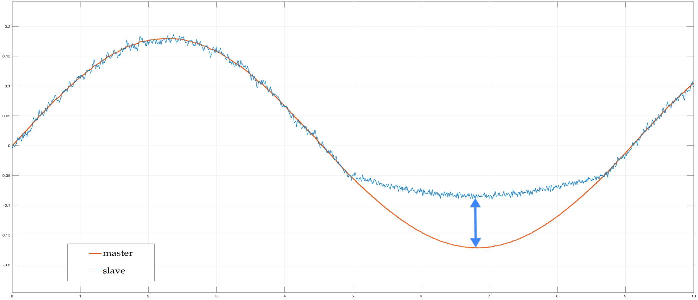
# Task execution: In contact

Rigid coupling: lower error



Position tracking error

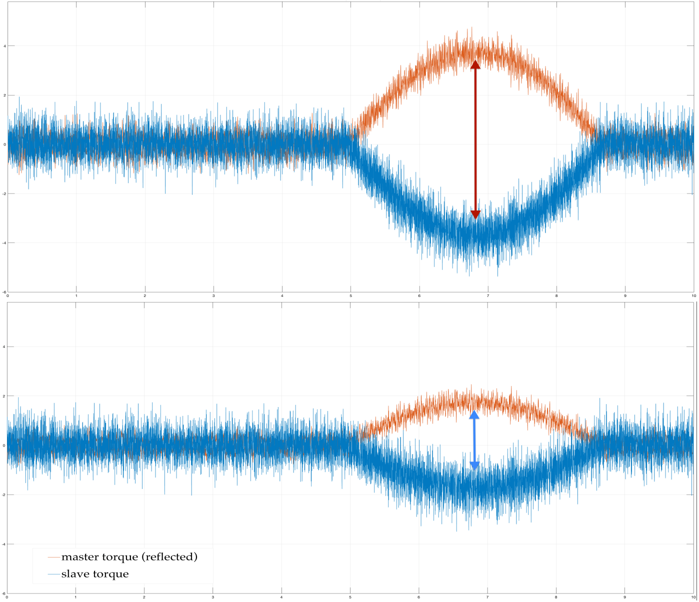
Virtual compliance: higher error



# Task execution: In contact

Rigid coupling: higher torque noise

Virtual compliance: lower torque noise



# Task execution: In contact

Qui ci sta il film.

# Conclusions

# Conclusions

Proposed solution:

- based on **virtual** spring-dumper system with additional inertia;
- desired **cut-off** frequencies obtained regulating the **virtual** spring stiffness.

Consequences:

- the proposed controller preserves the useful (*low*) frequency inputs and reject the noisy ones (*high*).
- In contact motion it leads to a position gap between master and slave. It can be used only in **soft material handling** tasks.

Thank you for your attention!