

# SYSTEMS AND METHODS FOR FEED-FORWARD PHASE AND TIMING CORRECTION OF HIGH-POWER OPTICAL PULSES FOR COHERENCE-CONTROLLED NUCLEAR FUSION

Inventor: Jonathan Washburn

January 25, 2026

## Abstract

Systems and methods are disclosed for imposing attosecond-scale timing and phase precision onto high-power optical pulses without requiring intrinsic stabilization of a high-power amplifier chain. The invention decouples power generation from timing precision by employing a feed-forward control architecture comprising a high-power laser source ("Cannon"), a precision optical master clock, a single-shot cross-correlation measurement unit, and a dual-stage optical delay line. By measuring the timing jitter of each high-power pulse relative to the master clock and applying a compensatory delay before the pulse reaches the target, the system achieves sub-femtosecond synchronization (e.g.,  $< 0.1$  fs) despite input jitter in the picosecond range. This enables the realization of Recognition Science (RS) fusion regimes where a coherent pulse train modifies the effective dielectric permittivity of the vacuum, thereby screening the Coulomb barrier and enhancing fusion probability.

## 1 Technical Field

The present disclosure relates to high-energy pulsed laser systems, optical timing and phase synchronization, and controlled nuclear fusion. In particular, the disclosure relates to feed-forward optical phase and timing correction systems for inertial confinement fusion (ICF) drivers and other pulsed drivers requiring sub-femtosecond synchronization to access vacuum-polarized fusion regimes.

## 2 Background

Standard inertial confinement fusion (ICF) relies on thermal compression of fuel pellets. Current state-of-the-art drivers (e.g., NIF) achieve timing precision in the range of 5-30 picoseconds. Recognition Science (RS) theory predicts that fusion cross-sections can be enhanced by orders of magnitude if the driving pulses maintain phase coherence with a fundamental time quantum ( $\tau_0 \approx 7.3$  fs) to within a tolerance of  $< 0.1\tau_0$  (approx. 0.7 fs).

Existing high-power lasers cannot achieve this stability due to thermal drift, vibration, and amplifier path length variations. Passive stabilization of kilometer-scale beamlines to nanometer tolerances is engineeringly infeasible. A new control architecture is required to bridge the gap between picosecond power and attosecond precision.

A naive alternative is *gating*: blocking or discarding pulses that are not sufficiently aligned. However, for picosecond-jitter sources, the duty cycle for sub-femtosecond alignment is extremely low (e.g.,  $< 0.01\%$ ), resulting in prohibitive energy waste.

Accordingly, there is a need for systems that can (i) measure pulse-to-reference misalignment at high precision on a single-shot basis and (ii) correct the misalignment in a feed-forward manner for the same pulse, thereby transferring clock-grade stability onto high-energy optical pulses.

## 3 Summary

In one aspect, a feed-forward “measure–buffer–correct” architecture is provided.

### Core concept

A stable optical reference defines an intended timing/phase schedule. Each high-power pulse is sampled and compared to the reference to estimate an instantaneous error. The main pulse is optically buffered to provide computational latency. An active optical corrector applies a compensating group delay and/or phase shift before the pulse reaches the target.

### Key advantages

- **Decoupling of power and precision:** the high-power chain may remain “sloppy” (picosecond jitter) while the delivered pulse train achieves sub-femtosecond alignment.
- **Vacuum Polarization:** Enables the “Vacuum Polarizer” mode of operation, where the coherent pulse train modifies the effective dielectric permittivity of the vacuum at the target site.
- **No energy waste gating:** instead of discarding misaligned pulses, the pulse is corrected.
- **Scalable to many beams:** a shared optical clock can synchronize many channels with local correction stages.

## 4 Brief Description of Drawings (Optional)

- **FIG. 1:** Block diagram of a feed-forward phase correction loop showing the Cannon, Clock, Sampler, and Corrector.
- **FIG. 2:** Example dual-stage delay correction (coarse mechanical delay + fine electro-optic group delay).
- **FIG. 3:** Example single-shot cross-correlation measurement unit.

## 5 Detailed Description

The following description is illustrative and not limiting. References to “one embodiment” may describe a subset of embodiments.

### 5.1 Definitions

- **Optical reference:** a phase-stable timing reference, including but not limited to an optical frequency comb, a mode-locked oscillator, a CEP-stabilized oscillator, or any optical clock providing a stable phase/timing basis.
- **Single-shot measurement:** a measurement that yields timing/phase error for an individual pulse without averaging across multiple pulses.
- **Group delay correction:** an adjustment that changes the arrival time of a pulse (e.g., by applying a controllable optical path length or dispersive phase).
- **Vacuum Polarization:** The modification of the vacuum’s dielectric properties by a coherent electromagnetic field, effectively screening electrostatic potentials.

### 5.2 System Architecture

An example system comprises:

1. a high-power pulsed optical source (“Cannon”) producing a pulse train with initial timing jitter (e.g.,  $> 1$  ps);
2. an optical splitter producing a sampled portion and a main portion of a given pulse;
3. a single-shot timing/phase measurement module that compares the sampled portion to an optical reference (“Clock”) and outputs an error estimate  $\delta t$  (timing) and/or  $\delta\varphi$  (phase);
4. an optical buffer routing the main portion through a delay path (e.g.,  $> 10$  meters), providing latency for computation and actuator response;
5. a feed-forward controller that transforms the measured error into a correction command; and

6. a variable optical delay element that applies a compensating group delay and/or phase correction to the main portion prior to target delivery, reducing jitter to the attosecond regime (e.g.,  $< 0.1$  fs).

### 5.3 Single-Shot Timing/Phase Measurement

In various embodiments, the measurement module comprises one or more of:

- nonlinear optical cross-correlation (sum-frequency generation, difference-frequency generation, or equivalent);
- spectral interferometry or dispersive Fourier transform methods;
- f–2f interferometry and carrier-envelope phase estimation;
- balanced optical heterodyne detection with the optical reference.

The module outputs, for each pulse, an estimated timing error  $\delta t$  relative to the reference schedule. In some embodiments, the estimate includes uncertainty bounds and quality flags.

### 5.4 Optical Buffer / Delay Path

The optical buffer provides a deterministic latency that exceeds the combined computation time and actuator response time. For a correction system requiring 100 ns of processing time, the delay path must exceed 30 meters. Non-limiting examples include:

- free-space vacuum delay lines (to avoid air turbulence dispersion);
- fiber delay lines (with dispersion compensation);
- optical cavities or recirculating delay loops;
- chirped dispersive paths.

### 5.5 Variable Optical Delay and Dual-Stage Correction

A practical system may require large correction range (picoseconds) and fine correction resolution (sub-femtosecond). In one embodiment, the variable optical delay comprises a dual-stage corrector:

- **Coarse stage:** a mechanical delay line (e.g., an “optical trombone” or piezo-actuated mirror), providing large-range correction (e.g.,  $\pm 100$  ps) with coarse precision (e.g.,  $\sim 100$  fs).
- **Fine stage:** an electro-optic, acousto-optic, or dispersive phase element (e.g., Lithium Niobate modulator) providing sub-femtosecond group delay resolution and high bandwidth (e.g., range  $\pm 500$  fs, precision  $< 0.1$  fs).

The controller partitions the correction into a coarse component and a fine component to meet dynamic range requirements (e.g., 20,000:1 dynamic range).

## 5.6 Multi-Beam Implementation

In multi-beam fusion drivers, each beam path may include a local feed-forward correction stage while sharing a common optical reference. The single-shot measurement may be performed per beam, or via representative sampling with per-channel calibration.

## 5.7 Fusion Application: Vacuum Screening

When applied to fusion drivers, the corrected pulse train is delivered to a target such that inter-pulse timing and/or phase satisfy a prescribed coherence schedule (e.g., derived from the Golden Ratio  $\phi$ ). This precise alignment achieves a coherence state  $C_\phi$  that modifies the effective dielectric permittivity of the vacuum at the target site ( $\epsilon_{\text{ledger}} > 1$ ). This "Vacuum Polarization" effect screens the Coulomb barrier between fuel nuclei, enhancing the fusion probability according to the scaling law  $S = 1/(1 + C_\phi + C_\sigma)$ .

## Claims

1. A system comprising: (a) a pulsed optical source configured to generate one or more high-power optical pulses; (b) an optical reference providing a stable phase and timing reference; (c) a splitter configured to generate, for a given pulse, a sampled portion and a main portion; (d) a single-shot measurement module configured to estimate a timing error of the given pulse relative to the optical reference based on the sampled portion; (e) an optical buffer configured to delay the main portion; and (f) a variable optical delay element configured to apply, to the main portion, a compensating group delay based on the estimated timing error prior to delivery to a target.
2. The system of claim 1, wherein the variable optical delay element is configured to align the main portion to the optical reference with a timing precision of less than 1 femtosecond.
3. The system of claim 1, wherein the single-shot measurement module comprises a non-linear optical cross-correlator configured to measure timing offset between the sampled portion and the optical reference.
4. The system of claim 1, wherein the optical reference comprises an optical frequency comb.
5. The system of claim 1, wherein the optical buffer comprises a delay path of sufficient length to provide a latency exceeding a computation time required to determine the compensating group delay.
6. The system of claim 1, wherein the variable optical delay element comprises a coarse delay stage and a fine delay stage, the coarse delay stage providing a larger delay range and the fine delay stage providing a smaller delay range with higher timing resolution.
7. The system of claim 6, wherein the coarse delay stage comprises a mechanically actuated optical path length adjuster and the fine delay stage comprises an electro-optic modulator configured to adjust group delay.

8. The system of claim 1, wherein the system is configured to compensate for an initial timing jitter of greater than 1 picosecond to achieve a final timing jitter of less than 0.1 femtoseconds.
9. The system of claim 1, further comprising a controller configured to compute the compensating group delay from the estimated timing error and to drive the variable optical delay element.
10. The system of claim 1, wherein the target is a nuclear fusion target and the system is configured to drive an inertial confinement fusion event by inducing a vacuum polarization effect that screens a Coulomb barrier.
11. A method comprising: (a) splitting, from a high-power optical pulse, a sampled portion and a main portion; (b) estimating, from the sampled portion, a timing error of the high-power optical pulse relative to a stable optical reference; (c) delaying the main portion in an optical buffer to provide time for computation and actuation; (d) applying a compensating group delay to the main portion based on the estimated timing error; and (e) delivering the main portion to a target after applying the compensating group delay.
12. The method of claim 11, wherein applying the compensating group delay aligns the main portion to a target schedule derived from the Golden Ratio ( $\phi$ ).
13. The method of claim 11, wherein delivering the main portion induces a coherence state in a vacuum surrounding the target, thereby increasing a dielectric permittivity of the vacuum and reducing an effective reaction barrier.
14. A non-transitory computer-readable medium storing instructions that, when executed by one or more processors, cause performance of operations comprising: receiving an estimated timing error for a pulse relative to an optical reference and outputting a control signal that drives a variable optical delay element to apply a compensating group delay to the pulse to achieve sub-femtosecond alignment.