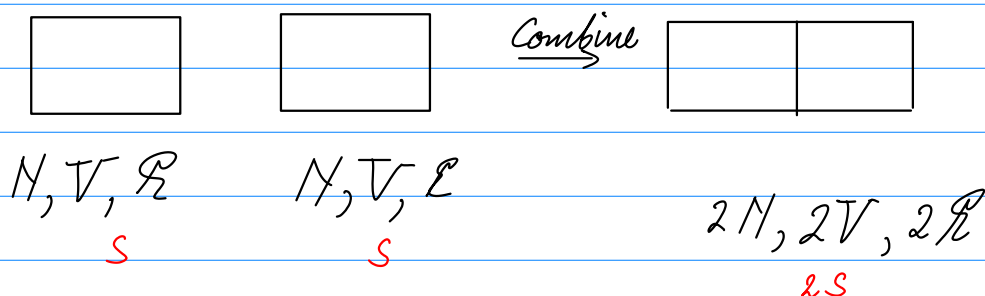


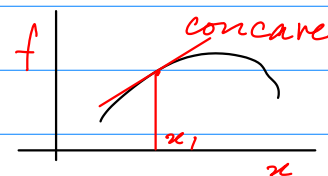
Thermodynamics

Extrinsic variables Scale with system size



Entropy: There exists a quantity, called the entropy
 S

Properties 1) extrinsic
2) concave.



Concave: $S(X^2) - S(X^1) \leq \left. \frac{\partial S}{\partial X} \right|_{X^1} (X^2 - X^1)$

$$X = N, V, E.$$

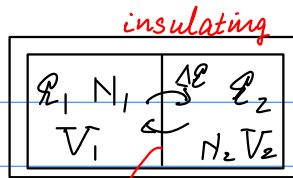
$$X^1 = (N^1, V^1, E^1) = X_j^1 \quad j = \overset{N}{1}, \overset{V}{2}, \overset{E}{3}$$

$$\underbrace{\frac{1}{T}}_{\text{temperature}} = \left. \frac{\partial S}{\partial E} \right)_{X_j \neq E} \geq 0$$

$\Rightarrow S$ always strives towards a maximum
(isolated system).

This maximum is reached at equilibrium

Thermally conducting, fixed wall



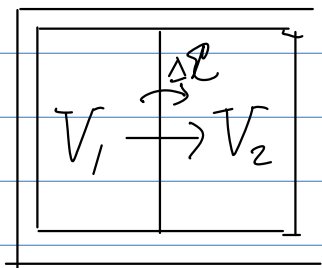
$$P_1 + P_2 = \text{const.} = P$$

$$\frac{\partial S}{\partial P_1} = \frac{\partial S_1}{\partial P_1} + \frac{\partial S_2}{\partial P_1} = \frac{\partial S_1}{\partial P_1} - \frac{\partial S_2}{\partial P_2} = 0$$

$$\frac{1}{T_1} = \frac{1}{T_2}$$

because we search for maximum of S!

Thermally conducting, moving wall



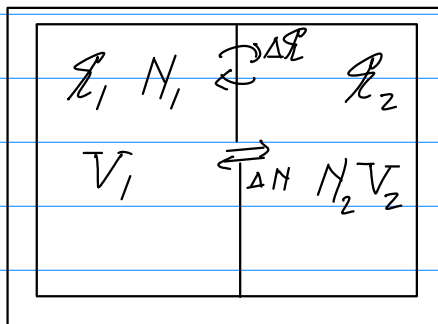
2 parameters P_1 and V_1
 $V_1 + V_2 = V = \text{fixed}$

$$\frac{\partial S_1}{\partial P_1} = \frac{\partial S_2}{\partial P_2} \rightarrow \frac{1}{T_1} = \frac{1}{T_2} = \frac{1}{T}$$

$$\frac{\partial S_1}{\partial V_1} = \frac{\partial S_2}{\partial V_2} = \frac{P_1}{T_1} = \frac{P_2}{T_2}$$

P: pressure

Conducting, fixed, permeable wall



2 parameters: P_1 and N_1

$$N_1 + N_2 = N = \text{fixed}$$

$$\frac{\partial S_1}{\partial N_1} = \frac{\partial S_2}{\partial N_2} = -\frac{\mu_2}{T_2} = -\frac{\mu_1}{T_1}$$

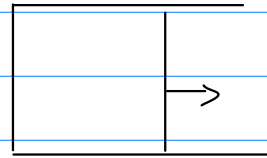
$$\mu_1 = \mu_2 \quad \text{chemical potential.}$$

1st law of thermodynamics:

$$d\mathcal{E} = \underbrace{dQ}_{\text{heat}} - \underbrace{dW}_{\text{work}}$$

exact non-exact.

$$dW = PdV$$



dQ : heat flow into system

dW : work done by the system

If we change N : $dW = PdV - \mu dN$

- Processes * quasi-static: always in equil.
* reversible: $\Delta S = 0$
* adiabatic: $dQ = 0$

Example quasi static process with $dW = 0$

$$dS = S(\mathcal{E} + dQ) - S(\mathcal{E}) = dQ \cdot \frac{\partial S}{\partial \mathcal{E}} = dQ \frac{1}{T}$$

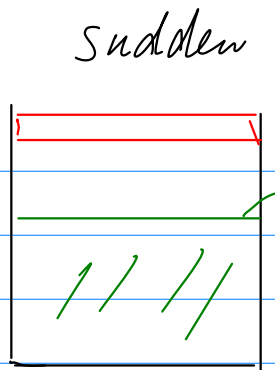
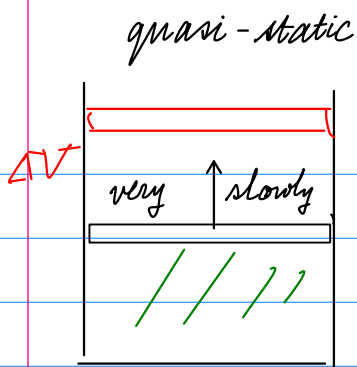
$$\rightarrow dQ = TdS. \quad \text{In general } dQ \leq TdS \quad \text{2nd law}$$

Example quasi-static, $\mathcal{E} = \text{const} \rightarrow d\mathcal{E} = 0$
 $N = \text{const.}$

$$d\mathcal{E} = dQ - dW = 0$$

$$TdS - PdV = 0 \quad P: \text{mechanical pressure}$$

$\rightarrow \frac{\partial S}{\partial V} = \frac{P}{T}$ So the mechanical pressure is the one we have met before: movable, conducting wall.



wall, suddenly pulled away.
adiabatic $\Delta Q = 0$
No work $\Delta W = 0$

If insulating,
 $dQ = 0$

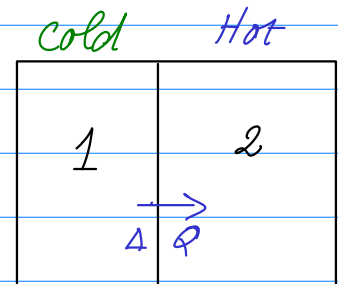
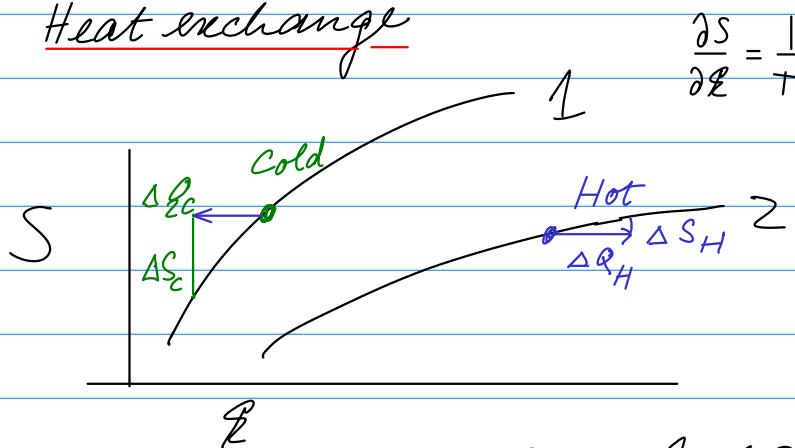
T decreases due to work
done by piston.

For ideal gas
 T remains
constant.

$$\Delta S \geq 0$$

$$\Delta S \geq \frac{\Delta Q}{T}$$

Heat exchange

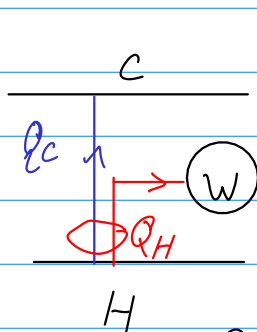


Heat flow from cold
to hot?

$$\Delta S = \Delta S_c + \Delta S_H < 0 \text{ Impossible, should be } \geq 0!$$

So: heat flow only from hot to cold.

$\Delta S = 0$ Reversible Carnot engine.



$$Q_H = Q_C + W$$

$$\Delta S_H = -Q_H/T_H \leq 0$$

$$\Delta S_C = Q_C/T_C \geq 0$$

$$\Delta S = \Delta S_H + \Delta S_C = 0 \rightarrow \frac{Q_H}{T_H} = \frac{Q_C}{T_C}$$

$$\text{Efficiency: } \eta = \frac{W}{Q_H} = 1 - \frac{Q_C}{Q_H} = 1 - \frac{T_C}{T_H} \text{ Carnot eff.} \\ = \eta_c$$

Now, relax the condition $\Delta S = 0$ allow $\Delta S > 0$.

$$W = -\Delta \mathcal{E}^H - \Delta \mathcal{E}^C$$

$$\Delta \mathcal{E} = \mathcal{E}^f - \mathcal{E}^i$$

$$= -T^H \Delta S^H - T^C \Delta S^C$$

$$\mathcal{E}_H = -\Delta \mathcal{E}^H = -T^H \Delta S^H$$

$$\eta = \frac{W}{\mathcal{E}_H} = 1 + \frac{T_C \Delta S^C}{T_H \Delta S^H} \leq 1 - \frac{T_C}{T_H} = \eta_c$$

$$\Delta S^C + \Delta S^H \geq 0 \Rightarrow + \frac{\Delta S^C}{\Delta S^H} \leq -1$$

$$\text{So } \eta \leq \eta_c$$

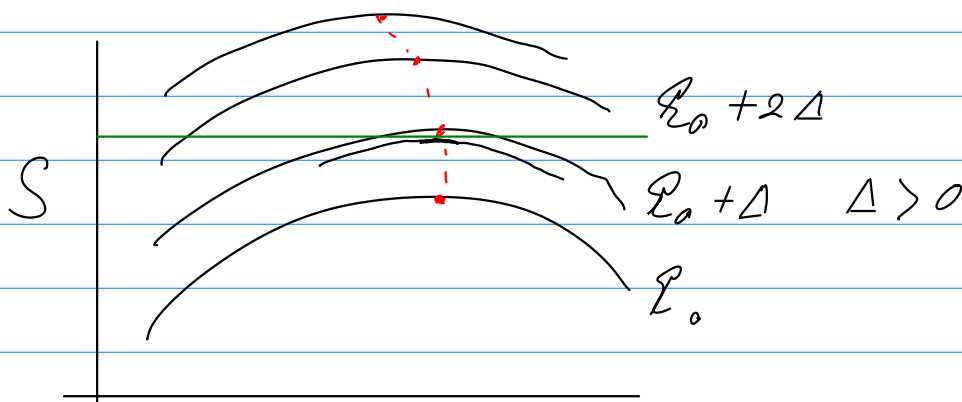
Carnot engine with $\Delta S = 0$ is the best we can do.

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Legendre transformation.

$$S(\mathcal{E}, V, N) \rightarrow \mathcal{E}(S, V, N)$$

$$\left. \frac{\partial S}{\partial \mathcal{E}} \right|_{V, N} = \frac{1}{T} \geq 0$$



$X = V, \text{ or } N_i$
 $S \rightarrow \max \quad \mathcal{E} \rightarrow \min.$

Mathematical Intermediate Legendre transf.

$$f(x, \xi) \rightarrow \xi^*: \frac{\partial f(x, \xi^*)}{\partial \xi} = 0 \quad \text{min.}$$

$$y = \frac{\partial f(x, \xi)}{\partial x} \rightarrow x = x(y, \xi). \quad \text{possible provided } f \text{ is convex}$$

Legendre transf: $g(y, \xi) = f(x, \xi) - xy$

$$\left. \frac{\partial g}{\partial \xi} \right|_y = \frac{\partial f}{\partial \xi} + \underbrace{\frac{\partial f}{\partial x} \frac{\partial x}{\partial \xi}}_y - \frac{\partial x}{\partial \xi} y = \frac{\partial f}{\partial \xi} \quad \begin{matrix} \text{IF:} \\ = 0 \\ \text{Max!} \end{matrix}$$

$$\left(L = \frac{m}{2} \dot{x}^2 - V(x) \quad p = \frac{\partial L}{\partial \dot{x}} = m \dot{x} \right. \\ \left. \dot{x} = p/m \right)$$

$\mathcal{E}(S, V, N)$ strives towards minimum.

$$\left. \frac{\partial \mathcal{E}}{\partial S} \right|_{V, N} = T (= y)$$

$$F = \mathcal{E} - TS = \text{Helmholtz free energy.}$$

F strives towards minimum.

$$F(T, V, N)$$

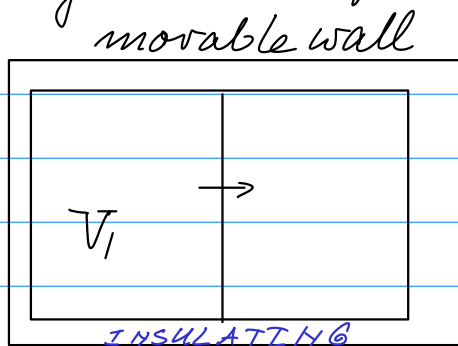
$$\text{Keep } T \text{ const } \Delta F = \Delta \mathcal{E} - T \Delta S$$

$$= \Delta Q - \Delta W - T \Delta S \stackrel{\text{use } T \Delta S \geq \Delta Q}{\leq} -\Delta W$$

work done by system

or: $\Delta W \leq -\Delta F$, hence $-\Delta F$ is the max. amount done by the system.

Legendre transformation revisited.



\mathcal{E} fixed.

System relaxes \rightarrow

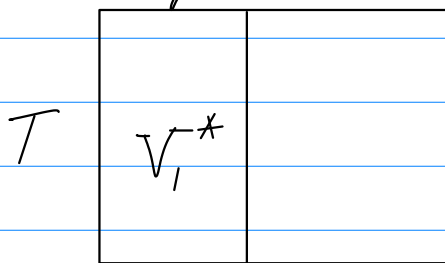
$$V_1 \rightarrow V_1^*$$

\hookrightarrow equilibrium value

At equilibrium, $T = \left. \frac{\partial \mathcal{E}}{\partial S} \right|_{V_1^*}$ Equil.: \mathcal{E}, T, V_1^*, S

also at equl: $\frac{\partial \mathcal{E}(S, V_1^*, N)}{\partial V_1} = 0$ $\frac{1}{T} = \left. \frac{\partial S}{\partial \mathcal{E}} \right|_{N, V_1}$

Now make the insulating wall conducting, and place the system in an environment at temp. T .



Nothing will change.

So, for a system at temperature T , V_1^* is the equil. volume.

So we should have $\left. \frac{\partial F}{\partial V_1} \right|_T (T, V_1^*) = 0$

That works for $F = \mathcal{E} - TS$ (Note $T = \left. \frac{\partial \mathcal{E}}{\partial S} \right|_V$)
because that is a Legendre transf.

$$F(T, V_1, N) = \mathcal{E}(S(\mathcal{E}, V_1), V_1) - T S(\mathcal{E}, V_1)$$

$$\left. \frac{\partial F}{\partial V_1} \right|_T = \left. \frac{\partial \mathcal{E}}{\partial V_1} \right|_S + \underbrace{\left. \frac{\partial \mathcal{E}}{\partial S} \right|_{V_1}}_{\substack{= T \\ T}} \left. \frac{\partial S}{\partial V_1} \right|_{\mathcal{E}} - T \left. \frac{\partial S}{\partial V_1} \right|_{\mathcal{E}} = \left. \frac{\partial \mathcal{E}}{\partial V_1} \right|_S \text{ at equil.} = 0.$$

So far: $\mathcal{E}(S, V, N)$

P. 2.9, 2.11, 2.14

$$F(T, V, N) = \mathcal{E} - TS$$

Helm-
holz

$$dF = d\mathcal{E} - TdS - SdT = \underbrace{TdS - PdV + \mu dN}_{\text{1st law}} - TdS - SdT$$

$$= -SdT - PdV + \mu dN$$

$$\left. \frac{\partial F}{\partial T} \right|_{N, V} = -S ; \left. \frac{\partial F}{\partial V} \right|_{T, N} = -P ; \left. \frac{\partial F}{\partial N} \right|_{T, V} = \mu$$

—//— eq of state

Leg. transf. of F with respect to V

Gibbs

$$G = F - V \left. \frac{\partial F}{\partial V} \right|_{T, N} = F + PV = \mathcal{E} - TS + PV = G(T, P, N)$$

$$dG = -SdT + VdP + \mu dN \rightarrow \left. \frac{\partial G}{\partial T} \right|_{P, N} = -S \text{ etc.}$$

Leg. transf of F w.r.t N

Grand
pot.

$$\Omega = F - \left. \frac{\partial F}{\partial N} \right|_{S, V} N = F - \mu N = \mathcal{E} - TS - \mu N = \Omega(T, V, \mu)$$

$$\rightarrow d\Omega = -SdT - PdV - Nd\mu \rightarrow -S = \left. \frac{\partial \Omega}{\partial T} \right|_{V, \mu} \text{ etc.}$$

Legendre transf of energy w.r.t V $\mathcal{E}(S, \textcircled{V}, N)$

Enthalpy

$$H = \mathcal{E} - \left. \frac{\partial \mathcal{E}}{\partial V} \right|_{S, N} V = \mathcal{E} + PV = H(S, P, N)$$

$$dH = TdS + VdP + \mu dN$$

Maxwell relations (P2.10)

$$\left(\frac{\partial F}{\partial V} \right)_{T,N} = -P \quad \left(\frac{\partial F}{\partial T} \right)_{V,N} = -S$$

$$\frac{\partial^2 F}{\partial V \partial T} = - \left(\frac{\partial P}{\partial T} \right)_{V,N} = - \left(\frac{\partial S}{\partial V} \right)_{T,N}$$

and many other relations.

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Euler relation (P2.15).

* S is a function of the extensive variables:

$$S = S(E, V, N)$$

* S itself is an extensive variable.

$$\text{So: } S(\lambda E, \lambda V, \lambda N) = \lambda S(E, V, N)$$

Take the derivative w.r.t. λ on left & right hand side and set $\lambda=1$

$$E \left(\frac{\partial S}{\partial E} \right)_{N,V} + V \left(\frac{\partial S}{\partial V} \right)_{N,E} + N \left(\frac{\partial S}{\partial N} \right)_{E,V} = S$$

$$\rightarrow E \cdot \frac{1}{T} + V \frac{P}{T} - N \frac{\mu}{T} = S, \text{ or}$$

$$\underline{E = TS - PV + \mu N} \quad (\text{Euler eqn}).$$

Consequence:

$$dE = \underline{TdS} + SdT - \underline{PdV} - VdP + \underline{\mu dN} + Nd\mu$$

Using $dE = TdS - PdV + \mu dN$, we obtain

$$SdT - VdP + Nd\mu = 0 \quad (\text{Gibbs-Duhem})$$

Gibbs free energy:

$$G = \mathcal{E} - TS + PV = \underbrace{TS - PV + \mu N}_{\mathcal{E}} - TS + PV \\ = \underline{\mu N}$$

Generalizations, magnetic systems. (P2.16)

$$S = S(\mathcal{E}, X_1, \dots, X_r) \quad X_i: \text{extensive variables.}$$

$$\text{and } \mathcal{E} = \mathcal{E}(S, X_1, \dots, X_r). \quad \left. \frac{\partial S}{\partial \mathcal{E}} \right|_{X_j} = \frac{1}{T} > 0$$

$$\text{Generalized forces: } f_i = \left. \frac{\partial \mathcal{E}}{\partial X_i} \right|_{X_j \neq i}$$

$$-d\mathcal{E} = dW = - \sum_i f_i dX_i \quad \text{intrinsic}$$

$$\text{Example } X_i = V, \text{ then } f_i = \frac{\partial \mathcal{E}}{\partial V} = -P$$

$$\text{So } dW = P dV.$$

$$\text{And } \mu = \left. \frac{\partial \mathcal{E}}{\partial N} \right|_{S, V} \quad \text{so this gives } dW = -\mu dN.$$

For a magnet, the external field H is the generalised force
The magnetisation M is the extrinsic variable

$$\left. \frac{\partial \mathcal{E}}{\partial M} \right|_{S, N} = +\mu_0 H, \quad \text{so } dW = -\mu_0 H dM$$

$$\text{So } d\mathcal{E} = T dS + \mu_0 H dM + \mu dN$$

Legendre transf. with respect to M

$$E(S, H, N) = \mathcal{E} - \mu_0 H M$$

'enthalpy'

Leg. transf. w.r.t. S :

$$G(T, H, N) = \mathcal{E} - TS - \mu_0 H M$$

$$\text{and } dg = -SdT - \mu_0 M dH + \mu dN.$$

Specific heats.

Q: How much heat do I have to put into a system to change its temperature by an amount dT ?

$$\text{Quasistatic: } dQ = TdS = C_V dT \quad V \text{ const.} \\ = C_P dT \quad P \text{ const.}$$

Keep V const, N const: $dE = dQ$ ($dW = 0$ since V const).

So $C_V = T \left(\frac{\partial S}{\partial T} \right)_{N,V} = \left(\frac{\partial E}{\partial T} \right)_{N,V}$

C_P ? $V = V(T, P, N)$ (eqn of state, derived from $P = -\left(\frac{\partial F}{\partial V} \right)_{T,N}$)

Suppose we have $S(T, V, N)$. (N const)

Then $C_P = T \left(\frac{\partial S}{\partial T} \right)_P = T \left(\frac{\partial S}{\partial T} \right)_V + T \left(\frac{\partial S}{\partial V} \right)_T \left(\frac{\partial V}{\partial T} \right)_P$

$= T \left(\frac{\partial S}{\partial T} \right)_V + T \left(\frac{\partial P}{\partial T} \right)_V \left(\frac{\partial V}{\partial T} \right)_P$

$\underbrace{T \left(\frac{\partial S}{\partial T} \right)_V}_{C_V} \quad \text{maxwell relation.}$

Math
interezzo

$$f(x, y) \rightarrow df = \left(\frac{\partial f}{\partial x} \right)_y dx + \left(\frac{\partial f}{\partial y} \right)_x dy$$

$$\rightarrow \left(\frac{\partial x}{\partial y} \right)_f = - \frac{\left(\frac{\partial f}{\partial y} \right)_x}{\left(\frac{\partial f}{\partial x} \right)_y} = - \frac{\left(\frac{\partial f}{\partial y} \right)_x}{\left(\frac{\partial f}{\partial x} \right)_y}$$

Hence: $\left(\frac{\partial V}{\partial T} \right)_P = - \left(\frac{\partial P}{\partial T} \right)_V \left(\frac{\partial V}{\partial P} \right)_T$

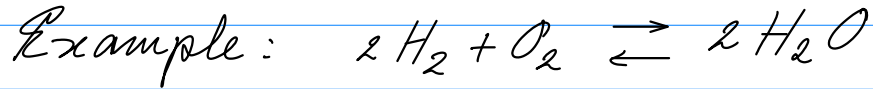
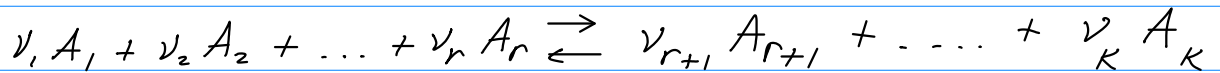
$$\rightarrow C_P = T \left(\frac{\partial S}{\partial T} \right)_P = C_V - T \left[\left(\frac{\partial P}{\partial T} \right)_V \right]^2 \left(\frac{\partial V}{\partial P} \right)_T = C_V + TV \alpha^2 / \kappa$$

where $\kappa = -\frac{1}{V} \left(\frac{\partial V}{\partial P} \right)_T$; $\alpha = \frac{1}{V} \left(\frac{\partial V}{\partial T} \right)_P$; $\rightarrow \alpha = \kappa \left(\frac{\partial P}{\partial T} \right)_V$.

compressibility

Ideal gases: $\frac{C_P}{C_V} = \gamma$

Chemical equilibrium (P 2.19)



$\nu_{r+1} \dots \nu_K$ negative

For a reaction: $\frac{\delta N_1}{\nu_1} = \frac{\delta N_2}{\nu_2} = \dots = \frac{\delta N_K}{\nu_K}$

Fix P and T : Gibbs free energy.

$$G = \sum_{i=1}^K \mu_i N_i$$

$$dG = 0 = \sum_i \mu_i dN_i \propto \sum_i \mu_i \nu_i$$

$$\rightarrow \sum_i \mu_i \nu_i = 0$$

\neq

Phase coexistence

Gas and liquid. $\overset{\nu_g = -\nu_l}{\mu_g = \mu_l} \equiv \mu$

$$N_g + N_l = N = \text{const.}$$

$$\rightarrow \Delta N_g = -\Delta N_l$$

$$\text{and } \Delta G = \Delta N_g \mu + \Delta N_l \mu = 0$$

So the Gibbs free energy is independent of N_g (N_l).

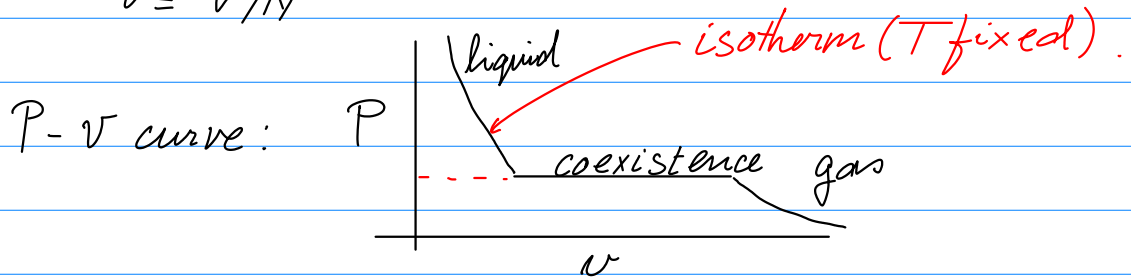
The two phases l and g occupy different volumes

v_l : volume per liquid particle

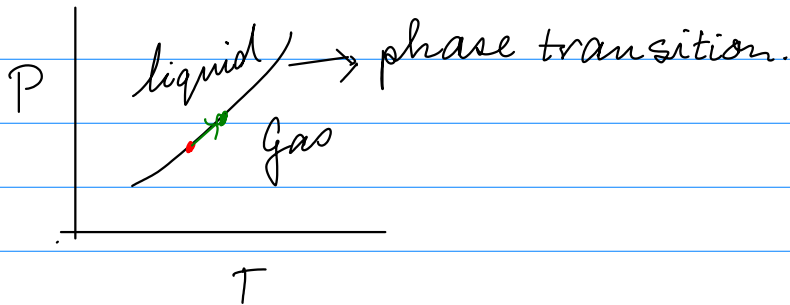
v_g : " " gas "

Total volume $V = N_l v_l + N_g v_g$.

$$v = V/N$$



Clausius - Clapeyron equation (P 2.21).



The phase transition is defined by

$$\mu_{\text{liq}}(P, T) = \mu_{\text{gas}}(P, T)$$

Consider $\mu_{\text{liq}}(P + \Delta P, T + \Delta T) = \mu_{\text{gas}}(P + \Delta P, T + \Delta T)$

obviously $\Delta \mu_{\text{liq}} = \Delta \mu_{\text{gas}}$ *similar.*

$$\mu_{\text{liq}}(P + \Delta P, T + \Delta T) - \mu_{\text{liq}}(P, T)$$

So we have $\left. \frac{\partial \mu_{\text{liq}}}{\partial P} \right|_T \Delta P + \left. \frac{\partial \mu_{\text{liq}}}{\partial T} \right|_P \Delta T = \left. \frac{\partial \mu_{\text{gas}}}{\partial P} \right|_T \Delta P + \left. \frac{\partial \mu_{\text{gas}}}{\partial T} \right|_P \Delta T$

Divide by ΔT : $\left. \frac{\partial \mu_{\text{liq}}}{\partial P} \right|_T \frac{\partial P}{\partial T} + \left. \frac{\partial \mu_{\text{liq}}}{\partial T} \right|_P = \left. \frac{\partial \mu_{\text{liq}}}{\partial P} \right|_T \frac{\partial P}{\partial T} + \left. \frac{\partial \mu_{\text{gas}}}{\partial T} \right|_P$

Now realise that $G = \mu N$ and

$$dG = -S dT + V dP + \mu dN$$

$$\text{So } \left(\frac{\partial \mu_{\text{liq}}}{\partial P} \right)_T = v_{\text{liq}} \quad \text{and} \quad \left(\frac{\partial \mu_{\text{liq}}}{\partial T} \right)_P = -S_{\text{liq}}$$

\downarrow
entropy per particle.

similar for μ_{gas}

$$\Rightarrow (v_{\text{liq}} - v_{\text{gas}}) \frac{dP}{dT} = -S_{\text{gas}} + S_{\text{liq}}$$

$$\text{so } \frac{dP}{dT} = \frac{S_{\text{gas}} - S_{\text{liq}}}{v_{\text{gas}} - v_{\text{liq}}} \geq 0 \quad \text{except eg for water between } 0 \text{ and } 4^\circ\text{C}.$$

$$\Delta Q/T$$

\hookrightarrow Latent heat.

Clausius Clapeyron.