

# Lecture 8b

Monday, October 24, 2005  
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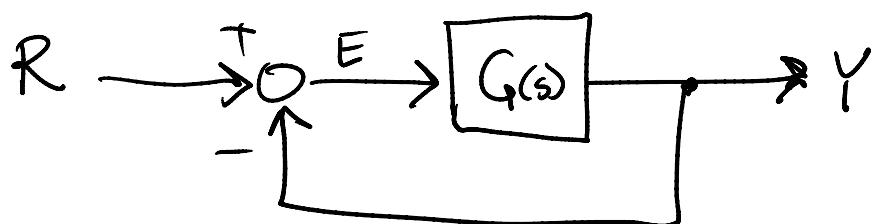
## Lecture 8b: Test Signals

	$r(t)$	$R(s)$
Impulse	$\delta(t)$	1
Step	1	$1/s$
Ramp	$t$	$1/s^2$
Parabola	$t^2$	$2/s^3$
Sine Wave	$\sin \omega t$	$\omega / (s^2 + \omega^2)$

later

NOTE:  $t^n \xleftarrow{\text{L}} \frac{n!}{s^{n+1}}$

We will show that control system's ability to track a test signal has to do with the number of poles at the origin or type. Consider



The general form for  $G(s)$  is

$$G(s) = \frac{\prod_{k=1}^Q (s_k + z_k)}{s^N \prod_{k=1}^M (s_k + p_k)}$$

where

- $z_1, \dots, z_Q$  are the zeros
- $p_1, \dots, p_M$  are the non-zero poles

and there are  $N$  poles at zero.

$N$  = system type

$N+M$  = system order

Now, consider the response to the various signals. For the above configuration

$$E(s) = R(s) - Y(s)$$

$$= R(s) - E(s) G(s)$$

$$\Rightarrow E(s) = \frac{1}{1+G(s)} R(s) .$$

A. Impulse Response  $R(s) = 1$

$$\lim_{s \rightarrow 0} s E(s) = \lim_{s \rightarrow 0} \frac{s}{1+G(s)} = \boxed{0}$$

$\Rightarrow$  Any stable system can track an impulse perfectly.

B. Step Response :  $R(s) = 1/s$

$$\lim_{s \rightarrow 0} sE(s) = \frac{1}{1+G(0)}$$

$\Rightarrow$  If  $N=0$ , then  $G(0)$  is finite,

so

$$e(\infty) = \frac{1}{1+G(0)} = \frac{1}{1+K_p}$$

$\Rightarrow$  If  $N > 0$ , then  $\lim_{s \rightarrow 0} G(s) = \infty$

so

$$e(\infty) = \frac{1}{\infty} = 0.$$

## C. Ramp Response

$$\begin{aligned}\lim_{s \rightarrow 0} s E(s) &= \lim_{s \rightarrow 0} s \cdot \frac{1}{1 + G(s)} \cdot \frac{1}{s^2} \\&= \lim_{s \rightarrow 0} \frac{1}{s + sG(s)} \\&= \lim_{s \rightarrow 0} \frac{1}{sG(s)}\end{aligned}$$

$\Rightarrow$  If  $N=0$  then  $e(\infty) = \infty$

$\Rightarrow$  If  $N=1$  then  $e(\infty) = \frac{1}{K_v}$  where

$$K_v \stackrel{\triangle}{=} \lim_{s \rightarrow 0} sG(s)$$

$\Rightarrow$  If  $N \geq 2$  then  $e(\infty) = 0$

## D. Parabola Response

$$\begin{aligned}\lim_{s \rightarrow 0} sE(s) &= \lim_{s \rightarrow 0} s \frac{1}{1+G(s)} \frac{2}{s^3} \\&= \lim_{s \rightarrow 0} \frac{1}{s^2 + s^2 G(s)} \\&= \lim_{s \rightarrow 0} \frac{1}{s^2 G(s)}\end{aligned}$$

$\Rightarrow$  If  $N=0$  or  $1$  then  $e(\infty) = \infty$

$\Rightarrow$  If  $N=2$  then  $e(\infty) = \frac{1}{K_A}$

where  $K_A = \lim_{s \rightarrow 0} s^2 G(s)$

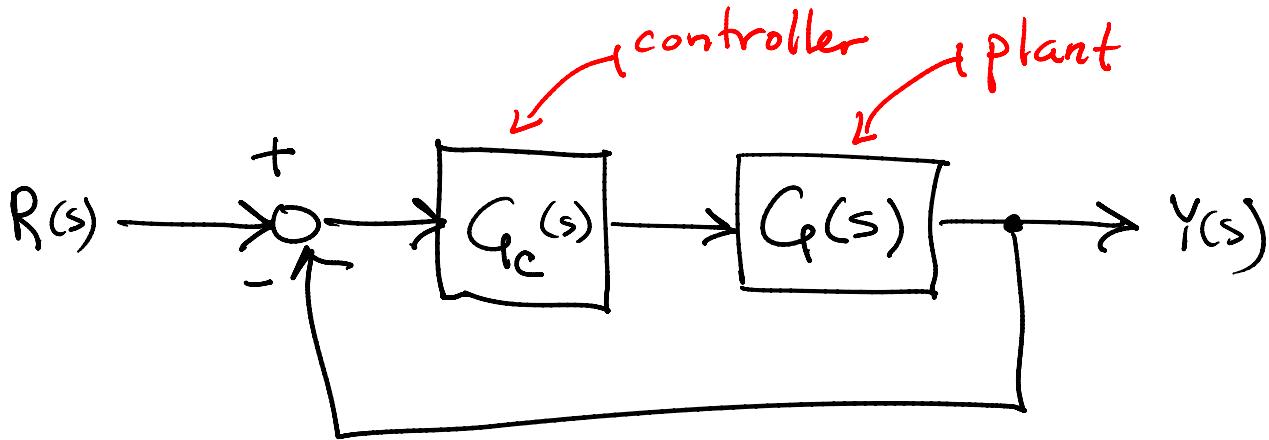
$\Rightarrow$  If  $N \geq 3$  then  $e(\infty) = 0$ .

So the type of the system determines the kind of signals it can track.

N	1	$1/s$	$1/s^2$	$1/s^3$
0	0	$\frac{1}{1+K_p}$	$\infty$	$\infty$
1	0	0	$\frac{1}{K_v}$	$\infty$
2	0	0	0	$\frac{1}{K_A}$
3	0	0	0	0
4	0	0	0	0
:	:	:	:	:

## IV. Control Design for S.S.E.

If you know what kind of signal you need to track and the type of plant you have, you can design a controller to change the type.



Example: Say  $G(s) = \frac{1}{s+1}$  and you want to track a step input with 10% error. Then you want

$$\frac{1}{1+K_p} = 0.1 \Rightarrow K_p = 9.$$

But  $K_p = G_c(s) G(s) = K \cdot \frac{1}{s+1}$

when  $s \rightarrow 0$ , this is  $K_p = K = 9$ . So just put  $G_c = K$ .

Example: Say  $G(s) = \frac{1}{s+1}$  and you want to track a step exactly. Then you want to define  $G_c(s)$  so that  $G_c(s)G(s)$  is type 1 (or greater). For instance,

$$G_c(s) = \frac{K_I}{s}$$

would work. Although you may not get good control over the transient this way. A better controller would be

$$\begin{aligned} G_c(s) &= K_p + \frac{K_I}{s} \\ &= \frac{K_p s + K_I}{s} \end{aligned}$$

which gives you control over damping as well.