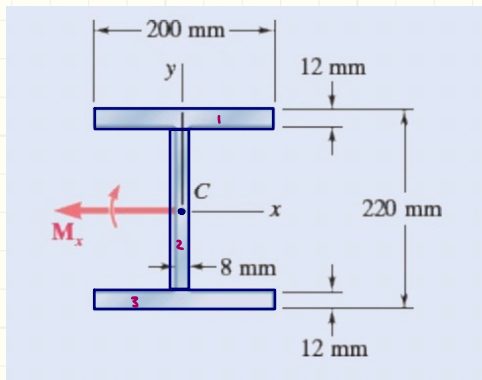


P 11.3



$$f_{\text{(ALLOWABLE)}} = 155 \text{ MPa}$$

$$I_{xx} = I_1 + I_2 + I_3$$

CENTROID:

$$\bar{x} = \bar{y} = \frac{200}{2} = 100 \text{ mm}$$

$$I_1 = \frac{bd^3}{12} + Ah^2 \quad \text{HEIGHT FROM CENTROID}$$

$$= \frac{(200)(12)^3}{12} + (200)(12)(214 - 110)^2 = 25987200 \text{ mm}^4$$

$$I_2 = \frac{bd^3}{12} + Ah^2$$

$$= \frac{(8)(196)^3}{12} + (8)(196)(6)^2 = 5019690.667 \text{ mm}^4$$

$$I_3 = \frac{bd^3}{12} + Ah^2$$

$$= \frac{(200)(12)^3}{12} + (200)(12)(110 - 6)^2 = 25987200 \text{ mm}^4$$

$$I_{xx} = I_1 + I_2 + I_3$$

$$= 56994090.67 \text{ mm}^4 \rightarrow 56.99 \times 10^6 \text{ mm}^4$$

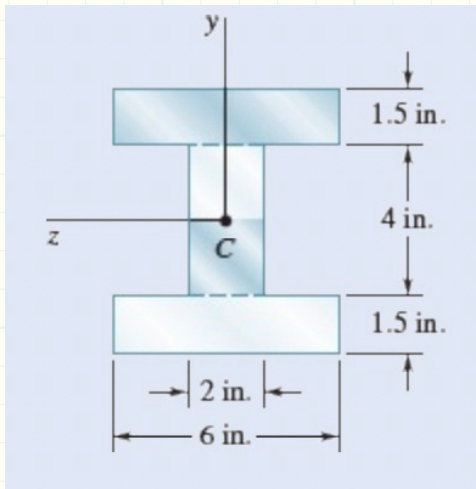
BENDING MOMENT

$$\frac{M}{I} = \frac{f}{y} \quad \begin{array}{l} \rightarrow \text{ALLOWABLE STRESS} \\ \rightarrow \text{CENTROID} \end{array}$$

MOMENT OF INERTIA

$$M = \frac{f \cdot I}{y} \rightarrow \frac{(155)(56.99 \times 10^6)}{110} = \boxed{80.31 \text{ kN} \cdot \text{m}} \rightarrow \text{LARGEST BENDING MOMENT}$$

P11.13



BENT ALONG HORIZONTAL AXIS
BENDING MOMENT IS 50 KIP·IN

BENDING STRESS:

$$\left. \begin{aligned} \sigma_x &= \frac{My}{I} \\ \sigma &= \frac{F}{A} \end{aligned} \right\} F = \frac{M \cdot y \cdot A}{I}$$

$$I_1 = I_3 = \frac{(6)(1.5)^3}{12} + (6)(1.5)(2 + 0.75)^2 = 69.75 \text{ in}^4$$

$$I_2 = \frac{(2)(4)^3}{12} = 10.667 \text{ in}^4$$

$$I = I_1 + I_2 + I_3 = 2(69.75) + 10.667 = 150.1667 \text{ in}^4$$

a) TOTAL FORCE ON TOP OF FLANGE:

$$A = 6 \cdot 1.5 = 9 \text{ in}^2$$

$$y = 2 + 0.75 = 2.75 \text{ in}$$

$$F = \frac{(50 \times 10^3)(2.75)(9)}{150.1667} = 8240.84 \text{ lb}$$

$$F = 8.240 \text{ Kips}$$

b) TOTAL FORCE ON SHADED PORTION OF WEB:

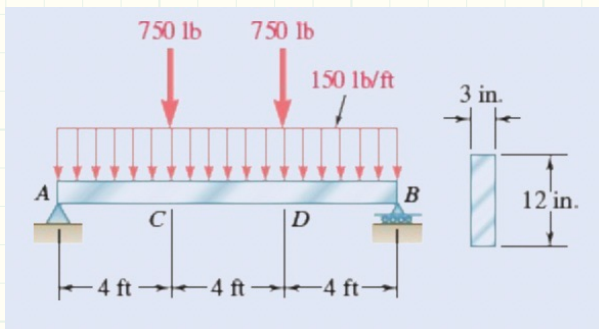
$$A = 2 \times 2 = 4 \text{ in}^2$$

$$y = 1 \text{ in}$$

$$F = \frac{(50 \times 10^3)(1)(4)}{150.1667} = 1331.85 \text{ lb}$$

$$F = 1.331 \text{ Kips}$$

P12.13



$\sum F_y = 0$
 $A + C - (2)(750) - (12)(150) = 0$
 $A + C = 3300 \rightarrow A = C = 1650 \text{ lb}$

A = C BY SYMMETRY

$\sum M_C = 0$

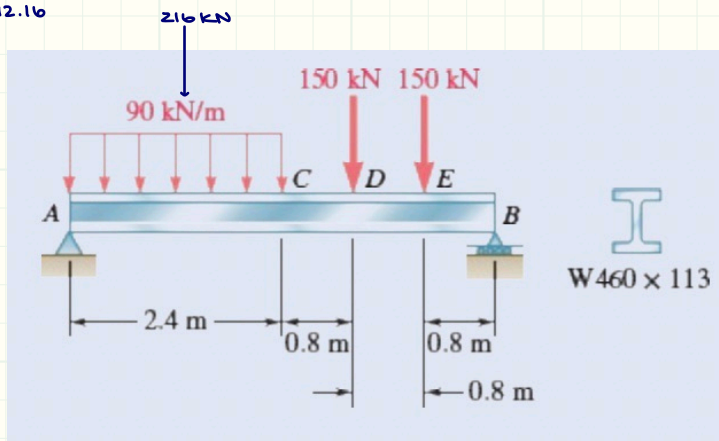
$-1650(4) + 150(4)(2) + M = 0$
 $M = 5400 \text{ lb}\cdot\text{ft}$
 $\hookrightarrow 64800 \text{ lb}\cdot\text{in}$

$S = \frac{1}{6}bh^2 \rightarrow \frac{1}{6}(3)(12)^2 = 72 \text{ in}^3$

NORMAL STRESS:

$\sigma = \frac{M}{S} = \frac{64800 \text{ lb}\cdot\text{in}}{72 \text{ in}^3} = 900 \text{ lb/in}^2 \rightarrow \boxed{900 \text{ psi}}$

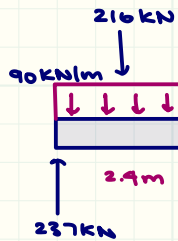
P 12.16



$$+\circlearrowleft \sum M_B = 0$$

$$-4.8 \cdot A + (3.6)(216) + (1.6)(150) + (0.8)(150) = 0$$

$$A = 237 \text{ kN}$$



$$+\circlearrowleft \sum M_C = 0$$

$$M - (2.4)(237) + (1.2)(216) = 0$$

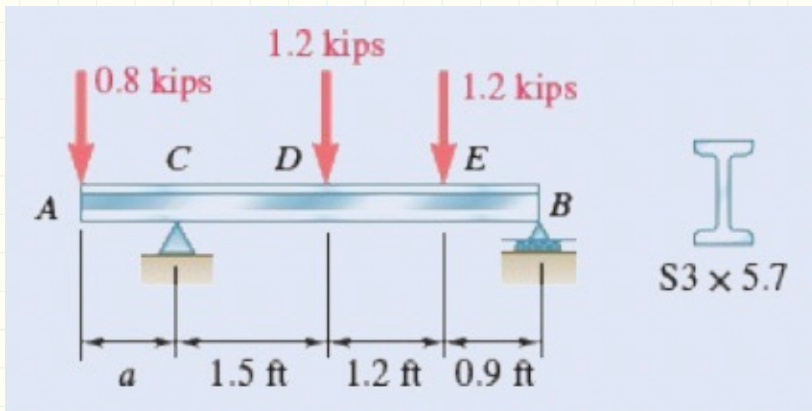
$$M = 309.6 \text{ kN} \cdot \text{m}$$

$$S = 2390 \times 10^6 \text{ mm}^3 \text{ (FROM APPENDIX)}$$

NORMAL STRESS:

$$\sigma = \frac{M}{S} = \frac{(309.6 \text{ kN} \cdot \text{m})}{(2390 \times 10^{-6} \text{ m}^3)} = 129.5 \times 10^6 \text{ Pa}$$

P12.27



$$\sum F_y = 0$$

$$C + D - 0.8 - 1.2 - 1.2 = 0$$

$$C + D = 3.2$$

$$\sum M_C = \sum M_B = 0$$

$$-0.8a + 1.2(1.5) + 1.2(2.7) - B(3.6) = 0$$

$$B = 1.4 - 0.222a$$

$$C = 3.2 - 1.4 - 0.222a \rightarrow 1.8 + 0.222a$$

a)

BENDING MOMENT AT C:

$$\begin{aligned} -M_C - 0.8a &= 0 \\ M_C &= -0.8a \end{aligned}$$

BENDING MOMENT AT D:

$$\begin{aligned} -0.8(a + 1.5) + C(1.5) - M_D &= 0 \\ M_D &= -0.8a - 1.2 + (1.8 + 0.222a)(1.5) \\ M_D &= 1.5 - 0.467a \end{aligned}$$

BENDING MOMENT AT E:

$$\begin{aligned} -B(0.9) + M_E &= 0 \\ M_E &= 0.9(1.4 - 0.222a) \\ M_E &= 1.26 - 0.2a \end{aligned}$$

$$\text{ASSUME } M_E = -M_C: |M_C| = M_E \rightarrow |M_C| = M_D \rightarrow 1.5 - 0.467a = 0.8a$$

$$0.8a = 1.26 - 0.2a$$

$$a = 1.20 \text{ ft.}$$

$$a = 1.20 \text{ ft.}$$

$$b) M_C = -0.8(1.26) = -1.008 \text{ kip} \cdot \text{ft}$$

$$M_D = 1.5 - 0.467(1.26) = 0.91158 \text{ kip} \cdot \text{ft}$$

$$M_E = 1.26 - 0.2(1.26) = 1.008 \text{ kip} \cdot \text{ft} \rightarrow \text{MAX VALUE}$$

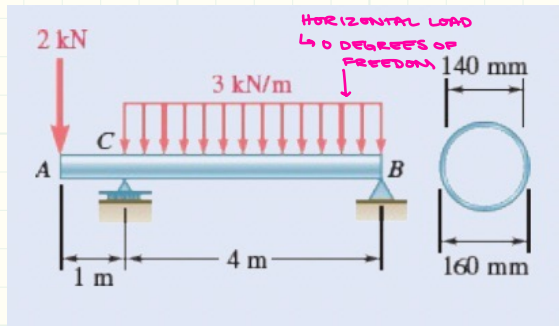
$$\hookrightarrow 12.096 \text{ kip} \cdot \text{in}$$

$$S = 1.67 \text{ in}^3 \text{ (FROM APPENDIX)}$$

NORMAL STRESS:

$$\sigma = \frac{M}{S} = \frac{(12.096)}{1.67} = 7.243 \text{ ksi}$$

P12.53



$$+\circlearrowleft \sum M_C = 0$$

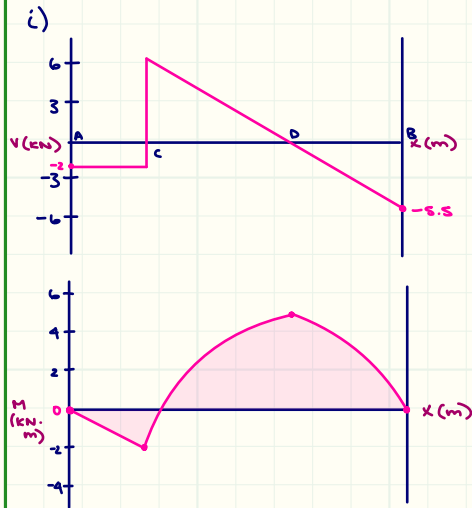
$$2(1) + B(4) - 12(2) = 0$$

$$B = 5.5 \text{ kN}$$

$$\sum F_y = 0$$

$$-2 + C - 12 + 5.5 = 0$$

$$C = 8.5 \text{ kN}$$



SHEAR FORCE:

$$A \text{ to } C \rightarrow V = -2 \text{ kN}$$

$$\text{RIGHT NEXT TO POINT C} \rightarrow C' \rightarrow V = -2 + 8.5 = 6.5 \text{ kN}$$

$$C' \text{ to } B \rightarrow 6.5 - 3(4) = -5.5 \text{ kN}$$

AREA OF SHEAR:

$$A \text{ to } C = \int v dx = (-2)(1) = -2$$

$$C \text{ to } D = \int v dx = \frac{1}{2} (2.1667)(6.5) = 7.0417$$

$$D \text{ to } B = \int v dx = \frac{1}{2} (-5.5)(3.833) = -5.0417$$

SIMILAR TRIANGLES:

$$\frac{d}{6.5} = \frac{4-d}{5.5} \rightarrow d = 2.1667 \text{ m}$$

$$4-d = 3.833 \text{ m}$$

BENDING MOMENT:

$$M_A = 0$$

$$M_C = M_A + -2 = -2 \text{ kN} \cdot \text{m}$$

$$M_D = M_C + 7.0417 = 5.0417 \text{ kN} \cdot \text{m}$$

$$M_B = -2 + 7.0417 - 5.0417 = 0$$

$$ii) \sigma = \frac{|M|}{S} \rightarrow \frac{5.0417 \times 10^3}{166.406 \times 10^{-6}} = 30.3 \times 10^3 \text{ Pa} \rightarrow \sigma_{\max} = 30.3 \text{ MPa}$$

$$S = \frac{I}{C} \rightarrow \frac{13.3125 \times 10^6}{80} = 166.406 \times 10^{-6} \text{ m}^3$$

$$I = \frac{\pi}{4} (d_o^4 - d_i^4)$$

$$I = \frac{\pi}{4} (80^4 - 70^4)$$

$$I = 13.3125 \times 10^6 \text{ mm}^4$$