

# Brief Review of Camphor Boats

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January 15, 2015

## 1 Radial Extent of Camphor Spread

For a fixed c-boat, the flux of camphor from the c-boat onto the air-water interface and sublimation of camphor molecules from the air-water interface result in a steady state radial distribution of camphor around the c-boat. We measured the radial extent (i.e., distance out to which camphor molecules spread before sublimation) of camphor spread for different diameters of the c-boats. Figures ??(a)-(d) show the radii of influence as a function of time for 1 mm, 2 mm, 3 mm and 4 mm diameter c-boats respectively. When there is *no* sublimation of the surface active molecules from the air-water interface,  $r(t) \propto t^{\frac{3}{4}}$ <sup>1</sup>. In case of camphor one would expect a slower trend as the sublimation depletes camphor from the air-water interface. However, we fitted the measured  $r(t)$  to  $(1 - e^{-t/\tau})$  as this function yielded the best fit results. We believe, this is *not* the correct functional form of the observed behavior as this yields  $r(t) \propto t$  at small times which is faster than the expected behavior ( $r(t) \propto t^{\frac{3}{4}}$ ) before sublimation dominates the flux of camphor onto the air-water interface.

### 1.1 Back-of-the-Envelope Thoughts

When a drop of surfactant is introduced on air-water interface, the surfactant molecules are drawn onto the interface to minimize the interfacial energy. The surfactant front spreads on air-water interface radially outwards with time as

$$r(t) \approx \left( \frac{\Delta\gamma^2}{\mu\rho} \right)^{\frac{1}{4}} t^{\frac{3}{4}} \quad (1)$$

Substituting  $\Delta\gamma = 20 \left[ \frac{\text{mN}}{\text{m}} \right]$ ,  $\mu = 10^{-3} \left[ \frac{\text{N.s}}{\text{m}^2} \right]$  and  $\rho = 10^3 \left[ \frac{\text{kg}}{\text{m}^3} \right]$ , we get

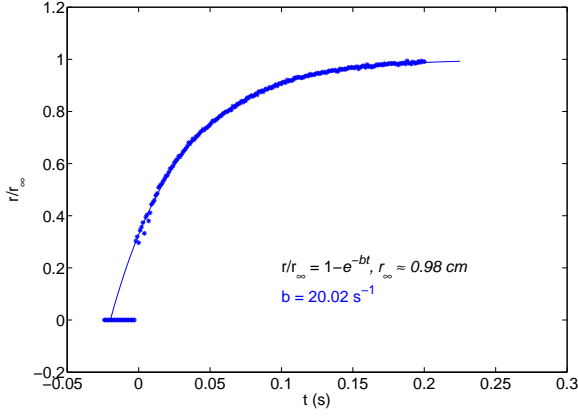
$$r(t) \approx \alpha t^{\frac{3}{4}}$$

where,  $\alpha = 0.14 \left[ \text{m.s}^{-0.75} \right]$ . The rate at which area increases is,

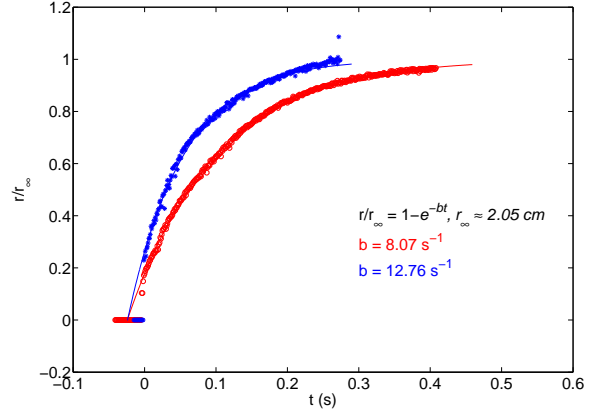
$$\frac{d}{dt}A(t) = \frac{3\pi}{2}\alpha^2 t^{\frac{1}{2}}$$

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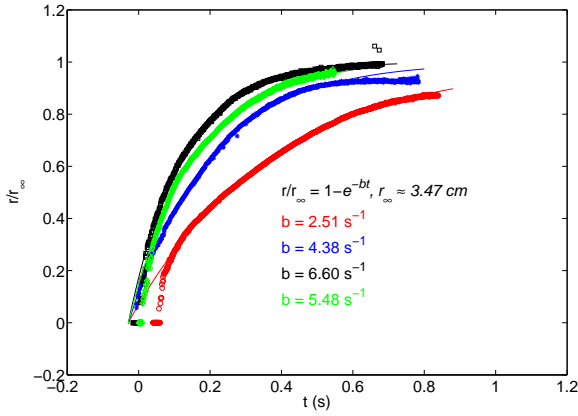
<sup>1</sup>M M Bandi, T Tallinen and L Mahadevan, Shock-driven jamming and periodic fracture of particulate rafts, *Europhys. Lett.*, 96, 36008, **2011**.



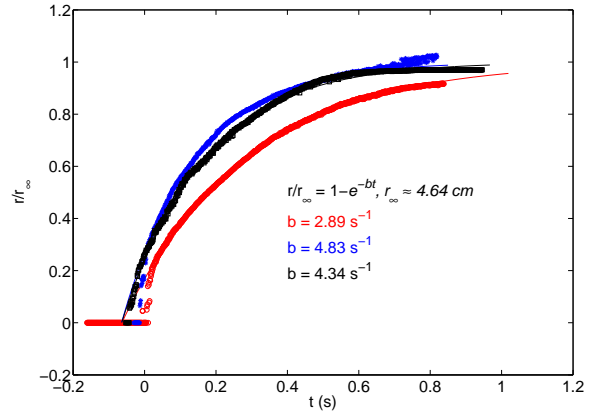
(a) Radius of Influence for 1 mm



(b) Radius of Influence for 2 mm



(c) Radius of Influence for 3 mm



(d) Radius of Influence for 4 mm

Figure 1: Radii of Influence for different diameters of c-boat

Effectively, one can think of sublimation as a process decreasing the surface area at a rate,  $kA_{\text{eff}}(t)$  where  $k$  is the sublimation rate and  $A_{\text{eff}}(t)$  area. Now one can write the rate equation for the effective area as,

$$\begin{aligned} \frac{d}{dt} A_{\text{eff}}(t) &= \frac{d}{dt} A(t) - kA_{\text{eff}}(t) \\ \frac{d}{dt} [e^{kt} A_{\text{eff}}(t)] &= \frac{3\pi}{2} \alpha^2 t^{\frac{1}{2}} e^{kt} \end{aligned}$$

Integrating we get,

$$A_{\text{eff}}(t) = e^{-kt} \left[ \pi \alpha^2 \int t^{\frac{1}{2}} e^{kt} dt + \text{const.} \right]$$

Integrating we get,

$$A_{\text{eff}}(t) = \frac{\pi\alpha^2}{k} \left[ t^{\frac{1}{2}} - \frac{1}{2kt^{\frac{1}{2}}} \left( 1 + \frac{1}{2kt} + \frac{1 \cdot 3}{(2kt)^2} + \frac{1 \cdot 3 \cdot 5}{(2kt)^3} + \dots \right) \right] + \text{const} \cdot e^{-kt} \quad (2)$$