

# **AE731**

## **Theory of Elasticity**

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Wichita State University, Department of Aerospace Engineering November 20, 2019

# upcoming schedule

- Nov 20 - Polar Coordinates in Airy Stress, Homework 7 Due
- Nov 25 - Polar Coordinates in Airy Stress
- Nov 27 - No Class (Thanksgiving Break)
- Dec 2 - Complex Methods
- Dec 4 - Final Review, Homework 8 Due
- Dec 11 - 3:00 - 4:50 Final Exam

# outline

- polar coordinates
- examples

# polar coordinates

# strain-displacement

- Reduced strain-displacement:

$$\epsilon_r = \frac{\partial u_r}{\partial r}, \epsilon_\theta = \frac{1}{r} \left( u_r + \frac{\partial u_\theta}{\partial \theta} \right), \epsilon_z = \frac{\partial u_z}{\partial z}$$

$$\epsilon_{r\theta} = \frac{1}{2} \left( \frac{1}{r} \frac{\partial u_r}{\partial \theta} + \frac{\partial u_\theta}{\partial r} - \frac{u_\theta}{r} \right)$$

$$\epsilon_{\theta z} = \frac{1}{2} \left( \frac{\partial u_\theta}{\partial z} + \frac{1}{r} \frac{\partial u_z}{\partial \theta} \right)$$

$$\epsilon_{zr} = \frac{1}{2} \left( \frac{\partial u_r}{\partial z} + \frac{\partial u_z}{\partial r} \right)$$

# strain-displacement

- Which becomes

$$\epsilon_r = \frac{\partial u_r}{\partial r}$$

$$\epsilon_\theta = \frac{1}{r} \left( u_r + \frac{\partial u_\theta}{\partial \theta} \right)$$

$$\epsilon_{r\theta} = \frac{1}{2} \left( \frac{1}{r} \frac{\partial u_r}{\partial \theta} + \frac{\partial u_\theta}{\partial r} - \frac{u_\theta}{r} \right)$$

# integration

- When we change variables in integration, we also need to account for the proper change in  $dV$
- $dV = dx dy dz \neq dr d\theta dz$
- We can find the correct  $dV$  by calculating the Jacobian

# jacobian

$$dV = dx dy dz = \left| \frac{\partial(x, y, z)}{\partial(r, \theta, z)} \right| dr d\theta dz$$

$$dV = \begin{vmatrix} \frac{\partial x}{\partial r} & \frac{\partial x}{\partial \theta} & \frac{\partial x}{\partial z} \\ \frac{\partial y}{\partial r} & \frac{\partial y}{\partial \theta} & \frac{\partial y}{\partial z} \\ \frac{\partial z}{\partial r} & \frac{\partial z}{\partial \theta} & \frac{\partial z}{\partial z} \end{vmatrix} dr d\theta dz = r dr d\theta dz$$



# hooke's law

- The tensor equation for Hooke's Law is valid in polar/cylindrical/spherical coordinates too
- We only need special equations when differentiating or integrating

$$\sigma_{ij} = \lambda \epsilon_{kk} \delta_{ij} + 2\mu \epsilon_{ij} - (3\lambda + 2\mu) \alpha \Delta T \delta_{ij}$$

$$\epsilon_{ij} = \frac{1 + \nu}{E} \sigma_{ij} - \frac{\nu}{E} \sigma_{kk} \delta_{ij} + \alpha \Delta T \delta_{ij}$$

# equilibrium

- We have already found the equilibrium equations in polar coordinates, they are

$$\frac{\partial \sigma_r}{\partial r} + \frac{1}{r} \frac{\partial \tau_{r\theta}}{\partial \theta} + \frac{1}{r} (\sigma_r - \sigma_\theta) + F_r = 0$$

$$\frac{\partial \tau_{r\theta}}{\partial r} + \frac{1}{r} \frac{\partial \sigma_\theta}{\partial \theta} + \frac{2}{r} \tau_{r\theta} + F_\theta = 0$$

# equilibrium

- The equilibrium equations can be written in terms of displacement (Navier equations)
- These are only useful when using a displacement formulation, but we are using stress functions
- Instead we need the Beltrami-Mitchell compatibility equations

# compatibility

- Substituting stress-strain relations into the compatibility equations gives

$$\nabla^2(\sigma_r + \sigma_\theta) = -\frac{1}{1-\nu} \left( \frac{\partial F_r}{\partial r} + \frac{F_r}{r} + \frac{1}{r} \frac{\partial F_\theta}{\partial \theta} \right) \quad (\text{Plane Strain})$$

$$\nabla^2(\sigma_r + \sigma_\theta) = -(1+\nu) \left( \frac{\partial F_r}{\partial r} + \frac{F_r}{r} + \frac{1}{r} \frac{\partial F_\theta}{\partial \theta} \right) \quad (\text{Plane Stress})$$

# airy stress functions

- When the body forces are zero, we find

$$\sigma_r = \frac{1}{r} \frac{\partial \phi}{\partial r} + \frac{1}{r^2} \frac{\partial^2 \phi}{\partial \theta^2}$$

$$\sigma_\theta = \frac{\partial^2 \phi}{\partial r^2}$$

$$\tau_{r\theta} = -\frac{\partial}{\partial r} \left( \frac{1}{r} \frac{\partial \phi}{\partial \theta} \right)$$

# airy stress functions

- When body forces are zero, we find the following biharmonic equation for the Beltrami-Mitchell equations

$$\nabla^4 \phi = 0$$

- Where the Laplacian is

$$\nabla^2 = \frac{\partial^2}{\partial r^2} + \frac{1}{r} \frac{\partial}{\partial r} + \frac{1}{r^2} \frac{\partial^2}{\partial \theta^2}$$

# polar coordinates

- Recall that an Airy Stress function must satisfy the Beltrami-Mitchell compatibility equations

$$\nabla^4 \phi = \left( \frac{\partial^2}{\partial r^2} + \frac{1}{r} \frac{\partial}{\partial r} + \frac{1}{r^2} \frac{\partial^2}{\partial \theta^2} \right)^2 \phi = 0$$

- One method which gives several useful solutions assumes that the Airy Stress function has the form  $\phi(r, \theta) = f(r)e^{b\theta}$

# polar coordinates

- Substituting this into the compatibility equations (and canceling the common  $e^{b\theta}$  term gives

$$f'''' + \frac{2}{r}f''' - \frac{1-2b^2}{r^2}f'' + \frac{1-2b^2}{r^3}f' + \frac{b^2(4+b^2)}{r^4}f = 0$$



# polar coordinates

- To solve this, we perform a change of variables, letting  $r = e^{\xi}$ , which gives

$$f'''' - 4f''' + (4 + 2b^2)f'' - 4b^2f' + b^2(4 + b^2)f = 0$$

- We now consider  $f$  to have the form  $f = e^{a\xi}$  which generates the characteristic equation

$$(a^2 + b^2)(a^2 - 4a + 4 + b^2) = 0$$

# polar coordinates

- This has solutions

$$a = \pm ib, \pm 2ib$$

OR

$$b = \pm ia, \pm i(a - 2)$$

# polar coordinates

- If we consider only solutions which are periodic in  $\theta$ , we find

$$\begin{aligned}\phi = & a_0 + a_1 \log r + a_2 r^2 + a_3 r^2 \log r \\ & + (a_4 + a_5 \log r + a_6 r^2 + a_7 r^2 \log r) \theta \\ & + \left( a_{11} r + a_{12} r \log r + \frac{a_{13}}{r} + a_{14} r^3 + a_{15} r \theta + a_{16} r \theta \log r \right) \cos \theta \\ & + \left( b_{11} r + b_{12} r \log r + \frac{b_{13}}{r} + b_{14} r^3 + b_{15} r \theta + b_{16} r \theta \log r \right) \sin \theta \\ & + \sum_{n=2}^{\infty} (a_{n1} r^n + a_{n2} r^{2+n} + a_{n3} r^{-n} + a_{n4} r^{2-n}) \cos n \theta \\ & + \sum_{n=2}^{\infty} (b_{n1} r^n + b_{n2} r^{2+n} + a_{n3} r^{-n} + b_{n4} r^{2-n}) \sin n \theta\end{aligned}$$

# polar coordinates

- For axisymmetric problems, all field quantities are independent of  $\theta$
- This reduces the general solution to

$$\phi = a_0 + a_1 \log r + a_2 r^2 + a_3 r^2 \log r$$

# polar coordinates

$\phi$	$\sigma_{rr}$	$\sigma_{r\theta}$	$\sigma_{\theta\theta}$
$r^2$	2	0	2
$\log r$	$1/r^2$	0	$-1/r^2$
$\theta$	0	$1/r^2$	0
$r^2 \log r$	$2 \log r + 1$	0	$2 \log r + 3$
$r^2 \theta$	$2\theta$	-1	$2\theta$
$r^3 \cos \theta$	$2r \cos \theta$	$2r \sin \theta$	$6r \cos \theta$
$r^3 \sin \theta$	$2r \sin \theta$	$-2r \cos \theta$	$6r \sin \theta$
$r\theta \sin \theta$	$2 \cos \theta / r$	0	0
$r\theta \cos \theta$	$-2 \sin \theta / r$	0	0
$r \log r \cos \theta$	$\cos \theta / r$	$\sin \theta / r$	$\cos \theta / r$
$r \log r \sin \theta$	$\sin \theta / r$	$-\cos \theta / r$	$\sin \theta / r$
$\cos \theta / r$	$-2 \cos \theta / r^3$	$-2 \sin \theta / r^3$	$2 \cos \theta / r^3$
$\sin \theta / r$	$-2 \sin \theta / r^3$	$2 \cos \theta / r^3$	$2 \sin \theta / r^3$



# polar coordinates

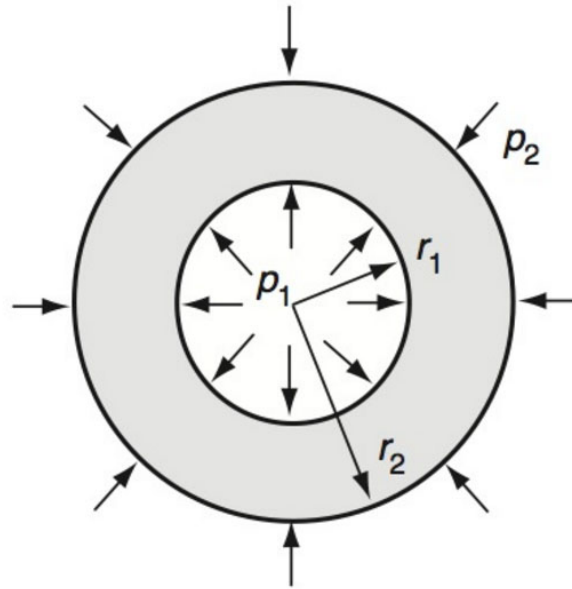
$r^4 \cos 2\theta$	0	$6r^2 \sin 2\theta$	$12r^2 \cos 2\theta$
$r^4 \sin 2\theta$	0	$-6r^2 \cos 2\theta$	$12r^2 \sin 2\theta$
$r^2 \cos 2\theta$	$-2 \cos 2\theta$	$2 \sin 2\theta$	$2 \cos 2\theta$
$r^2 \sin 2\theta$	$-2 \sin 2\theta$	$-2 \cos 2\theta$	$2 \sin 2\theta$
$\cos 2\theta$	$-4 \cos 2\theta / r^2$	$-2 \sin 2\theta / r^2$	0
$\sin 2\theta$	$-4 \sin 2\theta / r^2$	$2 \cos 2\theta / r^2$	0
$\cos 2\theta / r^2$	$-6 \cos 2\theta / r^4$	$-6 \sin 2\theta / r^4$	$6 \cos 2\theta / r^4$
$\sin 2\theta / r^2$	$-6 \sin 2\theta / r^4$	$6 \cos 2\theta / r^4$	$6 \sin 2\theta / r^4$
$r^n \cos n\theta$	$-n(n-1)r^{n-2} \cos n\theta$	$n(n-1)r^{n-2} \sin n\theta$	$n(n-1)r^{n-2} \cos n\theta$
$r^n \sin n\theta$	$-n(n-1)r^{n-2} \sin n\theta$	$-n(n-1)r^{n-2} \cos n\theta$	$n(n-1)r^{n-2} \sin n\theta$
$r^{n+2} \cos n\theta$	$-(n+1)(n-2)r^n \cos n\theta$	$(n+1)nr^n \sin n\theta$	$(n+2)(n+1)r^n \cos n\theta$
$r^{n+2} \sin n\theta$	$-(n+1)(n-2)r^n \sin n\theta$	$-(n+1)nr^n \cos n\theta$	$(n+2)(n+1)r^n \sin n\theta$
$\cos n\theta / r^n$	$-(n+1)n \cos n\theta / r^{n+2}$	$-(n+1)n \sin n\theta / r^{n+2}$	$(n+1)n \cos n\theta / r^{n+2}$
$\sin n\theta / r^n$	$-(n+1)n \sin n\theta / r^{n+2}$	$(n+1)n \cos n\theta / r^{n+2}$	$(n+1)n \sin n\theta / r^{n+2}$
$\cos n\theta / r^{n-2}$	$-(n+2)(n-1) \cos n\theta / r^n$	$-n(n-1) \sin n\theta / r^n$	$(n-1)(n-2) \cos n\theta / r^n$
$\sin n\theta / r^{n-2}$	$-(n+2)(n-1) \sin n\theta / r^n$	$n(n-1) \cos n\theta / r^n$	$(n-1)(n-2) \sin n\theta / r^n$



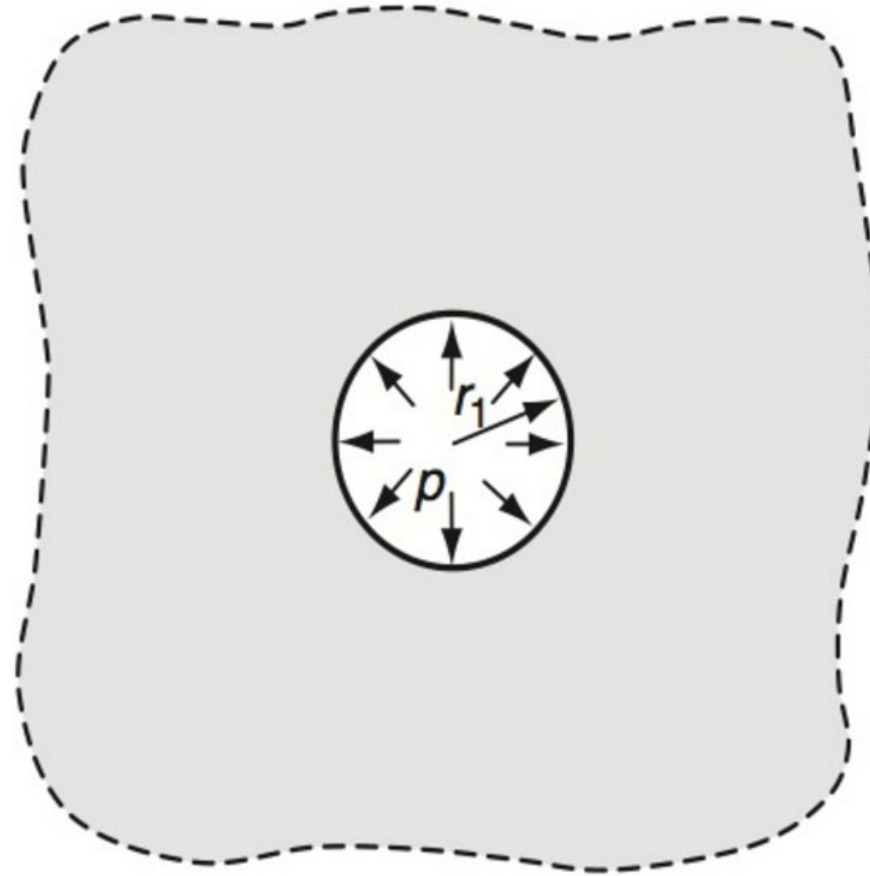


# examples

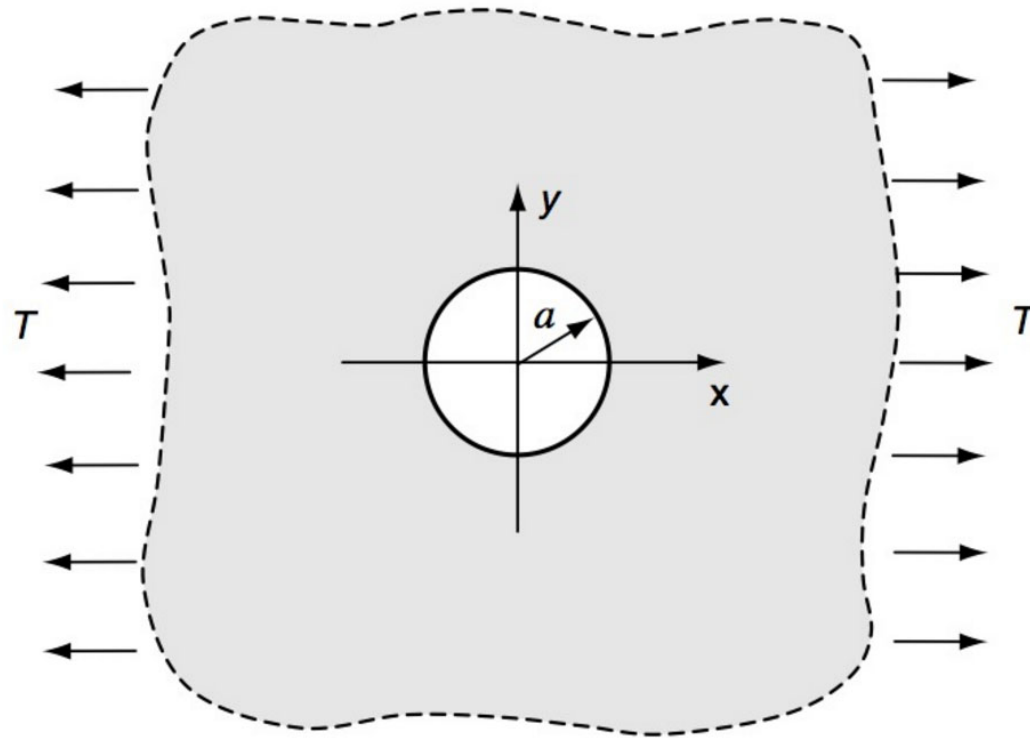
# tube under uniform pressure



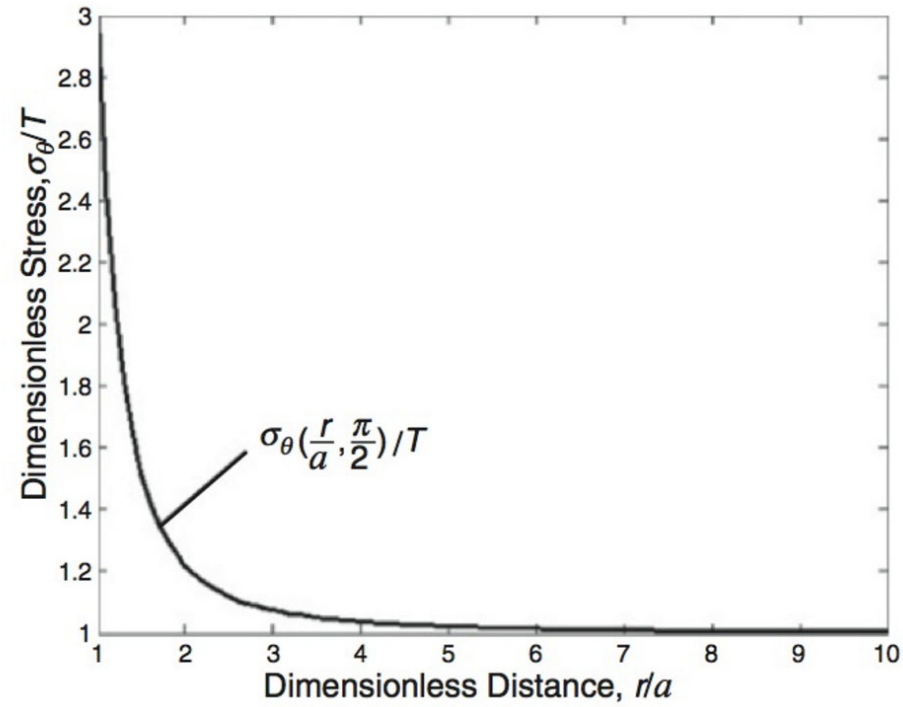
# pressurized hole



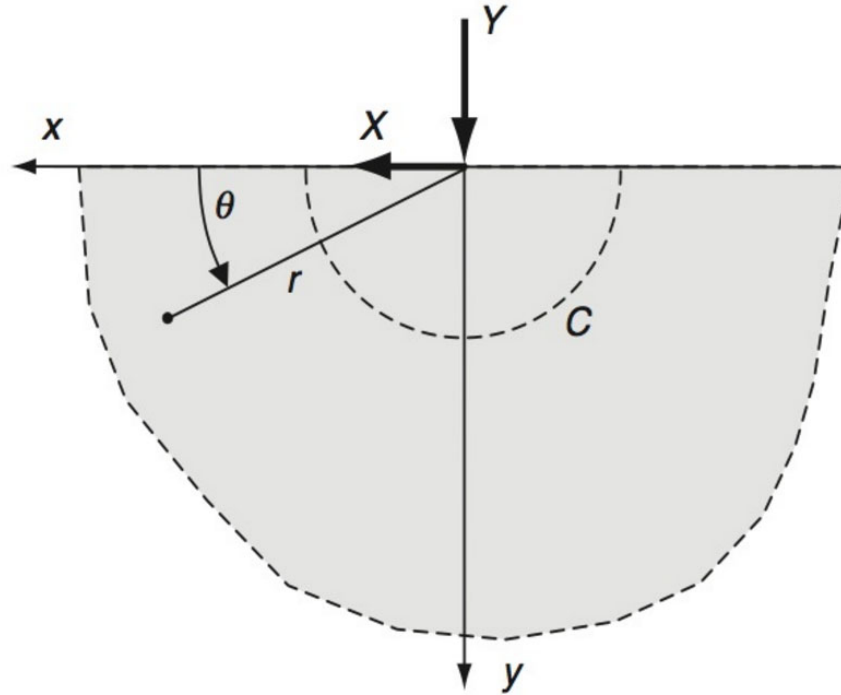
# stress-free hole in tension



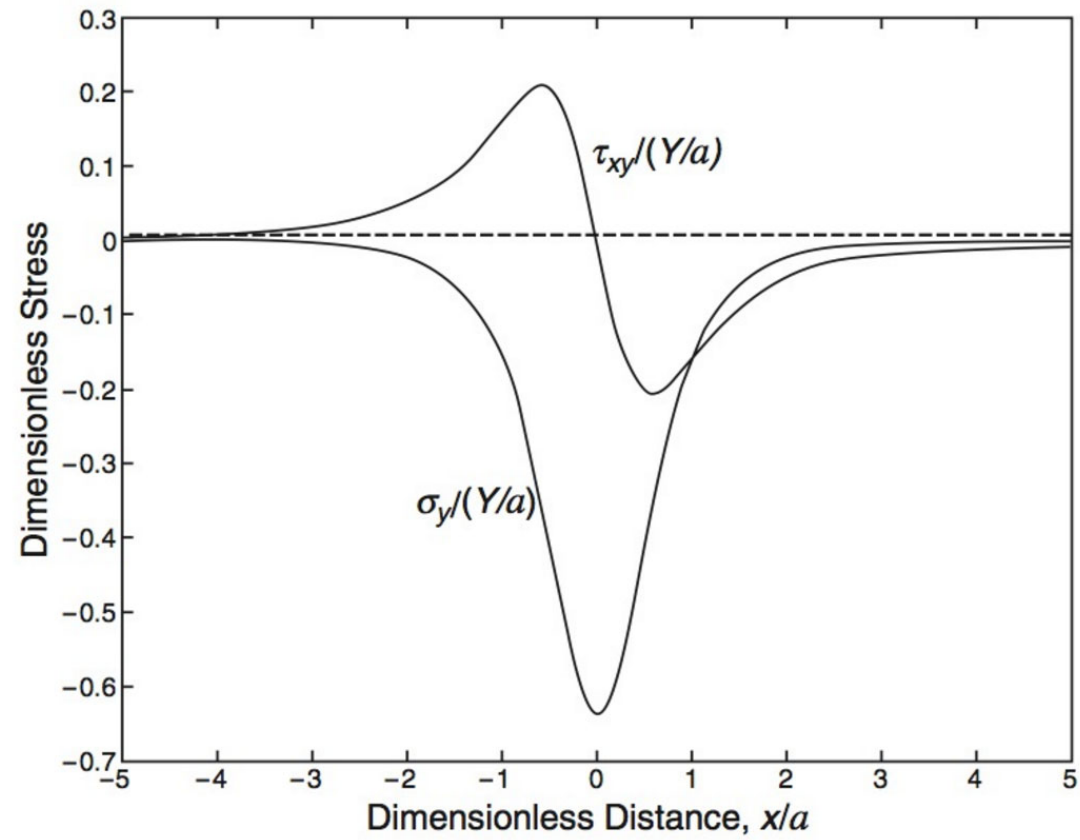
# stress-free hole in tension



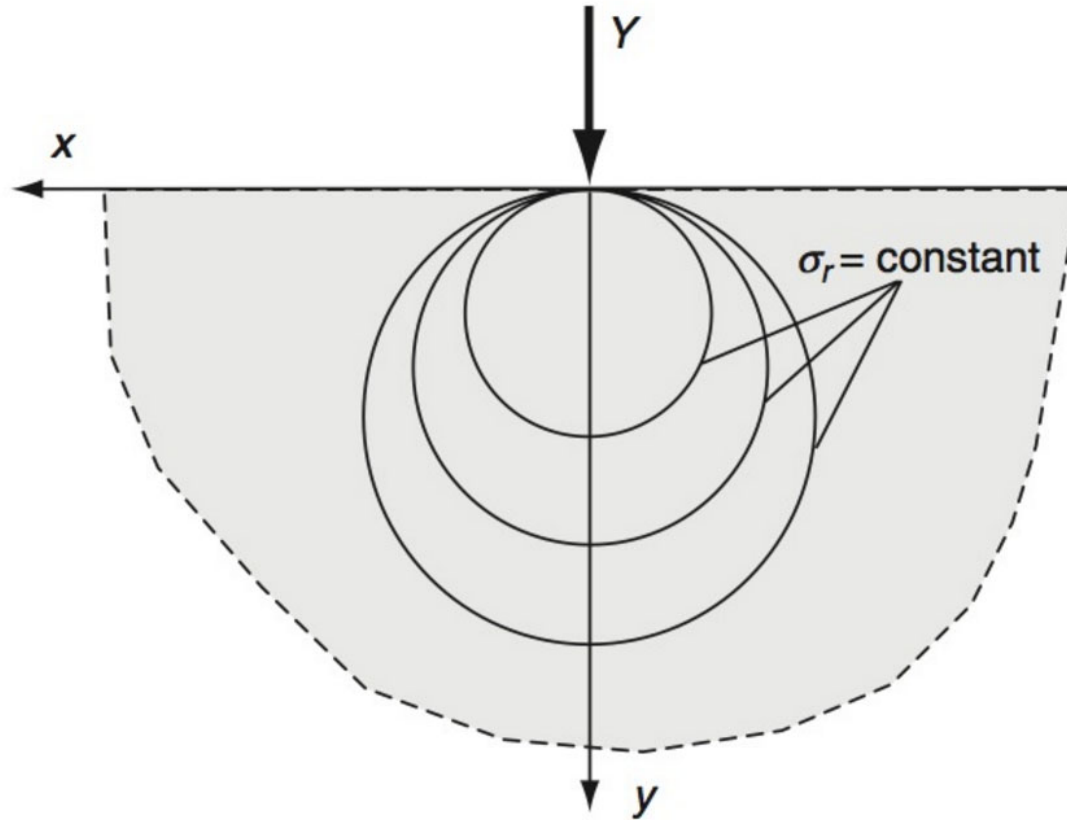
# concentrated force



# concentrated force

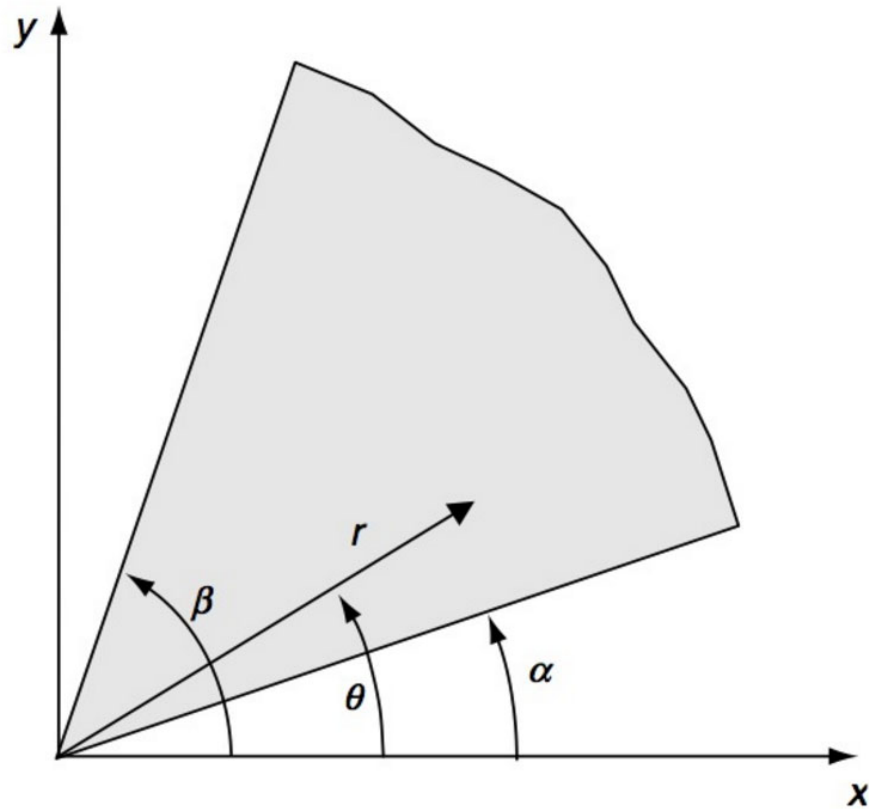


# concentrated force

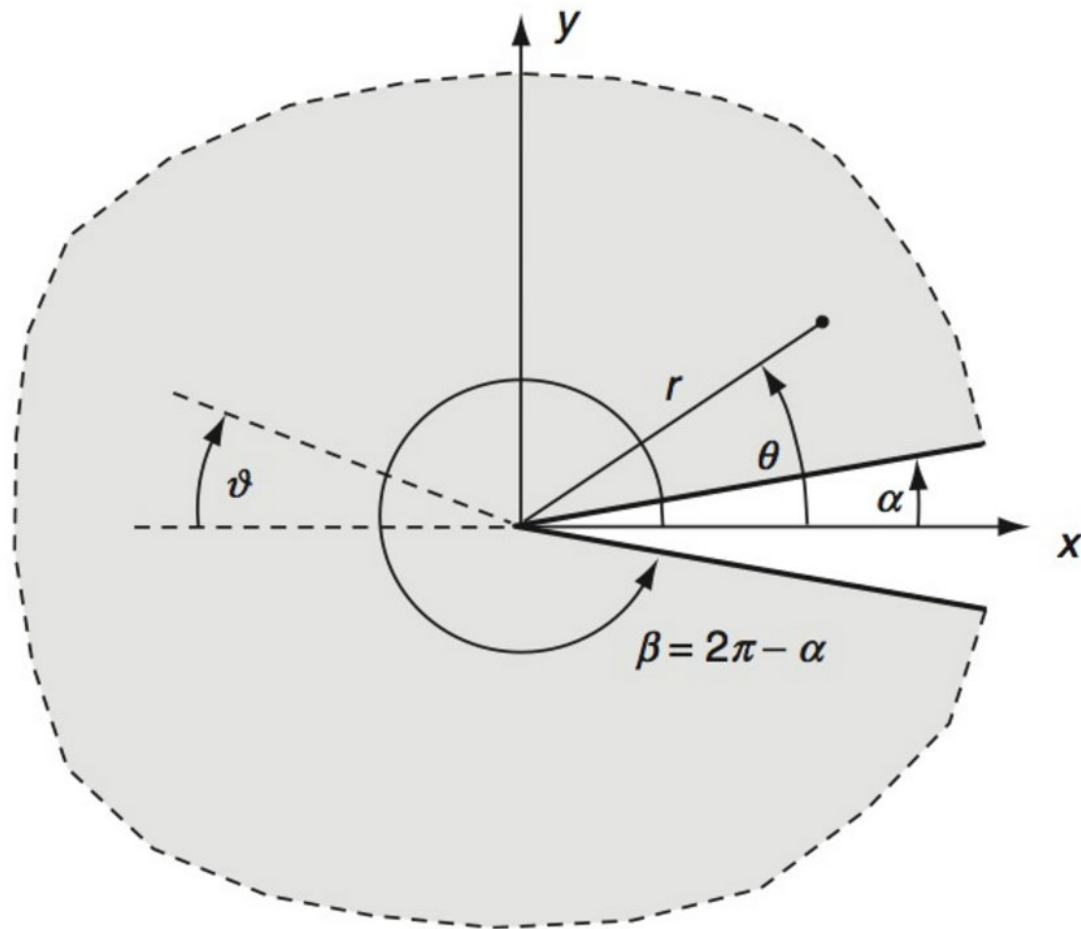




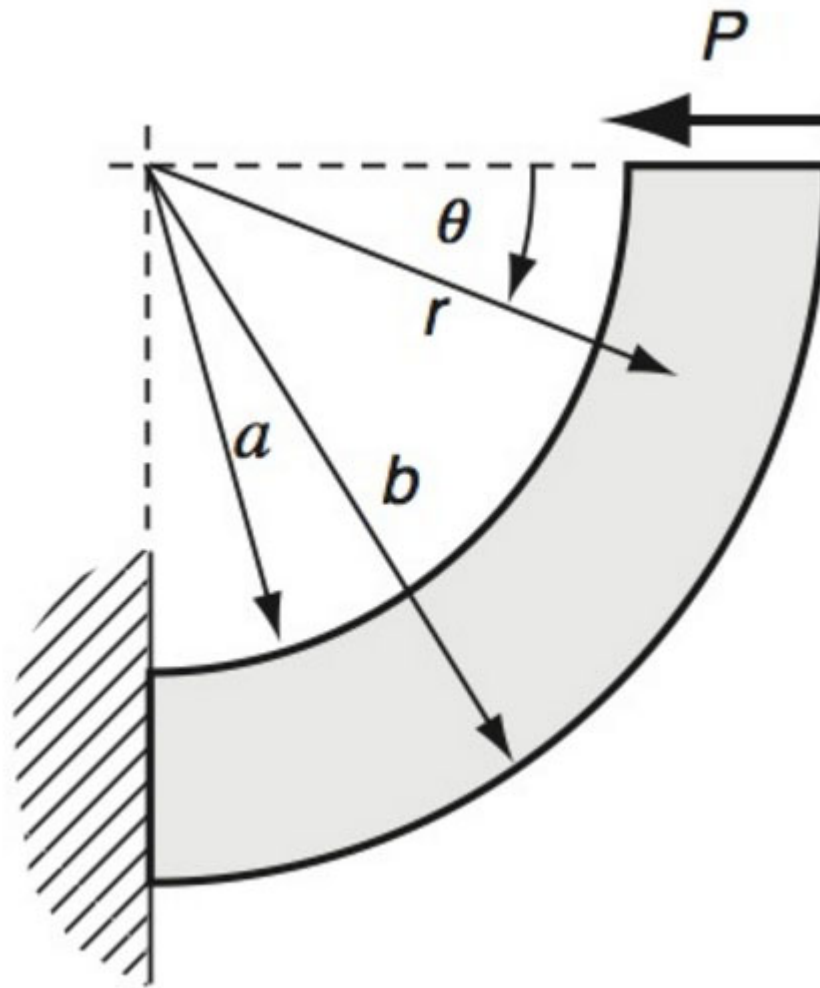
# wedge



# notch/crack



# curved beam



# rotating disk

