AE731

Theory of Elasticity

Dr. Nicholas Smith

Wichita State University, Department of Aerospace Engineering September 2, 2021

upcoming schedule

- Sep 2 Strain Transformation
- Sep 3 Homework 2 Due, Homework 1 Self-Grade Due
- Sep 7 Exam 1 Review
- Sep 9 Exam 1

2

outline

- example
- group problems
- principal strains
- special strain definitions
- strain transformation

example

 Calculate the deformation gradient, strain tensor, and rotation tensor for the given deformation

$$\left\{ \textit{u}_1 \ \textit{u}_2 \ \textit{u}_3 \right\} = \left\{ \textit{xy}^2 \textit{z} \ \textit{xz} \ \textit{z}^3 \right\}$$

• Deformation gradient:

$$F = u_{i,j} = \begin{bmatrix} y^2z & 2xyz & xy^2 \\ z & 0 & x \\ 0 & 0 & 3z^2 \end{bmatrix}$$

5

example

Strain tensor

$$e_{ij} = \frac{1}{2} (u_{i,j} + u_{j,i})$$

$$e_{ij} = \begin{bmatrix} y^2 z & xyz + \frac{1}{2}z & \frac{1}{2}xy^2 \\ xyz + \frac{1}{2}z & 0 & \frac{1}{2}x \\ \frac{1}{2}xy^2 & \frac{1}{2}x & 3z^2 \end{bmatrix}$$

6

Rotation tensor

$$\omega_{ij} = \frac{1}{2} (u_{i,j} - u_{j,i})$$

$$\omega_{ij} = \begin{bmatrix} 0 & xyz - \frac{1}{2}z & \frac{1}{2}xy^2 \\ -xyz + \frac{1}{2}z & 0 & \frac{1}{2}x \\ -\frac{1}{2}xy^2 & -\frac{1}{2}x & 0 \end{bmatrix}$$

7

example

 As we did with the deformation gradient, we can integrate the strain tensor to find the deformation (symmetric portion)

$$e_{ij} = \begin{bmatrix} yz & xz & xy \\ xz & 2y & \frac{1}{2}x^2 \\ xy & \frac{1}{2}x^2 & 3z^2 \end{bmatrix}$$

- We start by integrating the diagonal terms
- $u = \int yzdx = xyz + f(y,z)$
- $v = \int 2y dy = y^2 + g(v, z)$
- $w = \int 3z^2 dz = z^3 + h(x, y)$

9

example

Next we need to find the shear terms

$$e_{xy} = \frac{1}{2}(u_{,y} + v_{,x})$$

$$xz = \frac{1}{2}(xz + f_{,y} + g_{,x})$$

$$e_{xz} = \frac{1}{2}(u_{,z} + w_{,x})$$

$$xy = \frac{1}{2}(xy + f_{,z} + h_{,x})$$

$$e_{yz} = \frac{1}{2}(v_{,z} + w_{,y})$$

$$\frac{1}{2}x^2 = \frac{1}{2}(g_{,z} + h_{,y})$$

- Note that we cannot uniquely solve this (any arbitrary rotation ω can be added and will still produce a valid strain)
- Let f(y, z) = 0

$$g_{,x} = xz$$

$$g(x,z) = \frac{1}{2}x^2z$$

$$h_{,x} = xy$$

$$h(x,z) = \frac{1}{2}x^2y$$

11

example

$$\frac{1}{2}x^{2} = \frac{1}{2}(g_{,z} + h_{,y})$$

$$\frac{1}{2}x^{2} = \frac{1}{2}(\frac{1}{2}x^{2} + \frac{1}{2}x^{2})$$

$$u = xyz$$

$$v = y^{2} + \frac{1}{2}x^{2}z$$

$$w = z^{3} + \frac{1}{2}x^{2}y$$

group problems

group 1

 Sketch the deformed and undeformed shape of a rectangle under the following deformation

$$u = 0.7x + 0.1y$$
$$v = 0.3x + 1.2y$$

group 2

 For the following deformation, find the deformation gradient, strain, and rotation

$$u = xyz$$
$$v = xy + z$$
$$z = y^2z$$

14

group 3

 From the following strain field, find the displacements (you may assume no rotations)

$$\epsilon_{ij} = \begin{bmatrix} y & x+y \\ x+y & x \end{bmatrix}$$

principal strains

principal strains

 Principal strains are found in exactly the same way as principal values discussed in Chapter 1

$$\det[e_{ij} - e\delta_{ij}] = 0$$

 Invariants can also be found in the same fashion as in any other tensor

$$\vartheta_1 = e_1 + e_2 + e_3$$

 $\vartheta_2 = e_1 e_2 + e_2 e_3 + e_3 e_1$
 $\vartheta_3 = e_1 e_2 e_3$

principal strains

- Principal strains and invariants have some important physical meanings
- ϑ_1 is called the *cubical dilation*, and is related to the change in volume of the material
- Note that in the principal direction, there are no shear strains

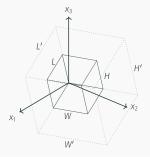
$$\begin{bmatrix} e_1 & 0 & 0 \\ 0 & e_2 & 0 \\ 0 & 0 & e_3 \end{bmatrix}$$

 This means that there is only extensional strain in the principal direction (i.e. a cube will remain a rectangular prism, the corners will maintain 90° angles)

17

volume change

 Consider a rectangular prism with edges oriented in the principal directions



volume change

- The volume before deformation is L = LWH
- The volume after deformation is given by V' = L'W'H'
- We can relate the side lengths after deformation to strains

$$e_1 = \frac{L^\prime - L}{L}$$

$$Le_1 + L = L'$$

• We can now write the volume as $V' = L(1 + e_1)W(1 + e_2)H(1 + e_3)$

19

volume change

- After multiplication, the deformed volume is given as
- $V' = LWH(1 + e_1 + e_2 + e_3 + e_1e_2 + e_2e_3 + e_1e_3 + e_1e_2e_3)$
- For small strains, e_i << 1, therefore e₁, e₂, and e₃ will be much larger than e₁e₂ + e₂e₃ + e₁e₃ + e₁e₂e₃)
- $V' = LWH(1 + e_1 + e_2 + e_3)$

volume change

 A "dilatation" is defined as the change in volume divided by the original volume

$$\frac{\Delta V}{V} = \frac{V' - V}{V}$$

Substituting the relationships found earlier

$$\frac{V'-V}{V} = \frac{LWH(1+e_1+e_2+e_3)-LWH}{LWH}$$

Which simplifies to

$$e_1 + e_2 + e_3 = \vartheta_1$$

2

special strain definitions

 This dilatation can be used to find the so-called spherical strain

$$\tilde{e}_{ij} = \frac{1}{3}e_{kk}\delta_{ij} = \frac{1}{3}\vartheta_1\delta_{ij}$$

 The deviatoric strain is found by subtracting the spherical strain from the strain tensor

$$\hat{e}_{ij} = e_{ij} - \frac{1}{3} e_{kk} \delta_{ij}$$

20

strain transformation

strain transformation

- The usual tensor transformation applies to the strain tensor as well
- $e'_{ij} = Q_{im}Q_{jn}e_{mn}$
- In many instances, however, we are only concerned with the strain within a plane (for example, when using strain gages).

23

strain transformation

• For an in-plane rotation (rotation about z-axis), we find

$$Q_{ij} = \begin{bmatrix} \cos\theta & \cos(90-\theta) & \cos 90 \\ \cos(90+\theta) & \cos\theta & \cos 90 \\ \cos 90 & \cos 90 & \cos 0 \end{bmatrix} = \begin{bmatrix} \cos\theta & \sin\theta & 0 \\ -\sin\theta & \cos\theta & 0 \\ 0 & 0 & 1 \end{bmatrix}$$

strain transformation

• If we multiply this out, for the in-plane strain terms $(e'_x, e'_y,$ and $e'_{xv})$ we find

$$\begin{aligned} e_x' &= e_x \cos^2 \theta + e_y \sin^2 \theta + 2e_{xy} \sin \theta \cos \theta \\ e_y' &= e_x \sin^2 \theta + e_y \cos^2 \theta - 2e_{xy} \sin \theta \cos \theta \\ e_{xy}' &= -e_x \sin \theta \cos \theta + e_y \sin \theta \cos \theta + e_{xy} (\cos^2 \theta - \sin^2 \theta) \end{aligned}$$

25

strain transformation

• This is often re-written using the double-angle formulas

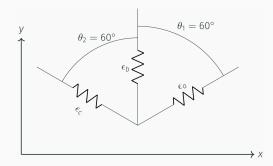
$$\begin{aligned} e_{x}' &= \frac{e_{x} + e_{y}}{2} + \frac{e_{x} - e_{y}}{2} \cos 2\theta + e_{xy} \sin 2\theta \\ e_{y}' &= \frac{e_{x} + e_{y}}{2} - \frac{e_{x} - e_{y}}{2} \cos 2\theta - e_{xy} \sin 2\theta \\ e_{xy}' &= \frac{e_{y} - e_{x}}{2} \sin 2\theta + e_{xy} \cos 2\theta \end{aligned}$$

strain transformation

- Many times it is easy to measure the axial strain directly with strain gages, but the shear strain cannot be easily measured
- We can use an extra, off-axis strain gage, together with the strain transformation equations, to calculate the shear strain
- Many companies already do this with "rosettes" which have strain gages at specified angles built-in

27

example



- Given that $\epsilon_a=0.005,\,\epsilon_b=-0.002,\,$ and $\epsilon_c=0.003,\,$ find $e_x,\,e_y$ and $e_{xy}.$
- Note that $e_y = \epsilon_b = -0.002$
- Set coordinate system so that $\epsilon_b = e_x'$
- Use equation for e'_{x} with $\theta=30$.

$$e'_{x} = \frac{e_{x} + e_{y}}{2} + \frac{e_{x} - e_{y}}{2} \cos 60 + e_{xy} \sin 60$$

29

example

- We have two unknowns in this equation, so we need another
- We can use the equation for e_y' with $\theta=60$ so that $\epsilon_b=e_x'$

$$e_y' = \frac{e_x + e_y}{2} - \frac{e_x - e_y}{2} \cos 120 - e_{xy} \sin 120$$

• Substituting known values and simplifying:

$$0.01 + 0.002 - 0.002\cos 60 = e_x(1 + \cos 60) + e_{xy}\sin 60$$
$$0.006 + 0.002 + 0.002\cos 120 = e_x(1 - \cos 120) - e_{xy}\sin 120$$

• And solving we find $e_x=0.006$, $e_y=-0.002$, and $e_{xy}=0.00231$