AE731

Theory of Elasticity

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upcoming schedule

- Sep 9 Strain Transformation
- Sep 11 Displacement and Strain
- Sep 16 Exam Review, Homework 2 Due
- Sep 18 Exam 1

outline

- example
- group problems
- principal strains
- special strain definitions
- strain transformation

• Calculate the deformation gradient, strain tensor, and rotation tensor for the given deformation

$$\left\{egin{array}{l} u_1 \ u_2 \ u_3 \end{array}
ight\} = \left\{egin{array}{l} xy^2z \ xz \ z^3 \end{array}
ight\}$$

• Deformation gradient:

$$F = u_{i,j} = egin{bmatrix} y^2z & 2xyz & xy^2 \ z & 0 & x \ 0 & 0 & 3z^2 \end{bmatrix}$$

• Strain tensor

$$e_{ij}=rac{1}{2}(u_{i,j}+u_{j,i})$$

$$e_{ij} = egin{bmatrix} y^2z & xyz + rac{1}{2}z & rac{1}{2}xy^2 \ xyz + rac{1}{2}z & 0 & rac{1}{2}x \ rac{1}{2}xy^2 & rac{1}{2}x & 3z^2 \end{bmatrix}$$

• Rotation tensor

$$\omega_{ij}=rac{1}{2}(u_{i,j}-u_{j,i})$$

$$\omega_{ij} = egin{bmatrix} 0 & xyz - rac{1}{2}z & rac{1}{2}xy^2 \ -xyz + rac{1}{2}z & 0 & rac{1}{2}x \ -rac{1}{2}xy^2 & -rac{1}{2}x & 0 \end{bmatrix}$$

• As we did with the deformation gradient, we can integrate the strain tensor to find the deformation (symmetric portion)

$$e_{ij} = egin{bmatrix} yz & xz & xy \ xz & 2y & rac{1}{2}x^2 \ xy & rac{1}{2}x^2 & 3z^2 \end{bmatrix}$$

- We start by integrating the diagonal terms
- $u = \int yzdx = xyz + f(y,z)$
- $v = \int 2y dy = y^2 + g(x, z)$
- $w = \int 3z^2 dz = z^3 + h(x, y)$

Next we need to find the shear terms

$$egin{align} e_{xy} &= rac{1}{2}(u_{,y} + v_{,x}) \ xz &= rac{1}{2}(xz + f_{,y} + g_{,x}) \ e_{xz} &= rac{1}{2}(u_{,z} + w_{,x}) \ xy &= rac{1}{2}(xy + f_{,z} + h_{,x}) \ e_{yz} &= rac{1}{2}(v_{,z} + w_{,y}) \ rac{1}{2}x^2 &= rac{1}{2}(g_{,z} + h_{,y}) \ \end{aligned}$$

- Note that we cannot uniquely solve this (any arbitrary rotation ω can be added and will still produce a valid strain)
- Let f(y, z) = 0

$$g_{,x}=xz \ g(x,z)=rac{1}{2}x^2z$$

$$h_{,x} = xy$$

$$h_{,x}=xy \ h(x,z)=rac{1}{2}x^2y$$

$$egin{align} rac{1}{2}x^2 &= rac{1}{2}(g_{,z} + h_{,y}) \ rac{1}{2}x^2 &= rac{1}{2}igg(rac{1}{2}x^2 + rac{1}{2}x^2igg) \ u &= xyz \ v &= y^2 + rac{1}{2}x^2z \ w &= z^3 + rac{1}{2}x^2y \ \end{pmatrix}$$

group problems

group 1

• Sketch the deformed and undeformed shape of a rectangle under the following deformation

$$u = 0.7x + 0.1y$$

$$v = 0.3x + 1.2y$$

group 2

• For the following deformation, find the deformation gradient, strain, and rotation

$$egin{aligned} u &= xyz \ v &= xy+z \ z &= y^2z \end{aligned}$$

group 3

• From the following strain field, find the displacements (you may assume no rotations)

$$\epsilon_{ij} = \left[egin{array}{ccc} y & x+y \ x+y & x \end{array}
ight]$$

principal strains

principal strains

- Principal strains are found in exactly the same way as principal values discussed in Chapter 1 $\det[e_{ij}e\delta_{ij}]=0$
- Invariants can also be found in the same fashion as in any other tensor

$$egin{aligned} artheta_1 &= e_1 + e_2 + e_3 \ artheta_2 &= e_1 e_2 + e_2 e_3 + e_3 e_1 \ artheta_3 &= e_1 e_2 e_3 \end{aligned}$$

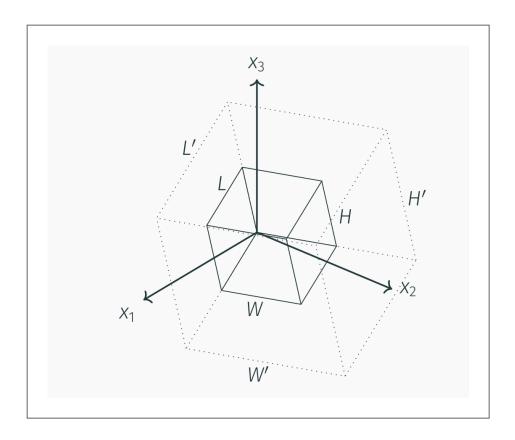
principal strains

- Principal strains and invariants have some important physical meanings
- ϑ_1 is called the *cubical dilation*, and is related to the change in volume of the material
- Note that in the principal direction, there are no shear strains

$$\left[egin{array}{ccc} e_1 & 0 & 0 \ 0 & e_2 & 0 \ 0 & 0 & e_3 \end{array}
ight]$$

• This means that there is only extensional strain in the principal direction (i.e. a cube will remain a rectangular prism, the corners will maintain 90° angles)

• Consider a rectangular prism with edges oriented in the principal directions



- The volume before deformation is V = LWH
- The volume after deformation is given by V' = L'W'H'
- We can relate the side lengths after deformation to strains

$$e_1 = rac{L'-L}{L} \ Le_1 + L = L'$$

• We can now write the volume as $V' = L(1 + e_1)W(1 + e_2)H(1 + e_3)$

- After multiplication, the deformed volume is given as
- $V' = LWH(1 + e_1 + e_2 + e_3 + e_1e_2 + e_2e_3 + e_1e_3 + e_1e_2e_3)$
- For small strains, $e_i \ll 1$, therefore e_1 , e_2 , and e_3 will be much larger than e_1e_2 , e_2e_3 , e_1e_3 and $e_1e_2e_3$.
- $V' = LWH(1 + e_1 + e_2 + e_3)$

• A "dilatation" is defined as the change in volume divided by the original volume

$$\frac{\Delta V}{V} = \frac{V' - V}{V}$$

• Substituting the relationships found earlier

$$rac{V'-V}{V}=rac{LWH(1+e_1+e_2+e_3)-LWH}{LWH}$$

Which simplifies to

$$e_1 + e_2 + e_3 = \vartheta_1$$

special strain definitions

spherical strain

• This dilatation can be used to find the so-called *spherical strain*

$${ ilde e}_{ij} = rac{1}{3} e_{kk} \delta_{ij} = rac{1}{3} artheta_1 \delta_{ij}$$

• The *deviatoric strain* is found by subtracting the spherical strain from the strain tensor

$$\hat{e}_{ij} = e_{ij} - rac{1}{3} e_{kk} \delta_{ij}$$

- The usual tensor transformation applies to the strain tensor as well
- $e_{ij}' = Q_{im}Q_{jn}e_{mn}$
- In many instances, however, we are only concerned with the strain within a plane (for example, when using strain gages).

• For an in-plane rotation (rotation about z-axis), we find

$$Q_{ij} = egin{bmatrix} \cos heta & \cos(90- heta) & \cos 90 \ \cos(90+ heta) & \cos heta & \cos 90 \ \cos 90 & \cos 90 & \cos 0 \end{bmatrix} = egin{bmatrix} \cos heta & \sin heta & 0 \ -\sin heta & \cos heta & 0 \ 0 & 0 & 1 \end{bmatrix}$$

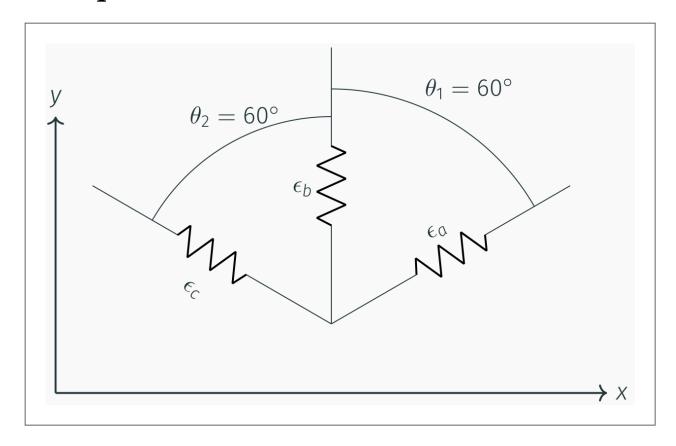
• If we multiply this out, for the in-plane strain terms $(e_\chi^{'}, e_\chi^{'},$ and $e_{\chi y}^{'})$ we find

$$egin{aligned} e_x' &= e_x \cos^2 heta + e_y \sin^2 heta + 2 e_{xy} \sin heta \cos heta \ e_y' &= e_x \sin^2 heta + e_y \cos^2 heta - 2 e_{xy} \sin heta \cos heta \ e_{xy}' &= -e_x \sin heta \cos heta + e_y \sin heta \cos heta + e_{xy} (\cos^2 heta - \sin^2 heta) \end{aligned}$$

• This is often re-written using the double-angle formulas

$$e_x'=rac{e_x+e_y}{2}+rac{e_x-e_y}{2} ext{cos }2 heta+e_{xy} ext{sin }2 heta \ e_y'=rac{e_x+e_y}{2}-rac{e_x-e_y}{2} ext{cos }2 heta-e_{xy} ext{sin }2 heta \ e_{xy}'=rac{e_y-e_x}{2} ext{sin }2 heta+e_{xy} ext{cos }2 heta$$

- Many times it is easy to measure the axial strain directly with strain gages, but the shear strain cannot be easily measured
- We can use an extra, off-axis strain gage, together with the strain transformation equations, to calculate the shear strain
- Many companies already do this with "rosettes" which have strain gages at specified angles built-in



- Given that ϵ_a = 0.005, ϵ_b = -0.002 and ϵ_c = 0.003, find e_x , e_y , and e_{xy} .
- Note that $e_y = \epsilon_b = -0.002$
- Set coordinate system so that $\epsilon_b = e_x'$.
- Use equation for e_{χ} with $\theta = 30$.

$$e_x' = rac{e_x + e_y}{2} + rac{e_x - e_y}{2} \cos 60 + e_{xy} \sin 60$$

- We have two unknowns in this equation, so we need another
- We can use the equation for e_y with $\theta = 60$ so that $\epsilon_b = e_x$

$$e_y' = rac{e_x + e_y}{2} - rac{e_x - e_y}{2} \cos 120 - e_{xy} \sin 120$$

• Substituting known values and simplifying:

$$egin{aligned} 0.01 + 0.002 - 0.002\cos 60 &= e_x(1+\cos 60) + e_{xy}\sin 60 \ 0.006 + 0.002 + 0.002\cos 120 &= e_x(1-\cos 120) - e_{xy}\sin 120 \end{aligned}$$

• And solving we find $e_x = 0.006$, $e_y = -0.002$, and $e_{xy} = 0.00231$.