

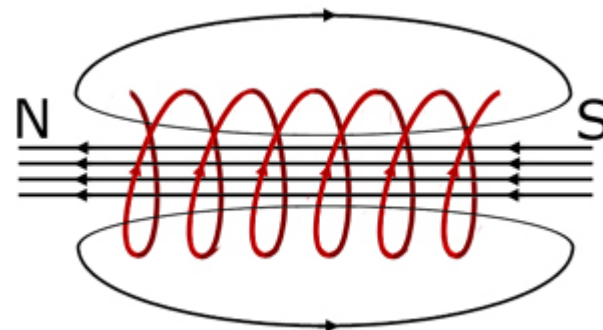


# Special Topic: Solenoids



# Applications of Solenoidal Fields

- Solenoids can provide an arbitrarily uniform magnetic field through a very large and/or extended volume
- Solenoids have long been used to create momentum tracking volumes in central high energy physics detectors.
- Solenoids can also be used to contain and transport low momentum particles (p up to a few 10's of MeV) by “trapping” in helical trajectories along the field lines
  - Concept originally applied to plasma containment
  - Currently drawing a great deal of interest as a way to transport very large emittance beams of low momentum particles
    - Particularly useful pions and muons for neutrino physics or muon application.





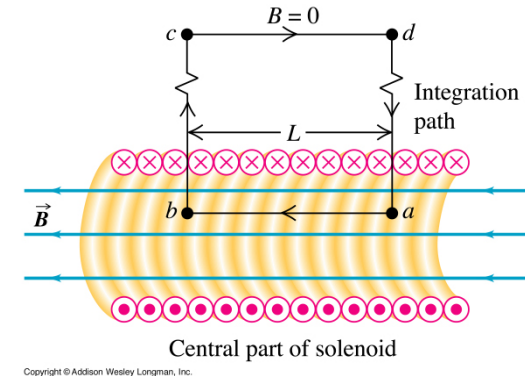
# The fields in a solenoid

- Within a long solenoid, the magnetic field is more or less uniform, calculated with

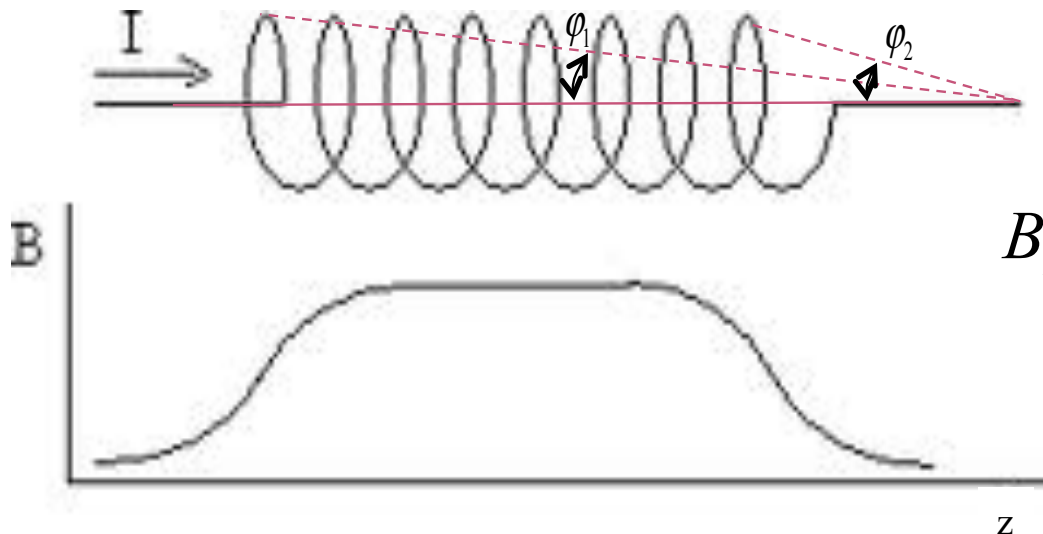
$$\oint \vec{B} \cdot d\vec{l} = BL = \mu_0 I_{\text{enc}} = \mu_0 n I L$$

winding pitch

$$\Rightarrow B = \mu_0 n I$$



- The exact formula is



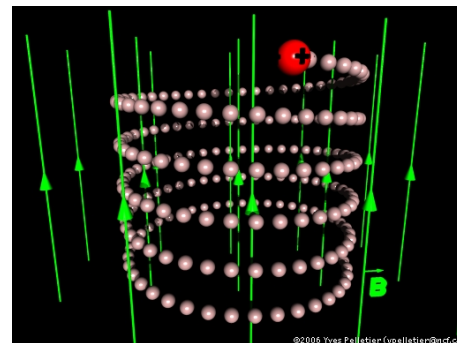
$$B_z = \frac{1}{2} \mu_0 n I (\cos \phi_1 - \cos \phi_2)$$



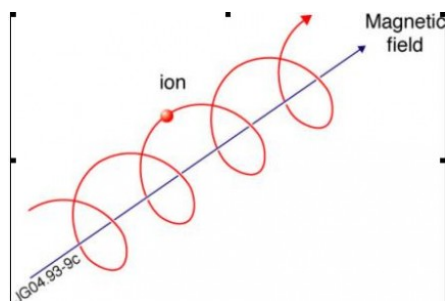
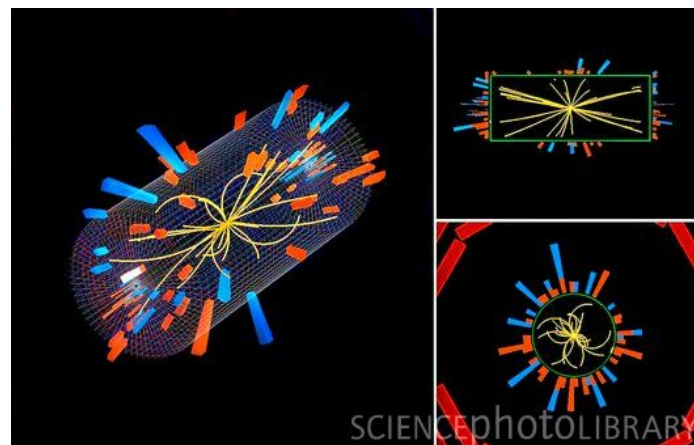
# Particle motion in a solenoidal field

- Generally, particles move in a helical trajectory

$$\rho = \frac{p}{qB}; \rho[m] = \frac{p[MeV/c] / 299}{B[T]}$$



- For high momentum particles, the curvature is used to measure the momentum
- Low momentum particles are effectively “trapped” along the field lines
  - 10 MeV/c particle will have a radius of 3 cm in a 1 T field



☒ Solenoids are a powerful tool to transport low momentum particles and can accommodate beams with very large emittances.



# Constants of the motion

- Both total momentum and angular momentum are conserved

$$p_0^2 = p_{\perp}^2 + p_{\parallel}^2 = \text{constant}$$

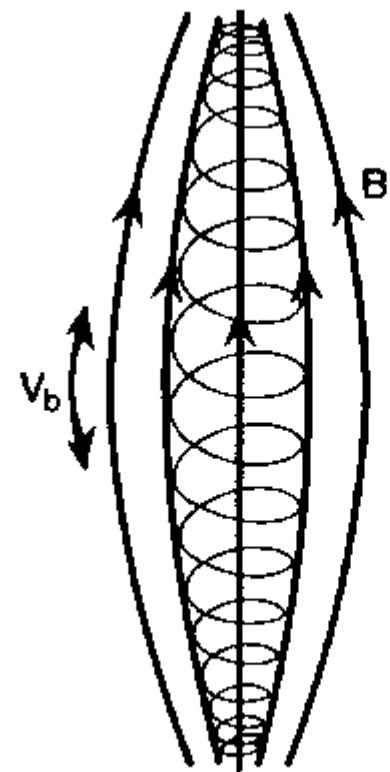
$$L = p_{\perp} \rho = \frac{p_{\perp}^2}{qB_{\parallel}} = \text{constant}$$

$$\Rightarrow p_{\perp}^2 = qLB_{\parallel}$$

$$p_{\parallel}^2 = p_0^2 - qLB_{\parallel}$$

- If  $qLB_{\parallel} > p_0^2$ , then particle will be reflected

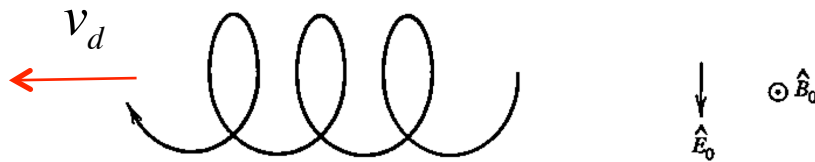
- Basis of “pinch confinement”



Bounce Motion

## “E cross B Drift”

An electric field transverse to the magnetic will cause a lateral drift, but the average acceleration will be zero.



$$\langle \vec{\dot{p}} \rangle = q\vec{E}_0 + q(\vec{v}_d \times \vec{B}_0) = 0$$

averaged over a cycle

assume

Cross the magnetic field into this

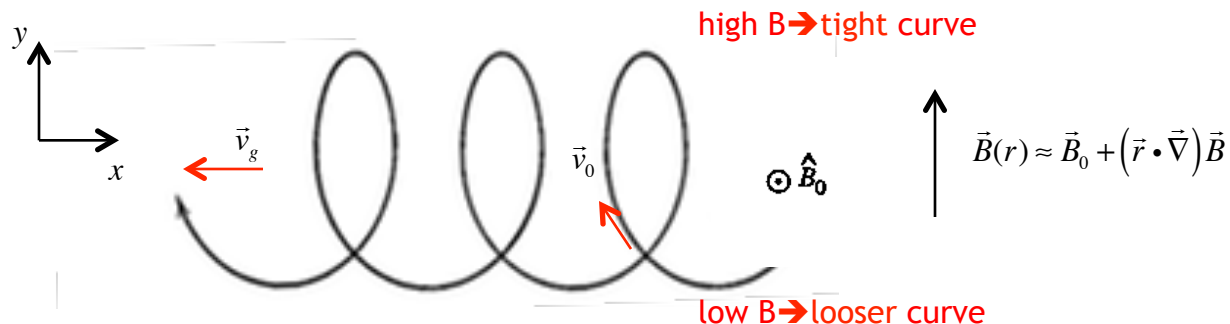
$$q \left[ \vec{B}_0 \times \vec{E}_0 + \vec{B}_0 \times (\vec{v}_d \times \vec{B}_0) \right] = 0$$

$$\vec{B}_0 \times \vec{E}_0 + B_0^2 \vec{v}_d - (\vec{B}_0 \cdot \vec{v}_d) \vec{B}_0 = 0$$

$$\vec{v}_d = \frac{\vec{E}_0 \times \vec{B}_0}{B_0^2}$$



# “Grad-B Drift”



We'll divide the motion in the cyclical part ( $v_0$ ) and the drift ( $v_g$ )

$$\begin{aligned} \frac{\vec{F}}{q} &= \vec{v}(t) \times \vec{B}(r) = \vec{v}_0(t) \times \vec{B}(r) + \vec{v}_g \times \vec{B}(r) \\ &\approx \vec{v}_0(t) \times \vec{B}_0 + \vec{v}_0(t) \times [(\vec{r} \cdot \vec{\nabla}) \vec{B}] + \vec{v}_g \times \vec{B}(r) + \vec{v}_g \times [(\vec{r} \cdot \vec{\nabla}) \vec{B}] \\ \longrightarrow \left\langle \frac{\vec{F}}{q} \right\rangle &= \left\langle \vec{v}_0(t) \times \vec{B}_0 \right\rangle + \left\langle \vec{v}_0(t) \times [(\vec{r} \cdot \vec{\nabla}) \vec{B}] \right\rangle + \left\langle \vec{v}_g \times \vec{B}_0 \right\rangle + \left\langle \vec{v}_g \times [(\vec{r} \cdot \vec{\nabla}) \vec{B}] \right\rangle \\ &= \left\langle \vec{v}_0(t) \times [(\vec{r} \cdot \vec{\nabla}) \vec{B}] \right\rangle + \vec{v}_g \times \vec{B}_0 = 0 \end{aligned}$$

Again, cross B into this and we get

$$\vec{B}_0 \times \left\langle \vec{v}_0(t) \times [(\vec{r} \cdot \vec{\nabla}) \vec{B}] \right\rangle + B_0^2 \vec{v}_g - (\vec{B}_0 \cdot \vec{v}_g) \vec{B}_0 = 0 \rightarrow \vec{v}_g = \frac{1}{B_0^2} \left\langle \vec{v}_0(t) \times [(\vec{r} \cdot \vec{\nabla}) \vec{B}] \right\rangle \times \vec{B}_0$$

For our example

$$\vec{B}_0 = B_0 \hat{z}$$

$$(\vec{r} \cdot \vec{\nabla}) \vec{B} = y \frac{\partial B}{\partial y} \vec{z}$$

$$\vec{v}_0(t) \times (\vec{r} \cdot \vec{\nabla}) \vec{B} = \begin{vmatrix} \hat{x} & \hat{y} & \hat{z} \\ v_{0,x}(t) & v_{0,y}(t) & 0 \\ 0 & 0 & y \frac{\partial B}{\partial y} \end{vmatrix} = v_{0,y}(t) y \frac{\partial B}{\partial y} \hat{x} - v_{0,x}(t) y \frac{\partial B}{\partial y} \hat{y}$$

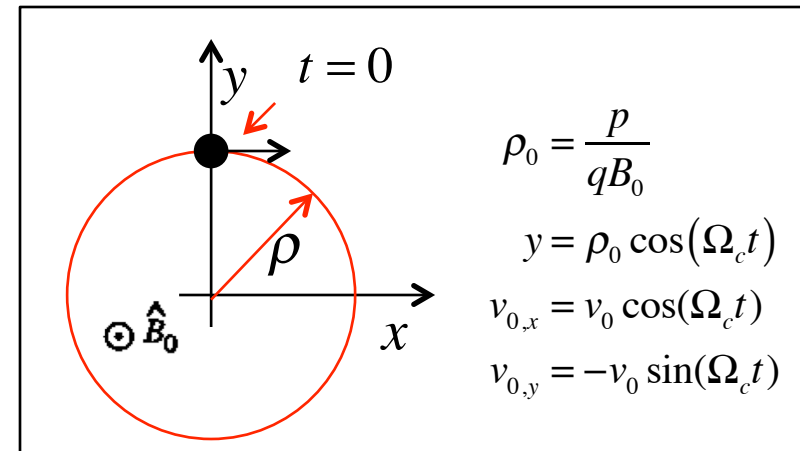
$$= -\rho_0 v_0 \cos(\Omega_s t) \sin(\Omega_s t) \frac{\partial B}{\partial y} \hat{x} - \rho_0 v_0 \cos^2(\Omega_s t) \frac{\partial B}{\partial y} \hat{y}$$

$$\langle \vec{v}_0(t) \times (\vec{r} \cdot \vec{\nabla}) \vec{B} \rangle = -\frac{1}{2} \rho_0 v_0 \frac{\partial B}{\partial y} \hat{y}$$

$$\vec{v}_g = \frac{1}{B_0^2} \langle \vec{v}_0(t) \times [(\vec{r} \cdot \vec{\nabla}) \vec{B}] \rangle \times \vec{B}_0$$

$$= -\frac{1}{2B_0} \rho_0 v_0 \frac{\partial B}{\partial y} \hat{x}$$

$$= \frac{1}{2B_0^2} \rho_0 v_0 (\vec{B}_0 \times \vec{\nabla} B)$$

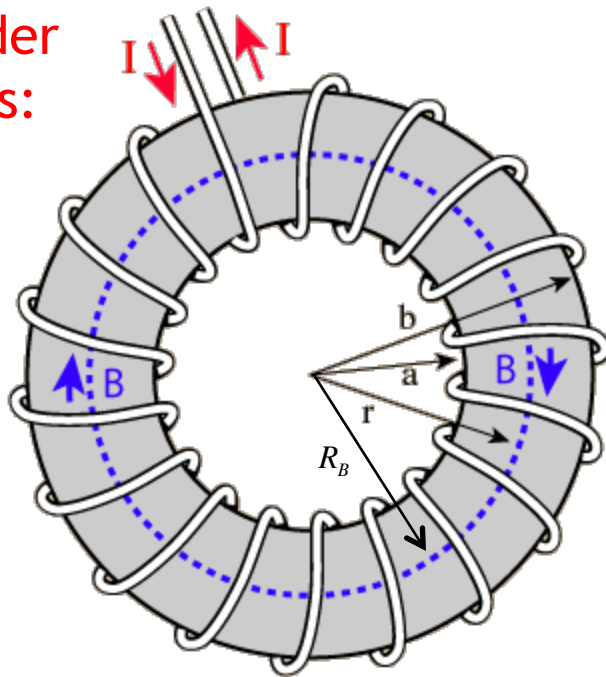






# Fields and drift in a Curved Solenoid

Consider  
a torus:



$$\int \vec{B} \cdot d\vec{l} = 2\pi r B = \mu_0 N I$$

$$B = \frac{\mu_0 N I}{2\pi r}$$

$$B_0 \equiv \frac{\mu_0 N I}{2\pi R_B} = \mu_0 n I \quad \text{field in center solenoid}$$

$$B = B_0 \frac{R_B}{r} \quad \leftarrow \text{Nominal radius of curvature}$$

$$\approx B_0 \left( 1 - \frac{x}{R_B} \right) \quad \leftarrow x \text{ measured outward from center of solenoid}$$

Clearly these formulas will also hold  
in an area of local curvature  $R_0$ .

As the particle moves along the field lines, it will experience a  
(fictitious) centrifugal force outward.

$$\vec{F}_c = m \frac{v_{\parallel}^2}{R_B} \hat{r} \quad \leftarrow \text{Component of velocity along } B \text{ field}$$

This is analogous to the effect of the electric field, so

$$\vec{E}_0 \rightarrow \frac{\vec{F}_c}{q} \Rightarrow \vec{v}_d = \frac{\vec{E}_0 \times \vec{B}_0}{B_0^2} \rightarrow \vec{v}_d = \frac{mv_{\parallel}^2}{qR_B B_0^2} \hat{r} \times \vec{B}_0$$

But we also have a gradient

$$\vec{\nabla} B = -\frac{B_0}{R_B} \hat{r}$$

$$\begin{aligned} v_g &= \frac{1}{2B_0^2} \rho_0 v_0 \left( \vec{B}_0 \times \vec{\nabla} B \right) = \frac{1}{2B_0 R_B} \left( \frac{\gamma m v_{\perp}}{q B_0} \right) v_{\perp} \left( \hat{r} \times \vec{B}_0 \right) \\ &= \frac{\gamma m v_{\perp}^2}{2q B_0^2 R_B} \left( \hat{r} \times \vec{B}_0 \right) \end{aligned}$$

velocity perpendicular to B

So the total drift velocity is

$$\begin{aligned} \vec{v}_{tot} &= \vec{v}_d + \vec{v}_g \\ &= \frac{m}{q R_B B_0^2} \left( \hat{r} \times \vec{B} \right) \left( v_{\parallel}^2 + \frac{1}{2} \gamma v_{\perp}^2 \right) \end{aligned}$$

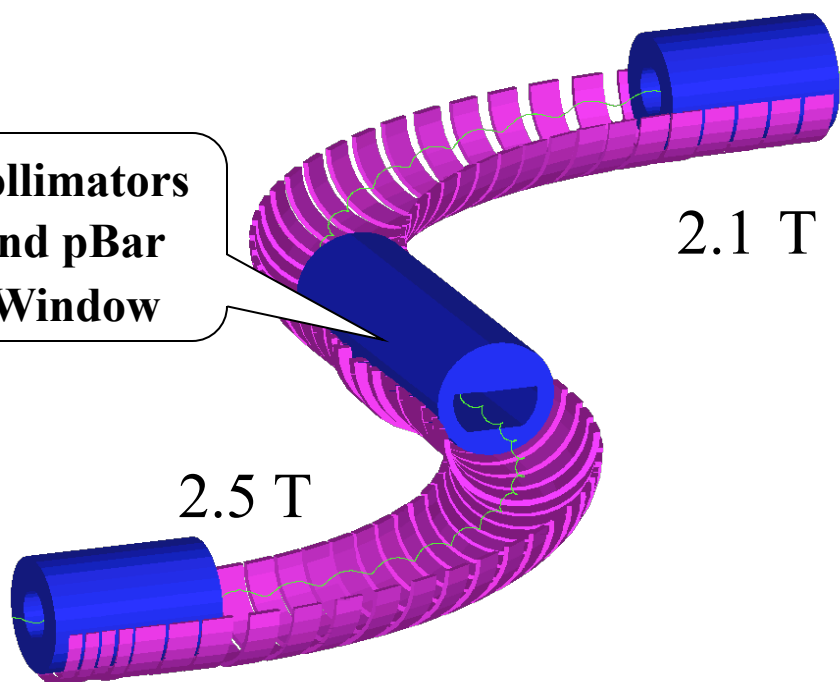
In most transport applications, this term will dominate

Depends on charge and direction of field, but not on direction of propagation within bend.

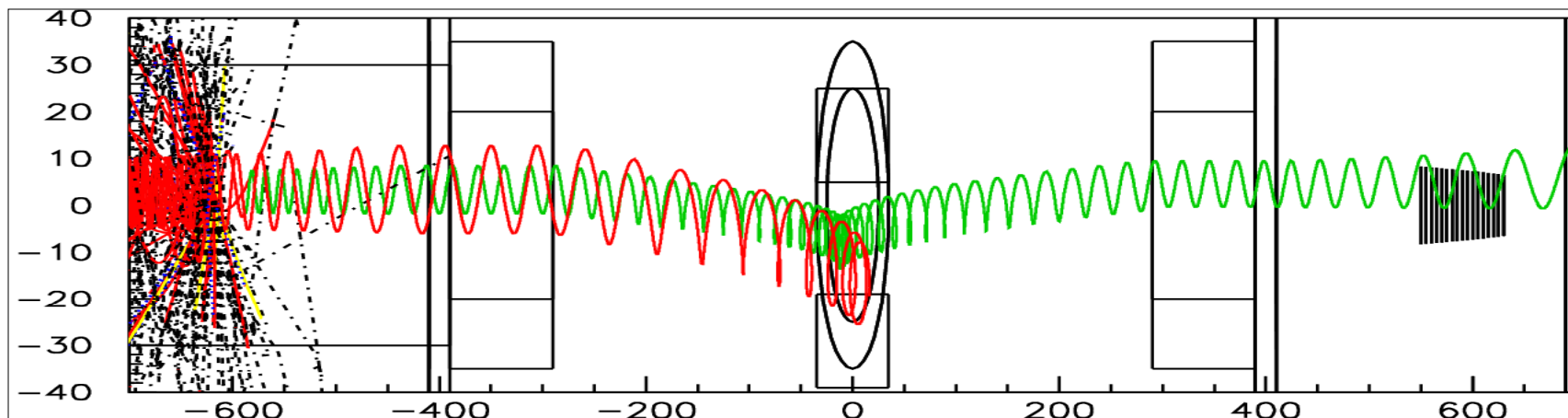
out of bend plane

## Example: Mu2e Experiment Transport Solenoid

Collimators  
and pBar  
Window



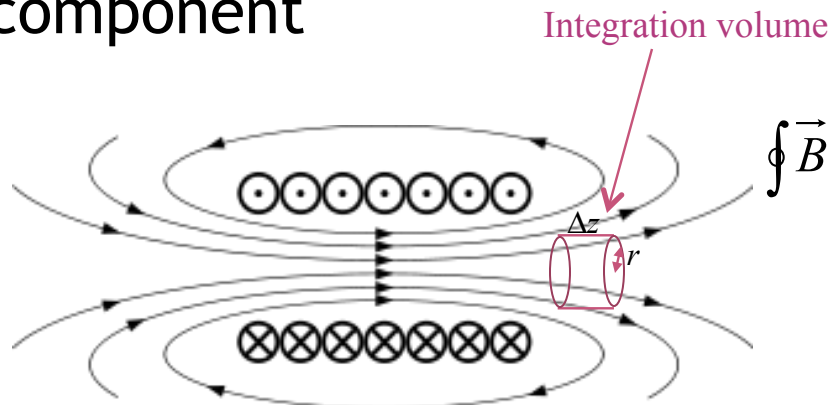
- Use curved solenoid to select negative muons with  $p < 90$  MeV/c
- Curvature drift and collimators sign and momentum select beam
- $dB/ds < 0$  in the straight sections to avoid trapping which would result in long transit times





# Fringe field of a solenoid

- ◉ Near the ends, the field of a solenoid will have a radial component



$$\begin{aligned}
 \oint \vec{B} \cdot d\vec{A} &= \pi r^2 (B_z(z + \Delta z) - B_z(z)) + 2\pi r \Delta z B_r \\
 &= \pi r^2 \Delta z B'_z + 2\pi r \Delta z B_r = 0 \\
 \Rightarrow B_r &= -\frac{r}{2} B'_z
 \end{aligned}$$

- ◉ For a long solenoid, this can be approximated near the end as

$$B_z \approx \frac{1}{2} \mu_0 n I (1 - \cos \phi_2) = \frac{1}{2} \mu_0 n I \left( 1 - \frac{z}{\sqrt{z^2 + R^2}} \right)$$

Measured from end

$$B_r = -\frac{r}{2} B'_z \approx \frac{r}{4} \mu_0 n I \left( \frac{1}{\sqrt{z^2 + R^2}} - \frac{z}{(z^2 + R^2)^{3/2}} \right)$$

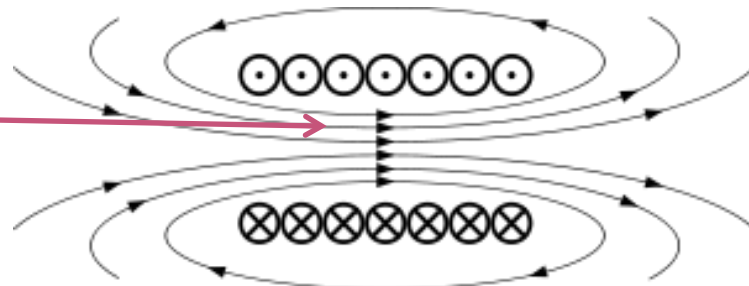


# Understanding solenoidal focusing

- Consider a particle coming toward a long solenoid parallel to the axis with velocity  $v_0$

- It will see a transverse kick (in the thin lens approximation)

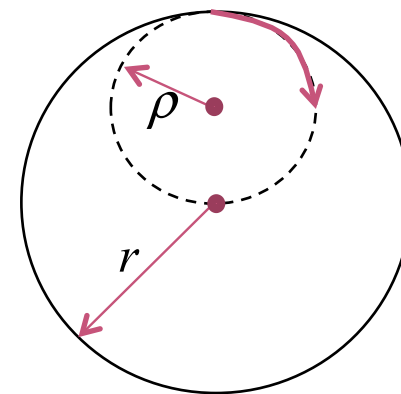
$$p_{\perp} \approx q \int B_r dz = -q \frac{r}{2} \int B'_z dz = -q \frac{r}{2} B_0$$



- It will begin to travel in a helix described by:

$$\rho = \frac{p_{\perp}}{qB_0} = \frac{r}{2}; \omega = \frac{p_{\perp}}{\gamma m \rho} = \frac{1}{\gamma} \Omega_s$$

- That is, the extrema of the helix will be the radius at the point of entry and the axis of the solenoid





# Focusing effect

- The radial position and velocity of the particle will be given by

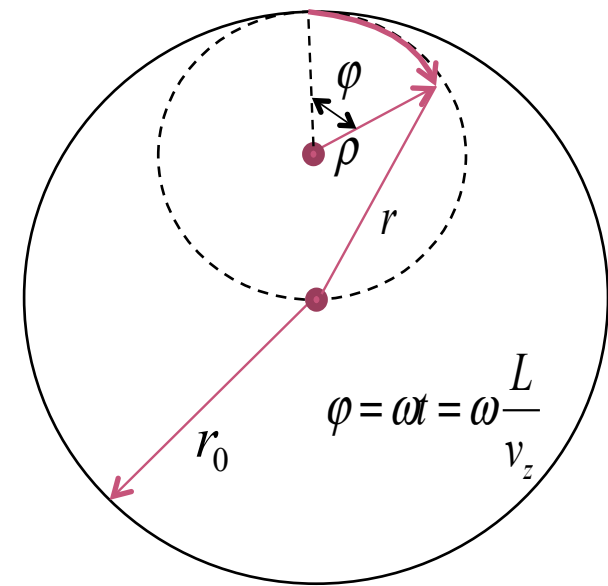
$$r^2 = 2\rho^2(1 + \cos\phi) = \frac{r_0^2}{2}(1 + \cos\phi) = r_0^2 \cos^2 \frac{\phi}{2}$$

$$\Rightarrow r = r_0 \cos \frac{\phi}{2}$$

$$\Rightarrow v_r = \dot{r} = -\frac{r_0}{2} \omega \sin \frac{\phi}{2} = -\frac{r_0}{2} \omega \sin \frac{\omega L / v_z}{2}$$

$$\approx -\frac{r_0}{4} \omega^2 \frac{L}{v_z} = \frac{r_0 \Omega_s^2}{4\gamma^2 v_z} L = \frac{r_0 q^2 B_0^2}{4\gamma^2 m^2 v_z} L$$

$$\boxed{\omega \frac{L}{v_z} \ll \pi}$$



- This results in a focusing angle

$$\theta \approx \frac{v_r}{v_z} \equiv -r_0 \frac{q^2 B_0^2}{4\gamma^2 m^2 v_z^2} L \approx -r_0 \frac{q^2 B_0^2}{4p^2} L$$



# Effective focal length and coupling

- ◉ The general form of the previous equation is

$$\theta \approx -r_0 \frac{q^2}{4p^2} \int B_0^2 dz \equiv -\frac{r_0}{f}$$

for unit charge

$$\Rightarrow \frac{1}{f} = \frac{q^2}{4p^2} \int B_0^2 dz = \frac{1}{4(B\rho)^2} \int B_0^2 dz =$$

- ◉ At the exit of the solenoid, the particles will receive an opposite transverse kick, but the magnitude will be reduced by  $r/r_0$ , resulting in a coupling between the planes
- ◉ Useful in low energy beam lines
  - Eg, immediately after ion sources
- ◉ Also useful in beam lines with large emittances
  - Eg, muon beams