

# Dynamic Model of Microgrids

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## A. Converter Model

The dynamics of the converters involve the low-pass filters, power controller ( $P$ - $\omega$  and  $Q$ - $V$  droop control), voltage controller (PI control), current controller (PI control), output LC filter, and coupling inductance.

Then the converter model can be formulated as follows [1]:

$$\omega = \omega^* - K_p(P - P^*) - \omega_{\text{ref}} \quad (1a)$$

$$\sqrt{(v_{\text{od}}^*)^2 + (v_{\text{oq}}^*)^2} = U^* - K_q(Q - Q^*) \quad (1b)$$

$$\dot{\delta} = \omega - \omega_n \quad (1c)$$

$$\dot{P} = \omega_c(-P + v_{\text{od}} \odot i_{\text{od}} + v_{\text{oq}} \odot i_{\text{oq}}) \quad (1d)$$

$$\dot{Q} = \omega_c(-Q + v_{\text{oq}} \odot i_{\text{od}} - v_{\text{od}} \odot i_{\text{oq}}) \quad (1e)$$

$$\dot{\phi}_{\text{d}} = v_{\text{od}}^* - v_{\text{od}} \quad (1f)$$

$$\dot{\phi}_{\text{q}} = v_{\text{oq}}^* - v_{\text{oq}} \quad (1g)$$

$$i_{\text{ld}}^* = F \odot i_{\text{od}} - \omega_n C_f \odot v_{\text{oq}} + K_{\text{pv}} \odot (v_{\text{od}}^* - v_{\text{od}}) + K_{\text{iv}} \odot \phi_{\text{d}} \quad (1h)$$

$$i_{\text{lq}}^* = F \odot i_{\text{oq}} + \omega_n C_f \odot v_{\text{od}} + K_{\text{pv}} \odot (v_{\text{oq}}^* - v_{\text{oq}}) + K_{\text{iv}} \odot \phi_{\text{q}} \quad (1i)$$

$$\dot{\gamma}_{\text{d}} = i_{\text{ld}}^* - i_{\text{ld}} \quad (1j)$$

$$\dot{\gamma}_{\text{q}} = i_{\text{lq}}^* - i_{\text{lq}} \quad (1k)$$

$$v_{\text{id}}^* = -\omega_n L_f \odot i_{\text{lq}} + K_{\text{pc}} \odot (i_{\text{ld}}^* - i_{\text{ld}}) + K_{\text{ic}} \odot \gamma_{\text{d}} \quad (1l)$$

$$v_{\text{iq}}^* = \omega_n L_f \odot i_{\text{ld}} + K_{\text{pc}} \odot (i_{\text{lq}}^* - i_{\text{lq}}) + K_{\text{ic}} \odot \gamma_{\text{q}} \quad (1m)$$

$$\dot{i}_{\text{ld}} = -r_f \odot L_f \odot i_{\text{ld}} + \omega_n i_{\text{lq}} + v_{\text{id}}^* \odot L_f - v_{\text{od}} \odot L_f \quad (1n)$$

$$\dot{i}_{\text{lq}} = -r_f \odot L_f \odot i_{\text{lq}} - \omega_n i_{\text{ld}} + v_{\text{iq}}^* \odot L_f - v_{\text{oq}} \odot L_f \quad (1o)$$

$$\dot{v}_{\text{od}} = \omega_n v_{\text{oq}} + i_{\text{ld}} \odot C_f - i_{\text{od}} \odot C_f \quad (1p)$$

$$\dot{v}_{\text{oq}} = -\omega_n v_{\text{od}} + i_{\text{lq}} \odot C_f - i_{\text{oq}} \odot C_f \quad (1q)$$

$$\dot{i}_{\text{od}} = -r_c \odot L_c \odot i_{\text{od}} + \omega_n i_{\text{oq}} + v_{\text{od}} \odot L_c - E_C v_{\text{Bd}} \odot L_c \quad (1r)$$

$$\dot{i}_{\text{oq}} = -r_c \odot L_c \odot i_{\text{oq}} - \omega_n i_{\text{od}} + v_{\text{oq}} \odot L_c - E_C v_{\text{Bq}} \odot L_c \quad (1s)$$

Eliminating the associated algebraic variables gives

$$\dot{\delta} = \omega^* - K_p(P - P^*) - \omega_{\text{ref}} \quad (2a)$$

$$\dot{P} = \omega_c(-P + v_{\text{od}} \odot i_{\text{od}} + v_{\text{oq}} \odot i_{\text{oq}}) \quad (2b)$$

$$\dot{Q} = \omega_c(-Q + v_{\text{oq}} \odot i_{\text{od}} - v_{\text{od}} \odot i_{\text{oq}}) \quad (2c)$$

$$\dot{\phi}_{\text{d}} = [\cos(\delta) \odot (U^* - K_q(Q - Q^*))] - v_{\text{od}} \quad (2d)$$

$$\dot{\phi}_{\text{q}} = [\sin(\delta) \odot (U^* - K_q(Q - Q^*))] - v_{\text{oq}} \quad (2e)$$

$$\dot{\gamma}_{\text{d}} = F \odot i_{\text{od}} - \omega_n C_f \odot v_{\text{oq}} + K_{\text{pv}} \odot ([\cos(\delta) \odot (U^* - K_q(Q - Q^*))] - v_{\text{od}}) + K_{\text{iv}} \odot \phi_{\text{d}} - i_{\text{ld}} \quad (2f)$$

$$\dot{\gamma}_{\text{q}} = F \odot i_{\text{oq}} + \omega_n C_f \odot v_{\text{od}} + K_{\text{pv}} \odot ([\sin(\delta) \odot (U^* - K_q(Q - Q^*))] - v_{\text{oq}}) + K_{\text{iv}} \odot \phi_{\text{q}} - i_{\text{lq}} \quad (2g)$$

$$\dot{i}_{\text{ld}} = [-r_f \odot i_{\text{ld}} + K_{\text{pc}} \odot (F \odot i_{\text{od}} - \omega_n C_f \odot v_{\text{oq}} + K_{\text{pv}} \odot ([\cos(\delta) \odot (U^* - K_q(Q - Q^*))] - v_{\text{od}}) + K_{\text{iv}} \odot \phi_{\text{d}} - i_{\text{ld}}) + K_{\text{ic}} \odot \gamma_{\text{d}} - v_{\text{od}}] \odot L_f \quad (2h)$$

$$\dot{i}_{\text{lq}} = [-r_f \odot i_{\text{lq}} + K_{\text{pc}} \odot (F \odot i_{\text{oq}} + \omega_n C_f \odot v_{\text{od}} + K_{\text{pv}} \odot ([\sin(\delta) \odot (U^* - K_q(Q - Q^*))] - v_{\text{oq}}) + K_{\text{iv}} \odot \phi_{\text{q}} - i_{\text{lq}}) + K_{\text{ic}} \odot \gamma_{\text{q}} - v_{\text{oq}}] \odot L_f \quad (2i)$$

$$\dot{v}_{\text{od}} = \omega_n v_{\text{oq}} + i_{\text{ld}} \odot C_f - i_{\text{od}} \odot C_f \quad (2j)$$

$$\dot{v}_{\text{oq}} = -\omega_n v_{\text{od}} + i_{\text{lq}} \odot C_f - i_{\text{oq}} \odot C_f \quad (2k)$$

$$\dot{i}_{\text{od}} = [-r_c \odot i_{\text{od}} + \omega_n i_{\text{oq}} \odot L_c + v_{\text{od}} - E_C v_{\text{Bd}}] \odot L_c \quad (2l)$$

$$\dot{i}_{\text{oq}} = [-r_c \odot i_{\text{oq}} - \omega_n i_{\text{od}} \odot L_c + v_{\text{oq}} - E_C v_{\text{Bq}}] \odot L_c \quad (2m)$$

## B. Load model

Three types of loads are considered: constant impedance load, induction motor load, and variable frequency induction-motor drive load. It is assumed that each load bus connects to a single type of loads.

The constant impedance loads are with the following dynamics:

$$\dot{\mathbf{i}}_{Ld} = -\mathbf{r}_L \odot \mathbf{L}_L \odot \mathbf{i}_{Ld} + \omega_n \mathbf{i}_{Lq} + \mathbf{E}_L \mathbf{v}_{Bd} \odot \mathbf{L}_L \quad (3a)$$

$$\dot{\mathbf{i}}_{Lq} = -\mathbf{r}_L \odot \mathbf{L}_L \odot \mathbf{i}_{Lq} - \omega_n \mathbf{i}_{Ld} + \mathbf{E}_L \mathbf{v}_{Bq} \odot \mathbf{L}_L \quad (3b)$$

The induction motor loads are with the following dynamics:

$$\dot{\mathbf{v}}_{Md} = \omega_n \mathbf{s}_M \odot \mathbf{v}_{Mq} - [\mathbf{v}_{Md} + \omega_n (\mathbf{L}_{Mo} - \mathbf{L}_{Mb}) \odot \mathbf{i}_{Mq}] \odot \mathbf{T}_{Mo} \quad (4a)$$

$$\dot{\mathbf{v}}_{Mq} = -\omega_n \mathbf{s}_M \odot \mathbf{v}_{Md} - [\mathbf{v}_{Mq} - \omega_n (\mathbf{L}_{Mo} - \mathbf{L}_{Mb}) \odot \mathbf{i}_{Md}] \odot \mathbf{T}_{Mo} \quad (4b)$$

$$\dot{\mathbf{s}}_M = [(\mathbf{a}_M + \mathbf{b}_M \odot \mathbf{s}_M + \mathbf{c}_M \odot \mathbf{s}_M^2) \odot \mathbf{T}_M^0 - (\mathbf{v}_{Md} \odot \mathbf{i}_{Md} + \mathbf{v}_{Mq} \odot \mathbf{i}_{Mq}) \odot \omega_n] \odot (2\mathbf{H}_M) \quad (4c)$$

$$\dot{\mathbf{i}}_{Md} = -\mathbf{r}_{Ms} \odot \mathbf{L}_{Mb} \odot \mathbf{i}_{Md} + \omega_n \mathbf{i}_{Mq} + (\mathbf{E}_M \mathbf{v}_{Bd} - \mathbf{v}_{Md}) \odot \mathbf{L}_{Mb} \quad (4d)$$

$$\dot{\mathbf{i}}_{Mq} = -\mathbf{r}_{Ms} \odot \mathbf{L}_{Mb} \odot \mathbf{i}_{Mq} - \omega_n \mathbf{i}_{Md} + (\mathbf{E}_M \mathbf{v}_{Bq} - \mathbf{v}_{Mq}) \odot \mathbf{L}_{Mb} \quad (4e)$$

with

$$\mathbf{L}_{Mo} = \mathbf{L}_{Ms} + \mathbf{L}_{Mm} \quad (5a)$$

$$\mathbf{L}_{Mb} = \mathbf{L}_{Ms} + (\mathbf{L}_{Mr} \mathbf{L}_{Mm}) \odot (\mathbf{L}_{Mr} + \mathbf{L}_{Mm}) \quad (5b)$$

$$\mathbf{T}_{Mo} = (\mathbf{L}_{Mr} + \mathbf{L}_{Mm}) \odot \mathbf{r}_{Mr} \quad (5c)$$

where  $\mathbf{L}_{Ms}$ ,  $\mathbf{L}_{Mm}$ ,  $\mathbf{L}_{Mr}$ ,  $\mathbf{r}_{Mr}$ ,  $\mathbf{r}_{Ms}$ , and  $\mathbf{H}_M$  are stator inductance, magnetizing inductance, rotor inductance, rotor resistance, stator resistance and inertia of the induction motor load, respectively;  $\mathbf{a}_M$ ,  $\mathbf{b}_M$ , and  $\mathbf{c}_M$  are the torque coefficients of the torque slip characteristics.

The variable frequency induction-motor drive loads are with the following dynamics [2], [3]:

$$\dot{\mathbf{i}}_{Ad} = -\mathbf{r}_A \odot \mathbf{L}_A \odot \mathbf{i}_{Ad} + \omega_n \mathbf{i}_{Aq} + (\mathbf{E}_D \mathbf{v}_{Bd} - \mathbf{v}_{Ad}) \odot \mathbf{L}_A \quad (6a)$$

$$\dot{\mathbf{i}}_{Aq} = -\mathbf{r}_A \odot \mathbf{L}_A \odot \mathbf{i}_{Aq} - \omega_n \mathbf{i}_{Ad} + (\mathbf{E}_D \mathbf{v}_{Bq} - \mathbf{v}_{Aq}) \odot \mathbf{L}_A \quad (6b)$$

$$\dot{\mathbf{i}}_r = \left( \frac{3\sqrt{2}}{\pi} \sqrt{\mathbf{v}_{Ad}^2 + \mathbf{v}_{Aq}^2} - \mathbf{r}_{DC} \odot \mathbf{i}_r - \mathbf{v}_{DC} \right) \odot \mathbf{L}_{DC} \quad (6c)$$

$$\dot{\mathbf{v}}_{DC} = \left( \mathbf{i}_r - \frac{\sqrt{3}}{2\sqrt{2}} \mathbf{i}_{Dd} \right) \odot \mathbf{C}_{DC} \quad (6d)$$

$$\Delta \dot{\omega}_{\max} = \left( \frac{\sqrt{3}}{2\sqrt{2}} \mathbf{i}_{Dd} - \mathbf{i}_{\max} \right) \odot \mathbf{K}_{\max} \odot \mathbf{T}_{\max} \quad (6e)$$

$$\Delta \dot{\omega} = -\mathbf{K}_{DP} \odot (\omega_n - \omega_m) \odot [(\mathbf{a}_D + \mathbf{b}_D \odot \mathbf{s}_D + \mathbf{c}_D \odot \mathbf{s}_D^2) \odot \mathbf{T}_D^0] - \mathbf{K}_{DP} \odot \left[ \left( \frac{\sqrt{3}}{2\sqrt{2}} \mathbf{i}_{Dd} - \mathbf{i}_{\max} \right) \odot \mathbf{K}_{\max} \odot \mathbf{T}_{\max} \right] + \mathbf{K}_{DI} \odot (\omega_{Dref} \alpha - \omega_m - \Delta \omega_{\max}) \quad (6f)$$

$$\dot{\omega}_m = (\omega_n - \omega_m) \odot [(\mathbf{a}_D + \mathbf{b}_D \odot \mathbf{s}_D + \mathbf{c}_D \odot \mathbf{s}_D^2) \odot \mathbf{T}_D^0] \quad (6g)$$

$$\dot{\mathbf{v}}_{Dd} = \omega_n \mathbf{s}_D \odot \mathbf{v}_{Dq} - [\mathbf{v}_{Dd} + \omega_n (\mathbf{L}_{Do} - \mathbf{L}_{Db}) \odot \mathbf{i}_{Dq}] \odot \mathbf{T}_{Do} \quad (6h)$$

$$\dot{\mathbf{v}}_{Dq} = -\omega_n \mathbf{s}_D \odot \mathbf{v}_{Dd} - [\mathbf{v}_{Dq} - \omega_n (\mathbf{L}_{Do} - \mathbf{L}_{Db}) \odot \mathbf{i}_{Dd}] \odot \mathbf{T}_{Do} \quad (6i)$$

$$\dot{\mathbf{s}}_D = [(\mathbf{a}_D + \mathbf{b}_D \odot \mathbf{s}_D + \mathbf{c}_D \odot \mathbf{s}_D^2) \odot \mathbf{T}_D^0 - (\mathbf{v}_{Dd} \odot \mathbf{i}_{Dd} + \mathbf{v}_{Dq} \odot \mathbf{i}_{Dq}) \odot \omega_n] \odot (2\mathbf{H}_D) \quad (6j)$$

$$\dot{\mathbf{i}}_{Dd} = -\mathbf{r}_{Ds} \odot \mathbf{L}_{Db} \odot \mathbf{i}_{Dd} + \omega_n \mathbf{i}_{Dq} + \left( \frac{\sqrt{3}}{2\sqrt{2}} \mathbf{v}_{DC} - \mathbf{v}_{Dd} \right) \odot \mathbf{L}_{Db} \quad (6k)$$

$$\dot{\mathbf{i}}_{Dq} = -\mathbf{r}_{Ds} \odot \mathbf{L}_{Db} \odot \mathbf{i}_{Dq} - \omega_n \mathbf{i}_{Dd} + (0 - \mathbf{v}_{Dq}) \odot \mathbf{L}_{Db} \quad (6l)$$

with

$$\mathbf{L}_{Do} = \mathbf{L}_{Ds} + \mathbf{L}_{Dm} \quad (7a)$$

$$\mathbf{L}_{Db} = \mathbf{L}_{Ds} + (\mathbf{L}_{Dr} \mathbf{L}_{Dm}) \odot (\mathbf{L}_{Dr} + \mathbf{L}_{Dm}) \quad (7b)$$

$$\mathbf{T}_{Do} = (\mathbf{L}_{Dr} + \mathbf{L}_{Dm}) \odot \mathbf{r}_{Dr} \quad (7c)$$

where  $\mathbf{L}_{Ds}$ ,  $\mathbf{L}_{Dm}$ ,  $\mathbf{L}_{Dr}$ ,  $\mathbf{r}_{Dr}$ ,  $\mathbf{r}_{Ds}$ , and  $\mathbf{H}_D$  are stator inductance, magnetizing inductance, rotor inductance, rotor resistance, stator resistance and inertia of the induction motor load, respectively;  $\mathbf{a}_D$ ,  $\mathbf{b}_D$ , and  $\mathbf{c}_D$  are the torque coefficients of the torque slip characteristics.

### C. Network model

The dynamics of branches are as follows:

$$\dot{\mathbf{i}}_{\text{Bd}} = -\mathbf{r}_{\text{B}} \odot \mathbf{L}_{\text{B}} \odot \mathbf{i}_{\text{Bd}} + \omega_{\text{n}} \mathbf{i}_{\text{Bq}} + \mathbf{E}_{\text{B}} \mathbf{v}_{\text{Bd}} \odot \mathbf{L}_{\text{B}} \quad (8a)$$

$$\dot{\mathbf{i}}_{\text{Bq}} = -\mathbf{r}_{\text{B}} \odot \mathbf{L}_{\text{B}} \odot \mathbf{i}_{\text{Bq}} - \omega_{\text{n}} \mathbf{i}_{\text{Bd}} + \mathbf{E}_{\text{B}} \mathbf{v}_{\text{Bq}} \odot \mathbf{L}_{\text{B}} \quad (8b)$$

The Kirchhoff's Current Law of each bus yields

$$\mathbf{0} = \mathbf{E}_{\text{C}}^{\text{T}} \mathbf{i}_{\text{od}} - \mathbf{E}_{\text{L}}^{\text{T}} \mathbf{i}_{\text{Ld}} - \mathbf{E}_{\text{M}}^{\text{T}} \mathbf{i}_{\text{Md}} - \mathbf{E}_{\text{D}}^{\text{T}} \mathbf{i}_{\text{Ad}} - \mathbf{E}_{\text{B}}^{\text{T}} \mathbf{i}_{\text{Bd}} \quad (9a)$$

$$\mathbf{0} = \mathbf{E}_{\text{C}}^{\text{T}} \mathbf{i}_{\text{oq}} - \mathbf{E}_{\text{L}}^{\text{T}} \mathbf{i}_{\text{Lq}} - \mathbf{E}_{\text{M}}^{\text{T}} \mathbf{i}_{\text{Mq}} - \mathbf{E}_{\text{D}}^{\text{T}} \mathbf{i}_{\text{Aq}} - \mathbf{E}_{\text{B}}^{\text{T}} \mathbf{i}_{\text{Bq}} \quad (9b)$$

### D. Full dynamic model in ODE form

Now we obtain the full dynamic model of the MG, in DAE form, as follows:

$$\dot{\tilde{\mathbf{x}}} = \tilde{\mathbf{f}}(\tilde{\mathbf{x}}, \mathbf{z}) \quad (10a)$$

$$\mathbf{0} = \tilde{\mathbf{g}}(\tilde{\mathbf{x}}) \quad (10b)$$

where (10a) collects (2), (3), (4), (6), and (8); (10b) represents (9); and

$$\tilde{\mathbf{x}} = \begin{bmatrix} \delta; \mathbf{P}; \mathbf{Q}; \phi_{\text{d}}; \phi_{\text{q}}; \gamma_{\text{d}}; \gamma_{\text{q}}; \mathbf{i}_{\text{ld}}; \mathbf{i}_{\text{lq}}; \mathbf{v}_{\text{od}}; \mathbf{v}_{\text{oq}}; \mathbf{i}_{\text{od}}; \mathbf{i}_{\text{oq}}; \\ \mathbf{i}_{\text{Ld}}; \mathbf{i}_{\text{Lq}}; \\ \mathbf{v}_{\text{Md}}; \mathbf{v}_{\text{Mq}}; \mathbf{s}_{\text{M}}; \mathbf{i}_{\text{Md}}; \mathbf{i}_{\text{Mq}}; \\ \mathbf{i}_{\text{Ad}}; \mathbf{i}_{\text{Aq}}; \mathbf{i}_{\text{r}}; \mathbf{v}_{\text{DC}}; \Delta\omega_{\text{max}}; \Delta\omega; \omega_{\text{m}}; \mathbf{v}_{\text{Dd}}; \mathbf{v}_{\text{Dq}}; \mathbf{s}_{\text{D}}; \mathbf{i}_{\text{Dd}}; \mathbf{i}_{\text{Dq}} \\ \mathbf{i}_{\text{Bd}}; \mathbf{i}_{\text{Bq}} \end{bmatrix} \quad (11a)$$

$$\mathbf{z} = [\mathbf{v}_{\text{Bd}}; \mathbf{v}_{\text{Bq}}] \quad (11b)$$

Next, we transform the DAE model to an ODE model. First, taking the derivative of both sides of (11b) and dividing (11a) accordingly gives

$$\dot{\tilde{\mathbf{x}}}_1 = \mathbf{f}_1(\tilde{\mathbf{x}}_1, \tilde{\mathbf{x}}_2, \mathbf{z}) \quad (12a)$$

$$\dot{\tilde{\mathbf{x}}}_2 = \mathbf{f}_2(\tilde{\mathbf{x}}_1, \tilde{\mathbf{x}}_2, \mathbf{z}) \quad (12b)$$

$$\mathbf{0} = \tilde{\mathbf{g}}_{\text{der}}(\tilde{\mathbf{x}}_2, \mathbf{z}) = \mathbf{M}_1 \tilde{\mathbf{x}}_2 + \mathbf{M}_2 \mathbf{z} \quad (12c)$$

where (12a) collects (2a)-(2i); (12b) collects (2j)-(2m), (3), (4), (6), and (8); and

$$\tilde{\mathbf{x}}_1 = [\delta; \mathbf{P}; \mathbf{Q}; \phi_{\text{d}}; \phi_{\text{q}}; \gamma_{\text{d}}; \gamma_{\text{q}}; \mathbf{i}_{\text{ld}}; \mathbf{i}_{\text{lq}}; \mathbf{s}_{\text{M}};] \quad (13a)$$

$$\tilde{\mathbf{x}}_2 = \begin{bmatrix} \mathbf{v}_{\text{od}}; \mathbf{v}_{\text{oq}}; \mathbf{i}_{\text{od}}; \mathbf{i}_{\text{oq}}; \\ \mathbf{i}_{\text{Ld}}; \mathbf{i}_{\text{Lq}}; \\ \mathbf{v}_{\text{Md}}; \mathbf{v}_{\text{Mq}}; \mathbf{i}_{\text{Md}}; \mathbf{i}_{\text{Mq}}; \\ \mathbf{i}_{\text{Ad}}; \mathbf{i}_{\text{Aq}}; \mathbf{i}_{\text{r}}; \mathbf{v}_{\text{DC}}; \Delta\omega_{\text{max}}; \Delta\omega; \omega_{\text{m}}; \mathbf{v}_{\text{Dd}}; \mathbf{v}_{\text{Dq}}; \mathbf{s}_{\text{D}}; \mathbf{i}_{\text{Dd}}; \mathbf{i}_{\text{Dq}} \\ \mathbf{i}_{\text{Bd}}; \mathbf{i}_{\text{Bq}} \end{bmatrix} \quad (13b)$$

Then, following [4], (12) can be transformed into the following ODE model

$$\dot{\tilde{\mathbf{x}}} = \tilde{\mathbf{f}}(\tilde{\mathbf{x}}, \mathbf{z}) \quad (14a)$$

$$\dot{\mathbf{z}} = \mathbf{h}(\tilde{\mathbf{x}}, \mathbf{z}) = - \left( \frac{\partial \tilde{\mathbf{g}}_{\text{der}}}{\partial \mathbf{z}}(\tilde{\mathbf{x}}_2, \mathbf{z}) \right)^{-1} \frac{\partial \tilde{\mathbf{g}}_{\text{der}}}{\partial \tilde{\mathbf{x}}_2}(\tilde{\mathbf{x}}_2, \mathbf{z}) \mathbf{f}_2(\tilde{\mathbf{x}}, \mathbf{z}) \quad (14b)$$

Finally, we derive the conditions for the existence of the ODE model and the equivalence of the above transformation. The ODE model exists iff the matrix  $\frac{\partial \tilde{\mathbf{g}}_{\text{der}}}{\partial \mathbf{z}}(\tilde{\mathbf{x}}_2, \mathbf{z})$  is invertible. We have

$$\frac{\partial \tilde{\mathbf{g}}_{\text{der}}}{\partial \mathbf{z}}(\tilde{\mathbf{x}}_2, \mathbf{z}) = -\mathbf{E}_{\text{C}}^{\text{T}} \mathbf{L}'_{\text{C}} \mathbf{E}_{\text{C}} - \mathbf{E}_{\text{L}}^{\text{T}} \mathbf{L}'_{\text{L}} \mathbf{E}_{\text{L}} - \mathbf{E}_{\text{B}}^{\text{T}} \mathbf{L}'_{\text{B}} \mathbf{E}_{\text{B}} - \mathbf{E}_{\text{M}}^{\text{T}} \mathbf{L}'_{\text{Mb}} \mathbf{E}_{\text{M}} - \mathbf{E}_{\text{D}}^{\text{T}} \mathbf{L}'_{\text{A}} \mathbf{E}_{\text{D}} \quad (15)$$

with  $\mathbf{L}'_{\text{C}} = [\text{diag}(\mathbf{L}_{\text{C}})]^{-1}$ , and  $\mathbf{L}'_{\text{L}}$ ,  $\mathbf{L}'_{\text{B}}$ ,  $\mathbf{L}'_{\text{Mb}}$ , and  $\mathbf{L}'_{\text{A}}$  being analogous. We can prove that  $\frac{\partial \tilde{\mathbf{g}}_{\text{der}}}{\partial \mathbf{z}}(\tilde{\mathbf{x}}_2, \mathbf{z})$  is invertible if the topology of the MG is connected. Further, according to [5], the equivalence between the ODE model and DAE model can be ensured with compatible initial conditions. Let  $[\tilde{\mathbf{x}}(t_0); \mathbf{z}(t_0)]$  denote the initial state at  $t = t_0$ , then the solutions of the ODE model and DAE model are identical if  $\mathbf{g}(\tilde{\mathbf{x}}(t_0)) = \mathbf{0}$ , which allows us to apply the results established for the ODE model to the DAE model and thus the real-life MG.

## REFERENCES

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