

Flexible Snow Model (FSM2) scientific documentation

Richard Essery

Draft, 27 May 2018

The Flexible Snow Model allows alternative process parametrizations to be combined in a complete model of the mass and energy balances of snow on the ground and in forest canopies. Existing models from which parametrizations are taken for inclusion in FSM2 include CLASS (Bartlett and Verseghy), CLM (Oleson et al.), Crocus (Vionnet et al.), ISBA (Boone) and MOSES (Essery). Parametrizations are selected by setting option numbers in a text file before the model is compiled. Parameter values and input data are read from text files when the model is run. Physical constants, meteorological driving variables, site characteristics, model state variables and parameters are listed in tables 1 to 5; refer to these tables for any variables that are not explicitly defined in the text.

1 Snow-free and snow-covered ground albedos

Bare ground with albedo α_0 and snow cover fraction f_s with albedo α_s have average albedo

$$\alpha_g = (1 - f_s)\alpha_0 + f_s\alpha_s. \quad (1)$$

The snow cover is a function of snow depth h parametrized as

$$f_s(h) = \tanh\left(\frac{h}{h_f}\right). \quad (2)$$

(add $h/(h + h_f)$ option)

1.1 Diagnosed snow albedo (option ALBED0=0)

Following a common approach in earlier generations of climate models (e.g. DKRZ 1992, Cox et al. 1999), snow albedo is diagnosed as a function of surface temperature

$$\alpha_s(T_*) = \alpha_{\min} + (\alpha_{\max} - \alpha_{\min}) \min\left(\frac{T_* - T_m}{T_\alpha}, 1\right). \quad (3)$$

1.2 Prognostic snow albedo (option ALBED0=1)

Based on CLASS and ISBA, decreasing albedo as snow ages with time t and increasing albedo as fresh snow falls at rate S_f are parametrized by

$$\frac{d\alpha_s}{dt} = \frac{1}{\tau_\alpha}(\alpha_{\min} - \alpha_s) + \frac{S_f}{S_\alpha}(\alpha_{\max} - \alpha_s), \quad (4)$$

where the timescale τ_α has different values τ_{cold} and τ_{melt} for cold and melting snow. Equation (4) is implemented by integrating over a timestep of length δt to give the change in snow albedo as

$$\delta\alpha_s = (\alpha_{\lim} - \alpha_s)(1 - e^{-\gamma\delta t}), \quad (5)$$

where

$$\gamma = \frac{1}{\tau_\alpha} + \frac{S_f}{S_\alpha} \quad (6)$$

and

$$\alpha_{\lim} = \frac{1}{\gamma} \left(\frac{1}{\tau_\alpha} \alpha_{\min} + \frac{S_f}{S_\alpha} \alpha_{\max} \right). \quad (7)$$

2 Snow density

2.1 Compaction

Snow may be assumed to have constant density ρ_0 (option `DENSTY=0`) or to compact at rate

$$\frac{d\rho_s}{dt} = f_\rho(\rho_s, T_s). \quad (8)$$

Snow density ρ_s in layer k with ice mass I and liquid water mass W at the beginning of timestep n is diagnosed as

$$\rho_{s,k}^{(n)} = \frac{I_k^{(n)} + W_k^{(n)}}{D_{s,k}}. \quad (9)$$

Equation (8) is then implemented as

$$\rho_{s,k}^{(n+1)} = \rho_{s,k}^{(n)} + f_\rho(\rho_{s,k}^{(n)}, T_{s,k}^{(n)}) \delta t. \quad (10)$$

Finally, the thickness of the compacted layer at the end of the timestep is calculated by inverting Equation (9).

2.1.1 Empirical maximum densities (option `DENSTY=1`)

Based on CLASS, the compaction rate function is

$$f_\rho = \frac{1}{\tau_\rho}(\rho_{\max} - \rho_s) \quad (11)$$

with the same time constant τ_ρ but different asymptotic values ρ_{cold} and ρ_{melt} for ρ_{\max} in cold and melting snow.

2.1.2 Viscous compaction by overburden (option `DENSTY=2`)

Following ISBA, the compaction rate function is

$$f_\rho = \rho_s \left\{ \frac{gm}{\eta} + d_a \exp[d_b(T_s - T_m) - d_c \max(\rho_s - \rho_c, 0)] \right\} \quad (12)$$

where

$$\eta = \eta_0 \exp[-\eta_a(T_s - T_m) + \eta_b \rho_s]. \quad (13)$$

and the snow mass overlying the middle of a layer is

$$m_k = \sum_{j=1}^{k-1} [I_j^{(n)} + W_j^{(n)}] + 0.5 [I_k^{(n)} + W_k^{(n)}]. \quad (14)$$

2.2 Fresh snow density

Fresh snow has fixed density ρ_f , so snowfall over a timestep increases the snow depth before compaction by $\rho_f^{-1} S_f \delta t$. Snow unloading from a forest canopy is added to snow on the ground with the bulk density of the snow. (*add variable fresh snow density option*).

3 Canopy radiative transfer

3.1 Shortwave radiation

Forest structure is defined by canopy height h , vegetation area index Λ (including leaves and stems) and vegetation fraction f_v , which is either parametrized as $1 - \exp(-\Lambda)$ or specified as an input. A forest canopy with intercepted snow mass S_v and interception capacity S_{cap} is assumed to have snow cover fraction

$$f_{cs} = \frac{S_v}{S_{\text{cap}}} \quad (15)$$

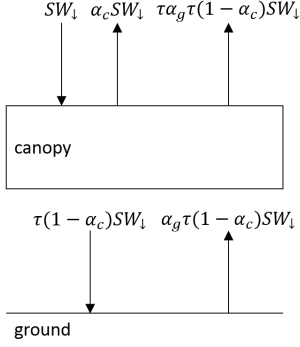


Figure 1: Reflection and transmission of shortwave radiation by a forest canopy and reflection by the ground surface.

and albedo

$$\alpha_c = f_v[(1 - f_{cs})\alpha_{c0} + f_{cs}\alpha_{cs}]. \quad (16)$$

As illustrated in Figure 1, the canopy is assumed to reflect fraction α_c and transmit fraction τ_c of incoming shortwave radiation SW_{\downarrow} , but radiation reflected from the ground is transmitted and absorbed by the canopy without further reflections (*could add a multiple reflection option*). The net absorption is

$$SW_v = (1 - \alpha_c)(1 + \alpha_g\tau_c)(1 - \tau_c)SW_{\downarrow} \quad (17)$$

by the forest canopy and

$$SW_g = (1 - \alpha_c)(1 - \alpha_g)\tau_c SW_{\downarrow} \quad (18)$$

by the ground or snow surface. The effective above-canopy albedo, including shortwave radiation reflected from the canopy and ground, is

$$\alpha = \alpha_c + (1 - \alpha_c)\alpha_g\tau_c^2. \quad (19)$$

3.1.1 Global shortwave radiation (option SWPART=0)

Usually, only measurements of global shortwave radiation are available. Canopy transmissivity for global radiation is set equal to sky view fraction, which is parametrized as

$$f_{\text{sky}} = \exp(-k_{\text{ext}}\Lambda) \quad (20)$$

by default but can also be specified directly as an input for sites which are not directly under trees ($\Lambda = 0$) but which are shaded by surrounding vegetation or topography ($f_{\text{sky}} < 1$).

3.1.2 Direct and diffuse shortwave radiation (option SWPART=1)

If global shortwave radiation is partitioned into direct and diffuse components (Appendix), Equations (17) and (18) are applied separately to the components. Equation (20) is used for the transmission of diffuse radiation and

$$\tau_{\text{dir}} = \exp(-k_{\text{ext}}\Lambda / \sin \theta) \quad (21)$$

is used for the first downwards transmission of direct radiation from the sun at elevation angle θ .

3.1.3 Two-stream radiative transfer (to be added as an option)

3.2 Longwave radiation

The net absorption of longwave radiation is

$$LW_v = (1 - f_{\text{sky}})(LW_{\downarrow} + \sigma T_*^4 - 2\sigma T_v^4) \quad (22)$$

by the forest canopy and

$$LW_g = f_{\text{sky}}LW_{\downarrow} - \sigma T_*^4 + (1 - f_{\text{sky}})\sigma T_v^4 \quad (23)$$

by the ground or snow surface. Upwelling longwave radiation above a forest canopy is

$$LW_{\uparrow} = f_{\text{sky}}\sigma T_*^4 + (1 - f_{\text{sky}})\sigma T_v^4. \quad (24)$$

4 Turbulent fluxes

4.1 Roughness lengths and aerodynamic resistances

Roughness lengths for snow-free ground and snow on fraction f_s of the ground are combined to give a ground roughness length

$$z_{0g} = z_{0f}^{1-f_s} z_{0s}^{f_s}. \quad (25)$$

For vegetation of height h covering fraction f_v of the ground, the roughness length and displacement height are $z_{0v} = R_{z0}h$ and $d = f_v R_d h$. The combined surface roughness length is

$$z_0 = z_{0g}^{1-f_v} z_{0v}^{f_v}. \quad (26)$$

The aerodynamic resistance network for turbulent exchanges of heat between the ground, vegetation and the atmosphere is shown in Figure 2. The resistance between the canopy air space and the atmosphere is

$$r_{aa} = \frac{1}{f_H k u_*} \ln \left(\frac{z_T - d}{z_0} \right) \quad (27)$$

with atmospheric stability factor f_H and friction velocity

$$u_* = k U_a \left[\ln \left(\frac{z_U - d}{z_0} \right) \right]^{-1}. \quad (28)$$

Vegetated and unvegetated fractions of the ground share a common surface temperature but have separate aerodynamic resistances that combine in parallel to give resistance

$$r_{ag} = \frac{1}{k u_*} \left[\frac{(1-f_v)f_h}{\ln(z_{0g}/z_{0h})} + f_v f_c C_{\text{dense}} \right]^{-1} \quad (29)$$

between the ground and the canopy air space, with sub-canopy stability factor f_c . Between vegetation and the canopy air space, the aerodynamic resistance is

$$r_{av} = \frac{C_{\text{veg}}}{\Lambda u_*^{1/2}}. \quad (30)$$

C_{dense} , C_{veg} and the ratio z_{0g}/z_{0h} between roughness lengths for momentum and heat are constant parameters. In the absence of vegetation ($\Lambda = f_v = 0$), resistances for heat transfer combine to give

$$r_h \equiv r_{aa} + r_{ag} = \frac{1}{f_h k U_a^2} \ln \left(\frac{z_U}{z_{0g}} \right) \ln \left(\frac{z_T}{z_{0h}} \right). \quad (31)$$

4.1.1 Neutral stability (option EXCHNG=0)

Atmospheric stability is neglected by setting $f_H = 1$.

4.1.2 Richardson number stability functions (option EXCHNG=1)

Atmospheric stability is characterized by a bulk Richardson number

$$\text{Ri}_B = \frac{g(z_U - d)^2 [T_a - f_v T_v - (1 - f_v) T_*]}{(z_T - d) T_a U_a^2}. \quad (32)$$

The aerodynamic resistances in Equation (27) and (29) are adjusted by factor

$$f_H = \begin{cases} [1 + 3b_h \text{Ri}_B (1 + b_h \text{Ri}_B)^{1/2}]^{-1} & \text{Ri}_B \geq 0 \\ 1 - 3b_h \text{Ri}_B [1 + c(-\text{Ri}_B)^{1/2}]^{-1} & \text{Ri}_B < 0 \end{cases} \quad (33)$$

with

$$c = 3b_h^2 k^2 \left(\frac{z_U}{z_0} \right)^{1/2} \left[\ln \left(\frac{z_U}{z_0} \right) \right]^{-2}. \quad (34)$$

from the ground to the canopy air space, and

$$H_v = \frac{\rho c_p}{r_{av}}(T_v - T_c) \quad (42)$$

from the vegetation to the canopy air space. Similarly, moisture fluxes are

$$E = \frac{\rho}{r_{aa}}(Q_c - Q_a) \quad (43)$$

upwards from the canopy air space,

$$E_g = \frac{\rho \psi_g}{r_{ag}}[Q_{\text{sat}}(T_*, P_s) - Q_c] \quad (44)$$

from the ground to the canopy air space, and

$$E_v = \frac{\rho \psi_v}{r_{av}}[Q_{\text{sat}}(T_v, P_s) - Q_c] \quad (45)$$

from the vegetation to the canopy air space, with moisture availability factor $\psi_v = 1$ if there is snow on the canopy or if $Q_{\text{sat}}(T_v) < Q_c$ (moisture flux onto the canopy) and

$$\psi_v = \frac{r_{av}}{r_{av} + r_{sg}} \quad (46)$$

otherwise.

5 Energy balance

5.1 Snow on short vegetation and bare ground

The surface energy balance

$$f(T_*) = LW_g + SW_g - G - H_g - LE_g - L_f M = 0 \quad (47)$$

with flux parametrizations substituted from Equations ? to (38) is a nonlinear equation for the unknown surface temperature and snowmelt rate M . From an initial guess of temperature T_{*0} and no melt, a linear estimate of T_* is given by

$$T_* = T_{*0} - f(T_{*0}) \left(\frac{df}{dT_*} \right)^{-1}. \quad (48)$$

A single application of Equation (48) gives an approximate solution, and repeated applications with T_* calculated in each iteration being used as T_{*0} in the next is the Newton-Raphson method for solving Equation (47). Neglecting the complicated temperature dependence of r_{aa} , this gives

$$T_* = T_{*0} + \frac{LW_g + SW_g - G - H_g - LE_g - L_f M}{4\sigma T_{*0}^3 + 2\lambda_1/\Delta h_1 + \rho(c_p + LD_g\psi_g)/r_h}. \quad (49)$$

where the fluxes in the numerator are calculated using $T_* = T_{*0}$, and

$$D_g = \left. \frac{dQ_{\text{sat}}}{dT} \right|_{T=T_{*0}} = \frac{LQ_{\text{sat}}(T_{*0})}{R_{\text{wat}}T_{*0}^2}. \quad (50)$$

Equation (49) is first evaluated with $M = 0$. If this gives $T_* > T_m$ and there is snow with ice mass I on the ground, Equation (49) is re-evaluated assuming that all of the snow melts and $M = I/\delta t$. If this gives $T_* < T_m$, the snow does not all melt and $T_* = T_m$ is known; Equation (47) is solved instead for the unknown melt rate by substitution of $T_* = T_m$ in the equations for the other fluxes.

5.2 Forest canopies and underlying ground

5.2.1 Zero-layer canopy model (option CANMOD=0)

The zero-layer canopy model does not attempt to calculate the canopy energy balance, instead assuming that the canopy temperature is equal to the air temperature. Substituting $T_v = T_a$ in Equations (40) to (45) and rearranging gives

$$H_g = \frac{\rho c_p}{r_h} (T_* - T_a) \quad (51)$$

with

$$r_h = r_{ag} + \left(\frac{1}{r_{aa}} + \frac{1}{r_{av}} \right)^{-1}. \quad (52)$$

and

$$E_g = \frac{\rho \psi_g}{r_h} (T_* - T_a) \quad (53)$$

with

$$\frac{r_h}{\psi_g} = r_{ag} + r_{sg} + \left(\frac{1}{r_{aa}} + \frac{\psi_v}{r_{av}} \right)^{-1}. \quad (54)$$

Surface temperature and melt rate are found by solving Equations (49) and (47) with the modified aerodynamic resistance and moisture factor from Equations (52) and (54) instead of Equations (31) and (39). The rate of moisture transfer from or to the canopy is

$$E_v = - \left(\frac{\psi_v r_{aa}}{\psi_v r_{aa} + r_{av}} \right) E_g. \quad (55)$$

5.2.2 One-layer canopy model (option CANMOD=1)

Energy and mass conservation equations

$$f_1 = (H - H_g - H_v)/(\rho c_p) = 0, \quad (56)$$

$$f_2 = (E - E_g - E_v)/\rho = 0, \quad (57)$$

$$f_3 = LW_g + SW_g - G - H_g - LE_g = 0, \quad (58)$$

and

$$f_4 = LW_v + SW_v - H_v - LE_v - C_{\text{can}} \frac{dT_v}{dt} = 0, \quad (59)$$

form a set of four nonlinear equations with four unknowns: Q_c , T_c , T_* and T_v . Writing vectors $\mathbf{f} = (f_1, f_2, f_3, f_4)^T$ and $\mathbf{x} = (Q_c, T_c, T_*, T_v)^T$, a solution is found by iterating

$$\mathbf{x} = \mathbf{x}_0 - \mathbf{J}^{-1} \mathbf{f}(\mathbf{x}_0) \quad (60)$$

where \mathbf{J} is the Jacobian matrix of \mathbf{f} with elements

$$J_{ij} = \frac{\partial f_i}{\partial x_j} \quad (61)$$

or

$$\mathbf{J} = \begin{bmatrix} 0 & -(r_{aa}^{-1} + r_{ag}^{-1} + r_{av}^{-1}) & r_{ag}^{-1} & r_{av}^{-1} \\ -(r_{aa}^{-1} + \psi_g r_{ag}^{-1} + \psi_v r_{av}^{-1}) & 0 & \psi_g D_g r_{ag}^{-1} & \psi_v D_v r_{av}^{-1} \\ -L\rho\psi_g r_{ag}^{-1} & -\rho c_p r_{ag}^{-1} & J_{33} & -4f_v \sigma T_v^3 \\ -L\rho\psi_v r_{av}^{-1} & -\rho c_p r_{av}^{-1} & -4f_v \sigma T_*^3 & J_{44} \end{bmatrix} \quad (62)$$

with

$$J_{33} = (c_p + L\psi_g D_g) \frac{\rho}{r_{ag}} + 4\sigma T_*^3 + 2 \frac{\lambda_1}{\Delta h_1} \quad (63)$$

and

$$J_{44} = \frac{C_{\text{can}}}{\delta t} + (c_p + L\psi_v D_v) \frac{\rho}{r_{av}} + 8f_v \sigma T_v^3 \quad (64)$$

Equation (60) is implemented by solving

$$\mathbf{J}(\mathbf{x} - \mathbf{x}_0) = \mathbf{f}(\mathbf{x}_0) \quad (65)$$

for \mathbf{x} by LU decomposition. If this gives $T_* > T_m$ and there is snow with ice mass I on the ground, Equation (58) is replaced by

$$f_3 = LW_g + SW_g - G - H_g - LE_g - L_f M. \quad (66)$$

It is first assumed that all of the snow melts and Equation (65) is solved again with $M = I/\delta t$. If this gives $T_* < T_m$, the snow does not all melt and the surface temperature is known but the melt rate is unknown. Fluxes in f are recalculated with $T_* = T_m$, elements in the third column of \mathbf{J} are replaced by $J_{13} = J_{23} = J_{43} = 0$ and $J_{33} = 1$, and $M = x_3/L_f$ is found from the solution of Equation (65).

5.2.3 Two-layer canopy model (*option to be added*)

6 Mass balance

A forest canopy can intercept a fraction of falling snow up to a maximum capacity which is either parametrized as $S_{\text{cap}} = c_{\text{vai}}\Lambda$ or read from a file. If the canopy holds snow mass S_v at the beginning of a timestep, the amount of snow intercepted in the timestep is

$$\delta S_v = (S_{\text{cap}} - S_v) \left[1 - \exp\left(-\frac{f_v S_f \delta t}{S_{\text{cap}}}\right) \right] \quad (67)$$

and the rate of snowfall reaching the ground is reduced to

$$T_f = S_f - \frac{\delta S_v}{\delta t}. \quad (68)$$

Snow sublimates from the canopy at rate E_v and unloads at rate $U_c = \tau_{\text{can}}^{-1} S_v$ with different values of the time constant τ_{can} for cold and melting snow; if $\tau_{\text{can}} \leq \delta t$, all of the snow will unload immediately from the canopy. Interception and storage of liquid water in the canopy are neglected. The combined mass balance equation for canopy snow is

$$\frac{dS_v}{dt} = S_f - T_f - U_c - E_v \quad (69)$$

If there is no forest canopy, the throughfall and unloading rates are obviously $T_f = S_f$ and $U_c = 0$. The mass balance equations for ice and liquid water in snow on the ground are

$$\frac{dI}{dt} = T_f + U_c - E_g - M + F \quad (70)$$

and

$$\frac{dW}{dt} = R_f + M - F - R_o. \quad (71)$$

If storage of liquid water in snow is neglected (option HYDROL=0), internal refreezing rate in the snow $F = 0$ and runoff rate at the base of the snow $R_o = R_f + M$. If bucket storage is selected (option HYDROL=1), snow layer k with porosity

$$\phi_k = 1 - \frac{I_k}{\rho_{\text{ice}} D_{s,k}} \quad (72)$$

can hold a maximum mass $\rho_{\text{wat}} \phi_k W_{\text{irr}}$ of liquid water.

Tables

Documentation	Code	Value
Specific heat capacity of air c_p	cp	1005 J K ⁻¹ kg ⁻¹
Specific heat capacity of ice c_{ice}	hcap_ice	2100 J K ⁻¹ kg ⁻¹
Specific heat capacity of water c_{wat}	hcap_wat	4180 J K ⁻¹ kg ⁻¹
Acceleration due to gravity g	g	9.81 m s ⁻²
Von Kármán constant k	vkman	0.4
Latent heat of fusion of water L_f	Lf	0.334×10^6 J kg ⁻¹
Latent heat of sublimation of ice L_s	Ls	2.835×10^6 J kg ⁻¹
Latent heat of vapourisation of water L_v	Lv	2.501×10^6 J kg ⁻¹
Gas constant for air R_{air}	Rair	287 J K ⁻¹ kg ⁻¹
Gas constant for water vapour R_{wat}	Rwat	462 J K ⁻¹ kg ⁻¹
Melting point of ice T_m	Tm	273.15 K
Thermal conductivity of air λ_{air}	hcon_air	0.025 W m ⁻¹ K ⁻¹
Thermal conductivity of clay λ_{clay}	hcon_clay	1.16 W m ⁻¹ K ⁻¹
Thermal conductivity of ice λ_{ice}	hcon_ice	2.24 W m ⁻¹ K ⁻¹
Thermal conductivity of sand λ_{sand}	hcon_sand	1.57 W m ⁻¹ K ⁻¹
Thermal conductivity of water λ_{wat}	hcon_wat	0.56 W m ⁻¹ K ⁻¹
Density of ice ρ_{ice}	rho_ice	917 kg m ⁻³
Density of water ρ_{wat}	rho_wat	1000 kg m ⁻³
Stefan-Boltzmann constant σ	sb	5.26×10^{-8} W m ⁻² K ⁻⁴

Table 1. Physical constants and quantities assumed to be constant in the code and documentation.

Documentation	Code	Units
Incoming longwave radiation LW_{\downarrow}	LW	W m ⁻²
Surface air pressure P_s	Ps	Pa
Specific humidity Q_a	Qa	kg kg ⁻¹
Rainfall rate R_f	Rf	kg m ⁻² s ⁻¹
Snowfall rate S_f	Sf	kg m ⁻² s ⁻¹
Incoming shortwave radiation SW_{\downarrow}	SW	W m ⁻²
Air temperature T_a	Ta	K
Wind speed U_a	Ua	m s ⁻¹

Table 2. Meteorological driving variables in the code and documentation

Documentation	Code	Units
Forest canopy		
Canopy air space specific humidity Q_c	Qcan	kg kg ⁻¹
Snow mass on canopy S_v	Sveg	W m ⁻²
Canopy air space T_c	Tveg	K
Vegetation temperature T_v	Tveg	K
Surface		
Surface skin temperature T_*	Tsrf	K
Snow on the ground (up to Nsmx layers)		
Number of snow layers N_{snow}	Nsnow	-
Thickness of snow layers D_s	Ds	m
Ice content of snow layers I	Sice	kg m ⁻²
Liquid water content of snow layers W	Sliq	kg m ⁻²
Temperature of snow layers T_s	Tsnow	K
Albedo of snow α_s	albs	-
Soil (Nsoil layers)		
Temperature of soil layers T_g	Tsoil	K
Volumetric moisture content of soil layers θ_g	theta	-

Table 3. Model state variables in the code and documentation.

Documentation	Code	Default
Snow-free albedo α_0	alb0	0.2
Canopy heat capacity C_{can}	canh	2500 Λ (J K ⁻¹ m ⁻²)
Soil clay fraction f_{clay}	fcly	0.3
Soil sand fraction f_{sand}	fsnd	0.6
Sky view fraction f_{sky}	fsky	$\exp(-k_{\text{ext}}\Lambda)$
Canopy cover fraction f_{veg}	fveg	$1 - \exp(-\Lambda)$
Canopy height h_{can}	hcan	0 m
Vegetation area index Λ	VAI	0
Snow-free ground roughness length z_{0g}	z0sf	0.1 m
Timestep δt	dt	3600 s
Temperature and humidity measurement height z_T	zT	2 m
Wind speed measurement height z_U	zU	10 m

Table 4. Site and driving data characteristics in the code and documentation.

Documentation	Code	Default
Maximum albedo for fresh snow α_{max}	asmx	0.8
Minimum albedo for melting snow α_{min}	asmn	0.5
Snow-free vegetation albedo α_{c0}	avg0	0.1
Snow-covered vegetation albedo α_{cs}	avgs	0.4
Atmospheric stability adjustment parameter b_h	bstb	5
Snow thermal conductivity exponent b_λ	bthr	2
Dense canopy turbulent transfer coefficient C_{dense}	cden	0.004
Canopy snow capacity per unit VAI c_{vai}	cvai	4.4 kg m ⁻²
Vegetation turbulent transfer coefficient C_{veg}	cveg	20
Snow cover fraction depth scale h_f	hfsn	0.1 m
Reference snow viscosity η_0	eta0	3.7×10^7 Pa s
Snow viscosity parameter η_a	etaa	0.081 K ⁻¹
Snow viscosity parameter η_b	etab	0.018 m ³ kg ⁻¹
Surface conductance for saturated soil g_{sat}	gsat	0.01 m s ⁻¹
Canopy radiation extinction coefficient k_{ext}	kext	0.5
Fixed snow thermal conductivity λ_0	kfix	0.24 W m ⁻¹ K ⁻¹
Displacement height to canopy height ratio R_d	rchd	0.67
Roughness length to canopy height ratio R_{z0}	rchz	0.1
Fixed snow density ρ_0	rho0	300 kg m ⁻³
Critical snow density ρ_c	rhoc	150 kg m ⁻³
Fresh snow density ρ_f	rhof	100 kg m ⁻³
Maximum density for cold snow ρ_{cold}	rcld	300 kg m ⁻³
Maximum density for melting snow ρ_{melt}	rmlt	500 kg m ⁻³
Snowfall to refresh albedo S_α	Salb	10 kg m ⁻²
Snow densification parameter d_a	snda	2.8×10^{-6} s ⁻¹
Snow densification parameter d_b	sndb	0.042 K ⁻¹
Snow densification parameter d_c	sndc	0.046 m ³ kg ⁻¹
Snow albedo decay temperature threshold T_α	Talb	-2°C
Canopy unloading time scale τ_{can} for cold snow	tcnc	240 h
Canopy unloading time scale τ_{can} for melting snow	tcnm	2.4 h
Cold snow albedo decay time scale τ_{cold}	tcld	1000 h
Melting snow albedo decay time scale τ_{melt}	tmlt	100 h
Snow compaction time scale τ_ρ	trho	200 h
Irreducible liquid water content of snow W_{irr}	Wirr	0.03
Ratio of roughness lengths for momentum and heat z_0/z_{0h}	z0zh	10
Snow surface roughness length z_{0s}	z0sn	0.01 m

Table 5. Model parameters in the code and documentation.