

Definitions

- Adiabatic Process** A process in which no heat transfer occurs
- Isothermal** All points on a surface are the same temperature
- Diffuse** No preferred direction for outgoing rays
- Specular** Preferred direction for outgoing rays
- Black Body** Perfect Emitter and Absorber ( $\epsilon = 1, \alpha = 1$ )
- Gray Body** Properties are independent of wavelength
- Radiance (G)** Flux of energy that irradiates a surface
- Radiosity (J)** total flux of radiative energy away from a surface
- Reflectivity ( $\rho$ )** How much of the irradiance is reflected
- Absorptibity ( $\alpha$ )** How much of the irradiance is absorbed
- Transmissivity ( $\tau$ )** How much of the irradiance passes through the material

When Assumptions Can Be Made

- Steady State:
- 1D Conduction: When conduction is significant in only a single direction
- $\tau = 0$ : material is opaque or thick ( $>1$  wavelength of light)

Governing Equation

$$E_{\text{in}} - E_{\text{out}} + E_{\text{gen}} = E_{\text{st}}$$

Conduction

Heat Diffusion Equation

Cartesian Coordinates:

$$\frac{\partial}{\partial x}\left(k\frac{\partial T}{\partial x}\right) + \frac{\partial}{\partial y}\left(k\frac{\partial T}{\partial y}\right) + \frac{\partial}{\partial z}\left(k\frac{\partial T}{\partial z}\right) + \dot{q}''' = \rho c_p \frac{\partial T}{\partial t}$$

Cylindrical Coordinates:

$$\frac{1}{r}\frac{\partial}{\partial r}\left(kr\frac{\partial T}{\partial r}\right) + \frac{1}{r^2}\frac{\partial}{\partial \phi}\left(k\frac{\partial T}{\partial \phi}\right) + \frac{\partial}{\partial z}\left(k\frac{\partial T}{\partial z}\right) + \dot{q}''' = \rho c_p \frac{\partial T}{\partial t}$$

Spherical Coordinates:

$$\frac{1}{r^2}\frac{\partial}{\partial r}\left(kr^2\frac{\partial T}{\partial r}\right) + \frac{1}{r^2\sin^2(\theta)}\frac{\partial}{\partial \phi}\left(k\frac{\partial T}{\partial \phi}\right) + \frac{1}{r^2\sin(\theta)}\frac{\partial}{\partial \theta}\left(k\sin\theta\frac{\partial T}{\partial \theta}\right) + \dot{q}''' = \rho c_p \frac{\partial T}{\partial t}$$

Boundary Conditions

- Constant Surface Temperature:  $T(0, t) = T_s$
- Constant Surface Heat Flux
  - Finite Heat Flux:  $-k\frac{\partial T}{\partial x}|_{x=0} = q_s''$
  - Adiabatic or Insulated Surface:  $-k\frac{\partial T}{\partial x}|_{x=0} = 0$
- Convection Surface Condition:  $-k\frac{\partial T}{\partial x}|_{x=0} = h[T_\infty - T(0, t)]$

Thermal Diffusivity

The ratio of how a material conducts thermal energy to how well it stores thermal energy.

$$\alpha = \frac{k}{\rho c_p}$$

Circuit Analogy

Cartesian Coordinates:

$$R_{\text{cond}} = \frac{L}{kA_s}$$

Cylindrical Coordinates:

$$R_{\text{cond}} = \frac{\ln\left(\frac{r_2}{r_1}\right)}{2\pi kL}$$

Spherical Coordinates:

$$R_{\text{cond}} = \frac{1}{4\pi k}\left(\frac{1}{r_1} - \frac{1}{r_2}\right)$$

Overall Heat Transfer Coefficient

Used for composite materials such as walls with different materials.

$$U = \frac{1}{R_{\text{tot}}A_s}$$

Contact Resistance

To account for gaps due to surface roughness between mating surfaces.

$$R_{\text{tc}}'' = \frac{T_A - T_B}{q_x''}$$

Porous Materials

These materials have pockets of liquid which greatly affects the thermal conductivity, so the average thermal conductivity is used to ease the calculates called  $k_{\text{eff}}$ .

Porosity (void fraction):  $\epsilon$  Fluid Thermal Conductivity:  $k_f$  Solid Thermal Conductivity:  $k_s$

$$k_{\text{eff,min}} = \frac{1}{\frac{1-\epsilon}{k_s} + \frac{\epsilon}{k_f}}$$

$$k_{\text{eff,max}} = \epsilon k_f + (1 - \epsilon)k_s$$

$$k_{\text{eff}} = \left[\frac{k_f + 2k_s - 2\epsilon(k_s - k_f)}{k_f + 2k_s + \epsilon(k_s - k_f)}\right]k_s$$

Fins (Extended Surfaces)

(Page 118 has table of fin efficiencies for various shapes Basic Heat and Mass Transfer)

$$m = \left(\frac{hP}{kA_c}\right)^{\frac{1}{2}} = \left(\frac{2h}{kt}\right)^{\frac{1}{2}} = \left(\frac{4h}{kD}\right)^{\frac{1}{2}}$$

Fin Effectiveness:

$$\epsilon_f = \left(\frac{kP}{hA_c}\right)^{\frac{1}{2}}$$

Fin Efficiency:

$$\eta_f = \frac{\tanh(mL)}{mL}$$

Resistance:

$$R_{t,f} = \frac{1}{hA_f\eta_f}$$

Transient Conduction

Biot Number

Ratio of thermal resistances between conduction and convection. If  $\text{Bi} \ll 1$  then the conduction resistance is much less than the convective resistance and it is safe to assume uniform temperature distribution.

$$\text{Bi} \equiv \frac{\bar{h}L}{k}$$

Fourier Number

Dimensionless Time

$$\text{Fo} \equiv \frac{\alpha t}{L_c^2}$$

Lumped Thermal Capacitance

Condition:  $\text{Bi} < 0.1$  (error associated with method is negligible)

$$\frac{\theta}{\theta_i} = \frac{T - T_\infty}{T_i - T_\infty} = \exp(-\text{Bi} \cdot \text{Fo})$$

Problem-Solving Strategy

(Page 209 Basic Heat and Mass Transfer)

- Calculate  $\text{Bi}$  and if  $\text{Bi} < 0.1$  then use Lumped Thermal Capacitance
- Calculate Fourier Number. If  $\text{Fo} < 0.05$  then Eqn 3.61 (pg. 194)
- Calculate Fourier Number. If  $0.05 < \text{Fo} < 0.2$  then Eqn 3.72 and 3.73 (pg. 205)
- Calculate Fourier Number. If  $\text{Fo} > 0.2$  then Eqn 3.75 - 3.77 (pg. 206)

Convection

Reynold's Number

$$\text{Re}_x = \frac{\rho u_\infty x}{\mu} = \frac{u_\infty x}{\nu}$$

Nusselt Number

$$\text{Nu} \equiv \frac{hL}{k_f}$$

Flat plate in Laminar Flow:

$$\text{Nu} = 0.664\text{Re}_L^{\frac{1}{2}}\text{Pr}^{\frac{1}{3}}$$

Prandtl Number

$$\text{Pr} \equiv \frac{\nu}{k}$$

Convective Heat Transfer Coefficient

$$h = -\frac{k}{T_w - T_\infty}\frac{\partial T}{\partial y}\Big|_{y=0}$$

Radiation

Stefan-Boltzmann Law

$$dq = dU + PdV$$

Energy Density ( $\epsilon$ )

Internal Energy ( $U$ ) =  $\epsilon V$

Pressure ( $P$ ) =  $\frac{1}{3}\epsilon$

Spectral Energy Density

$$E(\lambda) = \frac{k_B T}{\lambda^4}$$

$$E(f) = \frac{k_B T}{c^3}f^3$$

Boltzmann Const ( $k_B$ ) =  $1.38 \times 10^{-23} \frac{\text{J}}{\text{K}}$

Total Radiative Energy

$$E = \int_0^\infty E(\lambda)d\lambda = \int_0^\infty E(f)df$$

Emissivity (Emittance)

The fraction of emissive power a real body ( $E(T)$ ) emits compared to a black body ( $E_b(T)$ ).

$$\epsilon \equiv \frac{E(T)}{E_b(T)}$$

Emissive Power

$$E(T) = \epsilon \sigma_{\text{SB}}T^4$$

Kirchoff's Law

A body in thermodynamic equilibrium must emit as much energy as it absorbs in each direction at each wavelength. This is to avoid violating the 2nd Law of Thermodynamics.

$$\epsilon_\lambda(T, \theta, \phi) = \alpha_\lambda(T, \theta, \phi)$$

Diffuse Form:

$$\epsilon_\lambda(T) = \alpha_\lambda(T)$$

Diffuse and Gray Form:

$$\epsilon(T) = \alpha(T)$$

Wiens Displacement Relation

$$\lambda_{\text{peak}}T = \text{const} = 2898\mu\text{m}K$$

View Factors

The view factor is a correction to the Stefan-Boltzmann constant for black bodies. The view factor is a function of the surface area of two materials, the angle between the normals of each surface and the ray of radiation ( $\beta_1, \beta_2$ ), and the distance between the two surfaces. (See page 561 in AHTT for table of view factors)

$$F_{1-2} = \frac{1}{A_1}\int_{A_1}\int_{A_2}\frac{\cos(\beta_1)\cos(\beta_2)}{\pi s^2}dA_2dA_1$$

$$Q_{\text{net}(1-2)} = A_1F_{1-2}\sigma_{\text{SB}}(T_1^4 - T_2^4)$$

$$A_1F_{1-2} = A_2F_{2-1}$$

Irradiance

The flux of energy that irradiates a surface.

$$\rho + \alpha + \tau = 1$$

Radiosity

The total flux of radiative energy away from a surface.

$$J = E + \rho G = \epsilon E_b + \rho G$$

Circuit Analogy

Surface Resistance for a diffuse, gray surface:

$$R_{\text{surf}} = \frac{1 - \epsilon}{\epsilon A}$$

Geometrical Resistance for a diffuse, gray surface:

$$R_{\text{geo}} = \frac{1}{A_1F_{1-2}}$$

Total Heat Flux between two diffuse, gray surfaces:

$$Q_{\text{net}1-2} = \frac{\sigma_{\text{SB}}(T_1^4 - T_2^4)}{R_{\text{surf}1} + R_{\text{geo}1-2} + R_{\text{surf}2}}$$

Heat Pipes

$$L_c = \frac{V}{A_s}$$

General Equations of Usefulness

Hyperbolic Functions

$$\sinh x = \frac{e^x - e^{-x}}{2}$$

$$\cosh x = \frac{e^x + e^{-x}}{2}$$

$$\tanh x = \frac{e^x - e^{-x}}{e^x + e^{-x}}$$

Surface Area of a Sphere

$$A_s = 4\pi r^2$$

Volume of a Sphere

$$V = \frac{4}{3}\pi r^3$$

Surface Area of a Cylinder

$$A_s = 2\pi rh$$

Volume of a Cylinder

$$V = \pi r^2h$$

Error Function

$$\text{erf}(\eta) = \left(\frac{2}{\pi^{\frac{1}{2}}}\right)\int_0^\eta e^{-u^2}du$$

Complimentary Error Function:

$$\text{erfc}(\eta) = 1 - \text{erf}(\eta)$$