## Velocity Kinematics

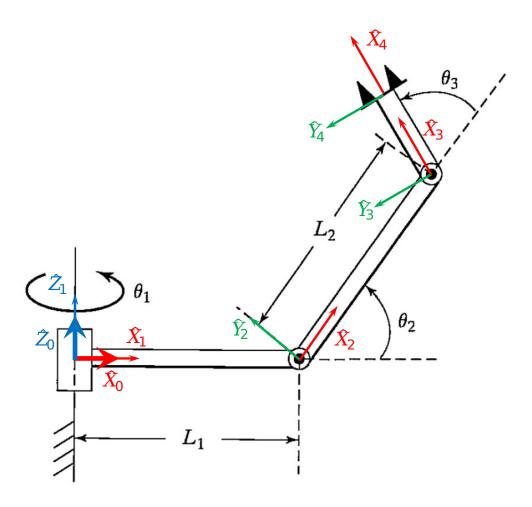


Figure 1: Link frame assignment.

Figure 1 illustrates an RRR manipulator with assigned link frames. Listing 1 provides MATLAB code to derive the transformation matrices from the DH parameters shown in Table 1. We will derive  $^4J(\Theta)$  through three different methods: velocity propagation from the base to the tip, static force propagation from the tip to the base, and direct differentiation of the kinematic equations.

$\overline{i}$	$\alpha_{i-1}$	$a_{i-1}$	$d_i$	$\theta_i$
1	0°	0	0	$\theta_1$
2	90°	$L_1$	0	$ heta_2$
3	0°	$L_2$	0	$\theta_3$
4	0°	$L_3$	0	$0^{\circ}$

Table 1: DH Parameters.

Listing 1: Transform matrices. Source code for link\_transform is provided in Listing 5 (Supplementary Material).

### 1 Velocity propagation from base to tip

To compute the velocity propagation through the manipulator, we start by defining the conditions at the base:

$$^{0}v_{0} = \begin{bmatrix} 0 & 0 & 0 \end{bmatrix}^{T} \tag{1}$$

$${}^{0}\omega_{0} = \begin{bmatrix} 0 & 0 & 0 \end{bmatrix}^{T} \tag{2}$$

The velocity propagation from frame i to i + 1 is defined by:

$${}^{i+1}v_{i+1} = {}^{i+1}R \left( {}^{i}v_{i} + {}^{i}\omega_{i} \times {}^{i}P_{i+1} \right)$$
(3)

$$^{i+1}\omega_{i+1} = {}_{i}^{i+1}R^{i}\omega_{i} + \dot{\theta}_{i+1}^{i+1}\hat{Z}_{i+1}$$

$$\tag{4}$$

These equations are iteratively applied from the base to the end-effector. Finally, the Jacobian,  ${}^4J(\Theta)$ , maps the joint velocities into the Cartesian velocity of the end-effector:

$${}^{4}v_{4} = {}^{4}J(\Theta)\dot{\Theta} \tag{5}$$

Thus, the Jacobian matrix  ${}^4J(\Theta)$  is obtained as follows:

$${}^{4}v_{4} = \begin{bmatrix} L_{2}s_{3}\dot{\theta}_{2} \\ L_{2}c_{3}\dot{\theta}_{2} + L_{3}(\dot{\theta}_{2} + \dot{\theta}_{3}) \\ -(L_{1} + L_{2}c_{2} + L_{3}c_{23})\dot{\theta}_{1} \end{bmatrix} = {}^{4}J(\Theta) \begin{bmatrix} \dot{\theta}_{1} \\ \dot{\theta}_{2} \\ \dot{\theta}_{3} \end{bmatrix}$$

$${}^{4}J(\Theta) = \begin{bmatrix} 0 & L_{2}s_{3} & 0\\ 0 & L_{2}c_{3} + L_{3} & L_{3}\\ -(L_{1} + L_{2}c_{2} + L_{3}c_{23}) & 0 & 0 \end{bmatrix}$$

The MATLAB code for this process is provided in Listing 2.

```
syms dth1 dth2 dth3
   dth = [dth1; dth2; dth3; 0];
   v = [0; 0; 0]; w = [0; 0; 0]; Z = [0; 0; 1];
6
       R = T(1:3, 1:3, i).';
       P = T(1:3, 4, i);
9
       v = R * (v + cross(w, P));
10
       w = R * w + dth(i) * Z;
11
12
13
  J1 = jacobian(v, dth(1:3));
14
  J1 = simplify(J1)
```

Listing 2: Velocity propagation from base to tip.

#### 2 Static force propagation from tip to base

To compute the static force propagation through the manipulator, we start by defining the conditions at the tip:

$$^{4}f_{4} = \begin{bmatrix} f_{x} & f_{y} & f_{z} \end{bmatrix}^{T} \tag{6}$$

$$^{4}n_{4} = \begin{bmatrix} 0 & 0 & 0 \end{bmatrix}^{T} \tag{7}$$

The static force propagation from frame i + 1 to i is defined by:

$${}^{i}f_{i} = {}^{i}_{i+1}R^{i+1}f_{i+1} \tag{8}$$

$${}^{i}n_{i} = {}^{i}_{i+1}R^{i+1}n_{i+1} + {}^{i}P_{i+1} \times {}^{i}f_{i}$$

$$(9)$$

$$\tau_i = {}^i n_i^T \, {}^i \hat{Z}_i \tag{10}$$

These equations are iteratively applied from the end-effector to the base. Finally, the transpose of the Jacobian matrix,  ${}^4J^T(\Theta)$ , maps the Cartesian forces acting at the end-effector into the equivalent joint torques:

$$\tau = {}^4J^T(\Theta)\,{}^4f_4\tag{11}$$

Thus, the Jacobian matrix  ${}^4J(\Theta)$  is obtained as follows:

$$\tau = \begin{bmatrix} -(L_1 + L_2c_2 + L_3c_{23})f_z \\ L_2(s_3f_x + c_3f_y) + L_3f_y \\ L_3f_y \end{bmatrix} = {}^4J^T(\Theta) \begin{bmatrix} f_x \\ f_y \\ f_z \end{bmatrix}$$

$${}^{4}J(\Theta) = \begin{bmatrix} 0 & L_{2}s_{3} & 0\\ 0 & L_{2}c_{3} + L_{3} & L_{3}\\ -(L_{1} + L_{2}c_{2} + L_{3}c_{23}) & 0 & 0 \end{bmatrix}$$

The MATLAB code for this process is provided in Listing 3.

```
syms fx fy fz
  f = [fx; fy; fz];
   t = sym(zeros(N, 1)); n = [0; 0; 0]; Z = [0; 0; 1];
6
   for i = N:-1:1
       R = T(1:3, 1:3, i);
       P = T(1:3, 4, i);
9
       f = R * f;
10
       n = R * n + cross(P, f);
11
       t(i) = n.' * Z;
12
   end
13
14
  J2 = jacobian(t(N-2:N), [fx; fy; fz]).';
  J2 = simplify(J2)
```

Listing 3: Static force propagation from tip to base.

#### 3 Direct differentiation of kinematic equations

To derive the Jacobian through direct differentiation, we start by calculating the partial derivatives of the end-effector's position with respect to the joint angles:

$${}^{0}J(\Theta) = \frac{\partial ({}^{0}P_{4})}{\partial \Theta} \tag{12}$$

This results in the Jacobian expressed in the base frame. To transform this Jacobian into the end-effector frame, we apply the rotation matrix:

$$^{4}J(\Theta) = {}_{0}^{4}R^{0}J(\Theta) \tag{13}$$

Thus, the Jacobian matrix  ${}^4J(\Theta)$  is obtained as follows:

$${}_{0}^{4}R = \begin{bmatrix} c_{1}c_{23} & s_{1}c_{23} & s_{23} \\ -c_{1}s_{23} & -s_{1}s_{23} & c_{23} \\ s_{1} & -c_{1} & 0 \end{bmatrix}$$

$${}^{0}J(\Theta) = \begin{bmatrix} -s_{1}(L_{1} + L_{2}c_{2} + L_{3}c_{23}) & -c_{1}(L_{2}s_{2} + L_{3}s_{23}) & -L_{3}c_{1}s_{23} \\ c_{1}(L_{1} + L_{2}c_{2} + L_{3}c_{23}) & -s_{1}(L_{2}s_{2} + L_{3}s_{23}) & -L_{3}s_{1}s_{23} \\ 0 & L_{2}c_{2} + L_{3}c_{23} & L_{3}c_{23} \end{bmatrix}$$

$${}^{4}J(\Theta) = \begin{bmatrix} 0 & L_{2}s_{3} & 0\\ 0 & L_{2}c_{3} + L_{3} & L_{3}\\ -(L_{1} + L_{2}c_{2} + L_{3}c_{23}) & 0 & 0 \end{bmatrix}$$

The MATLAB code for this process is provided in Listing 4.

```
1 R = eye(3); P = [0; 0; 0; 1];
2
3 for i = N:-1:1
4     R = R * T(1:3, 1:3, i).';
5     P = T(:, :, i) * P;
6 end
7
8 J3 = R * jacobian(P(1:3), [th1 th2 th3]);
9 J3 = simplify(J3)
```

Listing 4: Direct differentiation of kinematic equations.

# Supplementary Material

```
function T = link_transform(DH)
       N = size(DH, 1);
2
       T = sym(zeros(4, 4, N));
3
       for i = 1:N
            screw_X = [
6
                1 0 0 DH(i,2);
                0 cos(DH(i,1)) -sin(DH(i,1)) 0;
                0 sin(DH(i,1)) cos(DH(i,1)) 0;
                0 0 0 1
10
                ];
11
12
            screw_Z = [
13
                cos(DH(i,4)) - sin(DH(i,4)) 0 0;
14
                sin(DH(i,4)) cos(DH(i,4)) 0 0;
                0 0 1 DH(i,3);
16
                0 0 0 1
17
                ];
18
19
            T(:, :, i) = screw_X * screw_Z;
20
21
       end
   end
22
```

Listing 5: Derives transformation matrices using DH parameters.

```
clear; clc;
   syms th1 th2 th3 L1 L2 L3
3
   DH = [
       0
            0
                  0
                       th1;
       pi/2 L1
                  0
                       th2;
       0
            L2
                0
                       th3;
8
       0
            L3
                       0
9
       ];
11
  T = link_transform(DH);
12
  |N = size(T, 3);
13
14
   %% Velocity Propagation from Base to Tip
15
16
   syms dth1 dth2 dth3
17
18
19 dth = [dth1; dth2; dth3; 0];
20
```

```
v = [0; 0; 0]; w = [0; 0; 0]; Z = [0; 0; 1];
21
22
   for i = 1:N
23
       R = T(1:3, 1:3, i).';
24
       P = T(1:3, 4, i);
25
       v = R * (v + cross(w, P));
26
       w = R * w + dth(i) * Z;
27
28
   end
29
   J1 = jacobian(v, dth(1:3));
30
   J1 = simplify(J1)
31
32
   %% Static Force Propagation from Tip to Base
33
34
   syms fx fy fz
35
36
   f = [fx; fy; fz];
37
   t = sym(zeros(N, 1)); n = [0; 0; 0]; Z = [0; 0; 1];
39
40
   for i = N:-1:1
41
       R = T(1:3, 1:3, i);
42
       P = T(1:3, 4, i);
43
       f = R * f;
44
       n = R * n + cross(P, f);
45
       t(i) = n.' * Z;
46
47
48
   J2 = jacobian(t(N-2:N), [fx; fy; fz]).';
49
   J2 = simplify(J2)
51
   %% Direct Differentiation of the Kinematic Equations
52
53
   R = eye(3); P = [0; 0; 0; 1];
54
55
   for i = N:-1:1
56
       R = R * T(1:3, 1:3, i).';
57
       P = T(:, :, i) * P;
58
   end
59
60
   J3 = R * jacobian(P(1:3), [th1 th2 th3]);
61
   J3 = simplify(J3)
```

Listing 6: Complete source code.