Computer Animation & Physical Simulation

Lecture 8: Soft-Body Simulation – Hair I

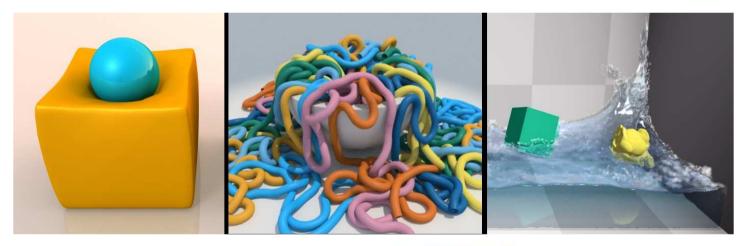
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What is a soft body?

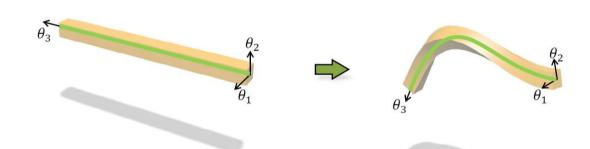
Unlike rigid body

- Shape of soft bodies can change visually
- The relative distance of two points on the object is not fixed



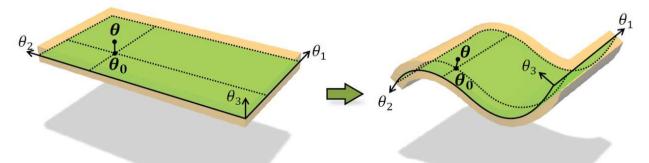
Type of Soft Body

- 1D soft body rod
 - A volumetric curve-like solid
 - Extent along tangent direction is much greater than along normal directions



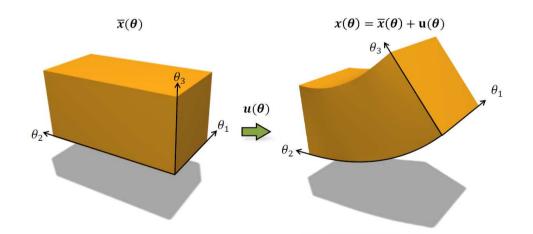
Type of Soft Body

- 2D soft body (thin) shell
 - A volumetric surface-like solid
 - Extent along tangent plan directions is much greater than along normal direction



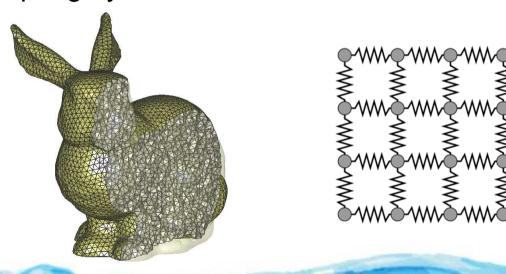
Type of Soft Body

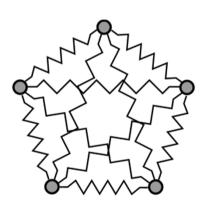
- 3D soft body (volumetric) solid
 - A volumetric body
 - No dominance on extension along specific directions



How to simulate soft body motion?

- Mass-spring system
 - Represent the solid with meshes
 - Apply spring dynamics to each mesh element

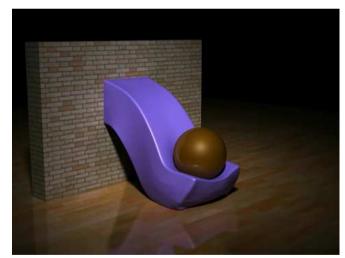


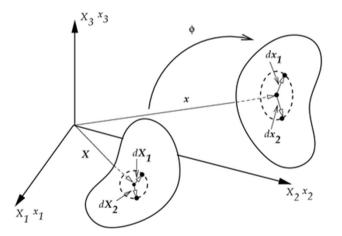


How to simulate soft body motion?

Continuum mechanics

- The substance is assumed to be continuously distributed
- Strain and stress relation through constitutive laws





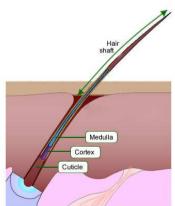
I. Hair Basics

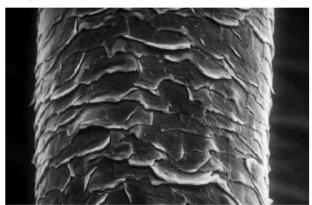


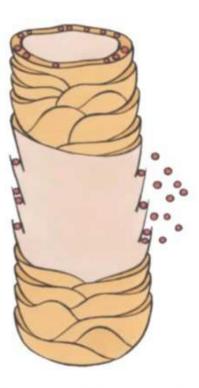
Structure of Hair

Close look of hair strand

- Hair fiber is a thin structure (0.1mm in diameter)
- Circular or oval cross section
- Different frictions along different directions







Physical Property of Hair

- Nonlinear dynamics
 - Bending and twisting instabilities



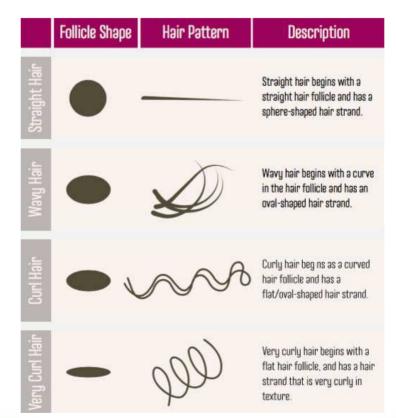
Physical Property of Hair

Different hair style

- Circular cross section: straight hair
- Oval cross section: curly hair







Hair Representation

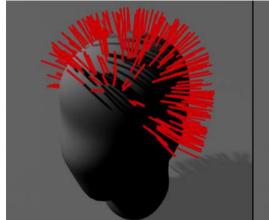
- Full representation
 - Each hair strand is represented explicitly by curves

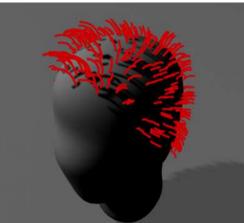


Hair Representation

- Clustered representation
 - The hair is represented by guide strands
 - Coherence between guide strands



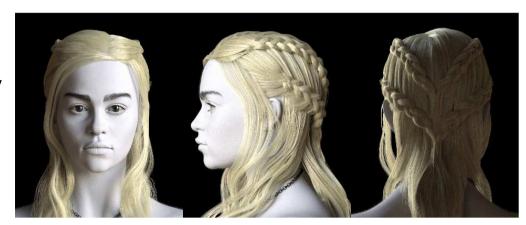




Hair Modeling

Geometric modeling

- Representing the hair geometry
- Hair styling (NURBS)



Physical modeling

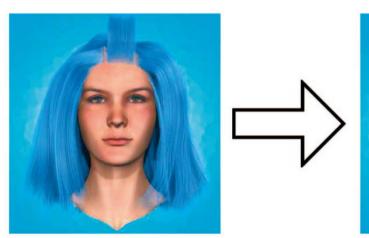
- No mature physical model
- Empirical construction
 - With physical arguments

$$\frac{\mathrm{d}}{\mathrm{d}t} \left(\frac{\partial T}{\partial \dot{q}_{iQ}} \right) - \frac{\partial T}{\partial q_{iQ}} + \frac{\partial U}{\partial q_{iQ}} + \frac{\partial D}{\partial \dot{q}_{iQ}} = \int_0^L \mathbf{J}_{iQ}(s, \mathbf{q}, t) \cdot \mathbf{F}(s, t) \, \mathrm{d}s$$

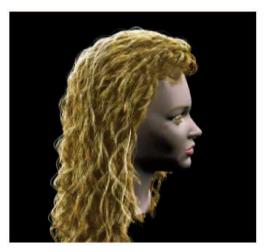
Super-Helix hair model

Hair Styling

- Creating a desired hairstyle
 - Purely geometric and physically-based









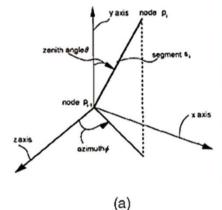
Hair Simulation

- Simulate the motion of hair
 - Given initial hair geometry (from modeling)
 - Based on a chosen physical model
 - Possibly interact with hair itself, other solids and fluids



Early Simulation Methods

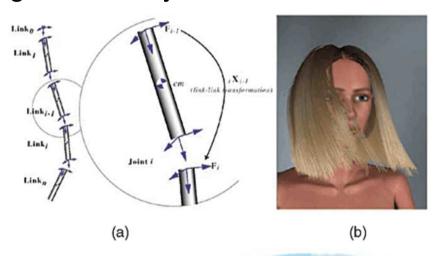
- One-dimensional projective equations
 - A chain of rigid sticks
 - Each stick is assimilated as a direction
 - Parameterized by its polar angles





Early Simulation Methods

- Rigid multi-body serial chain
 - Represented as a serial, rigid, multibody open chain
 - · Limited to straight hair, curly hair is not modeled



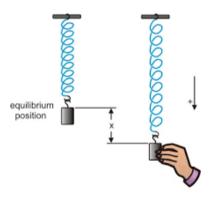
II. Mass-Spring System for Hair Simulation

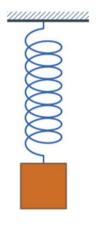
Mass-Spring Model

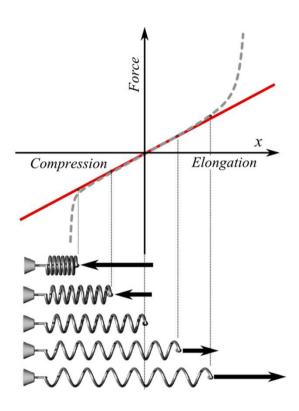
Linear elastic model

- The spring is connected to a non-negligible mass m
- Hook's law

$$ec{F}=-kec{x}$$







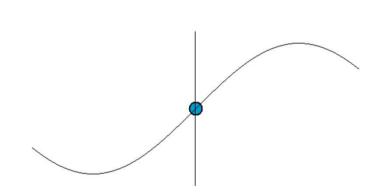
Mass-Spring Model

- Harmonic oscillator
 - Without damping

$$F=ma=mrac{\mathrm{d}^2x}{\mathrm{d}t^2}=m\ddot{x}=-kx$$

Analytical solution

$$x(t) = A\cos(\omega t + \phi)$$



Mass-Spring Model

Harmonic oscillator

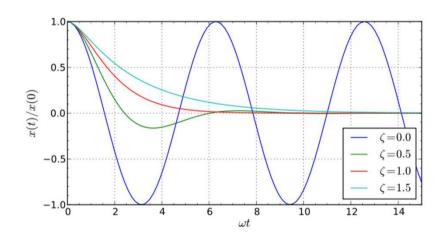
With damping

$$rac{\mathrm{d}^2x}{\mathrm{d}t^2} + 2\zeta\omega_0rac{\mathrm{d}x}{\mathrm{d}t} + \omega_0^2x = 0,$$

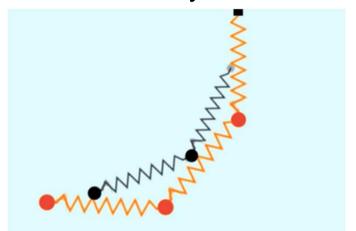
where

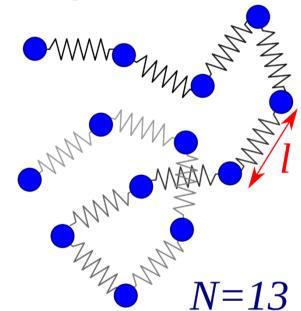
$$\omega_0=\sqrt{rac{k}{m}}$$
 is called the 'undamped angular frequency of the oscillator' and $c=rac{c}{m}$ is called the 'damping ratio'

$$\zeta = rac{c}{2\sqrt{mk}}$$
 is called the 'damping ratio'.



- A system of mass objects connected by springs
 - An object is modeled as point masses
 - Objects are connected by one or more springs





- Governing dynamic equation
 - Using linear spring model
 - With linear damping

$$m_i \ddot{\mathbf{x}}_i = -\gamma_i \dot{\mathbf{x}}_i + \sum_j \mathbf{g}_{ij} + \mathbf{f}_i$$

 \mathbf{g}_{ij} : forces exerted on mass i by spring between masses i and j

Governing dynamic equation

Writing the equation for entire system

$$M\ddot{x} + C\dot{x} + Kx = f$$

M: mass matrix, diagonal

C: damping matrix, diagonal

K: stiffness matrix, encodes spring forces from nearby connected springs

Re-expression in first-order system

$$\dot{\mathbf{v}} = \mathbf{M}^{-1} \left(-\mathbf{C}\mathbf{v} - \mathbf{K}\mathbf{x} + \mathbf{f} \right)$$

$$\dot{\mathbf{x}} = \mathbf{v}$$

velocity of mass point

- Numerical solution
 - Explicit Euler time discretization

$$\frac{d}{dt} \begin{pmatrix} \mathbf{x} \\ \dot{\mathbf{x}} \end{pmatrix} = \frac{d}{dt} \begin{pmatrix} \mathbf{x} \\ \mathbf{v} \end{pmatrix} = \begin{pmatrix} \mathbf{v} \\ \mathbf{M}^{-1} \mathbf{f}(\mathbf{x}, \mathbf{v}) \end{pmatrix}$$

$$\mathbf{x}_0 = \mathbf{x}(t_0)$$
 and $\mathbf{v}_0 = \mathbf{v}(t_0)$ $\Delta \mathbf{x} = \mathbf{x}(t_0 + h) - \mathbf{x}(t_0)$ and $\Delta \mathbf{v} = \mathbf{v}(t_0 + h) - \mathbf{v}(t_0)$

$$\left(\begin{array}{c} \Delta \mathbf{x} \\ \Delta \mathbf{v} \end{array}\right) = h \left(\begin{array}{c} \mathbf{v_0} \\ \mathbf{M}^{-1} \mathbf{f_0} \end{array}\right)$$

Numerical solution

- Implicit Euler discretization
- Linearize

$$\frac{d}{dt}\begin{pmatrix} \mathbf{x} \\ \dot{\mathbf{x}} \end{pmatrix} = \frac{d}{dt}\begin{pmatrix} \mathbf{x} \\ \mathbf{v} \end{pmatrix} = \begin{pmatrix} \mathbf{v} \\ \mathbf{M}^{-1}\mathbf{f}(\mathbf{x}, \mathbf{v}) \end{pmatrix}$$

$$\begin{pmatrix} \Delta \mathbf{x} \\ \Delta \mathbf{v} \end{pmatrix} = h\begin{pmatrix} \mathbf{v}_0 + \Delta \mathbf{v} \\ \mathbf{M}^{-1}\mathbf{f}(\mathbf{x}_0 + \Delta \mathbf{x}, \mathbf{v}_0 + \Delta \mathbf{v}) \end{pmatrix}$$

$$\mathbf{f}(\mathbf{x}_0 + \Delta \mathbf{x}, \mathbf{v}_0 + \Delta \mathbf{v})$$

$$\begin{pmatrix} \Delta \mathbf{x} \\ \Delta \mathbf{v} \end{pmatrix} = h\begin{pmatrix} \mathbf{v}_0 + \Delta \mathbf{v} \\ \mathbf{M}^{-1}(\mathbf{f}_0 + \frac{\partial \mathbf{f}}{\partial \mathbf{x}} \Delta \mathbf{x} + \frac{\partial \mathbf{f}}{\partial \mathbf{v}} \Delta \mathbf{v}) \end{pmatrix}$$

$$\Delta \mathbf{v} = h\mathbf{M}^{-1}\begin{pmatrix} \mathbf{f}_0 + \frac{\partial \mathbf{f}}{\partial \mathbf{x}} h(\mathbf{v}_0 + \Delta \mathbf{v}) + \frac{\partial \mathbf{f}}{\partial \mathbf{v}} \Delta \mathbf{v} \end{pmatrix}$$

Numerical solution

- Implicit Euler discretization
- Regrouping

$$\Delta \mathbf{v} = h\mathbf{M}^{-1} \left(\mathbf{f_0} + \frac{\partial \mathbf{f}}{\partial \mathbf{x}} h(\mathbf{v_0} + \Delta \mathbf{v}) + \frac{\partial \mathbf{f}}{\partial \mathbf{v}} \Delta \mathbf{v} \right)$$

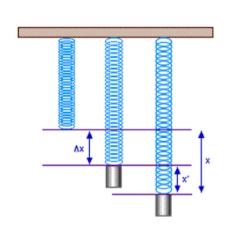


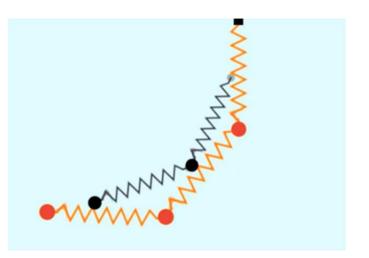
$$\left(\mathbf{I} - h\mathbf{M}^{-1} \frac{\partial \mathbf{f}}{\partial \mathbf{v}} - h^2 \mathbf{M}^{-1} \frac{\partial \mathbf{f}}{\partial \mathbf{x}}\right) \Delta \mathbf{v} = h\mathbf{M}^{-1} \left(\mathbf{f_0} + h \frac{\partial \mathbf{f}}{\partial \mathbf{x}} \mathbf{v_0}\right)$$

- We then solve for Δv (sparse linear system, conjugate gradient)
- Given $\Delta \mathbf{v}$, we then compute $\Delta \mathbf{x} = h(\mathbf{v_0} + \Delta \mathbf{v})$

Stretching force

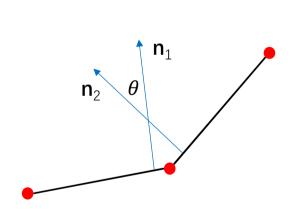
• Based on the length difference w.r.t rest shape

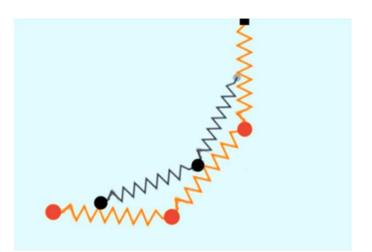




Bending force

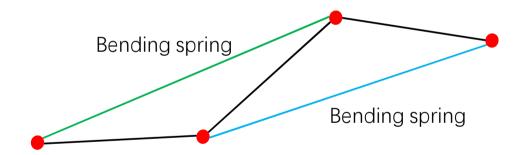
Based on the angle between adjacent normals of segments





Bending force

Place bending strings across a mass point



Problem

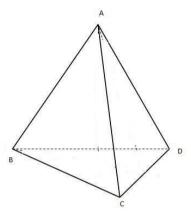
- · Some nonlinear behaviors cannot be handled
- Twisting



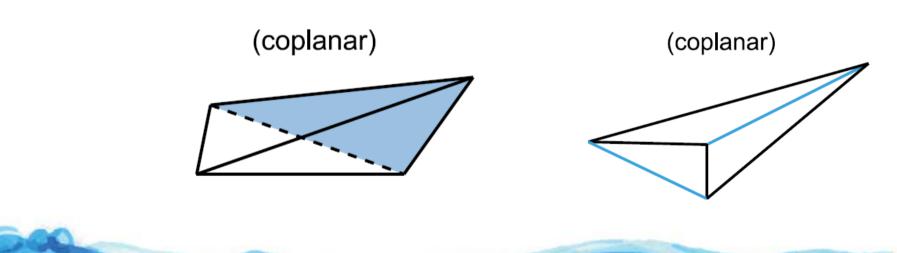
- Mass-spring system applied to solids
 - Tetrahedral mesh





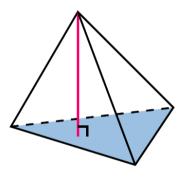


- Problem with volumetric simulations
 - Tetrahedron may collapse to zero volume
 - For both mass-spring and finite-element simulations

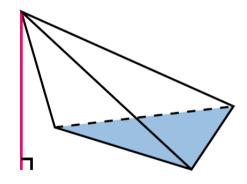


Point-face altitude spring

 Between each particle of the tetrahedron and a virtual node projected onto the plane of the opposite face



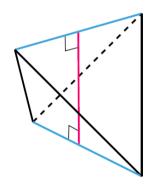
(a) Spring has all non-negative barycentric weights



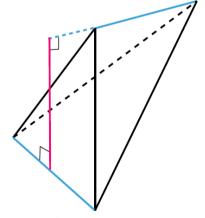
(b) Spring has negative barycentric weights

- Equal and opposite forces are applied to both the particle and the virtual node;
- The virtual node distributes its force barycentrically to the particles of the face

- Edge-edge altitude spring
 - Mutually orthogonal to the two lines containing the edges



(d) Spring has all non-negative barycentric weights

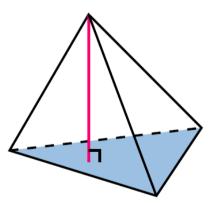


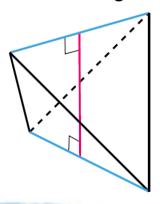
(e) Spring has negative barycentric weights

 The barycentric weights can also be negative if the virtual nodes are not on the segment

Fortunately, for any tetrahedron

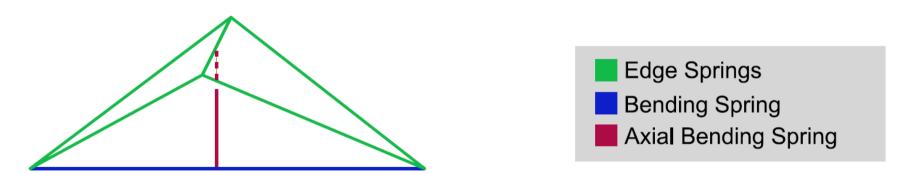
- There is at least one point/face or edge/edge altitude spring that has nonnegative barycentric weights
 - The edge/edge or point/face spring that currently has the least length is guaranteed to have all non-negative barycentric weights





Bending string

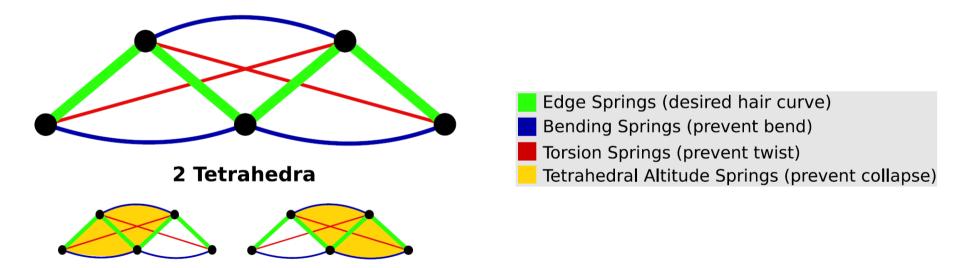
 A pair of triangles sharing an edge can have its bending modeled by two springs



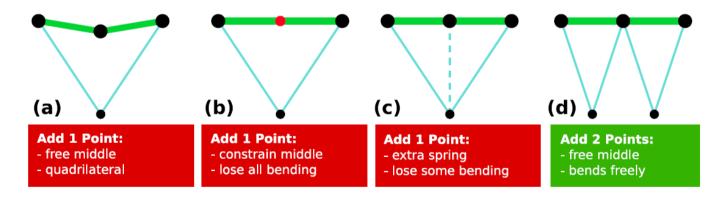
An advanced altitude spring hair model

- If we model a hair as a series of connected line segments
 - <u>Stretching</u>: edge springs between every consecutive particle
 - Bending: bending springs between every other particle
 - <u>Twist</u>: attaching torsion springs that connect each particle to a particle three particles away from it
 - <u>Orientation of hair</u>: edge springs and bending springs together form triangles that implicitly represent the orientation

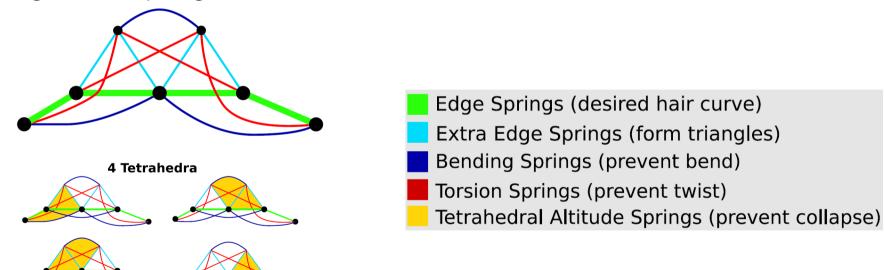
- An advanced altitude spring hair model
 - Curly hair springs



- An advanced altitude spring hair model
 - Straight hair springs
 - All the particles may be collinear: zero area tetrahedra
 - Introduce additional particles perturbed from the main hair axis (more rigid spring)



- An advanced altitude spring hair model
 - Straight hair springs



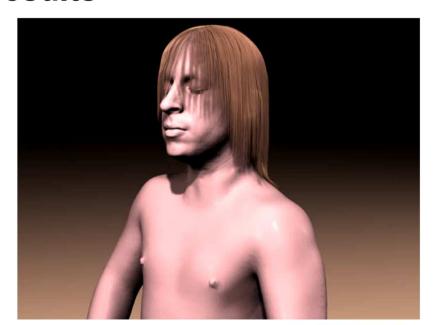
Strain limiting

- Complex head motions can cause severe stretching
- Apply momentum conserving velocity impulses to particles attached by springs that exceed 10% deformation

Self-repulsion

Using only the edge/edge repulsion







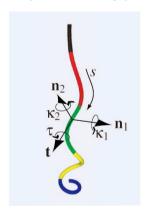


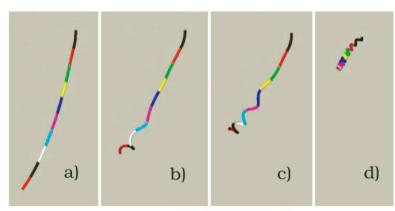


III. Physical Modeling for Hair Simulation

Kinematics

- Built upon the Cosserat and Kirchhoff theories of rods
- Centerline: $\mathbf{r}(s,t)$ $s \in [0,L]$
- Material (moving) frame: $\mathbf{n}_i(s,t)$ $\mathbf{r}'(s,t) = \mathbf{n}_0(s,t)$





Kinematics

- Kirchhoff model for elastic rod: <u>inextensibility</u> and <u>unshearability</u>
- The frame $\mathbf{n}_i(s,t)$ is <u>orthonormal</u> for all s
- Darboux vector

$$\mathbf{n}'_i(s,t) = \mathbf{\Omega}(s,t) \times \mathbf{n}_i(s,t)$$
 for $i = 0, 1, 2$.

Boundary condition

$$\begin{cases} \mathbf{r}(0,t) = \mathbf{r}_{c}(t) \\ \mathbf{n}_{i}(0,t) = \mathbf{n}_{i,c}(t) & \text{for } i = 0,1,2, \end{cases}$$

Rod's material curvatures & twist

$$\mathbf{n}_i'(s,t) = \mathbf{\Omega}(s,t) \times \mathbf{n}_i(s,t)$$
 for $i = 0,1,2$.

- Curvature along two directions: $(\kappa_{\alpha}(s,t))_{\alpha=1,2}$
- Twist: $\tau(s,t)$
- The coordinates of the vector $\Omega(s,t)$ in the local material frame

$$\mathbf{\Omega}(s,t) = \tau(s,t)\mathbf{n}_0(s,t) + \kappa_1(s,t)\mathbf{n}_1(s,t) + \kappa_2(s,t)\mathbf{n}_2(s,t)$$

- Introducing a redundant notation for the twist $\kappa_0 = au$
- We can refer to these parameters collectively $(\kappa_i(s,t))_{i=0,1,2}$

The degrees of freedom of a Kirchhoff rod

- Spatial discretization
 - Divide the strand $s \in [O,L]$ into N segments S_Q $1 \le Q \le N$
 - Define the material curvatures and twist with piecewise constant functions over these segments

$$q_{i,Q}(t)$$
 Constant functions of $(\kappa_i(s,t))_{i=0,1,2}$

Explicit formula for the material curvatures and twist

- Generalized coordinates and reconstruction
 - Gather all $q_{i,Q}(t)$ $q_{i,O}(t) \longrightarrow \mathbf{q}(t)$

$$q_{i,Q}(t) \longrightarrow \mathbf{q}(t)$$

Can be used to reconstruct the rod shape at any given time

$$\begin{split} \boldsymbol{\kappa}_i(s,t) &= \sum_{Q=1}^N q_{i,Q}(t) \, \chi_Q(s) \\ \boldsymbol{\Omega}(s,t) &= \boldsymbol{\tau}(s,t) \, \mathbf{n}_0(s,t) + \boldsymbol{\kappa}_1(s,t) \, \mathbf{n}_1(s,t) + \boldsymbol{\kappa}_2(s,t) \, \mathbf{n}_2(s,t) \\ \mathbf{n}_i'(s,t) &= \boldsymbol{\Omega}(s,t) \times \mathbf{n}_i(s,t) \quad \text{for } i = 0,1,2. \quad \left\{ \begin{array}{l} \mathbf{r}(0,t) = \mathbf{r}_c(t) \\ \mathbf{n}_i(0,t) = \mathbf{n}_{i,c}(t) \end{array} \right. \quad \text{for } i = 0,1,2, \end{split}$$

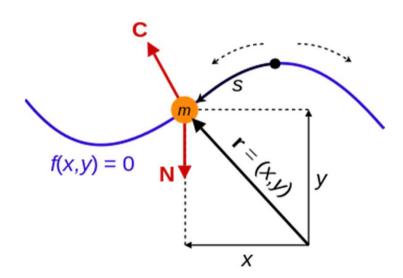
$$\mathbf{r}'(s,t) = \mathbf{n}_0(s,t) \quad \text{Can be integrated to obtain positions} \end{split}$$

- Dynamic equations for a Super-Helix
 - Newton dynamic equations

$$\mathbf{v}_1 = rac{d\mathbf{r}_1}{dt}, \mathbf{v}_2 = rac{d\mathbf{r}_2}{dt}, \dots, \mathbf{v}_N = rac{d\mathbf{r}_N}{dt} \qquad \qquad \sum \mathbf{F} = m rac{d^2\mathbf{r}}{dt^2}$$

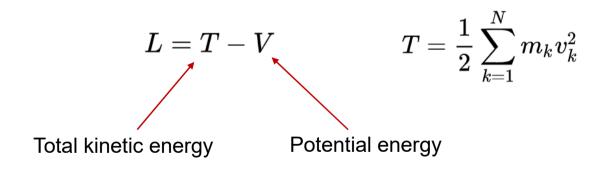
$$\mathbf{r}_1 = (x_1, y_1, z_1), \, \mathbf{r}_2 = (x_2, y_2, z_2)$$
 ...

Require impulse forces to maintain constraints



Dynamic equations for a Super-Helix

- Lagrangian dynamic equations
 - Use the energies in the system
 - Lagrangian: a function which summarizes the dynamics of the entire system



Lagrange's equations (First kind) $rac{\partial L}{\partial \mathbf{r}_k} - rac{\mathrm{d}}{\mathrm{d}t} rac{\partial L}{\partial \dot{\mathbf{r}}_k} + \sum_{i=1}^C \lambda_i rac{\partial f_i}{\partial \mathbf{r}_k} = 0$ Constraints

Dynamic equations for a Super-Helix

- Given deformable body whose configuration depends on generalized coordinates $\mathbf{q}(t)$
- Lagrangian mechanics provides a systematic method for deriving its equation of motion $\ddot{\mathbf{q}} = \mathbf{a}(\mathbf{q},\dot{\mathbf{q}},t)$

$$\frac{\mathrm{d}}{\mathrm{d}t} \left(\frac{\partial T}{\partial \dot{q}_{iQ}} \right) - \frac{\partial T}{\partial q_{iQ}} + \frac{\partial U}{\partial q_{iQ}} + \frac{\partial D}{\partial \dot{q}_{iQ}} = \int_{0}^{L} \mathbf{J}_{iQ}(s, \mathbf{q}, t) \cdot \mathbf{F}(s, t) \, \mathrm{d}s$$
Work due to external forces

Dynamic equations for a super-helix

Lagrangian mechanics formulation

$$\frac{\mathrm{d}}{\mathrm{d}t} \left(\frac{\partial T}{\partial \dot{q}_{iQ}} \right) - \frac{\partial T}{\partial q_{iQ}} + \frac{\partial U}{\partial q_{iQ}} + \frac{\partial D}{\partial \dot{q}_{iQ}} = \int_0^L \mathbf{J}_{iQ}(s, \mathbf{q}, t) \cdot \mathbf{F}(s, t) \, \mathrm{d}s$$

- Kinetic energy: $T(\mathbf{q}, \dot{\mathbf{q}}, t) = \frac{1}{2} \int_0^L \rho S\left(\dot{\mathbf{r}}^{\mathrm{SH}}(s, \mathbf{q})\right)^2 \mathrm{d}s$
- Internal energy: $U(\mathbf{q},t) = \frac{1}{2} \int_0^L \sum_{i=0}^2 (EI)_i \left(\kappa_i^{\rm SH}(s,\mathbf{q}) \kappa_i^{\rm n}(s) \right)^2 \mathrm{d}s$
- Dissipation potential: $D(\mathbf{q}, \dot{\mathbf{q}}, t) = \frac{1}{2} \int_0^L \gamma \sum_{i=0}^2 \left(\dot{\kappa}_i^{\mathrm{SH}}(s, \mathbf{q}) \right)^2 \mathrm{d}s$

- Dynamic equations for a super-helix
 - Lagrangian mechanics formulation

$$\frac{\mathrm{d}}{\mathrm{d}t} \left(\frac{\partial T}{\partial \dot{q}_{iQ}} \right) - \frac{\partial T}{\partial q_{iQ}} + \frac{\partial U}{\partial q_{iQ}} + \frac{\partial D}{\partial \dot{q}_{iQ}} = \int_0^L \mathbf{J}_{iQ}(s, \mathbf{q}, t) \cdot \mathbf{F}(s, t) \, \mathrm{d}s$$

- Jacobian: $\mathbf{J}_{iQ} = \partial \mathbf{r}^{\mathrm{SH}}(s,\mathbf{q})/\partial q_{iQ}$
- Force contributions: hair weight, viscous drag, interaction forces with surrounding strands and body

$$\mathbf{F}(s,t) = \rho S \mathbf{g} - \nu \dot{\mathbf{r}}^{SH}(s,\mathbf{q}) + \mathbf{F}^{i}(s,t)$$

- Dynamic equations for a super-helix
 - Lagrangian mechanics formulation

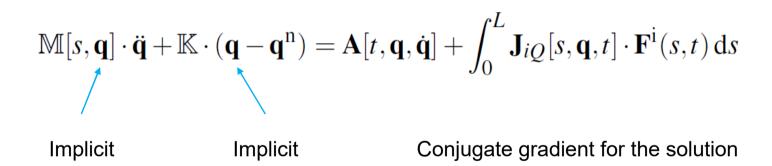
$$\frac{\mathrm{d}}{\mathrm{d}t} \left(\frac{\partial T}{\partial \dot{q}_{iQ}} \right) - \frac{\partial T}{\partial q_{iQ}} + \frac{\partial U}{\partial q_{iQ}} + \frac{\partial D}{\partial \dot{q}_{iQ}} = \int_0^L \mathbf{J}_{iQ}(s, \mathbf{q}, t) \cdot \mathbf{F}(s, t) \, \mathrm{d}s$$



$$\mathbb{M}[s,\mathbf{q}]\cdot\ddot{\mathbf{q}} + \mathbb{K}\cdot(\mathbf{q}-\mathbf{q}^n) = \mathbf{A}[t,\mathbf{q},\dot{\mathbf{q}}] + \int_0^L \mathbf{J}_{iQ}[s,\mathbf{q},t]\cdot\mathbf{F}^i(s,t)\,\mathrm{d}s$$

qⁿ defines the rest position in generalized coordinates

- Time discretization
 - Classical Newton semi-implicit scheme with fixed time step



- Hair strand interpolation
 - Different interpolation styles
 - Interpolate smoothly at the root, but clustered at the tip



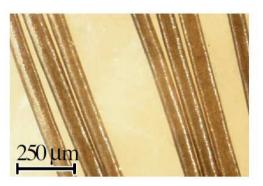
Determine parameters

- Density ρ =1.3 $g \cdot cm^{(-3)}$
- Natural curliness:

$$\kappa_1^{\rm n} = 1/r_{\rm h}$$
 $\kappa_2^{\rm n} = 0$
 $\tau^{\rm n} = \frac{\Delta_{\rm h}}{2\pi r_{\rm h}^2}$

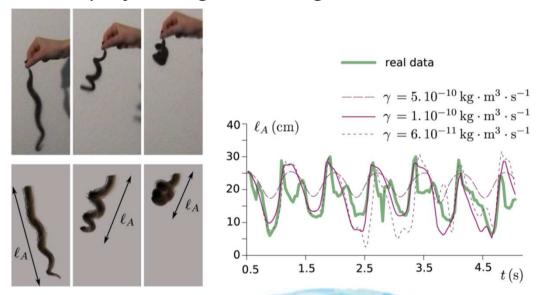
Parameter values for natural hair

	Asian (smooth)	Caucasian 1 (wavy)	Caucasian 2 (curly)	African (fuzzy)
Radius (µm)	50	35	50	50
Ellipticity	1	1.1	1.1	1.2
Helix radius (cm)	0	1	0.6	0.1
Helix step (cm)	0	0.5	0.5	1
Young's mod. (GPa)	1	2	1.5	0.5
Poisson's ratio	0.48	0.48	0.48	0.48





- Fitting data experimentally
 - Friction (in collision) by fitting hair lengths



Animation

Super-Helices

for Predicting the Dynamics

of Natural Hair

IV. Data-Driven Approach

A Reduced Model for Interactive Hairs

- High-quality hair simulation is expensive
 - Building upon precomputed simulation data
 - Constructs a reduced model
 - Optimally represent hair motion with a small number of guide hairs and the corresponding interpolation relationships



A Reduced Model for Interactive Hairs

A Reduced Model for Interactive Hairs

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Next Lecture: Soft-Body Simulation – Hair II